# Ghemical \& Intirstrial Piping Systems 

For over 60 years NOV Fiber Glass Systems has been the industry leader in the Chemical \& Industrial market with composite piping systems designed to provide chemical and abrasion resistance. Our extensive line of products has grown to include the leading trade names in this market, creating an unequaled worldwide offering to battle corrosion and erosion.

This globally manufactured group of products has become the world's most widely trusted product offering founded upon two essential elements: third party verified ASTM qualifications and decades of experience in tough services. The third party testing provides our customers with confidence that the physical properties we publish are based on test data, not theory. The wide scope of applications within such a diverse market provides our customers confidence that the products' reliability extends beyond rigorous testing into the real world of actual long-term performance in applications where upset conditions and thermal cycling are reality.

Typical applications range from potable water to brine and from harsh chemical feed, waste and vent applications to process lines in nearly every sector of industry imaginable: power generation, metals \& minerals, food service, LNG, automotive, aerospace \& defense, biotech and pharmaceutical, university and district heating and cooling, general, fine \& specialty chemical process industry, petroleum refining, pulp \& paper, municipal and industrial waste water treatment.

| ASTM Test Methods and Specifications |  |
| :--- | :--- |
| D1599 | Standard Test Method for Resistance to Short-Time Hydraulic Pressure of Plastic Pipe, Tubing, and Fittings |
| D2105 | Standard Test Method for Longitudinal Tensile Properties of "Fiberglass" (Glass-Fiber-Reinforced Thermosetting- <br> Resin) Pipe and Tube |
| D695 | Standard Test Method for Compressive Properties of Rigid Plastics |
| D2412 | Standard Test Method for Determination of External Loading Characteristics of Plastic Pipe by Parallel-Plate <br> Loading |
| D2925 | Standard Test Method for Beam Deflection of "Fiberglass" (Glass-Fiber-Reinforced Thermosetting Resin) Pipe <br> Under Full Bore Flow |
| D4024 | Standard Specification for Machine Made "Fiberglass" (Glass-Fiber-Reinforced Thermosetting Resin) Flanges |
| D5685 | Standard Specification for "Fiberglass" (Glass-Fiber-Reinforced Thermosetting-Resin) Pressure Pipe Fittings |
| D2996 | Standard Specification for Filament-Wound "Fiberglass" (Glass-Fiber-Reinforced Thermosetting-Resin) Pipe |
| D2997 | Standard Specification for Centrifugally Cast "Fiberglass" (Glass-Fiber-Reinforced Thermosetting-Resin) Pipe |
| D2992 | Standard Practice for Obtaining Hydrostatic or Pressure Design Basis for "Fiberglass" (Glass-Fiber-Reinforced <br> Thermosetting-Resin) Pipe and Fittings |

## Filament Wound Piping Systems

For more than 40 years, Green Thread ${ }^{\circledR}$, Red Thread ${ }^{\circledR}$ and Bondstrand ${ }^{\circledR}$ products have been used in potable water, firewater mains, saltwater cooling, saltwater disposal, heating \& cooling water systems and wastewater systems across the automotive, power generation, municipal, institutional and aerospace applications.


Filament Winding Process
Resin-impregnated glass fibers are wound onto a mandrel in a predetermined pattern under controlled tension. This process results in a pipe that is approximately $75 \%$ glass-reinforced for optimum internal pressure capability.

## Centrifugally Cast Piping Systems

With a 100\% resin corrosion barrier, Centricast ${ }^{\circledR}$ piping systems provide the most chemically resistant pipe in the market. These products have 60 years of successful history in the steel pickling, chloro-alkali, pharmaceutical, power generation and chemical processing industries.


## Centrifugal Casting Process

Woven glass fiber (or fabric) in a motor-driven steel tube is saturated with resin while the tube rotates at high speed. Fiber reinforcement in both the hoop and axial directions affords excellent thermal expansion and beam-bending properties.

## Epoxy Piping Systems



RB-2530 pipe is available in 1"-14" diameters, with pressure ratings from 125-300 psig and temperatures up to $250^{\circ} \mathrm{F}\left(121^{\circ} \mathrm{C}\right)$, and is recommended for most caustics, salts, solvents, many acids and chemical process solutions, including steel pickling. It also handles abrasive slurries.


RB-1520 pipe is available in $11 / 2 "-14$ " diameters, with pressure ratings from $125-300$ psig and temperatures up to $250^{\circ} \mathrm{F}\left(121^{\circ} \mathrm{C}\right)$, and is recommended for chemical process solutions, solvents, acids, caustics and salt solutions.


Green Thread HP pipe is available in 1"-42" diameters with pressure ratings up to 725 psig and temperatures up to $230^{\circ} \mathrm{F}\left(110^{\circ} \mathrm{C}\right)$, and is recommended for dilute acids and caustics, produced/hot water, industrial waste and condensate return. (Primary Market-North America)


Red Thread HP pipe is available in 2"-42" diameters with pressure ratings up to 362 psig and temperatures up to $210^{\circ} \mathrm{F}\left(99^{\circ} \mathrm{C}\right)$ Pipe sizes $2^{\prime \prime}-6^{\prime \prime}$ have special profile threads for quick and reliable assembly. The product is recommended for general industrial service. (Primary Market-North America)


Bondstrand 2000 pipe is available in 1"-16" diam eters with pressure ratings up to 450 psig and tem peratures up to $250^{\circ} \mathrm{F}\left(121^{\circ} \mathrm{C}\right)$. This product is recommended for dilute acids and caustics, produced hot water, industrial waste and condensate returns.


Bondstrand 2400 pipe is available in $2 "-40$ " diameters with pressure ratings up to 725 psig and temperatures up to $250^{\circ} \mathrm{F}\left(121^{\circ} \mathrm{C}\right)$. Recommended for salt waters, brackish water, fire protection, potable/ waste water and sewage, oil field reinjection, crude oil transmission and mild chemicals.


Bondstrand 3000, 3200, and 3300 series piping are manufactured using aromatic amine or anhydride epoxy. They are recommended for general industrial service up to $210^{\circ} \mathrm{F}\left(99^{\circ} \mathrm{C}\right)$. The 3000 series pipe is available in 2 " -16 " diameters with pressure ratings up to 450 psig. The 3200 and 3300 series pipe are available in 8 "-16" diameters with pressure ratings of 200 and 300 psig, respectively.


Bondstrand 4000 pipe is available in 1"-16" diameters with pressure ratings from 150 to 300 psi and temperatures up to $250^{\circ} \mathrm{F}\left(121^{\circ} \mathrm{C}\right)$ and is recommended for acid drains, chemical processes, slurries, food processing, non-oxidizing chemicals and acids.


Bondstrand 7000 pipe is available in 2"-16" with a pressure rating of 150 psig and temperatures up to $210^{\circ} \mathrm{F}\left(99^{\circ} \mathrm{C}\right)$. Pipe is recommended for general industrial and jet fuel services where static electrical charge build-up is possible.

## Note: <br> HP pressure classes are 16, 20, 25, 32, 40 and 50 bar. Bondstrand 2400 pressure classes are 10, 12, 14, 16, 20, 25, 32, 40 and 50 bar. <br> The above pressure classes are not available in all sizes.

## Vinyl Ester Piping Systems



CL2030 pipe is available in 1"-14" diameters with pressure ratings up to 150 psig and is recommended for most chlorinated and acidic mixtures up to $175^{\circ} \mathrm{F}\left(80^{\circ} \mathrm{C}\right)$ and other chemicals up to $200^{\circ} \mathrm{F}$ $\left(93^{\circ} \mathrm{C}\right)$. This pipe is manufactured with a 100 mil liner.


CL1520 pipe is available in 1"-14" diameters with pressure ratings up to 150 psig and is recommended for most chlorinated and acidic mixtures up to $175^{\circ} \mathrm{F}\left(80^{\circ} \mathrm{C}\right)$ and other chemicals up to $200^{\circ} \mathrm{F}$ $\left(93.3^{\circ} \mathrm{C}\right)$. This pipe is manufactured with a 50 mil liner.


Bondstrand 5000 is available in 1"-16" diameters with temperature range up to $200^{\circ} \mathrm{F}\left(93^{\circ} \mathrm{C}\right)$. This is a custom vinyl ester pipe available in Asia, Europe and South America and is recommended for most chlorinated and acidic mixtures. This pipe is manufactured with a 50 mil liner.


Polyplaster pipe is hand lay up pipe in diameters 1 " -8 " and is wound on a C.A.M. machine up to 100 inch. A variety of vinyl ester/polyester resin systems and liner thicknesses can be specified. Joint is butt and wrap.

## Advanced Performance Specialty Products



Down Hole Tubing \& Casing products are capable of pressures up to 3500 psi and temperatures of $210^{\circ} \mathrm{F}$ for corrosive applications like $\mathrm{CO}_{2}$, saltwater/brine and other such services for methane gas, chemical disposal or simply brackish water wells. Diameters are available from $11 / 2 "$ through 9 " for pressures up to 3500 psi and diameters up to 24 " for lower pressure brackish/RO water wells.


Fiberspar LinePipe products are continuous spoolable piping systems with HDPE liners over wrapped with a glass fiber epoxy thermoset matrix for corrosive and abrasive applications up to 2500 psi and up to $180^{\circ} \mathrm{F}$. Diameters are available in $21 / 2$ " through $6 \frac{1}{2}$ " and continuous lengths up to 2 miles. A down hole version is also available.


High Pressure products are available in sizes ranging from $11 / 2$ " through 36 " for pressures of 150 psi up to 4000 psi at temperatures up to $210^{\circ} \mathrm{F}$. Typical applications include water, hydraulic fluid, and other difficult industrial applications in a variety of industries including severe elevation changes.


## Secondary Containment

Two-piece secondary containment fittings are available in $3 "-16$ " diameters for primary pipe sizes up to 14 ". The systems are designed for maximum field flexibility, ease of installation and the ability to use one size larger containment. When higher pressure, larger diameter or severe temperature changes are required, special fittings can be provided to handle the added requirements.

## Other Considerations

In many instances NOV Fiber Glass Systems' products can be hydroblasted, steam cleaned and heat-traced; please contact FGS for details.

FGS has Factory Mutual Listing for Red Thread FM and Bondstrand 3200/6000 piping. Bondstrand 3200 has UL and ULC listing for buried fire protection systems.


Approved

The following FGS pipe systems have UL and NSF 61 Listing for drinking water: Red Thread HP, Green Thread HP,
Bondstrand 2000, 2400 series and 7000 pipe.


WATER QUALITY

ANSI/NSF 61
Drinking Water System
Components 35GH
Water Contact Temp: 23C

## Joining Systems



Key Lock ${ }^{\circledR}$ - Self-restrained mechanical joint provides quick assembly by means of locking keys inserted between bell and spigot. Used to install Bondstrand 2400 series pipe in sizes 2" through 40" (50 - 1000 mm ).


Taper x Taper - Matched taper joint secured with epoxy adhesive. Selflocking feature resists movement, facilitating joining on RT/GT HP $16 / 20 / 25$ bar piping without awaiting adhesive cure.


Quick ${ }^{\circledR}$ Lock - Straight spigot/ tapered socket adhesive bonded joint for precise make-up to facilitate close tolerance piping. Used for 1"-16" (25-400 mm) Bondstrand 2000/4000/5000/6000/7000 piping.

## Engineering Design



The NOV Fiber Glass Systems' "Success by Design" engineering software sets the industry standard for design assistance. From material selection to flow calculations and comparisons; anchor, guide and support calculations; and thermal expansion solutions, this design package assists the engineer and owner in designing a highly successful system. Our applications engineers can assist you in the selection of the proper piping system for your application.


T.A.B. ${ }^{\text {TM }}$ - Threaded and bonded joining system. Double-lead threads provide quick and secure adhesive connections. Available for 2 " through 6" Red Thread pipe sizes.

Flanged - Available for all piping systems and diameters; factory assembled or shipped loose for assembly in the field.

Butt \& Wrap - Plain end pipe or pipe and fittings butted together and wrapped with multiple layers of resin-saturated mat or woven roving. Use with all piping systems.
Socket Joint - Adhesive bonded straight socket joint with positive stops. This is the standard for Centricast piping systems.


## Installation and Fabrication

With eight regional fabrication locations in North America and others around the world, NOV Fiber Glass Systems can rapidly fabricate your project for minimum field installation. All of our shops are staffed with ASME B31.3 certified bonders. Certification of field installation crews to the same ASME standard is available.


|  | SALES OFFICES | Middle East | Downhole Solutions |
| :---: | :---: | :---: | :---: |
|  | San Antonio, Texas | Dubai, United Arab Emirates |  |
|  | Oilfield Products | Phone: 97148865660 |  |
|  | Phone: 2104777500 |  |  |
|  |  | Asia, Pacific Rim |  |
|  | Little Rock, Arkansas | Singapore |  |
|  | C\&I/Fuel Handling Products | Phone: 6568616118 |  |
|  | Phone: 5015684010 |  |  |
|  |  | Harbin China | Drilling Solutions |
|  | Burkburnett, Texas | Phone: 8645187091718 | Driling Solutions |
|  | Marine Offshore \& Fuel Handling |  |  |
|  | Phone: 9405691471 | Shanghai, China |  |
|  |  | Phone: 862158881677 |  |
|  | Mineral Wells, Texas |  |  |
|  | Centron Products | Suzhou, China |  |
|  | Phone: 9403251341 | Phone: 8651285180099 |  |
|  | Houston, Texas | Europe, Africa, Caspian | Engineering and Project Management Solutions |
|  | Fiberspar Products | Geldermalsen, The Netherlands |  |
|  | Phone: 7138492609 | Phone: 31345587587 |  |
|  | Johnstown, Colorado |  |  |
|  | Fiberspar Products |  |  |
| Headquarters | Phone: 9705782000 | MANUFACTURING FACILITIES |  |
|  | Canada | Burkburnett, Texas, USA |  |
| 17115 San Pedro Avenue Suite 200 | Use U.S.A. Contacts | Mineral Wells, Texas, USA | Lifting and Handling Solutions |
| San Antonio, Texas 78232 USA |  | Little Rock, Arkansas ,USA |  |
| Phone: 2104777500 | Mexico, Caribbean, | San Antonio, Texas, USA |  |
|  | Central America | Sand Springs, Oklahoma, USA |  |
|  | Use U.S.A. Contacts | Wichita, Kansas, USA Johnstown, Colorado, USA |  |
|  | South America | Houston, Texas USA |  |
|  | Recife, Pernambuco, Brazil | Betim, Brazil |  |
|  | Phone: 558135010023 | Recife, Brazil |  |
|  |  | Harbin, China | Production Solutions |
|  | Central Asia / Russia | Suzhou, China |  |
|  | Aktau, Kazakhstan | Malaysia |  |
|  | Phone: 77015141087 | Singapore |  |
|  |  | Sohar, Oman |  |

## Supply Chain Solutions

## Tubular and Corrosion Control Solutions

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## Well Service and Completion Solutions

## Applications

- Chemical Processing Liquids
- Food Processing Liquids
- Potable Water
- Cooling Water
- Condensate Return
- Industrial Wastewater
- Mildly Corrosive Liquids
- Crude Oil \& Gas


## Materials and Construction

Red Thread HP16 pipe is manufactured by the filament winding process using aromatic amine-cured epoxy thermosetting resin to impregnate strands of continuous glass filaments. The pipe is rated up to 435 psig in accordance with API 15LR, 20 year design life at $200^{\circ} \mathrm{F}\left(93^{\circ} \mathrm{C}\right)$, serviceable up to $210^{\circ} \mathrm{F}\left(99^{\circ} \mathrm{C}\right)$ by applying a derating factor of 0.92 to all component ratings.

ASTM D-2996 Classification: RTRP-11AW1-3110
forstatic design basis.

## Fittings

Fittings are manufactured with the same chemical and temperature capabilities as the pipe. Depending on the configurations and size, the fittings construction method will be compression molded, contact molded, fabricated or filament wound. Fittings details are in two documents. Use CI1350 forsizes $2^{\prime \prime}-16^{\prime \prime}(50-400 \mathrm{~mm})$ and Cl1351 for $18^{\prime \prime}-42^{\prime \prime}(450-$ $1050 \mathrm{~mm})$. All fittings may not have the same pressure rating as the pipe. System rating is governed by the lowest rated component used.

## Joining System

- T.A.B. ${ }^{\text {TM }}$ - In sizes 2"- $\mathbf{6}^{\text {", }}$, pipe and couplings are supplied with a threaded and bonded (T. A. B) joining system. Double-lead threads provide quick secure adhesive connections during installation.
- Bell \& Spigot - The pipe and fittings are joined using the bell and spigot connection. Pipe is supplied with one end belled (integral bell orfactory-bonded coupling) and one end tapered in sizes 8 "-42". For $8^{\prime \prime}-42^{\prime \prime}$ sizes, the matched tapered joining method is used and the pipe is available in random 12 meter ( 40 feet) lengths.

Epoxy adhesive available from NOV Fiber Glass Systems is used to secure the joint.

- Flanged - Flanged connections are available for all components and diameters.

т.A.B.


Bell \& Spigot


Flanged

Nominal Dimensional Data

| Pipe Size |  | Inside Diameter |  | Outside Diameter ${ }^{(4)}$ |  | Reinforced Wall Thickness |  | Weight |  | Capacity |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | in | mm | in | mm | in | mm | lbs/ft | kg/m | gal/ft | 1/m |
| $2^{(1)}$ | 50 | 2.24 | 57 | 2.35 | 60 | 0.058 | 1.47 | 0.4 | 0.54 | 0.20 | 2.5 |
| $3^{(1)}$ | 80 | 3.36 | 85 | 3.54 | 98 | 0.086 | 2.18 | 0.8 | 1.20 | 0.46 | 5.7 |
| $4^{(2)}$ | 100 | 4.36 | 111 | 4.53 | 115 | 0.083 | 2.11 | 1.0 | 1.52 | 0.78 | 9.7 |
| $6^{(2)}$ | 150 | 6.41 | 163 | 6.65 | 169 | 0.122 | 3.10 | 2.2 | 3.21 | 1.68 | 20.9 |
| 8 | 200 | 8.36 | 212 | 8.61 | 219 | 0.127 | 3.23 | 2.9 | 4.35 | 2.85 | 35.4 |
| 10 | 250 | 10.36 | 263 | 10.67 | 271 | 0.156 | 3.96 | 4.5 | 6.62 | 4.38 | 54.4 |
| 12 | 300 | 12.28 | 312 | 12.65 | 321 | 0.185 | 4.70 | 6.3 | 9.31 | 6.16 | 76.4 |
| 14 | 350 | 14.03 | 356 | 14.51 | 369 | 0.238 | 6.05 | 9.2 | 13.70 | 8.03 | 99.7 |
| 16 | 400 | 16.03 | 407 | 16.57 | 421 | 0.272 | 6.91 | 12.0 | 17.90 | 10.50 | 130.0 |
| 18 | 450 | 17.82 | 453 | 18.38 | 467 | 0.277 | 7.04 | 13.6 | 20.20 | 13.00 | 161.0 |
| 20 | 500 | 19.83 | 504 | 20.40 | 518 | 0.286 | 7.26 | 15.6 | 23.30 | 16.00 | 199.0 |
| 24 | 600 | 23.83 | 605 | 24.50 | 622 | 0.334 | 8.48 | 21.9 | 32.60 | 23.20 | 288.0 |
| $30^{(3)}$ | 750 | 30.03 | 763 | 30.89 | 785 | 0.430 | 10.92 | 35.6 | 52.90 | 36.80 | 457.0 |
| $36^{(3)}$ | 900 | 36.03 | 915 | 37.05 | 941 | 0.510 | 12.95 | 50.6 | 75.30 | 53.00 | 658.0 |
| $42^{(3)}$ | 1050 | 42.03 | 1068 | 43.23 | 1098 | 0.600 | 15.24 | 69.4 | 103.00 | 72.10 | 895.0 |

${ }^{(1)}$ Reinforced wall thickness exceeds the requirement for 232 psig and may be operated up to 435 psig .
${ }^{(2)}$ Reinforced wall thickness exceeds the requirement for 232 psig and may be operated up to 362 psig.
${ }^{(3)}$ Qualified for 232 psig, see fittings ratings in CI1351 for exceptions.
${ }^{(4)}$ Outer diameter is for use in flexibility analysis. Consult factory representative for OD tolerances.

## Supports

The following engineering analysis must be performed to determine the maximum support spacing for the piping system. Proper pipe support spacing depends on the temperature and weight of the fluid carried in the pipe. The support spacing is calculated using continuous beam equations and the pipe bending modulus derived from long-term beam bending tests. The following tables were developed to ensure a design that limits beam mid-span deflection to $1 / 2$ inch and bending stresses to less than or equal to $1 / 8$ of the ultimate bending stress. Any additional weight on the piping system such as insulation or heat tracing requires further consideration. Restrained (anchored) piping systems operating at elevated temperatures often result in guide spacing requirements that are more stringent than simple unrestrained piping systems. In this case, the maximum guide spacing will dictate the support/guide spacing requirements for the system. Pipe support spans at changes in direction require special attention. Supported and unsupported fittings. at changes in direction are considered in the following tables and must be followed to properly design the piping system.

## Support Spacing vs. Specific Gravity

| Specific Gravity | 2.00 | 1.50 | 1.25 | 1.00 | 0.75 |
| :--- | :--- | :--- | :--- | :--- | :--- |
| Multiplier | 0.85 | 0.91 | 0.95 | 1.00 | 1.06 |

Example: $18^{\prime \prime}$ pipe @ $75^{\circ} \mathrm{F}\left(23.9^{\circ} \mathrm{C}\right)$ with 1.5 specific gravity fluid,
maximum support spacing $=35.2 \times 0.91=32.0 \mathrm{ft}$. ( 9.76 m )

Maximum Support Spacing for Uninsulated Pipe ${ }^{(1)}$

| Size | Continuous Spans of Pipe ${ }^{(2)}$ |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- |
|  | feet |  | meters |  |  |
| in | $\mathbf{m m}$ | $\mathbf{7 5}^{\circ} \mathbf{F}$ | $\mathbf{2 0 0}{ }^{\circ} \mathbf{F}$ | $\mathbf{2 4}^{\circ} \mathbf{C}$ | $\mathbf{9 3}^{\circ} \mathbf{C}$ |
| 2 | 50 | 14.0 | 10.1 | 4.3 | 3.1 |
| 3 | 80 | 17.1 | 12.4 | 5.2 | 3.8 |
| 4 | 100 | 18.2 | 13.2 | 5.6 | 4.0 |
| 6 | 150 | 22.1 | 16.0 | 6.7 | 4.9 |
| 8 | 200 | 24.0 | 17.4 | 7.3 | 5.3 |
| 10 | 250 | 26.6 | 19.3 | 8.1 | 5.9 |
| 12 | 300 | 29.0 | 21.0 | 8.8 | 6.4 |
| 14 | 350 | 31.8 | 23.1 | 9.7 | 7.0 |
| 16 | 400 | 34.0 | 24.7 | 10.4 | 7.5 |
| 18 | 450 | 35.2 | 25.5 | 10.7 | 7.8 |
| 20 | 500 | 36.5 | 26.5 | 11.1 | 8.1 |
| 24 | 600 | 39.7 | 28.8 | 12.1 | 8.8 |
| 30 | 800 | 44.8 | 32.5 | 13.7 | 9.9 |
| 36 | 900 | 49.0 | 35.5 | 14.9 | 10.8 |
| 42 | 1050 | 53.0 | 38.4 | 16.2 | 11.7 |

${ }^{(1)}$ For $\mathrm{Sg}=1.0$, consult manufacturer for heavier insulated pipe support spans. Span recommendations include no provision for weight of (fittings, valves, etc.) or thrusts at branches and turns. Heavy valves and other appurtenances must be supported separately.
${ }^{(2)}$ Calculated spans are based on $1 / 2$ " mid-span deflections to ensure good appearance and adequate drainage. Total system stresses should always be taken into account by the system design engineer when determining support spans.

There are seven basic rules to follow when designing piping system supports, anchors, and guides:

1. Do not exceed the recommended support span.
2. Support valves and heavy in-line equipment independently.

This applies to both vertical and horizontal piping.
3. Protect pipe from external abrasion.
4. Avoid point contact loads
5. Avoid excessive bending. This applies to handling, transporting, initial layout, and final installed position.
6. Avoid excessive vertical run loading. Vertical loads should be supported sufficiently to minimize bending stresses at outlets or changes in direction.
7. Provide adequate axial and lateral restraint to ensure line stability during rapid changes in flow.

Adjustment Factors for Various Spans With Unsupported Fitting at Change in Direction

|  | Span Type | Factor |
| :--- | :--- | :--- |
| LC | Continuous interior or fixed end spans | 1.00 |
| C | Second span from supported end or unsupported fitting | 0.80 |
| A+B | Sum of unsupported spans at fitting | $\leq 0.75^{\star}$ |
| D | Simple supported end span | 0.67 |

*For example: If continuous support is 10 ft . ( 3.04 m ), $\mathrm{A}+\mathrm{B}$ must not exceed 7.5 ft .( 2.28 m ) (A=3 ft. $(0.91 \mathrm{~m})$ and $B=4.5 \mathrm{ft}$. $(1.37 \mathrm{~m})$ ) would satisfy this condition.


Adjustment Factors for Various Spans With Supported Fitting at Change in Direction

|  | Span Type | Factor |
| :--- | :--- | :--- |
| LC | Continuous interior or fixed end spans | 1.00 |
| A | Second span from simple supported end or unsupported fitting | 0.80 |
| B | Simple supported end span | 0.67 |



## Thermal Expansion

The effects of thermal gradients on piping systems may be significant and should be considered in every piping system stress analysis. Pipe line movements due to thermal expansion or contraction may cause
high stresses or even buckle a pipe line if improperly restrained. Several piping system designs are used to manage thermal expansion and contraction in above ground piping systems. They are listed below according to economic preference:

1. Use of inherent flexibility in directional changes.
2. Restraining axial movements and guiding to prevent buckling.
3. Use expansion loops to absorb thermal movements.
4. Use mechanical expansion joints to absorb thermal movements.

To perform a thermal analysis the following information is required:

1. Isometric layout of piping system
2. Physical and material properties of pipe
3. Design temperatures
4. Installation temperature (Final tie in temperature)
5. Terminal equipment load limits
6. Supportmovements

A comprehensive review of temperature effects on fiberglass pipe may be found in NOV Fiber Glass Systems' Engineering and Piping Design Guide, Section 3.

| Change in <br> Temperature |  | Pipe Change in <br> Length |  |
| :--- | :--- | :--- | :--- |
| ${ }^{\circ} \mathbf{F}$ | ${ }^{\circ} \mathbf{C}$ | in/100 ft | $\mathbf{c m} / \mathbf{1 0 0} \mathbf{~ m}$ |
| 25 | 13.9 | 0.32 | 2.67 |
| 50 | 27.8 | 0.64 | 5.35 |
| 75 | 41.7 | 0.96 | 8.02 |
| 100 | 55.6 | 1.28 | 10.7 |

## Testing

Hydrostatic testing is recommended to evaluate the integrity of all new piping installations. For systems operating below the system rating, a test pressure of 1.5 times the system operating pressure is recommended; however, the maximum test pressure must not exceed 1.3 times the lowest pressure rated fiberglass component in the piping system.
The hydro test pressure should be repeated up to ten cycles from 0 psig to the test pressure to provide a high degree of confidence in the piping system. The final pressurization cycle should be allowed to stabilize for 15-30 minutes, then inspected for leaks. Do not attempt to repair leaks while system is pressurized. The hydro test should be repeated after any re-work is performed.

When hydro testing, open high-point vents (ifused) to prevent entrapment of air in the lines as the system is slowly filled with water, then close the vents and slowly pressurize to the test pressure. Upon completion of hydro test, relieve the pressure on the system slowly, open vents and any drains to allow for complete drainage of the system.

## Water Hammer

Piping systems may be damaged by pressure surges due to water hammer. The use of soft start pumps and slow actuating valves will reduce the magnitude of surge pressures during operation and are highly recommended.

## Typical Mechanical Properties

| Pipe Property | $75^{\circ} \mathrm{F}$ | $24^{\circ} \mathrm{C}$ | $200^{\circ} \mathrm{F}$ | $93^{\circ} \mathrm{C}$ | Method |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | psi | MPa | psi | MPa |  |
| Axial Tensile |  |  |  |  |  |
| Ultimate Stress | 9,530 | 65.7 | 6,585 | 45.4 | ASTM D2105 |
| Modulus of Elasticity | $1.68 \times 10^{6}$ | 11,584 | $1.42 \times 10^{6}$ | 9,791 | ASTM D2105 |
| Poisson's Ratio, $v_{\text {ah }}\left(v_{\text {ha }}\right)^{(1)}$ | 0.35 (0.61) |  |  |  |  |
| Axial Compression |  |  |  |  |  |
| Ultimate Stress | 12,510 | 86.3 | 8,560 | 59.0 | ASTM D695 |
| Modulus of Elasticity | $0.677 \times 10^{6}$ | 4,668 | $0.379 \times 10^{6}$ | 2,613 | ASTM D695 |
| Beam Bending |  |  |  |  |  |
| Modulus of Elasticity (Long Term) | $2.6 \times 10^{6}$ | 17,927 | $0.718 \times 10^{6}$ | 4,951 | ASTM D2925 |
| Hydrostatic Burst |  |  |  |  |  |
| Ultimate Hoop Tensile Stress | 40,150 | 277 | 36,480 | 252 | ASTM D1599 |
| Hydrostatic Hoop Design Stress |  |  |  |  |  |
| Static 20 Year Life LTHS -95\% LCL | - | - | 18,203-14,689 | 125.5-101.3 | ASTM D2992-Procedure B |
| Static 50 Year Life LTHS -95\% LCL | - | - | 16,788-13,142 | 115.7-90.6 | ASTM D2992-Procedure B |
| Parallel Plate |  |  |  |  |  |
| Hoop Modulus of Elasticity | $3.02 \times 10^{6}$ | 20,822 | - | - | ASTM D2412 |
| Shear Modulus | $1.36 \times 10^{6}$ | 9,343 | $1.15 \times 10^{6}$ | 7,895 | - |

## Typical Physical Properties

| Pipe Property | Value | Value | Method |
| :--- | :--- | :--- | :--- |
| Thermal <br> Conductivity | $0.23 \mathrm{BTU} / \mathrm{hr} \cdot \mathrm{ft} \cdot{ }^{\circ} \mathrm{F}$ | $0.4 \mathrm{~W} / \mathrm{m}^{\circ} \mathrm{C}$ | ASTM D177 |
| Thermal <br> Expansion | $10.7 \times 10^{-6} \mathrm{in} / \mathrm{in} /{ }^{\circ} \mathrm{F}$ | $19.3 \times 10^{-6} \mathrm{~mm} / \mathrm{mm} /{ }^{\circ} \mathrm{C}$ | ASTM D696 |
| Absolute <br> Roughness | 0.00021 in | 0.00053 mm |  |
| Specific Gravity | 1.8 |  | ASTM D792 |

${ }^{(1)} V_{\text {ha }}=$ The ratio of axial strain to hoop strain resulting from stress in the hoop direction.
$v_{\mathrm{ah}}=$ The ratio of hoop strain to axial strain resulting from stress in the axial direction.
${ }^{(2)}$ The differential pressure between internal and external pressure which causes collapse.
${ }^{(3)}$ A 0.67 design factor is recommended for short duration vacuum service. A full vacuum is equal to $14.7 \mathrm{psig}(0.101 \mathrm{MPa})$ differential pressure at sea level.
${ }^{(4)} \mathrm{A} 0.33$ design factor is recommended for sustained (long-term) differential collapse pressure design and operation.

## Ultimate Collapse Pressure

| Size | Collapse Pressure $^{(2,3,4)}$ |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- |
|  | psig |  |  | $\mathbf{M P a}^{\circ}$ |  |
| In | $\mathbf{m m}$ | $\mathbf{7 5}^{\circ} \mathbf{F}$ | $\mathbf{2 0 0}^{\circ} \mathbf{F}$ | $\mathbf{2 4}^{\circ} \mathbf{C}$ | $\mathbf{9 3}^{\circ} \mathbf{C}$ |
| 2 | 50 | 177 | 133 | 1.22 | 0.92 |
| 3 | 80 | 171 | 129 | 1.18 | 0.89 |
| 4 | 100 | 69 | 51 | 0.48 | 0.35 |
| 6 | 150 | 69 | 51 | 0.48 | 0.35 |
| 8 | 200 | 29 | 20 | 0.20 | 0.14 |
| 10 | 250 | 27 | 20 | 0.19 | 0.13 |
| 12 | 300 | 27 | 20 | 0.19 | 0.14 |
| 14 | 350 | 45 | 33 | 0.31 | 0.23 |
| 16 | 400 | 45 | 33 | 0.31 | 0.23 |
| 18 | 450 | 31 | 23 | 0.22 | 0.16 |
| 20 | 550 | 23 | 16 | 0.16 | 0.11 |
| 24 | 600 | 20 | 14 | 0.14 | 0.10 |
| 30 | 750 | 21 | 15 | 0.14 | 0.10 |
| 36 | 900 | 21 | 15 | 0.14 | 0.10 |
| 42 | 1050 | 21 | 15 | 0.14 | 0.10 |

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## Fiber Glass Systems

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CI1200ENG March 2017

## Section 1 -Scope

This section covers the use of fiberglass reinforced plastic (FRP) pipe for mild chemical and water services up to $200^{\circ} \mathrm{F}$ and 435 psig steady pressure ratings which are diameter dependent. The pipe may be further serviced up to $210^{\circ} \mathrm{F}$ by applying a pressure derating factor of 0.92 to all component ratings.

The piping shall be furnished and installed complete with all fittings, joining materials, supports, specials, and other necessary appurtenances.

## Section 2-General Conditions

2.01 Coordination - Material furnished and work performed under this section shall be coordinated with related work and equipment specified under other sections.

| Valves | Section |  |
| :--- | :--- | :--- |
| Supports | Section | - |
| Equipment | Section |  |

2.02 Governing Standards - Except as modified or supplemented herein, all materials and construction methods shall comply with the applicable provisions of the following specifications and be tested using the following standards.

## Standard Specifications

| ASTM D2996 | Standard Specification for Filament-Wound "Fiberglass" (Glass- <br> Fiber-Reinforced-Thermosetting Resin) Pipe |
| :--- | :--- |
| ASTM D4024 | Standard Specification for Reinforced Thermosetting Resin (RTR) <br> Flanges |
| ASTM D5685 | Standard Specification for "Fiberglass" (Glass-Fiber-Reinforced- <br> Thermosetting-Resin) Pressure Pipe Fittings |

## Standard Test Methods

| ASTM D2992 | Standard Test Method for Obtaining Hydrostatic or Pressure Design <br> Basis for "Fiberglass" (Glass-Fiber-Reinforced-Thermosetting Resin) <br> Pipe and Fittings |
| :--- | :--- |
| ASTM D2925 | Standard Test Method for Measuring Beam Deflection of Reinforced <br> Thermosetting Plastic Pipe Under Full Bore Flow |
| ASTM D1599 | Standard Test Method for Short-Time Hydraulic Failure Pressure of <br> Plastic Pipe, Tubing and Fittings |
| ASTM D2105 | Standard Test Method for Longitudinal Tensile Properties of <br> "Fiberglass" (Glass-Fiber-Reinforced-Thermosetting Resin) Pipe <br> and Tube |
| ASTM D2412 | Standard Test Method for Determination of External Loading <br> Characteristics of Plastic Pipe by Parallel-Plate Loading |
|  |  |

2.04 Operating Conditions - In addition to the above minimum design requirements, the system shall meet the following minimum operating conditions:
a. Operating Pressure
b. Operating Temperature
c. Fluid Conveyed
d. Test Pressure
2.05 Quality Assurance - Pipe manufacturer's quality program shall be in compliance with ISO 9001 and/or API Q1.
2.06 Delivery, Storage and Handling - Pipe and fittings shall be protected from damage due to impact and point loading. Pipe shall be properly supported to avoid damage due to flexural strains. The contractor shall not allow dirt, debris, or other extraneous materials to get into pipe and fittings. All factory machined areas shall be protected from sunlight until installed.
2.07 Acceptable Manufacturers - NOV Fiber Glass Systems, (501) 568-4010, or approved equal.

## Section 3 - Materials and Construction

3.01 2"-42" Pipe - The pipe shall be manufactured by the filament winding process using an amine cured epoxy thermosetting resin to impregnate strands of continuous glass filaments, which are wound around a mandrel at a $543 / 4^{\circ}$ winding angle under controlled tension. Pipe shall be heat cured and the cure shall be confirmed using a Differential Scanning Calorimeter.

Pipe shall be supplied with a matching tapered bell and a matching tapered spigot.

Pipe shall have a minimum continuous steady pressure rating of 232 psig at $200^{\circ}$ F in accordance with ASTM D2992 Procedure B.
3.02 Flanges and Fittings - All fittings shall be manufactured using the same type materials as the pipe. Fittings may be manufactured either by compression molding, spray-up/ contact molding, or filament winding methods.

Fittings shall be adhesive bonded matched tapered bell and spigot, threaded or grooved adapters, or flanged. Fittings shall be certified to ASTM D5685.

Flanges shall have ANSI B16.5 Class 150 bolt hole patterns.
3.03 Adhesive - Adhesive shall be manufacturer's standard for the piping system specified.
3.04 Gaskets - Gaskets shall be 1/8" thick, 60-70 durometer full-face type suitable for the service shown on the drawings and as recommended in the manufacturer's standard installation procedures.
3.05 Bolts, Nuts and Washers - ASTM A307, Grade B, hex head bolts shall be supplied. SAE washers shall be supplied on all nuts and bolts.
3.06 Acceptable Products - Red Thread HP16 as manufactured by NOV Fiber Glass Systems, or approved equal.

## Section 4 - Installation and Testing

4.01 Training and Certification - All joints installed or constructed in the field shall be assembled by employees of the contractor who have been trained and certified to the Bonding Procedure Specification (BPS) provided by the pipe manufacturer. The BPS shall meet or exceed the requirements of ASME B31.3, Section A328.2.1. The pipe manufacturer or their authorized representative shall train the contractor's employees in the proper joining and assembly procedures required for the project, including hands-on participation by the contractor's employees in accordance with the BPS. Each bonder shall fabricate one pipe-to-pipe and one pipe-to-fitting joint for qualification testing. The pipe size and test pressure used in the qualification assembly shall meet or exceed the minimum requirements of ASME B31.3. Only bonders who have successfully completed the qualification pressure test shall bond pipe and fittings.
4.02 Pipe Installation - Pipe shall be installed as specified and indicated on the drawings. The piping system shall be installed in accordance with the manufacturer's current published installation procedures.

Each pressure containing joint shall be clearly marked to identify the bonder in accordance with ASME B31.3, Section A328.5.1.
4.03 Testing - Hydrostatic testing is recommended to evaluate the integrity of all new piping installations. For systems operating below the system rating, a test pressure of 1.5 times the system operating pressure is recommended; however, the maximum test pressure must not exceed 1.3 times the lowest pressure rated fiberglass component in the piping system.

The hydro test pressure should be repeated up to ten cycles from 0 psig to the test pressure to provide a high degree of confidence in the piping system. The final pressurization cycle should be allowed to stabilize for 15-30 minutes, then inspected for leaks. Do not attempt to repair leaks while system is pressurized. The hydro test should be repeated after any re-work is performed.

When hydro testing, open high-point vents (if used) to prevent entrapment of air in the lines as the system is slowly filled with water, then close the vents and slowly pressurize to the test pressure. Upon completion of hydro test, relieve the pressure on the system slowly, open vents and any drains to allow for complete drainage of the system.

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## Red Thread ${ }^{\text {TM }}$ HP25 Piping System

(Specification Guide)

## Section 1 -Scope

This section covers the use of fiberglass reinforced plastic (FRP) pipe for mild chemical and water services up to $200^{\circ} \mathrm{F}$ and 435 psig steady pressure ratings which are diameter dependent. The pipe may be further serviced up to $210^{\circ} \mathrm{F}$ by applying a pressure derating factor of 0.92 to all component ratings.

The piping shall be furnished and installed complete with all fittings, joining materials, supports, specials, and other necessary appurtenances.

## Section 2-General Conditions

2.01 Coordination - Material furnished and work performed under this section shall be coordinated with related work and equipment specified under other sections.

| Valves | Section | $\square$ |
| :--- | :--- | :--- |
| Supports | Section |  |
| Equipment | Section |  |

2.02 Governing Standards - Except as modified or supplemented herein, all materials and construction methods shall comply with the applicable provisions of the following specifications and be tested using the following standards.

## Standard Specifications

| ASTM D2996 | Standard Specification for Filament-Wound "Fiberglass" (Glass- <br> Fiber-Reinforced-Thermosetting Resin) Pipe |
| :--- | :--- |
| ASTM D4024 | Standard Specification for Reinforced Thermosetting Resin (RTR) <br> Flanges |
| ASTM D5685 | Standard Specification for "Fiberglass" (Glass-Fiber-Reinforced- <br> Thermosetting-Resin) Pressure Pipe Fittings |

## Standard Test Methods

| ASTM D2992 | Standard Test Method for Obtaining Hydrostatic or Pressure Design <br> Basis for "Fiberglass" (Glass-Fiber-Reinforced-Thermosetting Resin) <br> Pipe and Fittings |
| :--- | :--- |
| ASTM D2925 | Standard Test Method for Measuring Beam Deflection of Reinforced <br> Thermosetting Plastic Pipe Under Full Bore Flow |
| ASTM D1599 | Standard Test Method for Short-Time Hydraulic Failure Pressure of <br> Plastic Pipe, Tubing and Fittings |
| ASTM D2105 | Standard Test Method for Longitudinal Tensile Properties of <br> "Fiberglass" (Glass-Fiber-Reinforced-Thermosetting Resin) Pipe <br> and Tube |
| ASTM D2412 | Standard Test Method for Determination of External Loading <br> Characteristics of Plastic Pipe by Parallel-Plate Loading |
|  |  |

2.04 Operating Conditions - In addition to the above minimum design requirements, the system shall meet the following minimum operating conditions:
a. Operating Pressure
b. Operating Temperature
c. Fluid Conveyed
d. Test Pressure
2.05 Quality Assurance - Pipe manufacturer's quality program shall be in compliance with ISO 9001 and/or API Q1.
2.06 Delivery, Storage and Handling - Pipe and fittings shall be protected from damage due to impact and point loading. Pipe shall be properly supported to avoid damage due to flexural strains. The contractor shall not allow dirt, debris, or other extraneous materials to get into pipe and fittings. All factory machined areas shall be protected from sunlight until installed.
2.07 Acceptable Manufacturers - NOV Fiber Glass Systems, (501) 568-4010, or approved equal.

## Section 3 - Materials and Construction

3.01 2"-24" Pipe - The pipe shall be manufactured by the filament winding process using an amine cured epoxy thermosetting resin to impregnate strands of continuous glass filaments, which are wound around a mandrel at a $543 / 4^{\circ}$ winding angle under controlled tension. Pipe shall be heat cured and the cure shall be confirmed using a Differential Scanning Calorimeter.

Pipe shall be supplied with a matching tapered bell and a matching tapered spigot.

Pipe shall have a minimum continuous steady pressure rating of 362 psig at $200^{\circ}$ F in accordance with ASTM D2992 Procedure B.
3.02 Flanges and Fittings - All fittings shall be manufactured using the same type materials as the pipe. Fittings may be manufactured either by compression molding, spray-up/ contact molding, or filament winding methods.

Fittings shall be adhesive bonded matched tapered bell and spigot, threaded or grooved adapters, or flanged. Fittings shall be certified to ASTM D5685.

Flanges shall have ANSI B16.5 Class 300 or 150 bolt hole patterns per specific application requirements.
3.03 Adhesive - Adhesive shall be manufacturer's standard for the piping system specified.
3.04 Gaskets - Gaskets shall be 1/8" thick, 60-70 durometer full-face type suitable for the service shown on the drawings and as recommended in the manufacturer'sstandard installation procedures.
3.05 Bolts, Nuts and Washers - ASTM A307, Grade B, hex head bolts shall be supplied. SAE washers shall be supplied on all nuts and bolts.
3.06 Acceptable Products - Red Thread HP25 as manufactured by NOV Fiber Glass Systems, or approved equal.

## Section 4 - Installation and Testing

4.01 Training and Certification - All joints installed or constructed in the field shall be assembled by employees of the contractor who have been trained and certified to the Bonding Procedure Specification (BPS) provided by the pipe manufacturer. The BPS shall meet or exceed the requirements of ASME B31.3, Section A328.2.1. The pipe manufacturer or their authorized representative shall train the contractor's employees in the proper joining and assembly procedures required for the project, including hands-on participation by the contractor's employees in accordance with the BPS. Each bonder shall fabricate one pipe-to-pipe and one pipe-to-fitting joint for qualification testing. The pipe size and test pressure used in the qualification assembly shall meet or exceed the minimum requirements of ASME B31.3. Only bonders who have successfully completed the qualification pressure test shall bond pipe and fittings.
4.02 Pipe Installation - Pipe shall be installed as specified and indicated on the drawings. The piping system shall be installed in accordance with the manufacturer's current published installation procedures.

Each pressure containing joint shall be clearly marked to identify the bonder in accordance with ASME B31.3, Section A328.5.1.
4.03 Testing - Hydrostatic testing is recommended to evaluate the integrity of all new piping installations. For systems operating below the system rating, a test pressure of 1.5 times the system operating pressure is recommended; however, the maximum test pressure must not exceed 1.3 times the lowest pressure rated fiberglass component in the piping system.

The hydro test pressure should be repeated up to ten cycles from 0 psig to the test pressure to provide a high degree of confidence in the piping system. The final pressurization cycle should be allowed to stabilize for 15-30 minutes, then inspected for leaks. Do not attempt to repair leaks while system is pressurized. The hydro test should be repeated after any re-work is performed.

When hydro testing, open high-point vents (if used) to prevent entrapment of air in the lines as the system is slowly filled with water, then close the vents and slowly pressurize to the test pressure. Upon completion of hydro test, relieve the pressure on the system slowly, open vents and any drains to allow for complete drainage of the system.

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## Section 1 -Scope

This section covers the use of fiberglass reinforced plastic (FRP) pipe for dilute acid, caustic, and mild solvent services up to $230^{\circ} \mathrm{F}$ and 435 psig steady pressure.
The piping shall be furnished and installed complete with all fittings, joining materials, supports, specials, and other necessary appurtenances.

## Section 2-General Conditions

2.01 Coordination - Material furnished and work performed under this section shall be coordinated with related work and equipment specified under othersections.

| Valves | Section | - |
| :--- | :--- | :--- |
| Supports | Section |  |
| Equipment | Section |  |

2.02 Governing Standards - Except as modified or supplemented herein, all materials and construction methods shall comply with the applicable provisions of the following specifications and be tested using the following standards.

## Standard Specifications

| ASTM D2996 | Standard Specification for Filament-Wound "Fiberglass" (Glass- <br> Fiber-Reinforced-Thermosetting Resin) Pipe |
| :--- | :--- |
| ASTM D4024 | Standard Specification for Reinforced Thermosetting Resin (RTR) <br> Flanges |

## Standard Test Methods

| ASTM D2992 | Standard Test Method for Obtaining Hydrostatic or Pressure Design <br> Basis for "Fiberglass" (Glass-Fiber-Reinforced-Thermosetting Resin) <br> Pipe and Fittings |
| :--- | :--- |
| ASTM D1599 | Standard Test Method for Short-Time Hydraulic Failure Pressure of <br> Plastic Pipe, Tubing and Fittings |
| ASTM D2105 | Standard Test Method for Longitudinal Tensile Properties of <br> "Fiberglass" (Glass-Fiber-Reinforced-Thermosetting Resin) Pipe <br> and Tube |
| ASTM D2412 | Standard Test Method for Determination of External Loading <br> Characteristics of Plastic Pipe by Parallel-Plate Loading |
| ASTM D2925 | Standard Test Method for Beam Deflection of "Fiberglass" (Glass- <br> Fiber-Reinforced Thermosetting Resin) Pipe Under Bore Flow |

2.04 Operating Conditions - In addition to the above minimum design requirements, the system shall meet the following minimum operating conditions:
a. Operating Pressure
b. Operating Temperature
c. Fluid Conveyed
d. Test Pressure
2.05 Quality Assurance - Pipe manufacturer's quality program shall be in compliance with ISO 9001 and/or API Q1.
2.06 Delivery, Storage and Handling - Pipe and fittings shall be protected from damage due to impact and point loading. Pipe shall be properly supported to avoid damage due to flexural strains. The contractor shall not allow dirt, debris, or other extraneous materials to get into pipe and fittings. All factory machined areas shall be protected from sunlight until installed.
2.07 Acceptable Manufacturers - NOV Fiber Glass Systems, (501) 568-4010, or approved equal.

## Section 3 - Materials and Construction

3.01 2"-42" Pipe - The pipe shall be manufactured by the filament winding process using an amine cured epoxy thermosetting resin to impregnate strands of continuous glass filaments, which are wound around a mandrel at a $543 / 4^{\circ}$ winding angle under controlled tension. Pipe shall be heat cured and the cure shall be confirmed using a Differential Scanning Calorimeter.

All pipe shall have a resin-rich corrosion barrier reinforced with surfacing veil. The corrosion barrier shall have a minimum resin content of $80 \%$. The minimum acceptable cured thickness of the corrosion barrier shall be as follows:

$$
\begin{array}{ll}
1^{\prime \prime}-1^{1 / 22^{\prime \prime}} & 12 \text { mil minimum } \\
2^{\prime \prime}-42^{\prime \prime} & 20 \text { mil minimum }
\end{array}
$$

Pipe shall be supplied with a matching tapered bell and a matching tapered spigot.

Pipe shall have a minimum continuous steady pressure rating of 232 psig at $200^{\circ}$ F in accordance with ASTM D2992 Procedure B.
3.02 Flanges and Fittings - All fittings shall be manufactured using the same type materials as the pipe. Fittings may be manufactured either by compression molding, spray-up/ contact molding, or filament winding methods.

Fittings shall be adhesive bonded matched tapered bell and spigot or flanged.

Flanges shall have ANSI B16.5 Class 150 bolt hole patterns.
3.03 Adhesive - Adhesive shall be manufacturer's standard for the piping system specified.
3.04 Gaskets-Gaskets shall be 1/8" thick, 60-70 durometer full-face type suitable for the service shown on the drawings and as recommended in the manufacturer's standard installation procedures.
3.05 Bolts, Nuts and Washers - ASTM F593, 304 stainless steel hex head bolts shall be supplied. SAE washers shall be supplied on all nuts and bolts.
3.06 Acceptable Products - Green Thread HP16 as manufactured by NOV Fiber Glass Systems, or approved equal.

## Section 4-Installation and Testing

4.01 Training and Certification - All joints installed or constructed in the field shall be assembled by employees of the contractor who have been trained by the pipe manufacturer. The pipe manufacturer or their authorized representative shall train the contractor's employees in the proper joining and assembly procedures required for the project, including hands-on participation by the contractor's employees. Each bonder shall fabricate one pipe-to-pipe and one pipe-to-fitting joint that shall pass the minimum pressure test for the application as stated in section 2.03. d without leaking.

Only bonders who have successfully completed the pressure test shall bond pipe and fittings.

Certification by the manufacturer shall be in compliance with ASME B31.3, Section A328.2 for the type of joint being made.
4.02 Pipe Installation - Pipe shall be installed as specified and indicated on the drawings.

The piping system shall be installed in accordance with the manufacturer's current published installation procedures.
4.03 Testing - Hydrostatic testing is recommended to evaluate the integrity of all new piping installations. For systems operating below the system rating, a test pressure of 1.5 times the system operating pressure is recommended; however, the maximum test pressure must not exceed 1.3 times the lowest pressure rated fiberglass component in the piping system.

The hydro test pressure should be repeated up to ten cycles from 0 psig to the test pressure to provide a high degree of confidence in the piping system. The final pressurization cycle should be allowed to stabilize for 15-30 minutes, then inspected for leaks. Do not attempt to repair leaks while system is pressurized. The hydro test should be repeated after any re-work is performed.
When hydro testing, open high-point vents (if used) to prevent entrapment of air in the lines as the system is slowly filled with water, then close the vents and slowly pressurize to the test pressure. Upon completion of hydro test, relieve the pressure on the system slowly, open vents and any drains to allow for complete drainage of the system.

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## Green Thread™ HP25 Piping System <br> (Specification Guide)

## Section 1 -Scope

This section covers the use of fiberglass reinforced plastic (FRP) pipe for dilute acid, caustic, and mild solvent services up to 362 psig steady pressure at $200^{\circ}$. Service up to $230^{\circ}$ F allowed with reduced pressure.
The piping shall be furnished and installed complete with all fittings, joining materials, supports, specials, and other necessary appurtenances.

## Section 2 - General Conditions

2.01 Coordination - Material furnished and work performed under this section shall be coordinated with related work and equipment specified under othersections.

| Valves | Section | - |
| :--- | :--- | :--- |
| Supports | Section | - |
| Equipment | Section |  |

2.02 Governing Standards - Except as modified or supplemented herein, all materials and construction methods shall comply with the applicable provisions of the following specifications and be tested using the following standards.

## Standard Specifications



## Standard Test Methods

| ASTM D2992 | Standard Test Method for Obtaining Hydrostatic or Pressure Design <br> Basis for "Fiberglass" (Glass-Fiber-Reinforced-Thermosetting Resin) <br> Pipe and Fittings |
| :--- | :--- |
| ASTM D1599 | Standard Test Method for Short-Time Hydraulic Failure Pressure of <br> Plastic Pipe, Tubing and Fittings |
| ASTM D2105 | Standard Test Method for Longitudinal Tensile Properties of <br> "Fiberglass" (Glass-Fiber-Reinforced-Thermosetting Resin) Pipe <br> and Tube |
| ASTM D2412 | Standard Test Method for Determination of External Loading <br> Characteristics of Plastic Pipe by Parallel-Plate Loading |
| ASTM D2925 | Standard Test Method for Beam Deflection of "Fiberglass" (Glass- <br> Fiber-Reinforced Thermosetting Resin) Pipe Under Bore Flow |

2.04 Operating Conditions - In addition to the above minimum design requirements, the system shall meet the following minimum operating conditions:
a. Operating Pressure
b. Operating Temperature
c. Fluid Conveyed
d. Test Pressure
2.05 Quality Assurance - Pipe manufacturer's quality program shall be in compliance with ISO 9001 and/or API Q1.
2.06 Delivery, Storage and Handling - Pipe and fittings shall be protected from damage due to impact and point loading. Pipe shall be properly supported to avoid damage due to flexural strains. The contractor shall not allow dirt, debris, or other extraneous materials to get into pipe and fittings. All factory machined areas shall be protected from sunlight until installed.
2.07 Acceptable Manufacturers - NOV Fiber Glass Systems, (501) 568-4010, or approved equal.

## Section 3 - Materials and Construction

3.01 2"-24" Pipe - The pipe shall be manufactured by the filament winding process using an amine cured epoxy thermosetting resin to impregnate strands of continuous glass filaments, which are wound around a mandrel at a $543 / 4^{\circ}$ winding angle under controlled tension. Pipe shall be heat cured and the cure shall be confirmed using a Differential Scanning Calorimeter.

All pipe shall have a resin-rich corrosion barrier reinforced with surfacing veil. The corrosion barrier shall have a minimum resin content of $80 \%$. The minimum acceptable cured thickness of the corrosion barrier shall be as follows:

$$
\text { 2" - 24" } \quad 20 \text { mil minimum }
$$

Pipe shall be supplied with a matching tapered bell and a matching tapered spigot.

Pipe shall have a minimum continuous steady pressure rating of 362 psig at $200^{\circ}$ F in accordance with ASTM D2992 Procedure B.
3.02 Flanges and Fittings - All fittings shall be manufactured using the same type materials as the pipe. Fittings may be manufactured either by compression molding, spray-up/ contact molding, or filament winding methods.

Fittings shall be adhesive bonded matched tapered bell and spigot or flanged.

Flanges shall have ANSI B16.5 Class 300 or Class 150 bolt hole pattern, as ordered.
3.03 Adhesive - Adhesive shall be manufacturer's standard for the piping system specified.
3.04 Gaskets-Gaskets shall be 1/8" thick, 60-70 durometer full-face type suitable for the service shown on the drawings and as recommended in the manufacturer's standard installation procedures.
3.05 Bolts, Nuts and Washers - ASTM F593, 304 stainless steel hex head bolts shall be supplied. SAE washers shall be supplied on all nuts and bolts.
3.06 Acceptable Products - Green Thread HP25 as manufactured by NOV Fiber Glass Systems, or approved equal.

## Section 4-Installation and Testing

4.01 Training and Certification - All joints installed or constructed in the field shall be assembled by employees of the contractor who have been trained by the pipe manufacturer. The pipe manufacturer or their authorized representative shall train the contractor's employees in the proper joining and assembly procedures required for the project, including hands-on participation by the contractor's employees. Each bonder shall fabricate one pipe-to-pipe and one pipe-to-fitting joint that shall pass the minimum pressure test for the application as stated in section 2.03. d without leaking.

Only bonders who have successfully completed the pressure test shall bond pipe and fittings.

Certification by the manufacturer shall be in compliance with ASME B31.3, Section A328.2 for the type of joint being made.
4.02 Pipe Installation - Pipe shall be installed as specified and indicated on the drawings.

The piping system shall be installed in accordance with the manufacturer's current published installation procedures.
4.03 Testing - Hydrostatic testing is recommended to evaluate the integrity of all new piping installations. For systems operating below the system rating, a test pressure of 1.5 times the system operating pressure is recommended; however, the maximum test pressure must not exceed 1.3 times the lowest pressure rated fiberglass component in the piping system.

The hydro test pressure should be repeated up to ten cycles from 0 psig to the test pressure to provide a high degree of confidence in the piping system. The final pressurization cycle should be allowed to stabilize for 15-30 minutes, then inspected for leaks. Do not attempt to repair leaks while system is pressurized. The hydro test should be repeated after any re-work is performed.
When hydro testing, open high-point vents (if used) to prevent entrapment of air in the lines as the system is slowly filled with water, then close the vents and slowly pressurize to the test pressure. Upon completion of hydro test, relieve the pressure on the system slowly, open vents and any drains to allow for complete drainage of the system.

## Fiber Glass Systems

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## Applications

- Chemical Processing Liquids
- Food Processing Liquids
- Potable Water
- Cooling Water
- Condensate Return
- Industrial Wastewater
- Mildly Corrosive Liquids
- Crude Oil \& Gas
- Produced Water
- Saltwater
- $\mathrm{CO}_{2}$


## Materials and Construction

All pipe is filament wound with continuous strands of glass filaments saturated with amine-cured epoxy thermosetting resin. The pipe wall includes an internal resin-rich corrosion barrier. The pipe is designed in accordance with API 15 LR at $200^{\circ} \mathrm{F}\left(93^{\circ} \mathrm{C}\right)$, serviceable up to $210^{\circ} \mathrm{F}\left(99^{\circ} \mathrm{C}\right)$ by applying a derating factor of 0.92 to all component ratings. The pressure rating is 362 psig (25 Bar) for a hydrostatic design life of 20 years per ASTM D2992 Procedure B. For 2"-6" (50-150 $\mathrm{mm})$ sizes, the matched tapered joining method is used and the pipe is available in random 30 foot ( 9.14 meter) lengths. For $8^{\prime \prime}-24^{\prime \prime}(200-600 \mathrm{~mm})$ sizes, the matched tapered joining method is used and the pipe is available in random 40 foot ( 12 meter) lengths. Pipe is supplied with one end belled (integral bell orfactory-bonded coupling) and one end tapered.

ASTM D-2996 Classification: RTRP-11AW1-3110 forstatic design basis.

## Fittings

Fittings are manufactured with the same chemical/temperature capabilities as the pipe. Depending on the configurations and size, the fittings construction method will be compression molded, contact molded, fabricated or filament wound.

## Joining System

- T.A.B. ${ }^{\text {TM }}$ - In sizes 2"- 6 ", pipe and couplings are supplied with a threaded and bonded (T. A. B) joining system. Double-lead threads provide quick secure adhesive connections during installation.
- Bell \& Spigot - The pipe and fittings are joined using the bell and spigot connection. Pipe is supplied with one end belled (integral bell orfactory-bonded coupling) and one end tapered in sizes 8 " $-24^{\prime \prime}$. For $8^{\prime \prime}-24^{\prime \prime}$ sizes, the matched tapered joining method is used and the pipe is available in random 12 meter ( 40 feet) lengths.
Epoxy adhesive is used to secure the joint. When properly installed, the system will operate at the maximum pressure rating of the pipe.
- Flanged - Flanged connections are available for all components and diameters.

т.A.B.


Bell \& Spigot


Flanged

Nominal Dimensional Data

| Pip |  | Inside Diameter |  | Outside Diameter ${ }^{(2)}$ |  | Reinforced Wall Thickness ${ }^{(1)}$ |  | Weight |  | Capacity |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | in | mm | in | mm | in | mm | lbs/ft | kg/m | gal/ft | 1/m |
| $2^{(1)}$ | 50 | 2.24 | 57 | 2.35 | 60 | 0.058 | 1.5 | 0.4 | 0.7 | 0.2 | 2.5 |
| $3^{(1)}$ | 80 | 3.36 | 85 | 3.54 | 90 | 0.086 | 2.2 | 0.8 | 1.2 | 0.5 | 5.7 |
| 4 | 100 | 4.36 | 111 | 4.53 | 115 | 0.083 | 2.1 | 1.0 | 1.5 | 0.8 | 9.7 |
| 6 | 150 | 6.40 | 163 | 6.65 | 169 | 0.122 | 3.1 | 2.2 | 3.2 | 1.7 | 20.9 |
| 8 | 200 | 8.36 | 212 | 8.68 | 221 | 0.164 | 4.2 | 3.8 | 5.6 | 2.9 | 35.4 |
| 10 | 250 | 10.36 | 263 | 10.76 | 273 | 0.203 | 5.2 | 5.8 | 8.7 | 4.4 | 54.4 |
| 12 | 300 | 12.28 | 312 | 12.76 | 324 | 0.241 | 6.1 | 8.2 | 12.2 | 6.2 | 76.4 |
| 14 | 350 | 14.03 | 356 | 14.58 | 370 | 0.275 | 7.0 | 10.7 | 15.9 | 8.0 | 100.0 |
| 16 | 400 | 16.03 | 407 | 16.66 | 423 | 0.314 | 8.0 | 13.9 | 20.7 | 10.6 | 130.0 |
| 18 | 450 | 17.83 | 453 | 18.54 | 471 | 0.357 | 9.1 | 17.6 | 26.2 | 13.0 | 161.0 |
| 20 | 500 | 19.83 | 504 | 20.62 | 524 | 0.397 | 10.1 | 21.8 | 32.4 | 16.0 | 199.0 |
| 24 | 600 | 23.83 | 605 | 24.78 | 629 | 0.477 | 12.1 | 31.5 | 46.9 | 23.2 | 288.0 |

${ }^{(1)}$ Reinforced wall thickness exceeds the requirement for 362 psig and may be operated up to 435 psig.
${ }^{(2)}$ Outer diameter is for use in flexibility analysis. Consult factory representative for pipe OD tolerances.
NOTE: System rating is determined by pressure ratings of fittings used in the piping system. See document CI1370 for individual fitting pressure ratings.

## Supports

The following engineering analysis must be performed to determine the maximum support spacing for the piping system. Proper pipe support spacing depends on the temperature, pressure and weight of the fluid carried in the pipe. The support spacing is calculated using continuous beam equations and the pipe bending modulus derived from long-term beam bending tests. The following tables were developed to ensure a design that limits beam mid-span deflection to $1 / 2$ inch to ensure good appearance and adequate drainage. Any additional weight on the piping system such as insulation or heat tracing requires further consideration. Restrained (anchored) piping systems operating at elevated temperatures often result in guide spacing requirements that are more stringent than simple unrestrained piping systems. In this case, the maximum guide spacing will dictate the support/guide spacing requirements for the system. Pipe support spans at changes in direction require special attention. Supported and unsupported fittings. at changes in direction are considered in the following tables and must be followed to properly design the piping system.

Support Spacing vs. Specific Gravity

| Specific Gravity | 2.00 | 1.50 | 1.25 | 1.00 | 0.75 |
| :--- | :--- | :--- | :--- | :--- | :--- |
| Multiplier | 0.85 | 0.91 | 0.95 | 1.00 | 1.06 |

Example: 18 " $(450 \mathrm{~mm})$ pipe @ $75^{\circ} \mathrm{F}\left(24^{\circ} \mathrm{C}\right)$ with 1.5 specific gravity fluid, maximum support spacing $=37.3^{\prime} \times 0.91=33.9 \mathrm{ft}$.

Maximum Support Spacing for Pipe ${ }^{(1)}$

| Size | Continuous Spans of Pipe $^{(2)}$ |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- |
|  | feet |  | meters $^{\prime}$ |  |  |  |
| in | $\mathbf{m m}$ | $\mathbf{7 5}^{\circ} \mathbf{F}$ | $\mathbf{2 0 0}^{\circ} \mathbf{F}$ | $\mathbf{2 4}^{\circ} \mathbf{C}$ | $\mathbf{9 3}^{\circ} \mathbf{C}$ |
| 2 | 50 | 14.0 | 10.2 | 4.27 | 3.10 |
| 3 | 80 | 17.1 | 12.4 | 5.22 | 3.79 |
| 4 | 100 | 18.2 | 13.2 | 5.56 | 4.03 |
| 6 | 150 | 22.1 | 16.0 | 6.74 | 4.89 |
| 8 | 200 | 25.4 | 18.4 | 7.75 | 5.62 |
| 10 | 250 | 28.3 | 20.5 | 8.63 | 6.25 |
| 12 | 300 | 30.8 | 22.3 | 9.40 | 6.81 |
| 14 | 350 | 32.9 | 23.9 | 10.04 | 7.28 |
| 16 | 400 | 35.2 | 25.5 | 10.74 | 7.78 |
| 18 | 450 | 37.3 | 27.0 | 11.38 | 8.25 |
| 20 | 500 | 39.3 | 28.5 | 12.00 | 8.70 |
| 24 | 600 | 43.1 | 31.3 | 13.15 | 9.53 |

${ }^{(1)}$ For $\mathrm{Sg}=1.0$, consult manufacturer for heavier insulated pipe support spans. Span
recommendations include no provision for weight of (fittings, valves, etc.) or thrusts at branches and turns. Heavy valves and other appurtenances must be supported separately.
${ }^{(2)}$ Calculated spans are based on $1 / 2$ " mid-span deflections to ensure good appearance and adequate drainage. Total system stresses should always be taken into account by the system design engineer when determining support spans.

There are seven basic rules to follow when designing piping system supports, anchors, and guides:

1. Do not exceed the recommended support span.
2. Support valves and heavy in-line equipment independently.

This applies to both vertical and horizontal piping.
3. Protect pipe from external abrasion.
4. Avoid point contact loads
5. Avoid excessive bending. This applies to handling, transporting, initial layout, and final installed position.
6. Avoid excessive vertical run loading. Vertical loads should be supported sufficiently to minimize bending stresses at outlets or changes in direction.
7. Provide adequate axial and lateral restraint to ensure line stability during rapid changes in flow.

Adjustment Factors for Various Spans With Unsupported Fitting at Change in Direction

|  | Span Type | Factor |
| :--- | :--- | :--- |
| LC | Continuous interior or fixed end spans | 1.00 |
| C | Second span from supported end or unsupported fitting | 0.80 |
| A+B | Sum of unsupported spans at fitting | $\leq 0.75^{\star}$ |
| D | Simple supported end span | 0.67 |

*For example: If continuous support is 10 ft . ( 3.04 m ), $\mathrm{A}+\mathrm{B}$ must not exceed 7.5 ft .( 2.28 m ) (A=3 ft. $(0.91 \mathrm{~m})$ and $B=4.5 \mathrm{ft}$. $(1.37 \mathrm{~m})$ ) would satisfy this condition.


Adjustment Factors for Various Spans With Supported Fitting at Change in Direction

|  | Span Type | Factor |
| :--- | :--- | :--- |
| LC | Continuous interior or fixed end spans | 1.00 |
| A | Second span from simple supported end or unsupported fitting | 0.80 |
| B | Simple supported end span | 0.67 |



## Thermal Expansion

The effects of thermal gradients on piping systems may be significant and should be considered in every piping system stress analysis. Pipe line movements due to thermal expansion or contraction may cause
high stresses or even buckle a pipe line if improperly restrained. Several piping system designs are used to manage thermal expansion and contraction in above ground piping systems. They are listed below according to economic preference:

1. Use of inherent flexibility in directional changes.
2. Restraining axial movements and guiding to prevent buckling.
3. Use expansion loops to absorb thermal movements.
4. Use mechanical expansion joints to absorb thermal movements.

To perform a thermal analysis the following information is required:

1. Isometric layout of piping system
2. Physical and material properties of pipe
3. Design temperatures
4. Installation temperature (Final tie in temperature)
5. Terminal equipment load limits
6. Supportmovements

A comprehensive review of temperature effects on fiberglass pipe may be found in NOV Fiber Glass Systems' Engineering and Piping Design Guide, Section 3.

| Change in <br> Temperature |  | Pipe Change in <br> Length |  |
| :--- | :--- | :--- | :--- |
| ${ }^{\circ} \mathbf{F}$ | ${ }^{\circ} \mathbf{C}$ | in/100 ft | $\mathbf{c m} / \mathbf{1 0 0} \mathbf{~ m}$ |
| 25 | 13.9 | 0.32 | 2.67 |
| 50 | 27.8 | 0.64 | 5.35 |
| 75 | 41.7 | 0.96 | 8.02 |
| 100 | 55.6 | 1.28 | 10.7 |

## Testing

Hydrostatic testing is recommended to evaluate the integrity of all new piping installations. For systems operating below the system rating, a test pressure of 1.5 times the system operating pressure is recommended; however, the maximum test pressure must not exceed 1.3 times the lowest pressure rated fiberglass component in the piping system.
The hydro test pressure should be repeated up to ten cycles from 0 psig to the test pressure to provide a high degree of confidence in the piping system. The final pressurization cycle should be allowed to stabilize for 15-30 minutes, then inspected for leaks. Do not attempt to repair leaks while system is pressurized. The hydro test should be repeated after any re-work is performed.

When hydro testing, open high-point vents (ifused) to prevent entrapment of air in the lines as the system is slowly filled with water, then close the vents and slowly pressurize to the test pressure. Upon completion of hydro test, relieve the pressure on the system slowly, open vents and any drains to allow for complete drainage of the system.

## Water Hammer

Piping systems may be damaged by pressure surges due to water hammer. The use of soft start pumps and slow actuating valves will reduce the magnitude of surge pressures during operation and are highly recommended.

## Typical Mechanical Properties

| Pipe Property | $75^{\circ} \mathrm{F}$ | $24^{\circ} \mathrm{C}$ | $200^{\circ} \mathrm{F}$ | $93^{\circ} \mathrm{C}$ | Method |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | psi | MPa | psi | MPa |  |
| Axial Tensile |  |  |  |  |  |
| Ultimate Stress | 9,530 | 65.7 | 6,585 | 45.4 | ASTM D2105 |
| Modulus of Elasticity | $1.68 \times 10^{6}$ | 11,584 | $1.42 \times 10^{6}$ | 9,791 | ASTM D2105 |
| Poisson's Ratio, $v_{\text {ah }}\left(v_{\text {ha }}\right)^{(1)}$ | 0.35 (0.61) |  |  |  |  |
| Axial Compression |  |  |  |  |  |
| Ultimate Stress | 12,510 | 86.3 | 8,560 | 59.0 | ASTM D695 |
| Modulus of Elasticity | $0.677 \times 10^{6}$ | 4,668 | $0.379 \times 10^{6}$ | 2,613 | ASTM D695 |
| Beam Bending |  |  |  |  |  |
| Modulus of Elasticity (Long Term) | $2.6 \times 10^{6}$ | 17,927 | $0.718 \times 10^{6}$ | 4,951 | ASTM D2925 |
| Hydrostatic Burst |  |  |  |  |  |
| Ultimate Hoop Tensile Stress | 40,150 | 277 | 36,480 | 252 | ASTM D1599 |
| Hydrostatic Hoop Design Stress |  |  |  |  |  |
| Static 20 Year Life LTHS - 95\% LCL | - | - | 18,203-14,689 | 125.5-101.3 | ASTM D2992-Procedure B |
| Static 50 Year Life LTHS -95\% LCL | - | - | 16,788-13,142 | 115.7-90.6 | ASTM D2992-Procedure B |
| Parallel Plate |  |  |  |  |  |
| Hoop Modulus of Elasticity | $3.02 \times 10^{6}$ | 20,822 | - | - | ASTM D2412 |
| Shear Modulus | $1.76 \times 10^{6}$ | 12,135 | $1.63 \times 10^{6}$ | 11,240 | - |

## Typical Physical Properties

| Pipe Property | Value | Value | Method |
| :--- | :--- | :--- | :--- |
| Thermal <br> Conductivity | $0.23 \mathrm{BTU} / \mathrm{hr} \cdot \mathrm{ft} \cdot{ }^{\circ} \mathrm{F}$ | $0.4 \mathrm{~W} / \mathrm{m}^{\circ} \mathrm{C}$ | ASTM D177 |
| Thermal <br> Expansion | $10.7 \times 10^{-6} \mathrm{in} / \mathrm{in} /{ }^{\circ} \mathrm{F}$ | $19.3 \times 10^{-6} \mathrm{~mm} / \mathrm{mm} /{ }^{\circ} \mathrm{C}$ | ASTM D696 |
| Absolute <br> Roughness | 0.00021 in | 0.00053 mm |  |
| Specific Gravity |  | 1.8 | ASTM D792 |

${ }^{(1)} V_{\text {ha }}=$ The ratio of axial strain to hoop strain resulting from stress in the hoop direction.
$V_{\mathrm{ah}}=$ The ratio of hoop strain to axial strain resulting from stress in the axial direction.
${ }^{(2)}$ The differential pressure between internal and external pressure which causes collapse.
${ }^{(3)}$ A 0.67 design factor is recommended for short duration vacuum service. A full vacuum is equal to $14.7 \mathrm{psig}(0.101 \mathrm{MPa})$ differential pressure at sea level.
${ }^{(4)} \mathrm{A} 0.33$ design factor is recommended for sustained (long-term) differential collapse pressure design and operation.

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## Fiber Glass Systems

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# Green Thread™ HP 16 

## Applications

- Chemical Processing Liquids
- Food Processing Liquids
- Potable Water
- Cooling Water
- Condensate Return
- Industrial Wastewater
- Mildly Corrosive Liquids
- Crude Oil \& Gas


## Materials and Construction

Pipe is manufactured by filament winding process using amine-cured epoxy thermosetting resin to impregnate strands of continuous glass filaments. The pipe wall includes an internal resin-rich corrosion barrier.

Green Thread HP 16 products are available in sizes 1"-42" (25-1,050 mm) diameters with a static pressure rating of $232 \mathrm{psig}(16 \mathrm{bar})$. The pipe is designed for continuous operation at $200^{\circ} \mathrm{F}\left(93^{\circ} \mathrm{C}\right)$ serviceable up to $230^{\circ} \mathrm{F}\left(110^{\circ} \mathrm{C}\right)$ by applying a derating factor of 0.76 to all component ratings. Sizes 1"-6" (25-150 mm) are available in $20^{\prime}(6 \mathrm{~m})$ lengths and sizes $8^{\prime \prime}-42^{\prime \prime}(150-1,050 \mathrm{~mm})$ are available in $19^{\prime}$ or $39^{\prime}(6$ or 12 m ) lengths.

ASTM D-2996 Classification: RTRP-11FX1-3110 forstatic design basis.

## Fittings

Fittings are manufactured with the same chemical and temperature capabilities as the pipe. Depending on the configurations and size, the fitting construction method will be compression molded, contact molded, fabricated or filament wound. Fitting details are in two documents. Use CI1350 forsizes $1^{\prime \prime}-16^{\prime \prime}$ ( $25-400 \mathrm{~mm}$ ) and Cl1351 for $188^{\prime \prime}-42^{\prime \prime}$ ( 450 $1050 \mathrm{~mm})$. All fittings may not have the same pressure rating as the pipe. A piping system design pressure rating is governed by the lowest rated component used in the system.

## Joining System

- Bell \& Spigot - Matched-taper joint secured with epoxy adhesive. Self-locking feature resists movement, facilitating joining runs of pipe without waiting for adhesive to cure.
- Flanged - Available for all piping systems and diameters; factory assembled or shipped loose for assembly in the field.
- Produced Water
- Saltwater
- $\mathrm{CO}_{2}$


Nominal Dimensional Data

| Pipe Size |  | Inside Diameter |  | Outside Diameter |  | Minimum Reinforced Wall Thickness |  | Liner Thickness |  | Weight ${ }^{(2)}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | in | mm | in | mm | in | mm | in | mm | lbs/ft | kg/m |
| $1^{(1)}$ | 25 | 1.19 | 30.2 | 1.34 | 34.0 | 0.057 | 1.45 | 0.015 | 0.38 | 0.2 | 0.4 |
| $11 / 2^{(1)}$ | 40 | 1.76 | 44.7 | 1.91 | 48.5 | 0.062 | 1.57 | 0.015 | 0.38 | 0.4 | 0.6 |
| $2^{(1)}$ | 50 | 2.15 | 54.6 | 2.34 | 59.4 | 0.075 | 1.91 | 0.020 | 0.51 | 0.6 | 0.8 |
| $3^{(1)}$ | 80 | 3.28 | 83.3 | 3.47 | 88.1 | 0.075 | 1.91 | 0.020 | 0.51 | 0.8 | 1.2 |
| $4^{(1)}$ | 100 | 4.28 | 108.7 | 4.47 | 113.5 | 0.075 | 1.91 | 0.020 | 0.51 | 1.1 | 1.6 |
| $6^{(1)}$ | 150 | 6.35 | 161.3 | 6.60 | 167.6 | 0.105 | 2.67 | 0.020 | 0.51 | 2.1 | 3.2 |
| 8 | 200 | 8.36 | 212.3 | 8.66 | 220.0 | 0.127 | 3.23 | 0.020 | 0.51 | 3.3 | 4.9 |
| 10 | 250 | 10.36 | 263.1 | 10.72 | 272.3 | 0.156 | 3.96 | 0.020 | 0.51 | 4.9 | 7.3 |
| 12 | 300 | 12.29 | 312.2 | 12.70 | 322.6 | 0.185 | 4.70 | 0.020 | 0.51 | 7.1 | 10.6 |
| 14 | 350 | 14.04 | 356.6 | 14.49 | 368.0 | 0.204 | 5.18 | 0.020 | 0.51 | 8.9 | 13.2 |
| 16 | 400 | 16.04 | 407.4 | 16.55 | 420.4 | 0.234 | 5.94 | 0.020 | 0.51 | 11.6 | 17.3 |
| 18 | 450 | 17.82 | 452.6 | 18.37 | 466.6 | 0.257 | 6.53 | 0.020 | 0.51 | 14.1 | 21.0 |
| 20 | 500 | 19.83 | 503.7 | 20.42 | 518.7 | 0.273 | 6.93 | 0.020 | 0.51 | 16.5 | 24.6 |
| 24 | 600 | 23.83 | 605.3 | 24.53 | 623.1 | 0.328 | 8.33 | 0.020 | 0.51 | 23.7 | 35.3 |
| 30 | 750 | 30.03 | 762.8 | 30.93 | 785.6 | 0.430 | 10.90 | 0.020 | 0.51 | 38.7 | 57.6 |
| 36 | 900 | 36.03 | 915.2 | 37.09 | 942.0 | 0.510 | 13.00 | 0.020 | 0.51 | 54.7 | 81.4 |
| 42 | 1050 | 42.03 | 1067.6 | 43.27 | 1099.0 | 0.600 | 15.20 | 0.020 | 0.51 | 74.8 | 111.3 |

${ }^{(1)}$ Minimum reinforced wall thickness exceeds the requirement for the 232 psi standard rating for HP16. The 1 " thru 3 " pipe sizes are rated to 435 psig and the 4 " and 6 " sizes to 300 psig.
${ }^{2)}$ Based on the minimum wall.

## Supports

Proper pipe supportspacing depends on the temperature and weight of the fluid in the pipe. The support spacing table is based on unrestrained continuous beam theory using the pipe bending modulus derived from long-term beam bending tests. The following tables were developed to ensure a design that limits beam mid-span deflection to $1 / 2$ inch to ensure good appearance and adequate drainage. Any additional loads on the piping system such as insulation, wind, seismic, etc. requires further consideration. Restrained (anchored) piping systems operating at elevated temperatures may result in guide spacing requirements that are shorter than unrestrained piping systems. In this case, the maximum guide spacing governs the supportspan requirements for the system. Pipe spans near elbows require special attention. Both supported and unsupported elbows are considered in the following tables and must be followed to properly design the piping system.

Support Spacing vs. Specific Gravity

| Specific Gravity | 2.00 | 1.50 | 1.25 | 1.00 | 0.75 |
| :--- | :--- | :--- | :--- | :--- | :--- |
| Multiplier | 0.86 | 0.92 | 0.96 | 1.00 | 1.07 |

Example: $6^{\prime \prime}$ pipe @ $75^{\circ} \mathrm{F}\left(23.9^{\circ} \mathrm{C}\right)$ with 1.5 specific gravity fluid,
maximum support spacing $=21.3 \times 0.92=19.6 \mathrm{ft}$.

Maximum Support Spacing for Uninsulated Pipe ${ }^{(1)}$

| Size |  | Continuous Spans of Pipe ${ }^{(2)}$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | feet |  | meters |  |
| in | mm | $75^{\circ} \mathrm{F}$ | $200^{\circ} \mathrm{F}$ | $24^{\circ} \mathrm{C}$ | $93^{\circ} \mathrm{C}$ |
| 1 | 25 | 11.7 | 8.5 | 3.6 | 2.6 |
| $11 / 2$ | 40 | 13.3 | 9.6 | 4.1 | 2.9 |
| 2 | 50 | 14.7 | 10.6 | 4.5 | 3.3 |
| 3 | 80 | 16.5 | 12.0 | 5.0 | 3.7 |
| 4 | 100 | 17.7 | 12.8 | 5.4 | 3.9 |
| 6 | 150 | 21.3 | 15.4 | 6.5 | 4.7 |
| 8 | 200 | 24.0 | 17.3 | 7.3 | 5.3 |
| 10 | 250 | 26.6 | 19.3 | 8.1 | 5.9 |
| 12 | 300 | 29.0 | 21.0 | 8.8 | 6.4 |
| 14 | 350 | 30.7 | 22.2 | 9.4 | 6.8 |
| 16 | 400 | 32.8 | 23.8 | 10.1 | 7.3 |
| 18 | 450 | 34.5 | 25.0 | 10.5 | 7.6 |
| 20 | 500 | 36.0 | 26.1 | 11.0 | 8.0 |
| 24 | 600 | 39.5 | 28.6 | 12.0 | 8.7 |
| 30 | 800 | 44.7 | 32.4 | 13.6 | 9.9 |
| 36 | 900 | 48.9 | 35.4 | 14.9 | 10.8 |
| 42 | 1050 | 52.9 | 38.3 | 16.1 | 11.7 |

${ }^{(1)}$ For $\mathrm{Sg}=1.0$, consult manufacturer for heavier insulated pipe support spans. Span
recommendations include no provision for weight of (fittings, valves, etc.) or thrusts at branches and turns. Heavy valves and other appurtenances must be supported separately.
${ }^{(2)}$ Calculated spans are based on $1 / 2$ " mid-span deflections to ensure good appearance and adequate drainage. Total system stresses should always be taken into account by the system design engineer when determining support spans.

There are seven basic guidelines to follow when designing an above ground piping system:

1. Do not exceed the recommended support span.
2. Support heavy valves and in-line equipment independently.
3. Protect pipe from external abrasion at supports.
4. Avoid point contact loads
5. Avoid excessive bending. This applies to handling, transporting, initial layout, and final installed position.
6. Avoid excessive vertical run loading. Vertical loads should be supported sufficiently to minimize bending stresses on pipe and fittings.
7. Provide adequate axial and lateral restraint to ensure line stability during rapid changes in flow (water hammer).

## Adjustment Factors for Various Spans With Unsupported Fitting at Change in Direction

|  | Span Type | Factor |
| :--- | :--- | :--- |
| LC | Continuous interior or fixed end spans | 1.00 |
| C | Second span from supported end or unsupported fitting | 0.80 |
| A+B | Sum of unsupported spans at fitting | $\leq 0.75^{\star}$ |
| D | Simple supported end span | 0.67 |

*For example: If continuous support is 10 ft . ( 3.04 m ), $\mathrm{A}+\mathrm{B}$ must not exceed 7.5 ft . $(2.28 \mathrm{~m})(\mathrm{A}=3 \mathrm{ft}$. ( 0.91 m ) and $\mathrm{B}=4.5 \mathrm{ft}$. ( 1.37 m )) would satisfy this condition.


Adjustment Factors for Various Spans With Supported Fitting at Change in Direction

|  | Span Type | Factor |
| :--- | :--- | :--- |
| LC | Continuous interior or fixed end spans | 1.00 |
| A | Second span from simple supported end or unsupported fitting | 0.80 |
| B | Simple supported end span | 0.67 |



## Thermal Expansion

The effects of thermal gradients on piping systems may be significant and should be considered in every piping system stress analysis. Pipe line movements due to thermal expansion or contraction may cause
high stresses or even buckle a pipe line if improperly restrained. Several piping system designs are used to manage thermal expansion and contraction in above ground piping systems. They are listed below according to economic preference:

1. Use of inherent flexibility in directional changes.
2. Restraining axial movements and guiding to prevent buckling.
3. Use expansion loops to absorb thermal movements.
4. Use mechanical expansion joints to absorb thermal movements.

To perform a thermal analysis the following information is required:

1. Isometric layout of piping system
2. Physical and material properties of pipe
3. Design temperatures
4. Installation temperature (Final tie in temperature)
5. Terminal equipment load limits
6. Supportmovements

A comprehensive review of temperature effects on fiberglass pipe may be found in NOV Fiber Glass Systems' Engineering and Piping Design Guide, Section 3.

| Change in <br> Temperature |  | Pipe Change in <br> Length |  |
| :--- | :--- | :--- | :--- |
| ${ }^{\circ} \mathbf{F}$ | ${ }^{\circ} \mathbf{C}$ | in/100 ft | $\mathbf{c m} / \mathbf{1 0 0} \mathbf{~ m}$ |
| 25 | 13.9 | 0.41 | 3.45 |
| 50 | 27.8 | 0.83 | 6.90 |
| 75 | 41.7 | 1.24 | 10.35 |
| 100 | 55.6 | 1.66 | 13.80 |

## Testing

Hydrostatic testing is recommended to evaluate the integrity of all new piping installations. For systems operating below the system rating, a test pressure of 1.5 times the system operating pressure is recommended; however, the maximum test pressure must not exceed 1.3 times the lowest pressure rated fiberglass component in the piping system.
The hydro test pressure should be repeated up to ten cycles from 0 psig to the test pressure to provide a high degree of confidence in the piping system. The final pressurization cycle should be allowed to stabilize for 15-30 minutes, then inspected for leaks. Do not attempt to repair leaks while system is pressurized. The hydro test should be repeated after any re-work is performed.

When hydro testing, open high-point vents (if used) to prevent entrapment of air in the lines as the system is slowly filled with water, then close the vents and slowly pressurize to the test pressure. Upon completion of hydro test, relieve the pressure on the system slowly, open vents and any drains to allow for complete drainage of the system.

## Water Hammer

Piping systems may be damaged by pressure surges due to water hammer. The use of soft start pumps and slow actuating valves will reduce the magnitude of surge pressures during operation and are highly recommended.

## Typical Mechanical Properties

| Pipe Property | $75^{\circ} \mathrm{F}$ | $24^{\circ} \mathrm{C}$ | $200^{\circ} \mathrm{F}$ | $93^{\circ} \mathrm{C}$ | Method |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | psi | MPa | psi | MPa |  |
| Axial Tensile |  |  |  |  |  |
| Ultimate Stress | 9,530 | 65.7 | 6,585 | 45.4 | ASTM D2105 |
| Modulus of Elasticity | $1.68 \times 10^{6}$ | 11,584 | $1.42 \times 10^{6}$ | 9,791 | ASTM D2105 |
| Poisson's Ratio, $v_{\text {ah }}\left(v_{\text {ha }}\right)^{(1)}$ | 0.35 (0.61) |  |  |  |  |
| Axial Compression |  |  |  |  |  |
| Ultimate Stress | 12,510 | 86.3 | 8,560 | 59.0 | ASTM D695 |
| Modulus of Elasticity | $0.677 \times 10^{6}$ | 4,668 | $0.379 \times 10^{6}$ | 2,613 | ASTM D695 |
| Beam Bending |  |  |  |  |  |
| Modulus of Elasticity (Long Term) | $2.6 \times 10^{6}$ | 17,927 | $0.718 \times 10^{6}$ | 4,951 | ASTM D2925 |
| Hydrostatic Burst |  |  |  |  |  |
| Ultimate Hoop Tensile Stress | 40,150 | 277 | 36,480 | 252 | ASTM D1599 |
| Hydrostatic Hoop Design Stress |  |  |  |  |  |
| Static 20 Year Life LTHS -95\% LCL | - | - | 20,787-17,155 | 143.3-118.3 | ASTM D2992-Procedure B |
| Static 50 Year Life LTHS -95\% LCL | - | - | 19,057-15,302 | 131.4-105.5 | ASTM D2992-Procedure B |
| Parallel Plate |  |  |  |  |  |
| Hoop Modulus of Elasticity | $3.02 \times 10^{6}$ | 20,822 | - | - | ASTM D2412 |
| Shear Modulus | $1.76 \times 10^{6}$ | 12,135 | $1.63 \times 10^{6}$ | 11,240 |  |

## Typical Physical Properties

| Pipe Property | Value | Value | Method |
| :--- | :--- | :--- | :--- |
| Thermal <br> Conductivity | $0.23 \mathrm{BTU} / \mathrm{hr} \cdot \mathrm{ft} \cdot{ }^{\circ} \mathrm{F}$ | $0.4 \mathrm{~W} / \mathrm{m}^{\circ} \mathrm{C}$ | ASTM D177 |
| Thermal <br> Expansion | $13.8 \times 10^{-6} \mathrm{in} / \mathrm{in} /{ }^{\circ} \mathrm{F}$ | $24.8 \times 10^{-6} \mathrm{~mm} / \mathrm{mm} /{ }^{\circ} \mathrm{C}$ | ASTM D696 |
| Absolute <br> Roughness | 0.00021 in | 0.00053 mm |  |
| Specific Gravity |  | 1.8 | ASTM D792 |

${ }^{(1)} V_{\text {ha }}=$ The ratio of axial strain to hoop strain resulting from stress in the hoop direction.
$v_{\mathrm{ah}}=$ The ratio of hoop strain to axial strain resulting from stress in the axial direction.
${ }^{(2)}$ The differential pressure between internal and external pressure which causes collapse.
${ }^{(3)}$ A 0.67 design factor is recommended for short duration vacuum service. A full vacuum is equal to $14.7 \mathrm{psig}(0.101 \mathrm{MPa})$ differential pressure at sea level.
${ }^{(4)}$ A 0.33 design factor is recommended for sustained (long-term) differential collapse pressure design and operation.

## Ultimate Collapse Pressure

| Size |  | Collapse Pressure ${ }^{(2,3,4)}$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | psig |  | MPa |  |
| in | mm | $75^{\circ} \mathrm{F}$ | $200^{\circ} \mathrm{F}$ | $24^{\circ} \mathrm{C}$ | $93^{\circ} \mathrm{C}$ |
| 1 | 25 | 550 | 430 | 3.79 | 2.96 |
| $11 / 2$ | 40 | 340 | 260 | 2.34 | 1.79 |
| 2 | 50 | 330 | 250 | 2.28 | 1.72 |
| 3 | 80 | 120 | 90 | 0.827 | 0.621 |
| 4 | 100 | 49 | 35 | 0.338 | 0.241 |
| 6 | 150 | 39 | 28 | 0.269 | 0.193 |
| 8 | 200 | 26 | 19 | 0.179 | 0.131 |
| 10 | 250 | 26 | 19 | 0.179 | 0.131 |
| 12 | 300 | 26 | 19 | 0.179 | 0.131 |
| 14 | 350 | 25 | 17 | 0.172 | 0.117 |
| 16 | 400 | 23 | 16 | 0.159 | 0.110 |
| 18 | 450 | 22 | 15 | 0.152 | 0.103 |
| 20 | 550 | 17 | 12 | 0.117 | 0.083 |
| 24 | 600 | 17 | 12 | 0.117 | 0.083 |
| 30 | 750 | 20 | 14 | 0.138 | 0.097 |
| 36 | 900 | 20 | 14 | 0.138 | 0.097 |
| 42 | 1050 | 20 | 14 | 0.138 | 0.097 |

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## Fiber Glass Systems

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## Green Thread'" HP 25 Product Data

Applications<br>- Dilute Acids<br>- Industrial Waste<br>- Produced Water<br>- Caustics<br>- Hot Water<br>- Condensate Return

Materials and Construction

Pipe manufactured by filament winding process using amine-cured epoxy thermosetting resin to impregnate strands of continuous glass filaments. The pipe wall includes an internal resin-rich corrosion barrier.

Pipe is available in $1^{\prime \prime}-24$ " ( $25-600 \mathrm{~mm}$ ) diameters with pressure ratings up to 360 psig ( 25 bar ). The pipe and fittings are designed for continuous operation at $200^{\circ} \mathrm{F}\left(93^{\circ} \mathrm{C}\right)$ and are serviceable up to $230^{\circ} \mathrm{F}\left(110^{\circ} \mathrm{C}\right)$ by applying a derating factor of 0.76 to all component ratings. Pipe diameters of $1^{\prime \prime}-6 "(25-150 \mathrm{~mm})$ are available in 20' $(6 \mathrm{~m})$ random lengths and the $8 "-24 "\left(150-600 \mathrm{~mm}\right.$ ) diameters are in $19^{\prime}$ or $39^{\prime}$ ( 6 or 12 m ) random lengths.

ASTM D-2996 Classifiction: RTRP - 11FX1-3110 for static design basis

## Fittings

Fittings are manufactured with the same chemical and temperature capabilities as the pipe. Depending on the configurations and size, the fitting construction method will be compression molded, contact molded, fabricated or filament wound. Fitting details are in document Cl 1370.

## Joining <br> Systems

## Bell \& Spigot

Matched-taper joint secured with epoxy adhesive. Self-locking feature resists movement, facilitating joining runs of pipe without waiting for adhesive to cure.


## Flanged

Available for all piping systems and diameters; factory assembled are shipped loose for assembly in the field


| Nominal Dimensional Data |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Pipe Size |  | I.D. |  | O.D. |  | Minimum Reinforced Wall Thickness |  | Liner Thickness |  | Weight |  |
| in | mm | in | mm | in | mm | in | mm | in | mm | Ibs/it | kg/m |
| $1{ }^{(1)}$ | 25 | 1.19 | 30.3 | 1.35 | 34.3 | 0.057 | 1.45 | 0.015 | 0.38 | 0.26 | 0.39 |
| $11 / 2^{(1)}$ | 40 | 1.76 | 44.7 | 1.93 | 49.0 | 0.062 | 1.57 | 0.015 | 0.38 | 0.4 | 0.61 |
| $2^{(1)}$ | 50 | 2.15 | 54.7 | 2.36 | 59.9 | 0.075 | 1.91 | 0.020 | 0.51 | 0.6 | 0.92 |
| $3{ }^{(1)}$ | 75 | 3.28 | 83.3 | 3.49 | 88.7 | 0.075 | 1.91 | 0.020 | 0.51 | 0.9 | 1.34 |
| 4 | 100 | 4.28 | 109 | 4.52 | 115 | 0.085 | 2.16 | 0.020 | 0.51 | 1.4 | 2.08 |
| 6 | 150 | 6.35 | 161 | 6.68 | 170 | 0.125 | 3.18 | 0.020 | 0.51 | 2.8 | 4.17 |
| 8 | 200 | 8.36 | 212 | 8.78 | 223 | 0.164 | 4.17 | 0.020 | 0.51 | 5.0 | 7.44 |
| 10 | 250 | 10.36 | 263 | 10.87 | 276 | 0.203 | 5.16 | 0.020 | 0.51 | 7.5 | 11.16 |
| 12 | 300 | 12.29 | 312 | 12.88 | 327 | 0.240 | 6.10 | 0.020 | 0.51 | 10.4 | 15.48 |
| 14 | 350 | 14.04 | 357 | 14.71 | 374 | 0.274 | 6.96 | 0.020 | 0.51 | 13.5 | 20.09 |
| 16 | 400 | 16.04 | 407 | 16.80 | 427 | 0.313 | 7.95 | 0.020 | 0.51 | 17.5 | 26.04 |
| 18 | 450 | 17.82 | 453 | 18.65 | 474 | 0.347 | 8.81 | 0.020 | 0.51 | 20.4 | 30.36 |
| 20 | 500 | 19.83 | 504 | 20.75 | 527 | 0.386 | 9.80 | 0.020 | 0.51 | 25.1 | 37.35 |
| 24 | 600 | 23.83 | 605 | 24.93 | 633 | 0.464 | 11.8 | 0.020 | 0.51 | 36.0 | 53.57 |

${ }^{(1)}$ Minimum reinforced wall thickness exceeds the requirement for the 25 Bar class and may be operated up to 30 Bar (435 psi). Note: System rating is determined by pressure ratings of fittings used in the piping system. See document Cl1370 for individual fitting pressure ratings.


Typical Physical Properties

| Thermal Expansion Coefficient - ASTM D696 | $8.5 \times 10^{-6} \mathrm{in} / \mathrm{in} /{ }^{\circ} \mathrm{F}$ | $15.3 \times 10^{-6} \mathrm{~mm} / \mathrm{mm} /{ }^{\circ} \mathrm{C}$ |
| :--- | :---: | :---: |
| Thermal Conductivity - ASTM D177 | $0.23 \mathrm{BTU} / \mathrm{hr}-\mathrm{ft}-{ }^{\circ} \mathrm{F}$ | $0.4 \mathrm{~W} / \mathrm{m}-{ }^{\circ} \mathrm{C}$ |
| Specific Gravity - ASTM D792 |  | 1.8 |
| Absolute Surface Roughness | 0.00021 in | 0.00053 mm |


| Ultimate Collapse Pressure |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Size |  | Collapse Pressure ${ }^{(1,2,3)}$ |  |  |  |
|  |  | psig |  | MPa |  |
| in | mm | $75^{\circ} \mathrm{F}$ | 200 ${ }^{\circ} \mathrm{F}$ | $24^{\circ} \mathrm{C}$ | $93^{\circ} \mathrm{C}$ |
| 1 | 25 | 576 | 451 | 3.97 | 3.11 |
| $11 / 2$ | 40 | 350 | 269 | 2.41 | 1.86 |
| 2 | 50 | 447 | 346 | 3.08 | 2.39 |
| 3 | 80 | 125 | 93 | 0.86 | 0.64 |
| 4 | 100 | 80 | 59 | 0.55 | 0.41 |
| 6 | 150 | 75 | 55 | 0.52 | 0.38 |
| 8 | 200 | 77 | 57 | 0.53 | 0.39 |
| 10 | 250 | 77 | 56 | 0.53 | 0.39 |
| 12 | 300 | 76 | 56 | 0.52 | 0.38 |
| 14 | 350 | 76 | 56 | 0.52 | 0.38 |
| 16 | 400 | 76 | 56 | 0.52 | 0.38 |
| 18 | 450 | 75 | 55 | 0.52 | 0.38 |
| 20 | 500 | 75 | 55 | 0.52 | 0.38 |
| 24 | 600 | 75 | 55 | 0.52 | 0.38 |

[^0]
## Supports

Proper pipe support spacing depends on the temperature and weight of the fluid in the pipe. The support spacing table is based on unrestrained continuous beam theory using the pipe bending modulus derived from long-term beam bending tests. The maximum spans lengths were developed to ensure a design that limits mid-span deflection to $1 / 2$ inch and dead weight bending to $1 / 8$ of the ultimate bending stress. Any additional loads on the piping system such as insulation, wind, seismic, etc. requires further consideration. Restrained (anchored) piping systems operating at elevated temperatures may result in guide spacing requirements that are shorter than unrestrained piping systems. In this case, the maximum guide spacing governs the support span requirements for the system. Pipe spans near elbows require special attention. Both supported and unsupported elbows are considered in the following tables and must be followed to properly design the piping system.

| Maximum Support Spacing for Pipe ${ }^{(1)}$ |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Size |  | Continuous Spans of Pipe ${ }^{(2)}$ |  |  |  |
|  |  | ft |  | m |  |
| in | mm | $75^{\circ} \mathrm{F}$ | $200^{\circ} \mathrm{F}$ | $24^{\circ} \mathrm{C}$ | $93^{\circ} \mathrm{C}$ |
| 1 | 25 | 11.6 | 8.4 | 3.54 | 2.57 |
| $11 / 2$ | 40 | 13.2 | 9.6 | 4.03 | 2.92 |
| 2 | 50 | 14.6 | 10.6 | 4.44 | 3.22 |
| 3 | 80 | 16.4 | 11.9 | 5.01 | 3.63 |
| 4 | 100 | 18.2 | 13.2 | 5.54 | 4.02 |
| 6 | 150 | 22.1 | 16.0 | 6.73 | 4.88 |
| 8 | 200 | 25.3 | 18.3 | 7.70 | 5.58 |
| 10 | 250 | 28.1 | 20.4 | 8.58 | 6.22 |
| 12 | 300 | 30.6 | 22.2 | 9.33 | 6.76 |
| 14 | 350 | 32.7 | 23.7 | 9.97 | 7.23 |
| 16 | 400 | 35.0 | 25.3 | 10.65 | 7.72 |
| 18 | 450 | 36.9 | 26.8 | 11.25 | 8.16 |
| 20 | 500 | 38.9 | 28.2 | 11.86 | 8.60 |
| 24 | 600 | 42.7 | 30.9 | 13.01 | 9.43 |
| ${ }^{(1)}$ Consult manufacturer for heavier insulated pipe support spacing. <br> ${ }^{(2)}$ Max. mid span deflection $1 / 2^{\prime \prime}(12.7 \mathrm{~mm})$ with specific gravity 1.0 . |  |  |  |  |  |

Support Spacing vs. Specific Gravity

| Specific Gravity | 2.00 | 1.50 | 1.25 | 1.00 | 0.75 |
| :---: | :--- | :--- | :--- | :--- | :--- |
| Multiplier | 0.86 | 0.92 | 0.96 | 1.00 | 1.07 |

Example: $8^{\prime \prime}$ pipe @ $75^{\circ} \mathrm{F}$ with 1.5 specific gravity fluid, maximum support spacing $=25.3 \times 0.92=23.3 \mathrm{ft}$.

There are seven basic guidelines to follow when designing an above ground piping system:

1. Do not exceed the recommended support span.
2. Support heavy valves and in-line equipment independently.
3. Protect pipe from external abrasion at supports.
4. Avoid point contact loads.
5. Avoid excessive bending. This applies to handling, transporting, initial layout, and final installed position.
6. Avoid excessive vertical loading to minimize bending stresses on pipe and fittings.
7. Provide adequate axial and lateral restraint to ensure line stability during rapid changes in flow (water hammer).

## Adjustment Factors for Various Spans With Unsupported Fitting at Change in Direction

| Span Type | Factor |  |
| :---: | :---: | :---: |
| a | Continuous interior or fixed end spans <br> Second span from supported end or <br> unsupported fitting | 1.00 |
| c+d | Sum of unsupported spans at fitting | 0.80 |
| e | Simple supported end span | $\leq 0.75^{*}$ |

Adjustment Factors for Various Spans With Supported Fitting at Change in Direction


## Thermal Expansion

The effects of thermal gradients on piping systems may be significant and should be considered in every piping system stress analysis. Pipe line movements due to thermal expansion or contraction may cause high stresses or even buckle a pipe line if improperly restrained. Several piping system designs are used to manage thermal expansion and contraction in above ground piping systems. They are listed below according to economic preference:

1. Use of inherent flexibility in directional changes.
2. Restraining axial movements and guiding to prevent buckling.
3. Use expansion loops to absorb thermal movements.
4. Use mechanical expansion joints to absorb thermal movements.

To perform a thermal analysis the following information is required:

1. Isometric layout of piping system
2. Physical and material properties of pipe
3. Design temperatures
4. Installation temperature (Final tie in temperature)
5. Terminal equipment load limits
6. Support movements

A comprehensive review of temperature effects on fiberglass pipe may be found in NOV Fiber Glass Systems' ENG1000 "Engineering and Piping Design Guide", Section 3.

## Testing

Hydrostatic testing is recommended to evaluate the integrity of all new piping installations. For systems operating below the system rating, a test pressure of 1.5 times the system operating pressure is recommended; however, the maximum test pressure must not exceed 1.25 times the lowest pressure rated fiberglass component in the piping system.

The hydro test pressure should be repeated up to ten cycles from 0 psig to the test pressure to provide a high degree of confidence in the piping system. The final pressurization cycle should be allowed to stabilize for 15-30 minutes, then inspected for leaks. Do not attempt to repair leaks while system is pressurized. The hydro test should be repeated after any re-work is performed.

When hydro testing, open high-point vents (if used) to prevent entrapment of air in the lines as the system is slowly filled with water, then close the vents and slowly pressurize to the test pressure. Upon completion of hydro test, relieve the pressure on the system slowly, open vents and any drains to allow for complete drainage of the system.

## Water Hammer

Piping systems may be damaged by pressure surges due to water hammer. The use of soft start pumps and slow actuating valves will reduce the magnitude of surge pressures during operation and are highly recommended.


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# Green Thread ${ }^{\text {TM }}$ HP 20 

## Applications

- Chemical Processing Liquids
- Food Processing Liquids
- Potable Water
- Cooling Water
- Condensate Return
- Industrial Wastewater
- Mildly Corrosive Liquids
- Crude Oil \& Gas


## Materials and Construction

Pipe manufactured by filament winding process using amine-cured epoxy thermosetting resin to impregnate strands of continuous glass filaments. The pipe wall includes an internal resin-rich corrosion barrier.

Pipe is available in 1"-24" (25-600 mm) diameters with pressure ratings up to 290 psig (20 bar). The pipe and fittings have an operating temperature of $200^{\circ} \mathrm{F}\left(93^{\circ} \mathrm{C}\right)$ serviceable up to $230^{\circ} \mathrm{F}\left(110^{\circ} \mathrm{C}\right)$ by applying a derating factor of 0.76 to all component ratings. Pipe diameters of $1^{\prime \prime}-6$ " ( $25-150 \mathrm{~mm}$ ) are available in $20^{\prime}(6 \mathrm{~m})$ random lengths and the $8^{\prime \prime}-24^{\prime \prime}(150-600 \mathrm{~mm})$ diameters are in $19{ }^{\prime}$ or $39^{\prime}$ ( 6 or 12 m ) random lengths.

ASTM D-2996 Classification: RTRP - 11FX13110 for static design basis.

## Fittings

Fittings are manufactured with the same chemical/temperature capabilities as the pipe. Depending on the particular part and size, fittings will be compression molded, contact molded, hand fabricated or filament wound. This piping system is designed to be used with Green Thread HP25 epoxy fittings.

## Joining System

- Bell \& Spigot - Matched-taper joint secured with epoxy adhesive. Self-locking feature resists movement, facilitating joining runs of pipe without waiting for adhesive to cure.
- Flanged - Available for all piping systems and diameters; factory assembled or shipped loose for assembly in the field.


Flanged

- Produced Water
- Saltwater
- $\mathrm{CO}_{2}$


Bell \& Spigot

Nominal Dimensional Data

| Pipe Size |  | Inside Diameter |  | Outside Diameter |  | Minimum Reinforced Wall Thickness |  | Liner Thickness |  | Weight ${ }^{(2)}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | in | mm | in | mm | in | mm | in | mm | lbs/ft | kg/m |
| $1^{(1)}$ | 25 | 1.19 | 30.2 | 1.34 | 34.0 | 0.057 | 1.45 | 0.015 | 0.38 | 0.2 | 0.4 |
| $1{ }^{1 / 2}{ }^{(1)}$ | 40 | 1.76 | 44.7 | 1.91 | 48.6 | 0.062 | 1.57 | 0.015 | 0.38 | 0.4 | 0.6 |
| $2^{(1)}$ | 50 | 2.15 | 54.0 | 2.34 | 59.5 | 0.075 | 1.91 | 0.020 | 0.51 | 0.6 | 0.8 |
| $3^{(1)}$ | 80 | 3.28 | 83.0 | 3.47 | 88.1 | 0.075 | 1.91 | 0.020 | 0.51 | 0.8 | 1.2 |
| 4 | 100 | 4.28 | 109.0 | 4.47 | 114.0 | 0.075 | 1.91 | 0.020 | 0.51 | 1.1 | 1.6 |
| 6 | 150 | 6.35 | 161.0 | 6.60 | 168.0 | 0.105 | 2.67 | 0.020 | 0.51 | 2.1 | 3.2 |
| 8 | 200 | 8.36 | 212.0 | 8.66 | 220.0 | 0.131 | 3.33 | 0.020 | 0.51 | 3.6 | 5.4 |
| 10 | 250 | 10.36 | 263.0 | 10.73 | 273.0 | 0.162 | 4.11 | 0.020 | 0.51 | 5.3 | 7.9 |
| 12 | 300 | 12.29 | 312.0 | 12.71 | 323.0 | 0.192 | 4.88 | 0.020 | 0.51 | 7.4 | 11.0 |
| 14 | 350 | 14.04 | 367.0 | 14.52 | 369.0 | 0.219 | 5.56 | 0.020 | 0.51 | 9.5 | 14.1 |
| 16 | 400 | 16.04 | 407.0 | 16.58 | 421.0 | 0.250 | 6.35 | 0.020 | 0.51 | 12.3 | 18.3 |
| 18 | 450 | 17.82 | 453.0 | 18.42 | 468.0 | 0.278 | 7.06 | 0.020 | 0.51 | 15.8 | 23.5 |
| 20 | 500 | 19.83 | 504.0 | 20.49 | 520.0 | 0.309 | 7.85 | 0.020 | 0.51 | 18.6 | 27.7 |
| 24 | 600 | 23.83 | 605.0 | 24.61 | 625.0 | 0.371 | 9.42 | 0.020 | 0.51 | 26.7 | 39.7 |

${ }^{(1)}$ Minimum wall exceeds requirement for 20 Bar class, may be rated higher refer to fitting ratings.
${ }^{(2)}$ Based on the minimum wall.

## Supports

Proper pipe support spacing depends on the temperature and weight of the fluid in the pipe. The supportspans are based on unrestrained continuous beam theory using the pipe bending modulus derived from long-term beam bending tests. The following tables were developed to ensure a design that limits beam mid-span deflection to $1 / 2$ inch to ensure good appearance and adequate drainage. Any additional loads on the piping system such as insulation, wind, seismic, etc. requires further consideration. Restrained (anchored) piping systems operating at elevated temperatures may result in guide spacing requirements that are shorter than unrestrained piping systems. In this case, the maximum guide spacing governs the support span requirements for the system. Pipe spans near elbows require special attention. Both supported and unsupported elbows are considered in the following tables and must be followed to properly design the piping system.

Support Spacing vs. Specific Gravity

| Specific Gravity | 2.00 | 1.50 | 1.25 | 1.00 | 0.75 |
| :--- | :--- | :--- | :--- | :--- | :--- |
| Multiplier | 0.85 | 0.91 | 0.95 | 1.00 | 1.06 |

Example: $8^{\prime \prime}$ pipe @ $75^{\circ} \mathrm{F}\left(23.9^{\circ} \mathrm{C}\right)$ with 1.5 specific gravity fluid,
maximum support spacing $=24.1 \times 0.91=21.93 \mathrm{ft}$.

Maximum Support Spacing for Pipe ${ }^{(1)}$

| Size | Continuous Spans of Pipe ${ }^{(2)}$ |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- |
|  | feet |  | meters |  |  |
| in | $\mathbf{m m}$ | $\mathbf{7 5}^{\circ} \mathbf{F}$ | $\mathbf{2 0 0}^{\circ}$ F | $\mathbf{2 4}^{\circ} \mathbf{C}$ | $\mathbf{9 3}^{\circ} \mathbf{C}$ |
| 1 | 25 | 11.7 | 8.4 | 3.6 | 2.6 |
| $1 \mathbf{1} 2$ | 40 | 13.3 | 9.6 | 4.1 | 2.9 |
| 2 | 50 | 14.7 | 10.6 | 4.5 | 3.2 |
| 3 | 80 | 16.5 | 11.9 | 5.0 | 3.6 |
| 4 | 100 | 17.7 | 12.8 | 5.4 | 3.9 |
| 6 | 150 | 21.3 | 15.4 | 6.5 | 4.7 |
| 8 | 200 | 24.1 | 17.5 | 7.4 | 5.3 |
| 10 | 250 | 26.8 | 19.4 | 8.2 | 5.9 |
| 12 | 300 | 29.2 | 21.2 | 8.9 | 6.5 |
| 14 | 350 | 31.2 | 22.6 | 9.5 | 6.9 |
| 16 | 400 | 33.4 | 24.2 | 10.2 | 7.4 |
| 18 | 450 | 35.1 | 25.5 | 10.7 | 7.8 |
| 20 | 500 | 37.1 | 26.9 | 11.3 | 8.2 |
| 24 | 600 | 40.7 | 29.5 | 12.4 | 9.0 |

${ }^{(1)}$ For $\mathrm{Sg}=1.0$, consult manufacturer for heavier insulated pipe support spans. Span recommendations include no provision for weight of (fittings, valves, etc.) or thrusts at branches and turns. Heavy valves and other appurtenances must be supported separately.
${ }^{(2)}$ Calculated spans are based on $1 / 2^{\prime \prime}$ mid-span deflections to ensure good appearance and adequate drainage. Total system stresses should always be taken into account by the system design engineer when determining support spans.

There are seven basic guidelines to follow when designing an above ground piping system:

1. Do not exceed the recommended support span.
2. Support heavy valves and in-line equipment independently.
3. Protect pipe from external abrasion at supports.
4. Avoid point contact loads
5. Avoid excessive bending. This applies to handling, transporting, initial layout, and final installed position.
6. Avoid excessive vertical loading to minimize bending stresses on pipe and fittings.
7. Provide adequate axial and lateral restraint to ensure line stability during rapid changes in flow (water hammer).

Adjustment Factors for Various Spans With Unsupported Fitting at Change in Direction

|  | Span Type | Factor |
| :--- | :--- | :--- |
| LC | Continuous interior or fixed end spans | 1.00 |
| C | Second span from supported end or unsupported fitting | 0.80 |
| A+B | Sum of unsupported spans at fitting | $\leq 0.75^{\star}$ |
| D | Simple supported end span | 0.67 |

*For example: If continuous support is 10 ft . ( 3.04 m ), $\mathrm{A}+\mathrm{B}$ must not exceed 7.5 ft . $(2.28 \mathrm{~m})$ ( $\mathrm{A}=3 \mathrm{ft}$. $(0.91 \mathrm{~m})$ and $B=4.5 \mathrm{ft}$. $(1.37 \mathrm{~m})$ ) would satisfy this condition.


Adjustment Factors for Various Spans With Supported Fitting at Change in Direction

|  | Span Type | Factor |
| :--- | :--- | :--- |
| LC | Continuous interior or fixed end spans | 1.00 |
| A | Second span from simple supported end or unsupported fitting | 0.80 |
| B | Simple supported end span | 0.67 |



## Thermal Expansion

The effects of thermal gradients on piping systems may be significant and should be considered in every piping system stress analysis. Pipe line movements due to thermal expansion or contraction may cause
high stresses or even buckle a pipe line if improperly restrained. Several piping system designs are used to manage thermal expansion and contraction in above ground piping systems. They are listed below according to economic preference:

1. Use of inherent flexibility in directional changes.
2. Restraining axial movements and guiding to prevent buckling.
3. Use expansion loops to absorb thermal movements.
4. Use mechanical expansion joints to absorb thermal movements.

To perform a thermal analysis the following information is required:

1. Isometric layout of piping system
2. Physical and material properties of pipe
3. Design temperatures
4. Installation temperature (Final tie in temperature)
5. Terminal equipment load limits
6. Supportmovements

A comprehensive review of temperature effects on fiberglass pipe may be found in NOV Fiber Glass Systems' Engineering and Piping Design Guide, Section 3.

| Change in <br> Temperature |  | Pipe Change in <br> Length |  |
| :--- | :--- | :--- | :--- |
| ${ }^{\circ} \mathbf{F}$ | ${ }^{\circ} \mathbf{C}$ | in/100 ft | $\mathbf{c m} / \mathbf{1 0 0} \mathbf{~ m}$ |
| 25 | 13.9 | 0.41 | 3.45 |
| 50 | 27.8 | 0.83 | 6.90 |
| 75 | 41.7 | 1.24 | 10.35 |
| 100 | 55.6 | 1.66 | 13.80 |

## Testing

Hydrostatic testing is recommended to evaluate the integrity of all new piping installations. For systems operating below the system rating, a test pressure of 1.5 times the system operating pressure is recommended; however, the maximum test pressure must not exceed 1.5 times the lowest pressure rated fiberglass component in the piping system.
The hydro test pressure should be repeated up to ten cycles from 0 psig to the test pressure to provide a high degree of confidence in the piping system. The final pressurization cycle should be allowed to stabilize for 15-30 minutes, then inspected for leaks. Do not attempt to repair leaks while system is pressurized. The hydro test should be repeated after any re-work is performed.

When hydro testing, open high-point vents (ifused) to prevent entrapment of air in the lines as the system is slowly filled with water, then close the vents and slowly pressurize to the test pressure. Upon completion of hydro test, relieve the pressure on the system slowly, open vents and any drains to allow for complete drainage of the system.

## Water Hammer

Piping systems may be damaged by pressure surges due to water hammer. The use of soft start pumps and slow actuating valves will reduce the magnitude of surge pressures during operation and are highly recommended.

## Typical Mechanical Properties

| Pipe Property | $75^{\circ} \mathrm{F}$ | $24^{\circ} \mathrm{C}$ | $200^{\circ} \mathrm{F}$ | $93^{\circ} \mathrm{C}$ | Method |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | psi | MPa | psi | MPa |  |
| Axial Tensile |  |  |  |  |  |
| Ultimate Stress | 9,530 | 65.7 | 6,585 | 45.4 | ASTM D2105 |
| Modulus of Elasticity | $1.68 \times 10^{6}$ | 11,584 | $1.42 \times 10^{6}$ | 9,791 | ASTM D2105 |
| Poisson's Ratio, $v_{\text {ah }}\left(v_{\text {ha }}\right)^{(1)}$ | 0.35 (0.61) |  |  |  |  |
| Axial Compression |  |  |  |  |  |
| Ultimate Stress | 12,510 | 86.3 | 8,560 | 59.0 | ASTM D695 |
| Modulus of Elasticity | $0.677 \times 10^{6}$ | 4,668 | $0.379 \times 10^{6}$ | 2,613 | ASTM D695 |
| Beam Bending |  |  |  |  |  |
| Modulus of Elasticity (Long Term) | $2.6 \times 10^{6}$ | 17,927 | $0.718 \times 10^{6}$ | 4.951 | ASTM D2925 |
| Hydrostatic Burst |  |  |  |  |  |
| Ultimate Hoop Tensile Stress | 40,150 | 277 | 36,480 | 252 | ASTM D1599 |
| Hydrostatic Hoop Design Stress |  |  |  |  |  |
| Static 20 Year Life LTHS -95\% LCL | - | - | 20,787-17,155 | 143.3-118.3 | ASTM D2992-Procedure B |
| Static 50 Year Life LTHS -95\% LCL | - | - | 19,057-15,302 | 131.4-105.5 | ASTM D2992-Procedure B |
| Parallel Plate |  |  |  |  |  |
| Hoop Modulus of Elasticity | $3.02 \times 10^{6}$ | 20,822 | - | - | ASTM D2412 |
| Shear Modulus | $1.76 \times 10^{6}$ | 12,135 | $1.63 \times 10^{6}$ | 11,240 |  |

## Typical Physical Properties

| Pipe Property | Value | Value | Method |
| :--- | :--- | :--- | :--- |
| Thermal <br> Conductivity | $0.23 \mathrm{BTU} / \mathrm{hr} \cdot \mathrm{ft} \cdot{ }^{\circ} \mathrm{F}$ | $0.4 \mathrm{~W} / \mathrm{m}^{\circ} \mathrm{C}$ | ASTM D177 |
| Thermal <br> Expansion | $13.8 \times 10^{-6} \mathrm{in} / \mathrm{in}^{\circ} \mathrm{F}$ | $24.8 \times 10^{-6} \mathrm{~mm} / \mathrm{mm}^{\circ} \mathrm{C}$ | ASTM D696 |
| Absolute <br> Roughness | 0.00021 in | 0.00053 mm |  |
| Specific Gravity | 1.8 |  | ASTM D792 |

${ }^{(1)} V_{\text {ha }}=$ The ratio of axial strain to hoop strain resulting from stress in the hoop direction.
$v_{\mathrm{ah}}=$ The ratio of hoop strain to axial strain resulting from stress in the axial direction.
${ }^{(2)}$ The differential pressure between internal and external pressure which causes collapse.
${ }^{(3)}$ A 0.67 design factor is recommended for short duration vacuum service. A full vacuum is equal to $14.7 \mathrm{psig}(0.101 \mathrm{MPa})$ differential pressure at sea level.
${ }^{(4)} \mathrm{A} 0.33$ design factor is recommended for sustained (long-term) differential collapse pressure design and operation.

## Ultimate Collapse Pressure

| Size |  | Collapse Pressure ${ }^{(2,3,4)}$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | psig |  | MPa |  |
| in | mm | $75^{\circ} \mathrm{F}$ | $200^{\circ} \mathrm{F}$ | $24^{\circ} \mathrm{C}$ | $93^{\circ} \mathrm{C}$ |
| 1 | 25 | 550 | 430 | 3.79 | 2.96 |
| $11 / 2$ | 40 | 340 | 260 | 2.34 | 1.79 |
| 2 | 50 | 330 | 250 | 2.28 | 1.72 |
| 3 | 80 | 120 | 90 | 0.83 | 0.62 |
| 4 | 100 | 49 | 35 | 0.34 | 0.24 |
| 6 | 150 | 40 | 29 | 0.28 | 0.20 |
| 8 | 200 | 31 | 23 | 0.21 | 0.16 |
| 10 | 250 | 31 | 23 | 0.21 | 0.16 |
| 12 | 300 | 31 | 23 | 0.21 | 0.16 |
| 14 | 350 | 31 | 23 | 0.21 | 0.16 |
| 16 | 400 | 31 | 23 | 0.21 | 0.16 |
| 18 | 450 | 31 | 23 | 0.21 | 0.16 |
| 20 | 550 | 31 | 23 | 0.21 | 0.16 |
| 24 | 600 | 31 | 23 | 0.21 | 0.16 |

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## Fiber Glass Systems

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# Green Thread™ HP 25 

## Applications

- Chemical Processing Liquids
- Food Processing Liquids
- Potable Water
- Cooling Water
- Condensate Return
- Industrial Wastewater
- Mildly Corrosive Liquids
- Crude Oil \& Gas


## Materials and Construction

Pipe manufactured by filament winding process using amine-cured epoxy thermosetting resin to impregnate strands of continuous glass filaments. The pipe wall includes an internal resin-rich corrosion barrier.

Pipe is available in 1 "-24" ( $25-600 \mathrm{~mm}$ ) diameters with pressure ratings up to 362 psig (25 bar). The pipe and fittings have an operating temperature of $200^{\circ} \mathrm{F}\left(93^{\circ} \mathrm{C}\right)$ serviceable up to $230^{\circ} \mathrm{F}\left(110^{\circ} \mathrm{C}\right)$ by applying a derating factor of 0.76 to all component ratings. Pipe diameters of $1^{\prime \prime}-6$ " ( $25-150 \mathrm{~mm}$ ) are available in $20^{\prime}(6 \mathrm{~m})$ random lengths and the 8 "-24" (150-600 mm) diameters are in $19^{\prime}$ or $39^{\prime}(6$ or 12 m$)$ random lengths.

ASTM D-2996 Classification: RTRP - 11FX13110 for static design basis.

## Fittings

Fittings are manufactured with the same chemical and temperature capabilities as the pipe. Depending on the particular part and size, fittings will be compression molded, contact molded, hand fabricated or filament wound. Fitting details are in document Cl1360.

## Joining System

- Bell \& Spigot - Matched-taper joint secured with epoxy adhesive. Self-locking feature resists movement, facilitating joining runs of pipe without waiting for adhesive to cure.
- Flanged - Available for all piping systems and diameters; factory assembled or shipped loose for assembly in the field.
- Produced Water
- Saltwater
- $\mathrm{CO}_{2}$


Nominal Dimensional Data

| Pipe Size |  | Inside Diameter |  | Outside Diameter |  | Minimum Reinforced Wall Thickness |  | Liner Thickness |  | Weight ${ }^{(2)}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | in | mm | in | mm | in | mm | in | mm | lbs/ft | kg/m |
| $1^{(1)}$ | 25 | 1.19 | 30.2 | 1.34 | 34.0 | 0.057 | 1.45 | 0.015 | 0.38 | 0.3 | 0.4 |
| $11^{1 / 2}$ | 40 | 1.76 | 44.7 | 1.91 | 49.0 | 0.062 | 1.57 | 0.015 | 0.38 | 0.4 | 0.6 |
| $2^{(1)}$ | 50 | 2.15 | 54.0 | 2.34 | 59.5 | 0.075 | 1.91 | 0.020 | 0.51 | 0.6 | 0.8 |
| $3^{(1)}$ | 80 | 3.28 | 83.0 | 3.47 | 88.1 | 0.075 | 1.91 | 0.020 | 0.51 | 0.8 | 1.2 |
| 4 | 100 | 4.28 | 109.0 | 4.49 | 114.0 | 0.085 | 2.16 | 0.020 | 0.51 | 1.2 | 1.8 |
| 6 | 150 | 6.35 | 161.0 | 6.64 | 169.0 | 0.125 | 3.18 | 0.020 | 0.51 | 2.5 | 3.7 |
| 8 | 200 | 8.36 | 212.0 | 8.73 | 222.0 | 0.164 | 4.17 | 0.020 | 0.51 | 4.2 | 6.3 |
| 10 | 250 | 10.36 | 263.0 | 10.81 | 275.0 | 0.203 | 5.16 | 0.020 | 0.51 | 6.3 | 9.4 |
| 12 | 300 | 12.29 | 312.0 | 12.81 | 327.0 | 0.240 | 6.10 | 0.020 | 0.51 | 8.7 | 13.0 |
| 14 | 350 | 14.04 | 367.0 | 14.63 | 372.0 | 0.274 | 6.96 | 0.020 | 0.51 | 11.3 | 16.8 |
| 16 | 400 | 16.04 | 407.0 | 16.71 | 424.0 | 0.313 | 7.95 | 0.020 | 0.51 | 14.6 | 21.7 |
| 18 | 450 | 17.82 | 453.0 | 18.55 | 471.0 | 0.347 | 8.81 | 0.020 | 0.51 | 17.9 | 26.6 |
| 20 | 500 | 19.83 | 504.0 | 20.64 | 524.0 | 0.386 | 9.80 | 0.020 | 0.51 | 22.1 | 32.9 |
| 24 | 600 | 23.83 | 605.0 | 24.80 | 630.0 | 0.464 | 11.80 | 0.020 | 0.51 | 32.0 | 47.6 |

${ }^{(1)}$ Minimum reinforced wall thickness exceeds the requirement for the 25 Bar class and may be operated up to 30 Bar ( 435 psi ).
${ }^{(2)}$ Based on the minimum wall.
NOTE: System rating is determined by pressure ratings of fittings used in the piping system. See document CI1370 for individual fitting pressure ratings.

## Supports

Proper pipe support spacing depends on the temperature and weight of the fluid in the pipe. The support spacing table is based on unrestrained continuous beam theory using the pipe bending modulus derived from long-term beam bending tests. The following tables were developed to ensure a design that limits beam mid-span deflection to $1 / 2$ inch to ensure good appearance and adequate drainage. Any additional loads on the piping system such as insulation, wind, seismic, etc. requires further consideration. Restrained (anchored) piping systems operating at elevated temperatures may result in guide spacing requirements that are shorter than unrestrained piping systems. In this case, the maximum guide spacing governs the support span requirements for the system. Pipe spans near elbows require special attention. Both supported and unsupported elbows are considered in the following tables and must be followed to properly design the piping system.

Support Spacing vs. Specific Gravity

| Specific Gravity | 2.00 | 1.50 | 1.25 | 1.00 | 0.75 |
| :--- | :--- | :--- | :--- | :--- | :--- |
| Multiplier | 0.86 | 0.92 | 0.96 | 1.00 | 1.07 |

Example: $8^{\prime \prime}$ pipe @ $75^{\circ} \mathrm{F}\left(23.9^{\circ} \mathrm{C}\right)$ with 1.5 specific gravity fluid,
maximum support spacing $=25.4 \times 0.92=23.4 \mathrm{ft}$.

## Maximum Support Spacing for Pipe ${ }^{(1)}$

| Size | Continuous Spans of Pipe ${ }^{(2)}$ |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- |
|  | feet |  | meters |  |  |
| in | $\mathbf{m m}$ | $\mathbf{7 5}^{\circ} \mathbf{F}$ | $\mathbf{2 0 0}^{\circ}$ F | $\mathbf{2 4}^{\circ} \mathbf{C}$ | $\mathbf{9 3}^{\circ} \mathbf{C}$ |
| 1 | 25 | 11.7 | 8.5 | 3.6 | 2.6 |
| $1 \mathbf{1} 2$ | 40 | 13.3 | 9.7 | 4.1 | 2.9 |
| 2 | 50 | 14.7 | 10.7 | 4.5 | 3.3 |
| 3 | 80 | 16.5 | 12.0 | 5.0 | 3.7 |
| 4 | 100 | 18.2 | 13.2 | 5.5 | 4.0 |
| 6 | 150 | 22.2 | 16.1 | 6.8 | 4.9 |
| 8 | 200 | 25.4 | 18.4 | 7.8 | 5.6 |
| 10 | 250 | 28.3 | 20.5 | 8.6 | 6.3 |
| 12 | 300 | 30.8 | 22.3 | 9.4 | 6.8 |
| 14 | 350 | 32.9 | 23.8 | 10.0 | 7.3 |
| 16 | 400 | 35.2 | 25.5 | 10.7 | 7.8 |
| 18 | 450 | 37.1 | 26.9 | 11.3 | 8.2 |
| 20 | 500 | 39.1 | 28.3 | 11.9 | 8.6 |
| 24 | 600 | 42.8 | 31.0 | 13.1 | 9.5 |

${ }^{(1)}$ For $\mathrm{Sg}=1.0$, consult manufacturer for heavier insulated pipe support spans. Span recommendations include no provision for weight of (fittings, valves, etc.) or thrusts at branches and turns. Heavy valves and other appurtenances must be supported separately.
${ }^{(2)}$ Calculated spans are based on $1 / 2^{\prime \prime}$ mid-span deflections to ensure good appearance and adequate drainage. Total system stresses should always be taken into account by the system design engineer when determining support spans.

There are seven basic guidelines to follow when designing an above ground piping system:

1. Do not exceed the recommended support span.
2. Support heavy valves and in-line equipment independently.
3. Protect pipe from external abrasion at supports.
4. Avoid point contact loads
5. Avoid excessive bending. This applies to handling, transporting, initial layout, and final installed position.
6. Avoid excessive vertical loading to minimize bending stresses on pipe and fittings.
7. Provide adequate axial and lateral restraint to ensure line stability during rapid changes in flow (water hammer).

Adjustment Factors for Various Spans With Unsupported Fitting at Change in Direction

|  | Span Type | Factor |
| :--- | :--- | :--- |
| LC | Continuous interior or fixed end spans | 1.00 |
| C | Second span from supported end or unsupported fitting | 0.80 |
| A+B | Sum of unsupported spans at fitting | $\leq 0.75^{\star}$ |
| D | Simple supported end span | 0.67 |

*For example: If continuous support is 10 ft . ( 3.04 m ), $\mathrm{A}+\mathrm{B}$ must not exceed 7.5 ft . $(2.28 \mathrm{~m})$ ( $\mathrm{A}=3 \mathrm{ft}$. $(0.91 \mathrm{~m})$ and $B=4.5 \mathrm{ft}$. $(1.37 \mathrm{~m})$ ) would satisfy this condition.


Adjustment Factors for Various Spans With Supported Fitting at Change in Direction

|  | Span Type | Factor |
| :--- | :--- | :--- |
| LC | Continuous interior or fixed end spans | 1.00 |
| A | Second span from simple supported end or unsupported fitting | 0.80 |
| B | Simple supported end span | 0.67 |



## Thermal Expansion

The effects of thermal gradients on piping systems may be significant and should be considered in every piping system stress analysis. Pipe line movements due to thermal expansion or contraction may cause
high stresses or even buckle a pipe line if improperly restrained. Several piping system designs are used to manage thermal expansion and contraction in above ground piping systems. They are listed below according to economic preference:

1. Use of inherent flexibility in directional changes.
2. Restraining axial movements and guiding to prevent buckling.
3. Use expansion loops to absorb thermal movements.
4. Use mechanical expansion joints to absorb thermal movements.

To perform a thermal analysis the following information is required:

1. Isometric layout of piping system
2. Physical and material properties of pipe
3. Design temperatures
4. Installation temperature (Final tie in temperature)
5. Terminal equipment load limits
6. Supportmovements

A comprehensive review of temperature effects on fiberglass pipe may be found in NOV Fiber Glass Systems' Engineering and Piping Design Guide, Section 3.

| Change in <br> Temperature |  | Pipe Change in <br> Length |  |
| :--- | :--- | :--- | :--- |
| ${ }^{\circ} \mathbf{F}$ | ${ }^{\circ} \mathbf{C}$ | $\mathbf{i n / 1 0 0 ~ f t ~}$ | $\mathbf{c m} / \mathbf{1 0 0} \mathbf{~ m}$ |
| 25 | 13.9 | 0.26 | 0.65 |
| 50 | 27.8 | 0.51 | 1.35 |
| 75 | 41.7 | 0.77 | 1.94 |
| 100 | 55.6 | 1.02 | 2.59 |
| 125 | 69.4 | 1.28 | 3.24 |

## Testing

Hydrostatic testing is recommended to evaluate the integrity of all new piping installations. For systems operating below the system rating, a test pressure of 1.5 times the system operating pressure is recommended; however, the maximum test pressure must not exceed 1.3 times the lowest pressure rated fiberglass component in the piping system.
The hydro test pressure should be repeated up to ten cycles from 0 psig to the test pressure to provide a high degree of confidence in the piping system. The final pressurization cycle should be allowed to stabilize for 15-30 minutes, then inspected for leaks. Do not attempt to repair leaks while system is pressurized. The hydro test should be repeated after any re-work is performed.

When hydro testing, open high-point vents (ifused) to prevent entrapment of air in the lines as the system is slowly filled with water, then close the vents and slowly pressurize to the test pressure. Upon completion of hydro test, relieve the pressure on the system slowly, open vents and any drains to allow for complete drainage of the system.

## Water Hammer

Piping systems may be damaged by pressure surges due to water hammer. The use of soft start pumps and slow actuating valves will reduce the magnitude of surge pressures during operation and are highly recommended.

## Typical Mechanical Properties

| Pipe Property | $75^{\circ} \mathrm{F}$ | $24^{\circ} \mathrm{C}$ | $200^{\circ} \mathrm{F}$ | $93^{\circ} \mathrm{C}$ | Method |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | psi | MPa | psi | MPa |  |
| Axial Tensile |  |  |  |  |  |
| Ultimate Stress | 9,530 | 65.7 | 6,585 | 45.4 | ASTM D2105 |
| Modulus of Elasticity | $1.68 \times 10^{6}$ | 11,584 | $1.42 \times 10^{6}$ | 9,791 | ASTM D2105 |
| Poisson's Ratio, $v_{\text {ah }}\left(v_{\text {ha }}\right)^{(1)}$ | 0.35 (0.61) |  |  |  |  |
| Axial Compression |  |  |  |  |  |
| Ultimate Stress | 12,510 | 86.3 | 8,560 | 59.0 | ASTM D695 |
| Modulus of Elasticity | $0.677 \times 10^{6}$ | 4,668 | $0.379 \times 10^{6}$ | 2,613 | ASTM D695 |
| Beam Bending |  |  |  |  |  |
| Modulus of Elasticity (Long Term) | $2.6 \times 10^{6}$ | 17,927 | $0.718 \times 10^{6}$ | 4.951 | ASTM D2925 |
| Hydrostatic Burst |  |  |  |  |  |
| Ultimate Hoop Tensile Stress | 40,150 | 277 | 36,480 | 252 | ASTM D1599 |
| Hydrostatic Hoop Design Stress |  |  |  |  |  |
| Static 20 Year Life LTHS -95\% LCL | - | - | 20,787-17,155 | 143.3-118.3 | ASTM D2992-Procedure B |
| Static 50 Year Life LTHS -95\% LCL | - | - | 19,057-15,302 | 131.4-105.5 | ASTM D2992-Procedure B |
| Parallel Plate |  |  |  |  |  |
| Hoop Modulus of Elasticity | $3.02 \times 10^{6}$ | 20,822 | - | - | ASTM D2412 |
| Shear Modulus | $1.76 \times 10^{6}$ | 12,135 | $1.63 \times 10^{6}$ | 11,240 | - |

## Typical Physical Properties

| Pipe Property | Value | Value | Method |
| :--- | :--- | :--- | :--- |
| Thermal <br> Conductivity | $0.23 \mathrm{BTU} / \mathrm{hr} \cdot \mathrm{ft} \cdot{ }^{\circ} \mathrm{F}$ | $0.4 \mathrm{~W} / \mathrm{m}^{\circ} \mathrm{C}$ | ASTM D177 |
| Thermal <br> Expansion | $8.5 \times 10^{-6} \mathrm{in} / \mathrm{in}^{\circ} \mathrm{F}$ | $15.3 \times 10^{-6} \mathrm{~mm} / \mathrm{mm}^{\circ} \mathrm{C}$ | ASTM D696 |
| Absolute <br> Roughness | 0.00021 in | 0.00053 mm |  |
| Specific Gravity | 1.8 |  |  |

${ }^{(1)} V_{\text {ha }}=$ The ratio of axial strain to hoop strain resulting from stress in the hoop direction.
$v_{\mathrm{ah}}=$ The ratio of hoop strain to axial strain resulting from stress in the axial direction.
${ }^{(2)}$ The differential pressure between internal and external pressure which causes collapse.
${ }^{(3)}$ A 0.67 design factor is recommended for short duration vacuum service. A full vacuum is equal to $14.7 \mathrm{psig}(0.101 \mathrm{MPa})$ differential pressure at sea level.
${ }^{(4)} \mathrm{A} 0.33$ design factor is recommended for sustained (long-term) differential collapse pressure design and operation.

## Ultimate Collapse Pressure

| Size |  | Collapse Pressure ${ }^{(2,3,4)}$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | psig |  | MPa |  |
| in | mm | $75^{\circ} \mathrm{F}$ | $200^{\circ} \mathrm{F}$ | $24^{\circ} \mathrm{C}$ | $93^{\circ} \mathrm{C}$ |
| 1 | 25 | 550 | 430 | 3.97 | 3.11 |
| $11 / 2$ | 40 | 340 | 260 | 2.41 | 1.86 |
| 2 | 50 | 330 | 250 | 3.08 | 2.39 |
| 3 | 80 | 120 | 90 | 0.86 | 0.64 |
| 4 | 100 | 75 | 55 | 0.52 | 0.38 |
| 6 | 150 | 75 | 55 | 0.52 | 0.38 |
| 8 | 200 | 75 | 55 | 0.52 | 0.38 |
| 10 | 250 | 75 | 55 | 0.52 | 0.38 |
| 12 | 300 | 75 | 55 | 0.52 | 0.38 |
| 14 | 350 | 75 | 55 | 0.52 | 0.38 |
| 16 | 400 | 75 | 55 | 0.52 | 0.38 |
| 18 | 450 | 75 | 55 | 0.52 | 0.38 |
| 20 | 550 | 75 | 55 | 0.52 | 0.38 |
| 24 | 600 | 75 | 55 | 0.52 | 0.38 |

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# Green Thread™ HP 32 

## Applications

- Chemical Processing Liquids
- Food Processing Liquids
- Potable Water
- Cooling Water
- Condensate Return
- Industrial Wastewater
- Mildly Corrosive Liquids
- Crude Oil \& Gas


## Materials and Construction

All pipe manufactured by filament winding process using amine-cured epoxy thermosetting resin to impregnate strands of continuous glass filaments. Pipe wall includes a minimum $0.020^{\prime \prime}(0.50 \mathrm{~mm})$ resinrich corrosion barrier (liner).

Pipe is available in 2"-16" (50-400 mm) diameters with static pressure ratings of 464 psig (32 bar). The pipe and fittings are designed for continuous operation at $200^{\circ} \mathrm{F}\left(93^{\circ} \mathrm{C}\right)$ serviceable up to $230^{\circ} \mathrm{F}\left(110^{\circ} \mathrm{C}\right)$ by applying a derating factor of 0.76 to all component ratings. Pipe diameters of $1^{\prime \prime}-6^{\prime \prime}(25-150 \mathrm{~mm})$ are available in $20^{\prime}(6 \mathrm{~m})$ random lengths and the $8^{\prime \prime}-16^{\prime \prime}$ (200-400 mm) diameters are in $19^{\prime}$ or $39^{\prime}(6$ or 12 m ) random lengths.

ASTM D-2996 Classification: RTRP - 11FX13110 for static design basis.

## Fittings

Fittings are filament wound with the same chemical, temperature and pressure capabilities as the pipe. Reference document Cl1370 for fitting dimensions. 2"-12" (50-300 mm ) fittings use HP 40 dimensions. 14 " and 16 " (350-400 mm) fittings use HP 32 dimensions.

## Joining System

- Bell \& Spigot - Matched-taper joint secured with epoxy adhesive. Self-locking feature resists movement, facilitating joining runs of pipe without waiting for adhesive to cure.
- Flanged - Available for all piping systems and diameters; factory assembled or shipped loose for assembly in the field.


Flanged

- Produced Water
- Saltwater
- $\mathrm{CO}_{2}$


Bell \& Spigot

Nominal Dimensional Data

| Pip |  | Inside Diameter |  | Outside Diameter |  | Minimum Reinforced Wall Thickness |  | Weight ${ }^{(2)}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | in | mm | in | mm | in | mm | lbs/ft | kg/m |
| 2 | 50 | 2.15 | 55 | 2.34 | 59 | 0.075 | 1.91 | 0.60 | 0.89 |
| 3 | 80 | 3.28 | 83 | 3.49 | 87 | 0.084 | 2.13 | 0.91 | 1.35 |
| 4 | 100 | 4.28 | 109 | 4.54 | 115 | 0.109 | 2.77 | 1.50 | 2.23 |
| 6 | 150 | 6.35 | 161 | 6.71 | 170 | 0.161 | 4.09 | 3.10 | 4.61 |
| 8 | 200 | 8.36 | 212 | 8.83 | 224 | 0.212 | 5.39 | 5.60 | 8.33 |
| 10 | 250 | 10.36 | 263 | 10.93 | 277 | 0.262 | 6.66 | 8.4 | 12.50 |
| 12 | 300 | 12.29 | 312 | 12.95 | 329 | 0.311 | 7.90 | 12.3 | 18.30 |
| 14 | 350 | 14.04 | 356 | 14.79 | 377 | 0.355 | 9.02 | 15.2 | 22.62 |
| 16 | 400 | 16.04 | 407 | 16.90 | 429 | 0.405 | 10.29 | 20.1 | 29.91 |

${ }^{(2)}$ Based on the minimum wall.

## Supports

Proper pipe support spacing depends on the temperature and weight of the fluid in the pipe. The support spacing table is based on unrestrained continuous beam theory using the pipe bending modulus derived from long-term beam bending tests. The following tables were developed to ensure a design that limits beam mid-span deflection to $1 / 2$ inch to ensure good appearance and adequate drainage. Any additional loads on the piping system such as insulation, wind, seismic, etc. requires further consideration. Restrained (anchored) piping systems operating at elevated temperatures may result in guide spacing requirements that are shorter than unrestrained piping systems. In this case, the maximum guide spacing governs the support span requirements for the system. Pipe spans near elbows require special attention. Both supported and unsupported elbows are considered in the following tables and must be followed to properly design the piping system.

Support Spacing vs. Specific Gravity

| Specific Gravity | 2.00 | 1.50 | 1.25 | 1.00 | 0.75 |
| :--- | :--- | :--- | :--- | :--- | :--- |
| Multiplier | 0.86 | 0.92 | 0.96 | 1.00 | 1.06 |

Example: $8^{\prime \prime}$ pipe @ $75^{\circ} \mathrm{F}\left(23.9^{\circ} \mathrm{C}\right)$ with 1.5 specific gravity fluid,
maximum support spacing $=26.9 \times 0.92=24.7 \mathrm{ft}$.

Maximum Support Spacing for Uninsulated Pipe ${ }^{(1)}$

| Size | Continuous Spans of Pipe $^{(2)}$ |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- |
|  | feet | meters |  |  |  |
| in | $\mathbf{m m}$ | $\mathbf{7 5}^{\circ} \mathbf{F}$ | $\mathbf{2 0 0}^{\circ} \mathbf{F}$ | $\mathbf{2 4}^{\circ} \mathbf{C}$ | $\mathbf{9 3}^{\circ} \mathbf{C}$ |
| 2 | 50 | 14.7 | 10.6 | 4.48 | 3.23 |
| 3 | 80 | 16.9 | 12.2 | 5.15 | 3.72 |
| 4 | 100 | 19.3 | 14.0 | 5.88 | 4.27 |
| 6 | 150 | 23.5 | 17.0 | 7.16 | 5.18 |
| 8 | 200 | 26.9 | 19.5 | 8.20 | 5.94 |
| 10 | 250 | 30.0 | 21.7 | 9.14 | 6.62 |
| 12 | 300 | 32.5 | 23.7 | 9.92 | 7.19 |
| 14 | 350 | 34.9 | 25.3 | 10.64 | 7.71 |
| 16 | 400 | 37.4 | 27.1 | 11.40 | 8.26 |

${ }^{(1)}$ For $\mathrm{Sg}=1.0$, consult manufacturer for heavier insulated pipe support spans. Span recommendations include no provision for weight of (fittings, valves, etc.) or thrusts at branches and turns. Heavy valves and other appurtenances must be supported separately.
${ }^{(2)}$ Calculated spans are based on $1 / 2^{\prime \prime}$ mid-span deflections to ensure good appearance and adequate drainage. Total system stresses should always be taken into account by the system design engineer when determining support spans.

There are seven basic guidelines to follow when designing an above ground piping system:

1. Do not exceed the recommended support span.
2. Support heavy valves and in-line equipment independently.
3. Protect pipe from external abrasion at supports.
4. Avoid point contact loads
5. Avoid excessive bending. This applies to handling, transporting, initial layout, and final installed position.
6. Avoid excessive vertical loading to minimize bending stresses on pipe and fittings.
7. Provide adequate axial and lateral restraint to ensure line stability during rapid changes in flow (water hammer).

Adjustment Factors for Various Spans With Unsupported Fitting at Change in Direction

|  | Span Type | Factor |
| :--- | :--- | :--- |
| LC | Continuous interior or fixed end spans | 1.00 |
| C | Second span from supported end or unsupported fitting | 0.80 |
| A+B | Sum of unsupported spans at fitting | $\leq 0.75^{\star}$ |
| D | Simple supported end span | 0.67 |

*For example: If continuous support is 10 ft . $(3.04 \mathrm{~m}), \mathrm{A}+\mathrm{B}$ must not exceed 7.5 ft . $(2.28 \mathrm{~m})(\mathrm{A}=3 \mathrm{ft}$. $(0.91 \mathrm{~m})$ and $B=4.5 \mathrm{ft}$. $(1.37 \mathrm{~m})$ ) would satisfy this condition.


Adjustment Factors for Various Spans With Supported Fitting at Change in Direction

|  | Span Type | Factor |
| :--- | :--- | :--- |
| LC | Continuous interior or fixed end spans | 1.00 |
| A | Second span from simple supported end or unsupported fitting | 0.80 |
| B | Simple supported end span | 0.67 |



## Thermal Expansion

The effects of thermal gradients on piping systems may be significant and should be considered in every piping system stress analysis. Pipe line movements due to thermal expansion or contraction may cause
high stresses or even buckle a pipe line if improperly restrained. Several piping system designs are used to manage thermal expansion and contraction in above ground piping systems. They are listed below according to economic preference:

1. Use of inherent flexibility in directional changes.
2. Restraining axial movements and guiding to prevent buckling.
3. Use expansion loops to absorb thermal movements.
4. Use mechanical expansion joints to absorb thermal movements.

To perform a thermal analysis the following information is required:

1. Isometric layout of piping system
2. Physical and material properties of pipe
3. Design temperatures
4. Installation temperature (Final tie in temperature)
5. Terminal equipment load limits
6. Supportmovements

A comprehensive review of temperature effects on fiberglass pipe may be found in NOV Fiber Glass Systems' Engineering and Piping Design Guide, Section 3.

| Change in <br> Temperature |  | Pipe Change in <br> Length |  |
| :--- | :--- | :--- | :--- |
| ${ }^{\circ} \mathbf{F}$ | ${ }^{\circ} \mathbf{C}$ | in/100 ft | $\mathbf{c m} / \mathbf{1 0 0} \mathbf{~ m}$ |
| 25 | 13.9 | 0.41 | 3.45 |
| 50 | 27.8 | 0.83 | 6.90 |
| 75 | 41.7 | 1.24 | 10.35 |
| 100 | 55.6 | 1.66 | 13.80 |

## Testing

Hydrostatic testing is recommended to evaluate the integrity of all new piping installations. For systems operating below the system rating, a test pressure of 1.5 times the system operating pressure is recommended; however, the maximum test pressure must not exceed 1.3 times the lowest pressure rated fiberglass component in the piping system.
The hydro test pressure should be repeated up to ten cycles from 0 psig to the test pressure to provide a high degree of confidence in the piping system. The final pressurization cycle should be allowed to stabilize for 15-30 minutes, then inspected for leaks. Do not attempt to repair leaks while system is pressurized. The hydro test should be repeated after any re-work is performed.

When hydro testing, open high-point vents (ifused) to prevent entrapment of air in the lines as the system is slowly filled with water, then close the vents and slowly pressurize to the test pressure. Upon completion of hydro test, relieve the pressure on the system slowly, open vents and any drains to allow for complete drainage of the system.

## Water Hammer

Piping systems may be damaged by pressure surges due to water hammer. The use of soft start pumps and slow actuating valves will reduce the magnitude of surge pressures during operation and are highly recommended.

## Typical Mechanical Properties

| Pipe Property | $75^{\circ} \mathrm{F}$ | $24^{\circ} \mathrm{C}$ | $200^{\circ} \mathrm{F}$ | $93^{\circ} \mathrm{C}$ | Method |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | psi | MPa | psi | MPa |  |
| Axial Tensile |  |  |  |  |  |
| Ultimate Stress | 9,530 | 65.7 | 6,585 | 45.4 | ASTM D2105 |
| Modulus of Elasticity | $1.68 \times 10^{6}$ | 11,584 | $1.42 \times 10^{6}$ | 9,791 | ASTM D2105 |
| Poisson's Ratio, $v_{\text {ah }}\left(v_{\text {ha }}\right)^{(1)}$ | 0.35 (0.61) |  |  |  |  |
| Axial Compression |  |  |  |  |  |
| Ultimate Stress | 12,510 | 86.3 | 8,560 | 59.0 | ASTM D695 |
| Modulus of Elasticity | $0.677 \times 10^{6}$ | 4,668 | $0.379 \times 10^{6}$ | 2,613 | ASTM D695 |
| Beam Bending |  |  |  |  |  |
| Modulus of Elasticity (Long Term) | $2.6 \times 10^{6}$ | 17,927 | $0.718 \times 10^{6}$ | 4.951 | ASTM D2925 |
| Hydrostatic Burst |  |  |  |  |  |
| Ultimate Hoop Tensile Stress | 40,150 | 277 | 36,480 | 252 | ASTM D1599 |
| Hydrostatic Hoop Design Stress |  |  |  |  |  |
| Static 20 Year Life LTHS -95\% LCL | - | - | 20,787-17,155 | 143.3-118.3 | ASTM D2992-Procedure B |
| Static 50 Year Life LTHS -95\% LCL | - | - | 19,057-15,302 | 131.4-105.5 | ASTM D2992-Procedure B |
| Parallel Plate |  |  |  |  |  |
| Hoop Modulus of Elasticity | $3.02 \times 10^{6}$ | 20,822 | - | - | ASTM D2412 |
| Shear Modulus | $1.76 \times 10^{6}$ | 12,135 | $1.63 \times 10^{6}$ | 11,240 | - |

## Typical Physical Properties

| Pipe Property | Value | Value | Method |
| :--- | :--- | :--- | :--- |
| Thermal <br> Conductivity | $0.23 \mathrm{BTU} / \mathrm{hr} \cdot \mathrm{\circ t}{ }^{\circ} \mathrm{F}$ | $0.4 \mathrm{~W} / \mathrm{m}^{\circ} \mathrm{C}$ | ASTM D177 |
| Thermal <br> Expansion | $13.8 \times 10^{-6} \mathrm{in} / \mathrm{in}^{\circ} \mathrm{F}$ | $24.8 \times 10^{-6} \mathrm{~mm} / \mathrm{mm}^{\circ} \mathrm{C}$ | ASTM D696 |
| Absolute <br> Roughness | 0.00021 in | 0.00053 mm |  |
| Specific Gravity | 1.8 |  |  |

${ }^{(1)} V_{\text {ha }}=$ The ratio of axial strain to hoop strain resulting from stress in the hoop direction.
$v_{\mathrm{ah}}=$ The ratio of hoop strain to axial strain resulting from stress in the axial direction.
${ }^{(2)}$ The differential pressure between internal and external pressure which causes collapse.
${ }^{(3)}$ A 0.67 design factor is recommended for short duration vacuum service. A full vacuum is equal to $14.7 \mathrm{psig}(0.101 \mathrm{MPa})$ differential pressure at sea level.
${ }^{(4)}$ A 0.33 design factor is recommended for sustained (long-term) differential collapse pressure design and operation.

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## Ultimate Collapse Pressure

| Size | Collapse Pressure $^{(2,3,4)}$ |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- |
|  | psig |  |  | MPa |  |
| in | $\mathbf{m m}$ | $\mathbf{7 5}^{\circ} \mathbf{F}$ | $\mathbf{2 0 0}^{\circ} \mathbf{F}$ | $\mathbf{2 4}^{\circ} \mathbf{C}$ | $\mathbf{9 3}^{\circ} \mathbf{C}$ |
| 2 | 50 | 330 | 250 | 2.28 | 1.72 |
| 3 | 80 | 160 | 120 | 1.10 | 0.83 |
| 4 | 100 | 160 | 120 | 1.10 | 0.83 |
| 6 | 150 | 160 | 120 | 1.10 | 0.83 |
| 8 | 200 | 160 | 120 | 1.10 | 0.83 |
| 10 | 250 | 160 | 120 | 1.10 | 0.83 |
| 12 | 300 | 160 | 120 | 1.10 | 0.83 |
| 14 | 350 | 160 | 120 | 1.10 | 0.83 |
| 16 | 400 | 160 | 120 | 1.10 | 0.83 |

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# Green Thread ${ }^{\text {TM }}$ HP 40 

## Applications

- Chemical Processing Liquids
- Food Processing Liquids
- Potable Water
- Cooling Water
- Condensate Return
- Industrial Wastewater
- Mildly Corrosive Liquids
- Crude Oil \& Gas


## Materials and Construction

All pipe manufactured by filament winding process using amine-cured epoxy thermosetting resin to impregnate strands of continuous glass filaments. Pipe wall includes a minimum $0.020^{\prime \prime}(0.50 \mathrm{~mm})$ resinrich corrosion barrier (liner).

Pipe is available in 2"-12" ( $50-300 \mathrm{~mm}$ ) diameters with static pressure ratings of 580 psig ( 40 bar). The pipe and fittings are designed for continuous operation at $200^{\circ} \mathrm{F}\left(93^{\circ} \mathrm{C}\right)$ serviceable up to $230^{\circ} \mathrm{F}\left(110^{\circ} \mathrm{C}\right)$ by applying a derating factor of 0.76 to all component ratings. Pipe diameters of $1^{\prime \prime}-6^{\prime \prime}(25-150 \mathrm{~mm})$ are available in $20^{\prime}(6 \mathrm{~m})$ random lengths and the $8^{\prime \prime}-12^{\prime \prime}$ ( $200-300 \mathrm{~mm}$ ) diameters are in $19^{\prime}$ or $39^{\prime}(6$ or 12 m ) random lengths.

ASTM D-2996 Classification: RTRP - 11FX13110 for static design basis.

## Fittings

Fittings are filament wound with the same chemical, temperature and pressure capabilities as the pipe. For 2"-12" ( $50-300 \mathrm{~mm}$ ) use HP32/40 Bar fittings in document Cl1370.

## Joining System

- Bell \& Spigot - Matched-taper joint secured with epoxy adhesive. Self-locking feature resists movement, facilitating joining runs of pipe without waiting for adhesive to cure.
- Flanged - Available for all piping systems and diameters; factory assembled or shipped loose for assembly in the field.


Flanged

- Produced Water
- Saltwater
- $\mathrm{CO}_{2}$


Bell \& Spigot

Nominal Dimensional Data

| Pipe Size |  | Inside Diameter |  | Outside <br> Diameter |  | Minimum Reinforced Wall Thickness |  | Liner Thickness |  | Weight ${ }^{(1)}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | in | mm | in | mm | in | mm | in | mm | lbs/ft | kg/m |
| 2 | 50 | 2.15 | 55 | 2.34 | 60 | 0.075 | 1.91 | 0.02 | 0.51 | 0.6 | 0.93 |
| 3 | 80 | 3.28 | 83 | 3.53 | 90 | 0.105 | 2.67 | 0.02 | 0.51 | 1.1 | 1.65 |
| 4 | 100 | 4.28 | 109 | 4.60 | 117 | 0.137 | 3.48 | 0.02 | 0.51 | 1.8 | 2.74 |
| 6 | 150 | 6.35 | 161 | 6.80 | 173 | 0.203 | 5.16 | 0.02 | 0.51 | 3.9 | 5.80 |
| 8 | 200 | 8.36 | 212 | 8.93 | 227 | 0.266 | 6.76 | 0.02 | 0.51 | 6.6 | 9.84 |
| 10 | 250 | 10.36 | 263 | 11.06 | 281 | 0.330 | 8.38 | 0.02 | 0.51 | 10.0 | 14.88 |
| 12 | 300 | 12.29 | 312 | 13.11 | 333 | 0.391 | 9.93 | 0.02 | 0.51 | 14.0 | 20.83 |

## Supports

Proper pipe support spacing depends on the temperature and weight of the fluid in the pipe. The support spacing table is based on unrestrained continuous beam theory using the pipe bending modulus derived from long-term beam bending tests. The following tables were developed to ensure a design that limits beam mid-span deflection to $1 / 2$ inch to ensure good appearance and adequate drainage. Any additional loads on the piping system such as insulation, wind, seismic, etc. requires further consideration. Restrained (anchored) piping systems operating at elevated temperatures may result in guide spacing requirements that are shorter than unrestrained piping systems. In this case, the maximum guide spacing governs the support span requirements for the system. Pipe spans near elbows require special attention. Both supported and unsupported elbows are considered in the following tables and must be followed to properly design the piping system.

## Maximum Support Spacing for Uninsulated Pipe ${ }^{(1)}$

| Size |  | Continuous Spans of Pipe ${ }^{(2)}$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | feet |  | meters |  |
| in | mm | $75^{\circ} \mathrm{F}$ | $200^{\circ} \mathrm{F}$ | $24^{\circ} \mathrm{C}$ | $93^{\circ} \mathrm{C}$ |
| 2 | 50 | 14.7 | 10.6 | 4.48 | 3.23 |
| 3 | 80 | 17.8 | 12.9 | 5.43 | 3.93 |
| 4 | 100 | 20.3 | 14.7 | 6.19 | 4.48 |
| 6 | 150 | 24.7 | 17.9 | 7.53 | 5.46 |
| 8 | 200 | 28.3 | 20.6 | 8.63 | 6.28 |
| 10 | 250 | 31.6 | 22.9 | 9.63 | 6.98 |
| 12 | 300 | 34.3 | 24.9 | 10.45 | 7.59 |

${ }^{(1)}$ For $\mathrm{Sg}=1.0$, consult manufacturer for heavier insulated pipe support spans. Span recommendations include no provision for weight of (fittings, valves, etc.) or thrusts at branches and turns. Heavy valves and other appurtenances must be supported separately.
${ }^{(2)}$ Calculated spans are based on $1 / 2^{\prime \prime}$ mid-span deflections to ensure good appearance and adequate drainage. Total system stresses should always be taken into account by the system design engineer when determining support spans.

There are seven basic guidelines to follow when designing an above ground piping system:

1. Do not exceed the recommended support span.
2. Support heavy valves and in-line equipment independently.
3. Protect pipe from external abrasion at supports.
4. Avoid point contact loads
5. Avoid excessive bending. This applies to handling, transporting, initial layout, and final installed position.
6. Avoid excessive vertical loading to minimize bending stresses on pipe and fittings.
7. Provide adequate axial and lateral restraint to ensure line stability during rapid changes in flow (water hammer).

Adjustment Factors for Various Spans With Unsupported Fitting at Change in Direction

|  | Span Type | Factor |
| :--- | :--- | :--- |
| LC | Continuous interior or fixed end spans | 1.00 |
| C | Second span from supported end or unsupported fitting | 0.80 |
| A+B | Sum of unsupported spans at fitting | $\leq 0.75^{\star}$ |
| D | Simple supported end span | 0.67 |

*For example: If continuous support is 10 ft . $(3.04 \mathrm{~m}), \mathrm{A}+\mathrm{B}$ must not exceed 7.5 ft . $(2.28 \mathrm{~m})(\mathrm{A}=3 \mathrm{ft}$. $(0.91 \mathrm{~m})$ and $\mathrm{B}=4.5 \mathrm{ft}$. ( 1.37 m )) would satisfy this condition.


Support Spacing vs. Specific Gravity

| Specific Gravity | 2.00 | 1.50 | 1.25 | 1.00 | 0.75 |
| :--- | :--- | :--- | :--- | :--- | :--- |
| Multiplier | 0.86 | 0.92 | 0.96 | 1.00 | 1.07 |

Example: $8^{\prime \prime}$ pipe @ $75^{\circ} \mathrm{F}\left(23.9^{\circ} \mathrm{C}\right)$ with 1.5 specific gravity fluid,
maximum support spacing $=28.3 \times 0.92=26.0 \mathrm{ft}$.

Adjustment Factors for Various Spans With Supported Fitting at Change in Direction

|  | Span Type | Factor |
| :--- | :--- | :--- |
| LC | Continuous interior or fixed end spans | 1.00 |
| A | Second span from simple supported end or unsupported fitting | 0.80 |
| B | Simple supported end span | 0.67 |



## Thermal Expansion

The effects of thermal gradients on piping systems may be significant and should be considered in every piping system stress analysis. Pipe line movements due to thermal expansion or contraction may cause high stresses or even buckle a pipe line if improperly restrained. Several piping system designs are used to manage thermal expansion and contraction in above ground piping systems. They are listed below according to economic preference:

1. Use of inherent flexibility in directional changes.
2. Restraining axial movements and guiding to prevent buckling.
3. Use expansion loops to absorb thermal movements.
4. Use mechanical expansion joints to absorb thermal movements.

To perform a thermal analysis the following information is required:

1. Isometric layout of piping system
2. Physical and material properties of pipe
3. Design temperatures
4. Installation temperature (Final tie in temperature)
5. Terminal equipment load limits
6. Support movements

A comprehensive review of temperature effects on fiberglass pipe may be found in NOV Fiber Glass Systems' Engineering and Piping Design Guide, Section 3.

| Change in <br> Temperature |  | Pipe Change in <br> Length |  |
| :--- | :--- | :--- | :--- |
| ${ }^{\circ} \mathbf{F}$ | ${ }^{\circ} \mathbf{C}$ | $\mathbf{i n} / \mathbf{1 0 0} \mathbf{f t}$ | $\mathbf{c m} / \mathbf{1 0 0} \mathbf{~ \mathbf { ~ m }}$ |
| 25 | 13.9 | 0.41 | 3.45 |
| 50 | 27.8 | 0.83 | 6.90 |
| 75 | 41.7 | 1.24 | 10.35 |
| 100 | 55.6 | 1.66 | 13.80 |

## Testing

Hydrostatic testing is recommended to evaluate the integrity of all new piping installations. For systems operating below the system rating, a test pressure of 1.5 times the system operating pressure is recommended; however, the maximum test pressure must not exceed 1.3 times the lowest pressure rated fiberglass component in the piping system.

The hydro test pressure should be repeated up to ten cycles from 0 psig to the test pressure to provide a high degree of confidence in the piping system. The final pressurization cycle should be allowed to stabilize for 15-30 minutes, then inspected for leaks. Do not attempt to repair leaks while system is pressurized. The hydro test should be repeated after any re-work is performed.

When hydro testing, open high-point vents (if used) to prevent entrapment of air in the lines as the system is slowly filled with water, then close the vents and slowly pressurize to the test pressure. Upon completion of hydro test, relieve the pressure on the system slowly, open vents and any drains to allow for complete drainage of the system.

## Water Hammer

Piping systems may be damaged by pressure surges due to water hammer. The use of soft start pumps and slow actuating valves will reduce the magnitude of surge pressures during operation and are highly recommended.

## Typical Mechanical Properties

| Pipe Property | $75^{\circ} \mathrm{F}$ | $24^{\circ} \mathrm{C}$ | $200^{\circ} \mathrm{F}$ | $93^{\circ} \mathrm{C}$ | Method |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | psi | MPa | psi | MPa |  |
| Axial Tensile |  |  |  |  |  |
| Ultimate Stress | 9,530 | 65.7 | 6,585 | 45.4 | ASTM D2105 |
| Modulus of Elasticity | $1.68 \times 10^{6}$ | 11,584 | $1.42 \times 10^{6}$ | 9,791 | ASTM D2105 |
| Poisson's Ratio, $v_{\text {ah }}\left(v_{\text {ha }}\right)^{(1)}$ | 0.35 (0.61) |  |  |  |  |
| Axial Compression |  |  |  |  |  |
| Ultimate Stress | 12,510 | 86.3 | 8,560 | 59.0 | ASTM D695 |
| Modulus of Elasticity | $0.677 \times 10^{6}$ | 4,668 | $0.379 \times 10^{6}$ | 2,613 | ASTM D695 |
| Beam Bending |  |  |  |  |  |
| Modulus of Elasticity (Long Term) | $2.6 \times 10^{6}$ | 17,927 | $0.718 \times 10^{6}$ | 4.951 | ASTM D2925 |
| Hydrostatic Burst |  |  |  |  |  |
| Ultimate Hoop Tensile Stress | 40,150 | 277 | 36,480 | 252 | ASTM D1599 |
| Hydrostatic Hoop Design Stress |  |  |  |  |  |
| Static 20 Year Life LTHS -95\% LCL | - | - | 20,787-17,155 | 143.3-118.3 | ASTM D2992-Procedure B |
| Static 50 Year Life LTHS -95\% LCL | - | - | 19,057-15,302 | 131.4-105.5 | ASTM D2992-Procedure B |
| Parallel Plate |  |  |  |  |  |
| Hoop Modulus of Elasticity | $3.02 \times 10^{6}$ | 20,822 | - | - | ASTM D2412 |
| Shear Modulus | $1.76 \times 10^{6}$ | 12,135 | $1.63 \times 10^{6}$ | 11,240 |  |

## Typical Physical Properties

| Pipe Property | Value | Value | Method |
| :--- | :--- | :--- | :--- |
| Thermal <br> Conductivity | $0.23 \mathrm{BTU} / \mathrm{hr} \cdot \mathrm{ft} \cdot{ }^{\circ} \mathrm{F}$ | $0.4 \mathrm{~W} / \mathrm{m}^{\circ} \mathrm{C}$ | ASTM D177 |
| Thermal <br> Expansion | $13.8 \times 10^{-6} \mathrm{in} / \mathrm{in}^{\circ} \mathrm{F}$ | $24.8 \times 10^{-6} \mathrm{~mm} / \mathrm{mm}^{\circ} \mathrm{C}$ | ASTM D696 |
| Absolute <br> Roughness | 0.00021 in | 0.00053 mm |  |
| Specific Gravity | 1.8 |  |  |

${ }^{(1)} V_{\text {ha }}=$ The ratio of axial strain to hoop strain resulting from stress in the hoop direction.

## Ultimate Collapse Pressure

| Size | Collapse Pressure ${ }^{(2,3,4)}$ |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- |
|  | psig |  | $\mathbf{M P a}$ |  |  |  |
| in | $\mathbf{m m}$ | $\mathbf{7 5}^{\circ} \mathbf{F}$ | $\mathbf{2 0 0}^{\mathbf{}} \mathbf{F}$ | $\mathbf{2 4}^{\circ} \mathbf{C}$ | $\mathbf{9 3}^{\circ} \mathbf{C}$ |
| 2 | 50 | 330 | 250 | 2.28 | 1.72 |
| 3 | 80 | 280 | 215 | 1.93 | 1.48 |
| 4 | 100 | 280 | 215 | 1.93 | 1.48 |
| 6 | 150 | 280 | 215 | 1.93 | 1.48 |
| 8 | 200 | 280 | 215 | 1.93 | 1.48 |
| 10 | 250 | 280 | 215 | 1.93 | 1.48 |
| 12 | 300 | 280 | 215 | 1.93 | 1.48 |

$v_{\mathrm{ah}}=$ The ratio of hoop strain to axial strain resulting from stress in the axial direction.
${ }^{(2)}$ The differential pressure between internal and external pressure which causes collapse.
${ }^{(3)}$ A 0.67 design factor is recommended for short duration vacuum service. A full vacuum is equal to
$14.7 \mathrm{psig}(0.101 \mathrm{MPa})$ differential pressure at sea level.
${ }^{(4)} \mathrm{A} 0.33$ design factor is recommended for sustained (long-term) differential collapse pressure design and operation.

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## Fiber Glass Systems

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## Silver Streak ${ }^{\circledR}$ Product Data

- Flue Gas Desulfurization
- Limestone Slurry
- Ammonium Sulfate
- Gypsum Slurry

Materials and Construction

All pipe manufactured by filament winding process using amine-cured epoxy thermosetting resin to impregnate strands of continuous glass filaments with a resin-rich corrosion barrier. Manufactured with a proprietary blend of abrasion-resistant additives, Silver Streak piping is offered with a standard 80 mil nominal liner.

Pipe is available in 2" through 24" diameters with pressure ratings up to 225 psig static at a maximum operating temperature of $225^{\circ} \mathrm{F}$ and is ideal for yard piping. Silver Streak LD pipe, available in 30" through 54" diameters, is ideal for recirculating piping and operates at temperatures up to $200^{\circ} \mathrm{F}$ and pressures up to 150 psig.

The entire 80 mil nominal liner contains $80 \%$ resin/abrasion-resistant additives and $20 \%$ reinforcement. The pipe is rated for full vacuum service at $175^{\circ} \mathrm{F}$ and comes spigot $x$ spigot in 2" through 12" sizes and spigot $x$ spigot or bell $x$ spigot in 14 " through 24 " sizes.

## Fittings

Fittings are manufactured with the same chemical/temperature capabilities as the pipe. Depending on the particular part and size, fittings will be compression molded, contact molded, hand fabricated or filament wound.

## Joining Systems

## Bell \& Spigot

Matched-taper joint secured with epoxy adhesive. Self-locking feature resists movement, facilitating joining runs of pipe without awaiting adhesive
 cure.

| Nominal Dimensional Data (Liner Thickness = 0.080"/1.8 mm) |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { Pipe } \\ \text { Size (In) } \end{gathered}$ | I.D. |  | O.D. |  | Wall Thickness |  | Weight |  | Capacity |  |
|  | (In) | (mm) | (In) | (mm) | (In) | (mm) | (Lbs/Ft) | (kg/m) | (Gal/Ft) | ( $\mathrm{Ft} / \mathrm{F}^{\text {ct }}$ ) |
| 2 | 2.00 | 51 | 2.40 | 61 | 0.200 | 5.1 | 1.1 | 1.6 | 0.16 | 0.022 |
| 3 | 3.28 | 83 | 3.65 | 93 | 0.186 | 4.7 | 1.6 | 2.4 | 0.44 | 0.059 |
| 4 | 4.28 | 109 | 4.66 | 118 | 0.190 | 4.8 | 2.1 | 3.1 | 0.75 | 0.100 |
| 6 | 6.35 | 161 | 6.75 | 171 | 0.197 | 5.0 | 3.1 | 4.6 | 1.65 | 0.220 |
| 8 | 8.36 | 212 | 8.83 | 224 | 0.233 | 5.9 | 5.0 | 7.4 | 2.85 | 0.381 |
| 10 | 10.36 | 263 | 10.87 | 276 | 0.251 | 6.4 | 6.6 | 9.8 | 4.38 | 0.585 |
| 12 | 12.29 | 312 | 12.81 | 325 | 0.260 | 6.6 | 8.1 | 12.1 | 6.16 | 0.824 |
| 14 | 14.04 | 357 | 14.71 | 374 | 0.338 | 8.6 | 12.3 | 18.3 | 8.04 | 1.075 |
| 16 | 16.04 | 407 | 16.68 | 424 | 0.320 | 8.1 | 13.2 | 19.6 | 10.5 | 1.403 |
| 18 | 17.83 | 453 | 18.50 | 470 | 0.336 | 8.5 | 15.5 | 23.1 | 12.97 | 1.734 |
| 20 | 19.83 | 504 | 20.56 | 522 | 0.364 | 9.2 | 18.7 | 27.8 | 16.04 | 2.145 |
| 24 | 23.83 | 605 | 24.66 | 626 | 0.414 | 10.5 | 25.7 | 38.3 | 23.17 | 3.097 |
| Tolerances or maximum/minimum limits can be obtained from NOV Fiber Glass Systems. |  |  |  |  |  |  |  |  |  |  |



## Average Physical Properties

| Property |  | $\begin{gathered} 75^{\circ} F \\ \text { psi } \end{gathered}$ | $\begin{gathered} 24^{\circ} \mathrm{C} \\ \mathrm{MPa} \end{gathered}$ | $\begin{gathered} 225^{\circ} \mathrm{F} \\ \mathrm{psi} \end{gathered}$ | $\begin{aligned} & 107^{\circ} \mathrm{C} \\ & \mathrm{MPa} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Axial Tensile - ASTM D2105 Ultimate Stress Modulus of Elasticity |  | $\begin{gathered} 10,550 \\ 1.75 \times 10^{6} \end{gathered}$ | $\begin{gathered} 72.7 \\ 12,093 \end{gathered}$ | $\begin{gathered} 7,160 \\ 1.03 \times 10^{6} \end{gathered}$ | $\begin{array}{r} 49.4 \\ 7,102 \end{array}$ |
| Poisson's Ratio $\nu_{\text {a/h }}\left(\nu_{\text {h/a }}\right)$ |  | 0.35 (0.56) |  |  |  |
| Axial Compression - ASTM D694 Ultimate Stress Modulus of Elasticity |  | $\begin{gathered} 33,300 \\ 1.26 \times 10^{6} \end{gathered}$ | $\begin{aligned} & 229.6 \\ & 8,687 \end{aligned}$ | $\begin{aligned} & 17,800 \\ & 0.54 \times 10^{6} \end{aligned}$ | $\begin{aligned} & 122.7 \\ & 3,723 \end{aligned}$ |
| Beam Bending - ASTM D2925 Ultimate Stress Modulus of Elasticity (Long Term) |  | $\begin{gathered} 23,000 \\ 2.18 \times 10^{6} \end{gathered}$ | $\begin{gathered} 158.6 \\ 15,030 \end{gathered}$ | $\begin{gathered} 16,000 \\ 1.10 \times 10^{6} \end{gathered}$ | $\begin{aligned} & 110.3 \\ & 7,653 \end{aligned}$ |
| Hydrostatic Burst - ASTM D1599 Ultimate Hoop Tensile Stress |  | 46,300 | 319 | 49,500 | 341.3 |
| Ring Tensile - ASTM D2290 Minimum Hoop Tensile Stress |  | 27,280 | 188 | - | - |
| Hydrostatic Design - ASTM D2992, Procedure B - Hoop Tensile Stress *20 Year Static Life at $200^{\circ} \mathrm{F} / 93.3^{\circ} \mathrm{C}$ | $\begin{gathered} \text { (LTHS) } \\ \text { (LCL) } \end{gathered}$ | $\begin{aligned} & 27,715 \\ & 22,400 \end{aligned}$ | $\begin{aligned} & 191 \\ & 154 \end{aligned}$ | $\begin{aligned} & 16,945^{*} \\ & 14,654^{*} \end{aligned}$ | $\begin{aligned} & 116.8^{*} \\ & 101.0^{*} \end{aligned}$ |


| Thermal Expansion Coefficient - ASTM D696 | $1.26 \times 10^{-5} \mathrm{in} / \mathrm{in} /{ }^{\circ} \mathrm{F}$ | $1.58 \times 10^{-5} \mathrm{~mm} / \mathrm{mm} /{ }^{\circ} \mathrm{C}$ |
| :--- | :---: | :---: |
| Thermal Conductivity | $0.23 \mathrm{BTU} / \mathrm{hr}-\mathrm{ft}-{ }^{\circ} \mathrm{F}$ | $0.4 \mathrm{~W} / \mathrm{m}-{ }^{\circ} \mathrm{C}$ |
| Specific Gravity - ASTM D792 |  | 1.8 |
| Absolute Surface Roughness | 0.00021 Inch |  |
| Manning Roughness Coefficient, $\mathbf{n}$ |  | 0.009 |

## Testing:

Hydrostatic testing should be performed to evaluate the structural integrity of a new piping system installation. Test pressures of 1.5 times the design operating pressure but not exceeding 1.2 times the static pressure rating of the lowest rated fiberglass component in the piping system are recommended. Contact the company if test pressures exceed 450 psig before testing. The hydro test pressure should be repeated up to ten cycles from 0 psig to the test pressure to provide a high degree of confidence in the piping system. The final pressurization cycle should be allowed to stabilize for 15-30 minutes, then inspected for leaks. Do not attempt to repair leaks while system is pressurized. The hydro test should be repeated after any re-work is performed.

When hydro testing, open vents to prevent entrapment of air in the lines as the system is slowly filled with water. Then close the vents and slowly pressurize to the test pressure. Upon completion of hydrotest, relieve the pressure on the system slowly, open vents and any drains to allow for complete drainage of the system.

Piping systems with design temperatures above $150^{\circ} \mathrm{F}$ should be tested at 1.2 times the static pressure rating of the lowest rated fiberglass component in the system.

| Recommended Operating Ratings |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Loads bs) | Axial Co Loads M | $\begin{aligned} & \text { ressive } \\ & \text { (Lbs) }^{(1)} \end{aligned}$ | Bending Radius |  | Para ASTM D2 | $\begin{aligned} & \text { Plate Lo } \\ & 12 \text { @ 5\% } \end{aligned}$ | ng ection |
| Size <br> (In) |  | ature <br> $225^{\circ} \mathrm{F}$ |  | ture $225^{\circ} \mathrm{F}$ | Entire <br> Temp. <br> Range | (Ft Lbs) <br> Entire Temp. <br> Range | Stiffness Factor ( $\mathrm{In}^{3} / \mathrm{Lbs} / \mathrm{ln}^{2}$ ) | $\begin{gathered} \text { Pipe } \\ \text { Stiffness } \\ \text { (psi) } \end{gathered}$ | Hoop Modulus $\times 10^{6}$ (psi) |
| 2 | 1,900 | 1,300 | 6,600 | 3,000 | 75 | 130 | n/a | n/a | n/a |
| 3 | 2,700 | 1,800 | 8,500 | 4,000 | 110 | 280 | n/a | n/a | n/a |
| 4 | 3,600 | 2,400 | 11,000 | 6,000 | 140 | 480 | n/a | n/a | n/a |
| 6 | 5,600 | 3,800 | 17,000 | 9,000 | 210 | 1,100 | n/a | n/a | n/a |
| 8 | 9,500 | 6,500 | 30,000 | 16,000 | 270 | 2,480 | n/a | n/a | n/a |
| 10 | 13,000 | 8,900 | 41,000 | 22,000 | 340 | 4,200 | n/a | n/a | n/a |
| 12 | 16,000 | 11,000 | 51,000 | 27,000 | 400 | 6,200 | n/a | n/a | n/a |
| 14 | 26,000 | 18,000 | 85,000 | 45,000 | 460 | 11,000 | n/a | n/a | n/a |
| 16 | 28,000 | 19,000 | 90,000 | 48,000 | 520 | 14,000 | n/a | n/a | n/a |
| 18 | 33,000 | 22,000 | 100,000 | 56,000 | 580 | 18,000 | n/a | n/a | n/a |
| 20 | 41,000 | 28,000 | 130,000 | 70,000 | 640 | 25,000 | n/a | n/a | n/a |
| 24 | 58,000 | 39,000 | 180,000 | 99,000 | 770 | 42,000 | n/a | n/a | n/a |
| ${ }^{(1)}$ Compressive loads are for short columns only. |  |  |  |  |  |  |  |  |  |


| Pressure Ratings |  |  |  |
| :---: | :---: | :---: | :---: |
| Size <br> (In) | Maximum Internal Static <br> Pressure (psig) 225 | Maximum External Static <br> Pressure (psig) 175 |  |
| $2-24$ | 225 | Full Vacuum |  |

## ASTM D2996 Designation Codes:

| $2 "-24 "$ | RTRP-11FY1-3110 |
| :---: | :---: |


| Pipe Lengths Available |  |
| :---: | :---: |
| Size (In) | Random Length (Ft) |
| $2-6$ | 20 |
| $8-24$ | 40 |

## Water Hammer:

Care should be taken when designing a fiberglass piping system to eliminate sudden surges. Soft start pumps and slow actuating valves should be considered.

## Supports

Proper pipe support spacing depends on the temperature and weight of the fluid in the pipe. The support spacing table is based on unrestrained continuous beam theory using the pipe bending modulus derived from long-term beam bending tests. The maximum spans lengths were developed to ensure a design that limits mid-span deflection to $1 / 2$ inch and dead weight bending to $1 / 8$ of the ultimate bending stress. Any additional loads on the piping system such as insulation, wind, seismic, etc. requires further consideration. Restrained (anchored) piping systems operating at elevated temperatures may result in guide spacing requirements that are shorter than unrestrained piping systems. In this case, the maximum guide spacing governs the support span requirements for the system. Pipe spans near elbows require special attention. Both supported and unsupported elbows are considered in the following tables and must be followed to properly design the piping system.

There are seven basic rules to follow when designing piping system supports:

1. Do not exceed the recommended support span.
2. Support heavy valves and in-line equipment independently.
3. Protect pipe from external abrasion at supports.
4. Avoid point contact loads.
5. Avoid excessive bending. This applies to handling, transporting, initial layout, and final installed position.
6. Avoid excessive vertical loading to minimize bending stresses on pipe and fittings.
7. Provide adequate axial and lateral restraint to ensure line stability during rapid changes in flow.

| Maximum Support Spacing for Uninsulated Pipe ${ }^{(1)}$ |  |  |  |
| :---: | :---: | :---: | :---: |
| Pipe Size (In.) | Continuous Spans of Pipe (Ft.) ${ }^{(2)}$ |  |  |
|  | $75^{\circ} \mathrm{F}$ | $150^{\circ} \mathrm{F}$ | $225^{\circ} \mathrm{F}$ |
| 2 | 14.7 | 13.7 | 12.4 |
| 3 | 16.5 | 15.4 | 13.9 |
| 4 | 17.9 | 16.7 | 15.1 |
| 6 | 20.2 | 18.9 | 17.1 |
| 8 | 23.2 | 21.6 | 19.6 |
| 10 | 25.2 | 23.5 | 21.3 |
| 12 | 26.7 | 24.9 | 22.5 |
| 14 | 30.0 | 28.0 | 25.4 |
| 16 | 30.6 | 28.6 | 25.9 |
| 18 | 32.0 | 29.8 | 27.0 |
| 20 | 33.7 | 31.4 | 28.4 |
| 24 | 36.7 | 34.3 | 31.0 |
| ${ }^{(1)}$ Consult factory for insulated pipe support spacing. <br> ${ }^{(2)}$ Maximum mid-span deflection $1 / 2^{\prime \prime}$ with a specific gravity of 1.0. |  |  |  |

## Support Spacing vs. Specific Gravity

| Specific Gravity | 2.00 | 1.50 | 1.25 | 1.00 | 0.75 |
| :--- | :--- | :--- | :--- | :--- | :--- |
| Multiplier | 0.87 | 0.92 | 0.96 | 1.00 | 1.05 |

Example: 6 " pipe @ $150^{\circ} \mathrm{F}$ with 1.5 specific gravity fluid, maximum support spacing $=18.9 \times 0.92=17.4 \mathrm{ft}$.

Adjustment Factors for Various Spans With Unsupported Fitting at Change in Direction

Adjustment Factors for Various Spans With Supported Fitting at Change in Direction



## Thermal Expansion

The effects of thermal gradients on piping systems may be significant and should be considered in every piping system flexibility analysis. Pipe line movements due to thermal expansion or contraction may cause high stresses or even buckle a pipe line if improperly restrained. Several piping system designs are used to manage thermal expansion and contraction in above ground piping systems. They are listed below according to economic preference:

1. Using directional changes inherent flexibility
2. Restrain pipe axially and guide supports to control deflections and buckling
3. Use expansion loops to absorb thermal movements
4. Use mechanical expansion joints to absorb thermal movements

To perform a thermal analysis the following information is required:

1. An isometric layout of piping system
2. Physical geometry and material properties of pipe
3. Design temperatures
4. Installation temperature (Final tie in temperature)
5. Terminal equipment load limits
6. Support movements

A comprehensive review of temperature effects on fiberglass pipe may be found in NOV Fiber Glass Systems' Engineering and Piping Design Guide.

| Change in <br> Temperature <br> ${ }^{\circ} \mathrm{F}$ | Pipe Change <br> in Length <br> (In/100 Ft) |
| :---: | :---: |
| 25 | 0.38 |
| 50 | 0.76 |
| 75 | 1.13 |
| 100 | 1.51 |


| Restrained Thermal End Loads and Cuide Spacing |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\mathbf{1 2 5}^{\circ}$ Operating Temperature ${ }^{\circ} \mathrm{F}$ (Based on installation temperature of $\mathbf{7 5}{ }^{\circ} \mathrm{F}$ ) |  |  |  |  |  |  |  |

Note: If guide spacing exceeds support span length, then guide at each support.


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## SECTION 1 - Scope

This section covers the use of fiberglass reinforced plastic (FRP) pipe for medium duty slurry service such as limestone slurry to $225^{\circ} \mathrm{F}$ and 225 psig pressure.

The piping system shall be furnished and installed complete with all fittings, joining materials, supports, specials, and other necessary appurtenances.

## SECTION 2 - General Conditions

2.01 Coordination - Material furnished and work performed under this section shall be coordinated with related work and equipment specified under other sections.

| Valves | Section |
| :--- | :--- |
| Supports | Section |
| Equipment | Section |

2.02 Governing Standards - Except as modified or supplemented herein, all materials and construction methods shall comply with the applicable provisions of the following specifications and be tested using the following standards:

## Standard Specifications

| ASTM <br> D2996 | Standard Specification for Filament-Wound"Fi- <br> berglass" (Glass-Fiber-Reinforced-Thermosetting <br> Resin Pipe |
| :--- | :--- |
| ASTM | Standard Specification for Reinforced Thermo- <br> settting Resin (RTR) Flanges |
| ASTM <br> D5685 | Standard Specification for "Fiberglass" (Glass- <br> Fiber-Reinforced-Thermosetting Resin) Pressure <br> Pipe Fittings |

## Standard Test Methods

| ASTM <br> D1599 | Standard Test method for Short-Time Hydraulic <br> Failure Pressure of Plastic Pipe, Tubing and Fit- <br> tings |
| :--- | :--- |
| ASTM <br> D2105 | Standard Test Method for Longitudinal Tensile <br> Properties of "Fiberglass" (Glass-Fiber-Rein- <br> forced Thermosetting Resin) Pipe and Tube |
| ASTM <br> D2412 | Standard Test Method for Determination of Ex- <br> ternal Loading Characteristics of Plastic Pipe by <br> Parallel-Plate Loading |
| ASTM <br> D2925 | Standard Test Method for Beam Deflection of Fi- <br> berglass Pipe Under Full Bore Flow |
| ASTM <br> D2992 | Standard Practice for Obtaining Hydrostatic or <br> Pressure Design Basis for "Fiberglass" (Glass- <br> Fiber-Reinforced Thermosetting Resin) Pipe |

2.03 Operating Conditions - In addition to the above listed minimum design requirements, the system shall meet the following minimum operating conditions:
a. Operating Pressure
b. Operating Temperature
c. Fluid Conveyed
d. Test Pressure
2.04 Quality Assurance - Pipe manufacturer's quality program shall be in compliance with ISO 9001.
2.05 Delivery, Storage, and Handling - Pipe and fittings shall be protected from damage due to impact and point loading. Pipe shall be properly supported to avoid damage due to flexural strains. The contractor shall not allow dirt, debris, or other extraneous materials to get into pipe and fittings. All factory machined areas shall be protected from sunlight until installed.
2.06 Acceptable Manufacturers - NOV Fiber Glass Systems, 501-568-4010, or approved equal.

## SECTION 3 - Materials and Construction

3.01 2"-24" Pipe - The pipe shall be manufactured by the filament winding process using an amine cured epoxy thermosetting resin to impregnate strands of continuous glass filaments, which are wound around a mandrel at a $543 / 4^{\circ}$ winding angle under controlled tension. Pipe shall be heat cured and the cure shall be confirmed using a Differential Scanning Calorimeter.

All pipe shall have a resin-rich corrosion/abrasion resistant barrier reinforced with synthetic surfacing veil. The corrosion/ abrasion barrier shall contain a minimum resin/abrasion additive content of 80 percent and a reinforcement content of 20 percent. The minimum acceptable cured thickness of the corrosion/abrasion barrier shall be 80 mils nominal.
3.02 Flanges and Fittings - All fittings shall be manufactured using the same type materials as the pipe. Fittings may be manufactured either by spray-up/contact molding, contact molding/filament winding, or compression molding methods.

All fittings, except compression molded, shall have a minimum corrosion/abrasion barrier of 100 mils.

All elbows shall have a minimum radius of $11 / 2$ " $D$ ".
Fittings shall be adhesive bonded matched tapered bell and spigot or flanged.

Flanges shall have ANSI B16.5 Class 150 bolt hole patterns.
3.03 Adhesive - Adhesive shall be manufacturer's standard for the piping system specified.
3.04 Gaskets - Gaskets shall be $1 / 8$ " thick, 60-70 durometer full-face type suitable for the service shown on the drawings and as recommended in the manufacturer's standard installation procedures.
3.05 Bolts, Nuts, and Washers - ASTM A307, Grade B, hex head bolts shall be supplied. SAE washers shall be supplied on all nuts and bolts.
3.06 Acceptable Products - Silver Streak as manufactured by Fiber Glass Systems, or approved equal.

## SECTION 4 - Installation and Testing

4.01 Training and Certification. All joints installed or constructed in the field shall be assembled by employees of the contractor who have been trained by the pipe manufacturer. The pipe manufacturer or their authorized representative shall train the contractor's employees in the proper joining and assembly procedures required for the project, including hands-on training by the contractor's employees. Each bonder shall fabricate one pipe-to-pipe and one pipe-to-fitting joint that shall pass the minimum pressure test for the application without leaking.

Only bonders who have successfully completed the pressure test shall bond pipe and fittings.

Certification by the manufacturer shall be in compliance with ASME B31.3, Section A328.2 for the type of joint being made.
4.02 Pipe Installation. Pipe shall be installed as specified and indicated on the drawings.

The piping system shall be installed in accordance with the manufacturer's current published installation procedures.
4.03 Testing. Hydrostatic testing should be performed to evaluate the structural integrity of a new piping system installation. Test pressures of 1.5 times the design pressure but not exceeding 1.5 times the static pressure rating of the lowest rated fiberglass component in the piping system is recommended. The hydrotest pressure should be repeated up to ten times to provide a high degree of confidence in the piping system. The final pressurization should be allowed to stabilize for 15-30 minutes, then, inspected for leaks. Do not attempt to repair leaks while system is pressurized. The hydro test should be repeated after any re-work is performed.

When hydro testing open vents to prevent entrapment of air in the lines as the system is slowly filled with water. Then close the vents and slowly pressurize to the test pressure. Upon completion of hydro test, relieve the pressure on the system slowly, open vents and any drains to allow for complete drainage of the system.

Piping systems with design temperatures above $150^{\circ} \mathrm{F}$ should be tested at 1.5 times the static pressure rating of the lowest rated fiberglass component in the system.


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## SILVER STREAK ${ }^{\circledR}$ LD Abrasion Resistant Pipe



## PRODUCT

SILVER STREAK LD piping is specifically designed for flue gas desulfurization, FGD, recirculation piping applications. The pipe is a filament wound product using vinyl ester resins and continuous glass filaments. The standard 100 mil liner is manufactured using a proprietary blend of abrasion-resistant additives formulated specifically for limestone, gypsum and ammonium sulfate slurries. Custom liner thicknesses are available on special order.

Pipe and fittings are available in 30 " through 48 " diameter sizes with static pressure ratings up to 150 psig operating up to $200^{\circ} \mathrm{F}$ and full vacuum ratings. A recommended specification guide is available in Bulletin No. 2021.

## FITTINGS

Compatible vinyl ester fittings are manufactured with the same chemical resistance and temperature/pressure capabilities as the pipe. The fittings are mitered fabrications available in long radius when required.

## SHOP \& FIELD JOINING

Pipe can be cut and easily prepared for joining in the shop or field. Piping joints may be joined using flanges or Butt \& Wrap joints. See Socket Joint Installation Handbook, for installation procedures for your application.

## FEATURES \& BENEFITS

- Standard sizes include with 30 "-48" diameters
- Operating temperatures up to $200^{\circ} \mathrm{F}$
- Operating pressures up to 150 psig
- Full vacuum service
- Custom-fabricated assemblies are available.


## DIMENSIONAL DATA

| Nominal Pipe Size in. | Nominal I.D. |  | Nominal Wall Thickness |  | Nominal Liner |  | Nominal Weight |  | Max. Support Spacing ${ }^{(1)} @ 175^{\circ} \mathrm{F}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | in. | mm | in. | mm | in. | mm | lbs./ft. | kg/m | ft . | m |
| 30 | 30.19 | 767 | 0.65 | 16.5 | 0.100 | 2.54 | 50.3 | 75.3 | 33.5 | 10.2 |
| 36 | 36.19 | 919 | 0.73 | 18.5 | 0.100 | 2.54 | 68.1 | 101.3 | 36.1 | 11.0 |
| 42 | 42.19 | 1072 | 0.86 | 21.8 | 0.100 | 2.54 | 93.1 | 138.5 | 39.5 | 12.0 |
| 48 | 48.06 | 1221 | 0.94 | 23.9 | 0.100 | 2.54 | 116 | 172.6 | 48.4 | 14.7 |

[^1]
## TYPICAL PHYSICAL PROPERTIES

| Property | $\begin{array}{r} 75^{\circ} \mathrm{F} \\ \mathrm{psi} \end{array}$ | $\begin{array}{r} 175^{\circ} \mathrm{F} \\ \mathrm{psi} \end{array}$ | $\begin{gathered} 24^{\circ} \mathrm{C} \\ \mathrm{MPa} \end{gathered}$ | $79^{\circ} \mathrm{C}$ MPa |
| :---: | :---: | :---: | :---: | :---: |
| Axial Tensile - ASTM D2105 Ultimate Stress Modulus of Elasticity | $\begin{gathered} 9,300 \\ 1.50 \times 10^{6} \end{gathered}$ | 5,500 | $\begin{gathered} 64.1 \\ 10,342 \end{gathered}$ | $37.9$ |
| Poisson's Ratio | 0.35 |  |  |  |
| Axial Compression - ASTM D695 Ultimate Stress Modulus of Elasticity | $\begin{gathered} 17,900 \\ 1.40 \times 10^{6} \end{gathered}$ | $\begin{gathered} 14,700 \\ 9.00 \times 10^{5} \\ \hline \end{gathered}$ | $\begin{aligned} & 123 \\ & 9,653 \end{aligned}$ | $\begin{array}{r} 101 \\ 6,205 \end{array}$ |
| Beam Bending - ASTM D2925 <br> Ultimate Stress <br> Modulus of Elasticity (Long Term) | $\begin{gathered} 14,500 \\ 1.99 \times 10^{6} \end{gathered}$ | $\begin{gathered} 8,000 \\ 1.14 \times 10^{6} \end{gathered}$ | $\begin{gathered} 100 \\ 13,721 \end{gathered}$ | $\begin{array}{r} 55.2 \\ 7,860 \end{array}$ |
| Hydrostatic Burst - ASTM D1599 Ultimate Hoop Tensile Stress | 40,000 | 40,000 | 276 | 276 |
| Hydrostatic Design - ASTM D2992, Procedure B - Hoop Tensile Stress Static 50 Year Life | 12,000 | - | 82.7 | - |


| Coefficient of Linear Thermal Expansion - ASTM <br> D696 | $9.2 \times 10^{-6} \mathrm{in} / \mathrm{in} /{ }^{\circ} \mathrm{F}$ | $16.6 \times 10^{-6} \mathrm{~mm} / \mathrm{mm} /{ }^{\circ} \mathrm{C}$ |
| :--- | :---: | :---: |
| Thermal Conductivity | $0.11 \mathrm{BTU} / \mathrm{hr}-\mathrm{ft}-{ }^{\circ} \mathrm{F}$ | $0.19 \mathrm{~W}(\mathrm{~m})\left({ }^{\circ} \mathrm{C}\right)$ |
| Specific Gravity - ASTM D792 |  | $1.86\left(0.067 \mathrm{lb} / \mathrm{in}^{3}\right)$ |
| Flow Factor - SF / Hazen-Williams Coefficient | $\mathrm{C}-150$ |  |
| Surface Roughness | $1.7 \times 10^{-6} \mathrm{Feet}$ |  |
| Manning's " $\mathbf{n "}$ | 0.009 lnch |  |

## ASTM D2996 Designation Codes

$$
\begin{array}{l|l}
\hline 30 "-48 " & \text { RTRP-12ET1-3110 }
\end{array}
$$

## Vacuum Ratings

| Nominal Pipe Size | $75^{\circ} \mathrm{F}$ | $150^{\circ} \mathrm{F}$ | $175^{\circ} \mathrm{F}$ |
| :---: | :---: | :---: | :---: |
| Inches | psi | psi | psi |
| 30 | 18.3 | 15.0 | 13.0 |
| 36 | 16.3 | 13.3 | 11.3 |
| 42 | 17.8 | 14.5 | 12.6 |

> | QUALITY MANAGEMENT SYSTEM |
| :---: |
| CERTIFIED BY DNV |
| ISO 9001:2008 $=\overline{\text { LITTLE ROCK, AR }}$ |
| SAND SPRINGS, OK |
| SUZHOU, CHINA |
| FIBER GLASS SYSTEMS |

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## Silver Streak ${ }^{\text {TM }}$ LD Piping System

## Specification Guide

## SECTION 1 - Scope

This section covers the use of fiberglass reinforced plastic (FRP) pipe for medium duty slurry service such as limestone slurry up to $200^{\circ} \mathrm{F}$ and up to 150 psig pressure.

The piping shall be furnished and installed complete with all fittings, joining materials, supports, specials, and other necessary appurtenances.

## SECTION 2 - General Conditions

2.01 Coordination - Material furnished and work performed under this section shall be coordinated with related work and equipment specified under other sections.

| Valves | Section |
| :--- | :--- |
| Supports | Section |
| Equipment | Section |

2.02 Governing Standards - Except as modified or supplemented herein, all materials and construction methods shall comply with the applicable provisions of the following standards:

## Standard Test Methods

| ASTM <br> D1599 | Standard Test method for Short-Time Hydraulic <br> Failure Pressure of Plastic Pipe, Tubing and Fit- <br> tings |
| :--- | :--- |
| ASTM <br> D2105 | Standard Test Method for Longitudinal Tensile <br> Properties of "Fiberglass" (Glass-Fiber-Reinforced <br> Thermosetting Resin) Pipe and Tube |
| ASTM <br> D2412 | Standard Test Method for Determination of Ex- <br> ternal Loading Characteristics of Plastic Pipe by <br> Parallel-Plate Loading |
| ASTM <br> D2925 | Standard Test Method for Beam Deflection of Fi- <br> berglass Pipe Under Full Bore Flow |

2.03 Quality Assurance - Pipe manufacturer's quality program shall be in compliance with ISO 9001.
2.04 Delivery, Storage and Handling - Pipe and fittings shall be protected from damage due to impact and point loading. Pipe shall be properly supported to avoid damage due to flexural strains. The contractor shall not allow dirt, debris, or other extraneous materials to get into pipe and fittings. All factory machined areas shall be protected from sunlight until installed.
2.05 Acceptable Manufacturers - NOV Fiber Glass Systems (501) 568-4010 or approved equal.

## SECTION 3 - Materials and Construction

### 3.01 30"- 48" Pipe - The pipe shall be manufactured by

 the filament winding process using a vinyl ester or epoxy thermosetting resin to impregnate strands of continuous glass filaments, which are would around a mandrel at a $543 / 4^{\circ}$ winding angle under controlled tension. Pipe shall be heat cured and the cure shall be confirmed using a Differential Scanning Calorimeter.All pipe shall have a resin-rich corrosion/abrasion resistant barrier. The minimum acceptable cured thickness of the corrosion/abrasion barrier shell be 100 mils nominal.

Pipe 30"- 48" shall be supplied plain end.
3.02 Flanges and Fittings - All fittings shall be manufactured using the same type materials as the pipe. Fittings may be manufactured either by spray-up/contact molding, contact molding/filament winding, or compression molding methods.

All fittings, except compression molded, shall have a minimum corrosion/abrasion barrier of 100 mils.

All elbows shall have a minimum radius of $11 / 2$ Diameter
Fittings shall be adhesive bonded matched tapered bell and spigot, flanged or butt and wrap.

Flanges shall have ANSI B16.5, Class 150 bolt hole patterns.
3.03 Adhesive - Adhesive shall be manufacturer's standard for the piping system specified.
3.04 Gaskets - Gaskets shall be $1 / 4$ " thick, 60-70 durometer full-fact type suitable for the service shown on the drawings and as recommended in the manufacturer's standard installation procedures.
3.05 Bolts, Nuts and Washers - ASTM A307, Grade B, hex head bolts shall be supplied. Washers shall be supplied on all nuts and bolts.
3.06 Acceptable Products - Silver Streak LD as manufactured by NOV Fiber Glass Systems or approved equal.

## SECTION 4 - Installation and Testing

4.01 Training and Certification - All joints installed or constructed in the field shall be assembled by employees of the contractor who have been trained by the pipe manufacturer. The pipe manufacturer or their authorized representative shall train the contractor's employees in the proper joining and assembly procedures required for the project, including hands-on training by the contractor's employees. Each bonder shall fabricate one pipe-to-pipe and one pipe-to-fitting joint that shall pass the minimum pressure test for the application without leaking.

Only bonders who have successfully completed the pressure test shall bond pipe and fittings.

Certification by the manufacturer shall be in compliance with ASME B31.3, Section A328.2 for the type of joint being made.
4.02 Pipe Installation - Pipe shall be installed as specified and indicated on the drawings.

The piping system shall be installed in accordance with the manufacturer's current published installation procedures.
4.03 Testing - When testing 30" and larger pipe, a steady pressure test shall be conducted on the completed piping system. The pipe shall be subjected to a steady pressure test at $11 / 2$ times the design operating pressure as shown on the drawings.

Test pressure shall not exceed $11 / 2$ times the maximum rated pressure of the lowest rated element in the system.

The system shall be filled with water at the lowest point and air bled off from the highest point. Systems shall be brought up to test pressure slowly to prevent water hammer or overpressurization.

All pipe joints shall be water tight. All joints that are found to leak by observation or during testing shall be repaired by the contractor and retested.


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## Applications

- Bottom Ash
- Zinc Tailings
- Dredge Lines
- Copper Tailings
- Wet Fly Ash
- Taconite Tailings
- Smelter Slags
- Iron Ore Tailings
- Vanadium Ore Slurries
- Heavy Salt Slurries
- Wet Process Slurries
- Diatomaceous Earth
- Potash Tailings
- Uranium Ore Slurries
- Wood Pulp Slurries
- Concrete Slurries


## Materials and Construction

Ceram Core is a fiberglass reinforced epoxy resin pipe with a special abrasion resistant liner composed of small spherical beads of high alumina ceramic, held in an epoxy matrix. Because of its unique combination of ceramic beads and epoxy resin, Ceram Core pipe also exhibits excellent corrosion resistance.

Ceram Core piping is specifically designed for the severe abrasion conditions caused by sharp angular particles in high flow streams. Most noticeable is its successful service in handling bottom ash (see Field Tests). The pipe outlasts and outperforms steel, special alloys, and other lined pipe at competitive costs and is available in $6^{\prime \prime}-16^{\prime \prime}$ diameters in standard 25 foot ( 7.6 meters lengths $\pm 1 / 8^{\prime \prime}$ ), for slurry abrasion service up to $200^{\circ} \mathrm{F}\left(93^{\circ} \mathrm{C}\right)$. The system includes $45^{\circ}$ and $90^{\circ}$ elbows with a 3 -diameter sweep radius. Special angle fittings, including laterals, are available on request.

## Fittings

Fittings are manufactured with the same chemical/temperature capabilities as the pipe. Depending on the particular part and size, fittings will be compression molded, contact molded, hand fabricated or filament wound.

## Joining System

Flanged
Flanged connections are available for all components and diameters.

View of Joint Illustrations


Flanged

## Nominal Dimensional Data

| Pipe Size |  | Outside <br> Diameter |  | Inside <br> Diameter |  | Total Wall <br> Thickness |  | Liner Thickness |  | Max. Operating Pressure |  | Max. Operating Temperature* Hydraulic Service |  | Nominal Weight |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | in | mm | in | mm | in | mm | in | mm | psig | MPa | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | lbs/ft | kg/m |
| 6 | 150 | 6.70 | 170.18 | 6.125 | 155.58 | 0.288 | 7.32 | 0.13 | 3.3 | 225 | 1.55 | 200 | 93 | 5.6 | 8.33 |
| 8 | 200 | 8.71 | 221.23 | 8.095 | 205.61 | 0.308 | 7.82 | 0.13 | 3.3 | 225 | 1.55 | 200 | 93 | 7.8 | 11.60 |
| 10 | 250 | 10.78 | 273.81 | 10.16 | 258.06 | 0.310 | 7.87 | 0.13 | 3.3 | 225 | 1.55 | 200 | 93 | 9.8 | 14.60 |
| 12 | 300 | 12.98 | 329.69 | 12.30 | 312.42 | 0.340 | 8.64 | 0.13 | 3.3 | 225 | 1.55 | 200 | 93 | 12.8 | 19.00 |
| 14 | 350 | 14.75 | 374.52 | 14.02 | 356.11 | 0.363 | 9.22 | 0.13 | 3.3 | 100 | 0.69 | 200 | 93 | 15.4 | 22.90 |
| 16 | 400 | 16.80 | 426.72 | 16.02 | 406.91 | 0.390 | 9.91 | 0.13 | 3.3 | 100 | 0.69 | 200 | 93 | 18.8 | 28.00 |

(*) Consult NOV Fiber Glass Systems concerning all pneumatic applications with Ceram Core pipe.

## Significant Field Test

An Idaho mine installed a Ceram Core test spool in a zinc slurry to compare it to Schedule 80 steel. Normal life for the steel was one month. After 21 months, the Ceram Core spool was still in service.

A Ceram Core test spool was installed in a Wisconsin taconite operation. Carbon steel in this application lasted from 6 to 12 months without rotation. After 19 months without rotation, the Ceram Core spool showed little wear.

A 10-inch diameter, 18 -foot Ceram Core test spool was installed in bottom ash service at a major power station in Georgia. Similar test spools of other types of pipe including heavy wall abrasion resistant cast iron were also installed. After 30 months handling 53,000 tons of ash, the Ceram Core test spool showed a projected continuing wear life of over 17 years versus 3 years for the metallic pipe (see graph).
 This utility since expanded Ceram Core pipe use, in 8 "-12" diameters, to more than 6 miles at five separate plants.

Abrasion Resistant Piping Systems Comparison

| Property | Ceram Core Pipe |  |  | Basalt Pipe |  |  | High Chromium Cast Iron Pipe |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 8" | 10" | 12" | 8" | 10" | 12" | 8" | 10" | 12" |
| I.D. Hardness | Brinell - Exceeds 615 MOH-9 <br> Rockwell - R45N-79 |  |  | $\mathrm{MOH}-7.8$ |  |  | Brinell-300-500 <br> Rockwell - C-34-57 |  |  |
| Flow Factor (Hazen-Williams Coefficient) | 130 |  |  | 100 |  |  | 100 |  |  |
| ${ }^{(1)}$ Weight per foot (lbs) | 7.2 | 9.8 | 12.8 | 58 | 70 | 83 | 55 | 60-70 | 75-93 |
| Standard Length (ft) | 25 |  |  | 18 |  |  | 18 |  |  |
| Weight per length of 10" pipe (lbs) | $245{ }^{(1)}$ |  |  | 1,260 |  |  | 1,170 |  |  |
| Typical fitting weight $90^{\circ}$ elbow (lbs) | 75 | 125 | 190 | 326 | 398 | 462 | 465 | 760 | 1,130 |

[^2]Labor Estimate Example (Inside Building)

| Pipe | Estimated man <br> hours/ft of pipe <br> installed | Estimated man <br> hours to install <br> $\mathbf{6 , 0 0 0}$ ft of pipe |  |
| :--- | :--- | :--- | :--- |
| 10" Ceram Core | 0.302 | 1,814 |  |
| 10" Cast Iron | 0.810 | 4,860 |  |
| 10" Basalt | 1.140 | 6,840 |  |
| Fittings | $\mathbf{9 0 ^ { \circ }}$ | $\mathbf{4 5 ^ { \circ }}$ | Laterals |
| 10" Ceram Core | 3.39 | 3.26 | 5.89 |
| 10" Cast Iron | 7.87 | 7.37 | 10.80 |
| 10" Basalt | 10.23 | 9.58 | 14.04 |

## Testing

Hydrostatic testing is recommended to evaluate the integrity of all new piping installations. CERAM CORE piping systems may be hydro tested to 1.5 times the maximum operating pressure rating. Note: The lateral fittings pressure ratings are lower than the pipe and standard fittings requiring special consideration. All other fittings match the pipe pressure ratings.

When hydro testing, open high-point vents (if used) to prevent entrapment of air in the lines as the system is slowly filled with water, then close the vents and slowly pressurize to the test pressure. Upon completion of hydro test, relieve the pressure on the system slowly, open vents and any drains to allow for complete drainage of the system.

## Water Hammer

Piping systems may be damaged by pressure surges due to water hammer. The use of soft start pumps and slow actuating valves will reduce the magnitude of surge pressures during operation and are highly recommended.

## Ceram Core Joining Methods

Proper joining procedures are extremely important to obtain the maximum service life from Ceram Core pipe.

Ceram Core pipe flanges have been designed to align and seal properly when installed as directed. Particular attention must be given to accurately align pipe I.D.'s at all joints. Proper installation prevents undercutting of the lining and protects the piping system from premature wear.

Ceram Core pipe can be installed in a new or existing systems. Since dimensions vary with the application, NOV Fiber Glass Systems will design transition fittings as needed for each installation upon receipt of necessary dimensional information.

More detailed information on proper handling and installation is available in Ceram Core Installation Manual.

Self-aligning flanges are used on Ceram Core pipe and fittings to assure the inside diameters of the liners are properly aligned.
One filament wound epoxy resin aligning ring and one Buna $a^{T M} \mathrm{~N}$ O-ring, supplied by NOV Fiber Glass Systems, is used on each joint. See Ceram Core pipe installation instructions.

Buna $a^{\text {TM }}$ is a trademark of DuPont.

## Self-Aligning Flanges

Specially designed Ceram Core flanges make it easy to properly align pipe and fittings when installing to new or existing systems.


Maximum Support Spacing for Uninsulated Pipe ${ }^{(1)}$

| Nominal Pipe Size |  | Continuous Span ${ }^{(2)}$ |  |
| :--- | :--- | :--- | :--- |
| in | $\mathbf{m m}$ | $\mathbf{f t}$ | $\mathbf{m}$ |
| 6 | 150 | 22.1 | 6.75 |
| 8 | 200 | 24.6 | 7.50 |
| 10 | 250 | 26.2 | 7.99 |
| 12 | 300 | 28.7 | 8.75 |
| 14 | 350 | 30.5 | 9.30 |
| 16 | 400 | 32.4 | 9.88 |

${ }^{(1)}$ For $\mathrm{Sg}=1.0$, consult manufacturer for heavier insulated pipe support spans. Span recommendations include no provision for weight of (fittings, valves, etc.) or thrusts at branches and turns. Heavy valves and other appurtenances must be supported separately.
${ }^{(2)}$ Calculated spans are based on $1 / 2$ " mid-span deflections to ensure good appearance and adequate drainage. Total system stresses should always be taken into account by the system design engineer when determining support spans.

Support Span vs. Specific Gravity

| Specific Gravity | 1.25 | 1.5 | 2.0 |
| :--- | :--- | :--- | :--- |
| Adjustment Factor | 0.92 | 0.85 | 0.75 |

## Transition Fittings

Transition fittings are necessary to join Ceram Core pipe to systems with different inside diameters. It is essential that inside diameters of pipe-to-pipe and pipe-to-fittings be exactly matched. Mismatched I.D.'s can cause liners to be undercut and scooped away, causing premature failure.

Two flanged transition fittings generally will be required for each application. A typical concentric reducer transition fitting is shown that will join another type of flanged system having an inside diameter "XX" to a Ceram Core system having an inside diameter "CC."

## Connection to Other Piping

Ceram Core piping


Other Piping (flanged) - Detail A


## Fittings Information

Ceram Core abrasion resistant fittings $6^{\prime \prime}$ through 16" diameters are available in a variety of configurations - $45^{\circ}$ elbows and $90^{\circ}$ elbows ${ }^{(1)}$, $45^{\circ}$ laterals, flanges and $111^{1} 4^{\circ}, 15^{\circ}, 22 \frac{1}{2} 2^{\circ}, 30^{\circ}$, and $60^{\circ}$ elbows, are standard parts. Other odd degree elbows are available on request.

All fittings have liners composed of tiles similar in composition to the alumina ceramic beads used in the liner of Ceram Core pipe. Fittings are designed to resist high turbulence and high impact.

Ceram Core fittings have thermosetting resin and fiberglass reinforcement for physical strength. Self-aligning flanges are utilized on all fittings. ${ }^{(2)}$

Ceram Core sweep elbows have a center line radius of three times the nominal diameter (see dimension R in table).

$221 / 2^{\circ}$ ELBOW

(1) $14^{\prime \prime}$ and $16^{\prime \prime}$ sweep elbows available in $45^{\circ}$ or less only
(2) See NOV Fiber Glass Systems Ceram Core Installation Manual for bolt torque recommendations.

NOTE: Elbows and flanges pressure ratings match pipe ratings. 6 " -12 " laterals pressure rating are 100 psig; $14^{\prime \prime}$ and $16^{\prime \prime}$ are 80 psig. Do not pressurize over $1^{1 / 2}$ times the maximum operating pressure during hydrotest or due to surge pressure.

General Fittings Dimensions

| Pipe Size |  |  | A | B | C | D | E | F | H | I | J | L | M | N | 0 | P | R |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 6 | 150 | in | $231 / 2$ | $12^{7 / 8}$ | $11 / 2$ | $91 / 2$ | 7/8 D-8 Holes | 11 | 18 | 9 | 3 | 15 \%/8 | $101 / 4$ | 9 | $77 / 8$ | $71 / 4$ | 18 |
|  |  | mm | 597 | 329 | 38 | 241 | 22 D-8 Holes | 279 | 457 | 229 | 76 | 404 | 262 | 230 | 200 | 184 | 457 |
| 8 | 200 | in | $301 / 2$ | 16 3/8 | $13 / 4$ | $11^{1 / 2}$ | 7/8 D-8 Holes | $131 / 2$ | 22 | 11 | 4 | $203 / 8$ | $12 \mathrm{7} / 8$ | $11^{1 / 4}$ | 9 5/8 | $87 / 8$ | 24 |
|  |  | mm | 775 | 418 | 44 | 298 | $22 \mathrm{D}-8$ Holes | 349 | 559 | 279 | 102 | 517 | 328 | 287 | 246 | 225 | 610 |
| 10 | 250 | in | $373 / 4$ | $201 / 8$ | 2 | $141 / 4$ | 1 D-12 Holes | 16 | 28 | 14 | $43 / 4$ | 25 | 15 | 13 | 11 5/8 | 10 /8 | 30 |
|  |  | mm | 959 | 513 | 51 | 362 | 25 D-12 Holes | 406 | 711 | 356 | 121 | 637 | 402 | 349 | 297 | 271 | 762 |
| 12 | 300 | in | 44 5/8 | $231 / 2$ | $21 / 4$ | 17 | $1 \mathrm{D}-12$ Holes | 19 | 30 | 16 | 5 | $293 / 8$ | $181 / 4$ | 15 | 13 | $12^{1 / 8}$ | 36 |
|  |  | mm | 1113 | 598 | 57 | 432 | 25 D-12 Holes | 483 | 813 | 406 | 127 | 747 | 465 | 402 | 340 | 310 | 914 |
| 14 | 350 | in | - | $227 / 8$ | 21/2 | $18^{3 / 4}$ | $11 / 8$ D - 12 Holes | $203 / 4$ | 36 | 18 | $31 / 8$ | - | 16 | $137 / 8$ | 11 | $95 / 8$ | 42 |
|  |  | mm | - | 581 | 64 | 476 | 29 D-12 Holes | 527 | 914 | 457 | 79 | - | 425 | 352 | 279 | 244 | 1067 |
| 16 | 400 | in | - | $271 / 8$ | $21 / 2$ | $21^{1 / 4}$ | $11 / 8$ D - 16 Holes | $231 / 4$ | 42 | 21 | $31 / 8$ | - | $201 / 8$ | 16 | 13 | 12 | 48 |
|  |  | mm | - | 689 | 64 | 540 | 29 D-16 Holes | 591 | 1067 | 533 | 79 | - | 511 | 427 | 345 | 305 | 1219 |

NOTE:
Consult NOV Fiber Glass Systems concerning all pneumatic applications with Ceram Core pipe.
Tolerances or maximum/minimum limits can be obtained from NOV Fiber Glass Systems.
For corrosion resistance data in liquid systems, refer to NOV Fiber Glass Systems Chemical Resistance Guide and use data for Green Thread ${ }^{\text {TM }}$ Product.

## Typical Mechanical Properties

| Pipe Property | $75^{\circ} \mathrm{F}$ | $24^{\circ} \mathrm{C}$ | $200^{\circ} \mathrm{F}$ | $93^{\circ} \mathrm{C}$ | Method |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | psi | MPa | psi | MPa |  |
| Axial Tensile |  |  |  |  |  |
| Ultimate Stress | 9,530 | 65.7 | 6,585 | 45.4 | ASTM D2105 |
| Modulus of Elasticity | $1.68 \times 10^{6}$ | 11,583 | $1.42 \times 10^{6}$ | 9,791 | ASTM D2105 |
| Poisson's Ratio, $v_{\text {ah }}\left(v_{\text {ha }}\right)^{(1)}$ | 0.35 (0.61) |  |  |  |  |
| Axial Compression |  |  |  |  |  |
| Ultimate Stress | 12,510 | 86.3 | 8,560 | 59.0 | ASTM D695 |
| Modulus of Elasticity | $0.677 \times 10^{6}$ | 4,668 | $0.379 \times 10^{6}$ | 2,620 | ASTM D695 |
| Beam Bending |  |  |  |  |  |
| Ultimate Stress | 20,200 | 139.3 | 15,400 | 106.2 | ASTM D2925 |
| Modulus of Elasticity (Long Term) | $2.60 \times 10^{6}$ | 17,927 | $0.72 \times 10^{6}$ | 4,964 | ASTM D2925 |
| Hydrostatic Burst |  |  |  |  |  |
| Ultimate Hoop Tensile Stress | 40,150 | 276.8 | 36,480 | 251.5 | ASTM D1599 |
| Hydrostatic Design - Hoop Tensile Stress |  |  |  |  |  |
| Static 20 Year Life LTHS - 95\% LCL | - | - | 18,203-14,689 | 125.5-101.3 | ASTM D2992-Procedure B |
| Static 50 Year Life LTHS -95\% LCL | - | - | 16,788-13,142 | 115.7-90.6 | ASTM D2992-Procedure B |
| Parallel Plate |  |  |  |  |  |
| Hoop Modulus of Elasticity | $3.02 \times 10^{6}$ | 20,820 | $-$ | - | ASTM D2412 |
| Shear Modulus | $1.36 \times 10^{6}$ | 9,343 | $1.15 \times 10^{6}$ | 7,895 | - |

## Typical Physical Properties

| Pipe Property | Value | Value | Method |
| :--- | :--- | :--- | :--- |
| Thermal Conductivity | $0.23 \mathrm{BTU} / \mathrm{hr} \cdot \mathrm{ft} \cdot{ }^{\circ} \mathrm{F}$ | $0.4 \mathrm{~W} / \mathrm{m}^{\circ} \mathrm{C}$ | ASTM D177 |
| Thermal Expansion | $8.5 \times 10^{-6} \mathrm{in} / \mathrm{in}{ }^{\circ} \mathrm{F}$ | $15.3 \times 10^{-6} \mathrm{~mm} / \mathrm{mm}{ }^{\circ} \mathrm{C}$ | ASTM D696 |
| Absolute Roughness | 0.00021 in | 0.00053 mm | - |
| Specific Gravity |  | 1.8 | ASTM D792 |
| Hazen-Williams Coefficient |  | 150 | - |
| Manning's Roughness Coefficient | 0.009 | - |  |

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## Fiber Glass Systems

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## CERAM CORE ${ }^{\oplus}$ Piping System

## Specification Guide

## SECTION 1-Scope

This section covers the use of fiberglass reinforced plastic (FRP) pipe for severe abrasion conditions caused by sharp angular particles in high flow streams services up to $210^{\circ} \mathrm{F}$ and 225 psig steady pressure.

The piping system shall be furnished and installed complete with all fittings, joining materials, supports, specials, and other necessary appurtenances.

## SECTION 2-General Conditions

2.01 Coordination - Material furnished and work performed under this section shall be coordinated with related work and equipment specified under other sections.

| Valves | Section |
| :--- | :--- |
| Supports | Section |
| Equipment | Section |

2.02 Governing Standards - Except as modified or supplemented herein, all materials and construction methods shall comply with the applicable provisions of the following specifications and be tested using the following standards:

## Standard Specifications

| ASTM <br> D2996 | Standard <br> "Fiberglass" <br> mosetting Resin) Pipe <br> (Glass-Fiber-Reinforced-Ther- |
| :--- | :--- |
| ASTM <br> D4024 | Standard Specification for Reinforced Ther- <br> mosetting Resin (RTR) Flanges |

## Standard Test Methods

| ASTM <br> D2992 | Standard Practice for Obtaining Hydrostatic <br> or Pressure Design Basis for "Fiberglass" <br> (Glass-Fiber-Reinforced-Thermosetting Res- <br> in) Pipe and Fittings |
| :--- | :--- |
| ASTM <br> D2925 | Standard Practice for Measuring Beam De- <br> flection of Reinforced Thermosetting Plastic <br> Pipe Under Full Bore Flow |
| ASTM <br> D1599 | Standard Test Method for Short-Time Hy- <br> draulic Failure Pressure of Plastic Pipe, Tub- <br> ing and Fittings |
| ASTM <br> D2105 | Standard Test method for Longitudinal Ten- <br> sile Properties of "Fiberglass" (Glass-Fiber- <br> Reinforced-Thermosetting Resin) Pipe and <br> Tube |
| ASTM <br> D2412 | Standard Test Method for Determination of <br> External Loading Characteristics of Plastic <br> Plpe by Parallel-Plate Loading |

2.03 Operating Conditions - In addition to the above listed minimum design requirements, the system shall meet the following minimum operating conditions:
a. Operating Pressure
b. Operating Temperature
c. Fluid Conveyed
d. Test Pressure
2.04 Quality Assurance - Pipe manufacturer's quality program shall be in compliance with ISO 9001.
2.05 Delivery, Storage, and Handling - Pipe and fittings shall be protected from damage due to impact and point loading. Pipe shall be properly supported to avoid damage due to flexural strains. The contractor shall not allow dirt, debris, or other extraneous materials to get into pipe and fittings. All factory machined areas shall be protected from sunlight until installed.
2.06 Acceptable Manufacturers - NOV Fiber Glass Systems, 501-568-4010, or approved equal.

## SECTION 3 - Materials and Construction

$3.01 \quad$ 6"-16" Pipe - The pipe shall be manufactured by the filament winding process using an amine cured epoxy thermosetting resin to impregnate strands of continuous glass filaments, which are wound around a mandrel at a $54^{1} / 4^{\circ}$ winding angle under controlled tension. Pipe shall be heat cured and the cure shall be confirmed using a Differential Scanning Calorimeter.

All pipe shall have a liner consisting of ceramic beads suspended in an epoxy matrix. The minimum liner thickness shall be 130 mil nominal.

Pipe shall be supplied with self-aligning flanges to assure the inside diameters of the liners are properly aligned.

Pipe shall have a continuous steady pressure rating at $200^{\circ} \mathrm{F}$ as follows $6 "-12^{\prime \prime}$ at 225 psig and $14 "-16^{\prime \prime}$ at 100 psig in accordance with ASTM D2992 Procedure B.

All pipe shall be 100\% hydrotested at the factory before shipment at a minimum pressure of 100 psig .
3.02 Flanges and Fittings - Abrasion resistant elbows shall be three diameter sweep radius and have selfaligning flanged ends. They shall be glass reinforced thermosetting resin with abrasion resistant ceramic tile liner.

Flanges shall have ANSI B16.5 Class 150 bolt hole patterns. It is recommended that a protective coating be used on the bolts to facilitate removal for rotation.
3.04 O-Ring Seals - O-Rings shall be 60-70 durometer Shore A hardness elastomeric material. O-rings for the self-aligning flanged joints will be supplied by manufacturer.
3.05 Bolts, Nuts, and Washers - ASTM A307, Grade B, hex head bolts shall be supplied. SAE washers shall be supplied on all nuts and bolts.
3.06 Acceptable Products - Ceram Core as manufactured by NOV Fiber Glass Systems, or approved equal.

## SECTION 4 - Installation and Testing

4.01 Training and Certification - All joints installed or constructed in the field shall be assembled by employees of the contractor who have been trained by the pipe manufacturer. The pipe manufacturer or their authorized representative shall train the contractor's employees in the proper joining and assembly procedures required for the project, including hands-on participation by the contractor's employees.
4.02 Pipe Installation - Pipe shall be installed as specified and indicated on the drawings.

The piping system shall be installed in accordance with the manufacturer's current published installation procedures.
4.03 Testing - A hydrostatic pressure test shall be conducted on the completed piping system. The piping system should be pressurized to $11 / 2$ times the operating design pressure, and inspected. Then the pressurization should be maintained for 1-8 hours and the line inspected for leaks.

Field test pressures are limited to $11 / 2$ times the maximum cyclic rating of the lowest rated component in the system. The maximum test pressure should not exceed 338 psig. The system shall be filled with water at the lowest point and air bled off from the highest point. Systems shall be brought up to test pressure slowly to prevent water hammer or over-pressurization.

All pipe joints shall be water tight. All joints that are found to leak by observation or during testing shall be repaired by the contractor and retested.

QUALITY MANAGEMENT SYSTEM CERTIFIED BY DNV
= ISO 9001:2008 $=$
LITTLE ROCK, AR
SAND SPRINGS, OK SUZHOU, CHINA
FIBER GLASS SYSTEMS

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## Centricast RB-1520"' Product Data

Applications

- Dilute Acids
- Solvents
- Caustics
- Salts


## Materials and Construction

All pipe is manufactured with high strength glass fabrics and a highly resilient formulation of aromatic amine cured epoxy resin. A 50-mil integral corrosion barrier of pure resin provides excellent corrosion resistance. The pipe's proprietary resin formulation provides the toughness for many corrosive slurries. A 10-mil resin-rich reinforced external corrosion barrier provides excellent corrosion resistance and protection from ultraviolet (UV) radiation. Fiber Glass Systems warrants CENTRICAST RB-1520 pipe and fittings against UV degradation of physical properties and chemical resistance for 15 years.

Pipe is available in $\mathbf{1}^{1 / 2 "}$ through 14 " diameters with pressure ratings up to 150 psig at a maximum operating temperature of $225^{\circ}$. Centricast RB-1520 comes in $20^{\prime}$ nominal or exact lengths from 18.020.4 feet long.

## Fittings

Fittings are manufactured with the same chemical/temperature capabilities as the pipe. Depending on the particular part and size, fittings will be compression molded, contact molded, hand fabricated or filament wound.

## Joining <br> Systems

## Socket Joint

Adhesive bonded straight socket joint with positive stops. This is the standard for Centricast piping systems.


## Nominal Dimensional Data

| Pipe Size <br> (In) | I.D. |  | O.D. |  | Wall <br> Thickness |  | Reinforcement Thickness |  | Weight |  | Capacity |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | (In) | (mm) | (In) | (mm) | (In) | (mm) | (In) | (mm) | (Lbs/Ft) | (kg/m) | (Gal/Ft) | (CuFt/Ft) |
| $11 / 2$ | 1.55 | 39.4 | 1.90 | 48.3 | 0.18 | 4.4 | 0.12 | 2.9 | 0.58 | 0.86 | 0.10 | 0.013 |
| 2 | 2.06 | 52.2 | 2.38 | 60.3 | 0.16 | 4.1 | 0.10 | 2.5 | 0.68 | 1.01 | 0.17 | 0.023 |
| 3 | 3.18 | 80.8 | 3.50 | 88.9 | 0.16 | 4.1 | 0.10 | 2.5 | 1.03 | 1.53 | 0.41 | 0.055 |
| 4 | 4.18 | 106.2 | 4.50 | 114.0 | 0.16 | 4.1 | 0.10 | 2.5 | 1.34 | 1.99 | 0.71 | 0.095 |
| 6 | 6.27 | 159.0 | 6.63 | 168.0 | 0.18 | 4.6 | 0.12 | 3.0 | 2.23 | 3.32 | 1.60 | 0.214 |
| 8 | 8.23 | 209.0 | 8.63 | 219.0 | 0.20 | 5.1 | 0.14 | 3.6 | 3.24 | 4.82 | 2.76 | 0.369 |
| 10 | 10.30 | 262.0 | 10.75 | 273.0 | 0.22 | 5.6 | 0.16 | 4.1 | 4.45 | 6.63 | 4.34 | 0.580 |
| 12 | 12.30 | 312.0 | 12.75 | 324.0 | 0.24 | 6.1 | 0.18 | 4.6 | 5.77 | 8.59 | 6.14 | 0.821 |
| 14 | 13.50 | 343.0 | 14.00 | 356.0 | 0.24 | 6.1 | 0.18 | 4.6 | 6.35 | 9.45 | 7.46 | 0.997 |
| Tolerances or maximum/minimum limits can be obtained from NOV Fiber Glass Systems. |  |  |  |  |  |  |  |  |  |  |  |  |


| $\begin{aligned} & \text { Size } \\ & \text { (In) } \end{aligned}$ | Reinforcement End Area ( $\mathrm{In}^{2}$ ) | Reinforcement Moment of Inertia ( $\operatorname{In}^{4}$ ) | Reinforcement Section Modulus ( $\mathrm{In}^{3}$ ) | Nominal Wall End Area ( $\mathrm{In}^{2}$ ) |
| :---: | :---: | :---: | :---: | :---: |
| 11/2 | 0.67 | 0.27 | 0.28 | 0.97 |
| 2 | 0.71 | 0.46 | 0.39 | 1.11 |
| 3 | 1.07 | 1.54 | 0.88 | 1.68 |
| 4 | 1.38 | 3.35 | 1.49 | 2.18 |
| 6 | 2.45 | 13.00 | 3.92 | 3.64 |
| 8 | 3.73 | 33.60 | 7.79 | 5.29 |
| 10 | 5.32 | 74.60 | 13.90 | 7.28 |
| 12 | 7.11 | 140.00 | 22.00 | 9.43 |
| 14 | 7.82 | 187.00 | 26.70 | 10.40 |

Average Physical Properties

| Property | $\begin{gathered} 75^{\circ} \mathrm{F} \\ \mathrm{psi} \end{gathered}$ | $\begin{aligned} & 24^{\circ} \mathrm{C} \\ & \mathrm{MPa} \end{aligned}$ | $\begin{gathered} 200^{\circ} \mathrm{F} \\ \mathrm{psi} \end{gathered}$ | $\begin{gathered} 99^{\circ} \mathrm{C} \\ \mathrm{MPa} \end{gathered}$ | $\begin{gathered} 225^{\circ}{ }^{\circ} \\ \mathrm{psi} \end{gathered}$ | $107^{\circ} \mathrm{C}$ MPa |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Axial Tensile - ASTM D2105 |  |  |  |  |  |  |
| Ultimate Stress | 30,000 | 210 | 26,000 | 180 | 25,000 | 170 |
| Design Stress | 7,500 | 52 | 6,500 | 45 | 6,250 | 43 |
| Modulus of Elasticity | $2.5 \times 10^{6}$ | 17,200 | $2.2 \times 10^{6}$ | 15,200 | $2.1 \times 10^{6}$ | 14,500 |
| Poisson's Ratio v | 0.15 |  | 0.15 |  | 0.15 |  |
| Axial Compression - ASTM D695 |  |  |  |  |  |  |
| Ultimate Stress | 35,000 | 240 | 28,000 | 190 | 17,000 | 110 |
| Design Stress | 8,750 | 60 | 7,000 | 48 | 4,250 | 29 |
| Modulus of Elasticity | $3.2 \times 10^{6}$ | 22,000 | $2.8 \times 10^{6}$ | 19,300 | $2.7 \times 10^{6}$ | 18,600 |
| Beam Bending - ASTM D2925 |  |  |  |  |  |  |
| Ultimate Stress | 40,000 | 280 | 35,000 | 240 | 33,000 | 230 |
| Design Stress ${ }^{(1)}$ | 5,000 | 34 | 4,375 | 30 | 4,125 | 28 |
| Modulus of Elasticity (Long Term) | $3.7 \times 10^{6}$ | 26,000 | $3.2 \times 10^{6}$ | 22,000 | $3.1 \times 10^{6}$ | 21,000 |
| Hydrostatic Burst - ASTM D1599 |  |  |  |  |  |  |
| Ultimate Hoop Tensile Stress | 30,000 | 210 | 26,000 | 180 | 25,000 | 170 |
| Hoop Tensile Modulus of Elasticity | $2.4 \times 10^{6}$ | 17,000 | $2.1 \times 10^{6}$ | 14,500 | $2.0 \times 10^{6}$ | 13,800 |
| Hydrostatic Design - ASTM D2992, Procedure B - Hoop Tensile Stress Static 50 Year @ $75^{\circ} \mathrm{F}$ | 19,270 | 130 | - | - | - | - |


| Coefficient of Linear Thermal Expansion - ASTM D696 | Non-Insulated Pipe: $9.6 \times 10^{-6} \mathrm{in} / \mathrm{in} /{ }^{\circ} \mathrm{F} \cdot 17.4 \times 10^{-6} \mathrm{~mm} / \mathrm{mm} /{ }^{\circ} \mathrm{C}$ <br> Insulated Pipe: $\quad 13.0 \times 10^{-6} \mathrm{in} / \mathrm{in} /{ }^{\circ} \mathrm{F} \cdot 23.5 \times 10^{-6} \mathrm{~mm} / \mathrm{mm} /{ }^{\circ} \mathrm{C}$ |
| :---: | :---: |
| Thermal Conductivity | $0.07 \mathrm{BTU} /-\mathrm{hr}-\mathrm{ft}-{ }^{\circ} \mathrm{F} \cdot 0.04 \mathrm{~W} /-\mathrm{m}-{ }^{\circ} \mathrm{C}$ |
| Specific Gravity - ASTM D792 | 1.41 |
| Flow Factor - SF / Hazen-Williams Coefficient | 150 |
| Absolute Surface Roughness | 0.00021 Inch • 0.0053 mm |
| Manning's Roughness Coefficient, n | 0.009 |

## Testing:

See NOV Flber Glass Systems' Socket Joint Installation Handbook.

When possible, the piping system should be hydrostatically tested prior to beginning service. Care should be taken when testing to avoid water hammer. All anchors, guides and supports must be in place prior to testing the line.

Test pressure should not be more than $11 / 2$ times the working pressure of the piping system and never exceed $11 / 2$ times the rated operating pressure of the lowest rated component in the system.

## Water Hammer:

Care should be taken when designing an FRP piping system to eliminate sudden surges. Soft start pumps and slow actuating valves should considered.

| Pressure Ratings for Uninsulated Piping Systems ${ }^{(1)(2)}$ |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Maximum Internal Pressure <br> @ $225^{\circ} \mathrm{F}$ (psig) |  |  | Maximum <br> External Pressure ${ }^{(6)}$ |  |  |
| Pipe Size <br> (In) | Socket Pressure Fittings ${ }^{(3)}$ | Flanged Pressure Fittings ${ }^{(4)}$ | Other Pressure Fittings ${ }^{(5)}$ | $75^{\circ} \mathrm{F}$ | $150^{\circ} \mathrm{F}$ | $225{ }^{\circ} \mathrm{F}$ |
| $11 / 2$ | 300 | 150 | NA | 920 | 753 | 649 |
| 2 | 300 | 150 | 125 | 290 | 231 | 199 |
| 3 | 275 | 150 | 125 | 103 | 104 | 90 |
| 4 | 150 | 150 | 100 | 47 | 37 | 32 |
| 6 | 150 | 150 | 100 | 22 | 18 | 16 |
| 8 | 150 | 150 | 100 | 19 | 12 | 11 |
| 10 | 150 | 150 | 75 | 12 | 10 | 8 |
| 12 | 150 | 150 | 75 | 7 | 6 | 5 |
| 14 | 125 | 150 | - | 7 | 6 | 5 |

ASTM D2997
Designation Codes

| $1 \frac{1}{2 \prime} 2^{\prime}-4 "$ | RTRP-21CW-4556 |
| :---: | :---: |
| $6 "$ | RTRP-21CW-4555 |
| $8 "$ | RTRP-21CW-4554 |
| $10 "-12 "$ | RTRP-21CW-4553 |
| $14 "$ | RTRP-21CW-4552 |

(1) Static pressure ratings, typically created with use of a gear pump, turbine pump, centrifugal pump, or multiplex pump having 4 or more pistons or elevation head.
(2) For insulated and/or heat traced piping systems, use $100 \%$ of the uninsulated piping recommendations up to $200^{\circ} \mathrm{F}$ and reduce these ratings $50 \%$ for $200^{\circ} \mathrm{F}$ to $225^{\circ} \mathrm{F}$ operating temperatures. Centricast RB-1520 pipe and epoxy fittings can be used in drainage and vent systems up to $250^{\circ} \mathrm{F}$ operating temperatures. For compressible gasses consult the factory for pressure ratings. Heat cured adhesive joints are highly recommended for all piping systems carrying fluids at temperatures above $120^{\circ} \mathrm{F}$.
(3) Socket elbows, tees, reducers, couplings, flanges and nipples joined with WELDFAST ZC275 adhesive. (4) Flanged elbows, tees, reducers, couplings and nipples assembled at factory.
(5) Laterals, crosses, and saddles.
(6) Ratings shown are $50 \%$ of ultimate; 14.7 psi external pressure is equal to full vacuum.

Recommended Operating Ratings

| Size <br> (In) | Axial Tensile Loads Max. (Lbs) |  | Axial Compressive Loads Max. (Lbs) ${ }^{(1)}$ |  | Bending Radius Min. <br> (Ft) Entire Temp. Range | Torque Max. (Ft Lbs) Entire Temp. Range | Parallel Plate Loading ASTM D2412 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{aligned} & \text { Temp } \\ & \text { @ } 75^{\circ} \mathrm{F} \end{aligned}$ | rature <br> @ $225^{\circ} \mathrm{F}$ | Tem <br> @ $75^{\circ}$ F | perature <br> @ $225^{\circ} \mathrm{F}$ |  |  | Stiffiness Factor $\operatorname{In}^{3}$ Lbs/In ${ }^{2}$ | Pipe Stiffness (psi) | Hoop Modulus $\times 10^{6}$ (psi) |
| $11 / 2$ | 5,000 | 4,100 | 5,800 | 2,800 | 59 | 113 | 279 | 2,632 | 2.2 |
| 2 | 5,400 | 4,500 | 6.300 | 3,000 | 73 | 163 | 317 | 1,444 | 3.8 |
| 3 | 8,000 | 6,700 | 9,300 | 4,500 | 108 | 368 | 317 | 433 | 3.8 |
| 4 | 10,400 | 8,600 | 12,100 | 5,900 | 139 | 620 | 317 | 200 | 3.8 |
| 6 | 18,400 | 15,300 | 21,500 | 10,400 | 204 | 1,632 | 547 | 107 | 3.8 |
| 8 | 28,000 | 23,300 | 32,700 | 15,900 | 266 | 3,246 | 709 | 62 | 3.1 |
| 10 | 39,900 | 33,300 | 46,600 | 22,600 | 331 | 5,786 | 1,195 | 54 | 3.5 |
| 12 | 53,300 | 44,400 | 62,200 | 30,200 | 393 | 9,178 | 1,701 | 46 | 3.5 |
| 14 | 58,600 | 48,800 | 68,400 | 33,200 | 432 | 11,108 | 1,701 | 35 | 3.5 |

${ }^{(1)}$ Compressive loads are for short columns only. Buckling loads must be calculated when applicable.

## Support

Proper pipe support spacing depends on the temperature and weight of the fluid in the pipe. The support spacing table is based on unrestrained continuous beam theory using the pipe bending modulus derived from long-term beam bending tests. The maximum spans lengths were developed to ensure a design that limits mid-span deflection to $1 / 2$ inch and dead weight bending to $1 / 8$ of the ultimate bending stress. Any additional loads on the piping system such as insulation, wind, seismic, etc. requires further consideration. Restrained (anchored) piping systems operating at elevated temperatures may result in guide spacing requirements that are shorter than unrestrained piping systems. In this case, the maximum guide spacing governs the support span requirements for the system. Pipe spans near elbows require special attention. Both supported and unsupported elbows are considered in the following tables and must be followed to properly design the piping system.

There are seven basic rules to follow when designing piping system supports:

1. Do not exceed the recommended support span.
2. Support heavy valves and in-line equipment independently.
3. Protect pipe from external abrasion at supports.
4. Avoid point contact loads.
5. Avoid excessive bending. This applies to handling, transporting, initial layout, and final installed position.
6. Avoid excessive vertical loading to minimize bending stress on pipe and fittings.
7. Provide adequate axial and lateral restraint to ensure line stability during rapid changes in flow.

| Maximum Support Spacing for Uninsulated Pipe ${ }{ }^{11}$ |  |  |  |
| :---: | :---: | :---: | :---: |
| Pipe Size <br> (In.) | Continuous Spans of Pipe (Ft.) ${ }^{(2)}$ |  |  |
|  | $75^{\circ} \mathrm{F}$ | $150^{\circ} \mathrm{F}$ | $225^{\circ} \mathrm{F}$ |
| 1112 | 16.6 | 16.0 | 15.9 |
| 2 | 17.3 | 16.7 | 16.6 |
| 3 | 19.4 | 18.7 | 18.6 |
| 4 | 20.9 | 20.1 | 20.0 |
| 6 | 24.2 | 23.3 | 23.2 |
| 8 | 26.9 | 26.0 | 25.8 |
| 10 | 29.5 | 28.4 | 28.2 |
| 12 | 31.7 | 30.6 | 30.4 |
| 14 | 32.5 | 31.4 | 31.4 |
| ${ }^{(1)}$ Consult factory for insulated pipe support spacing. <br> ${ }^{(2)}$ Maximum mid-span deflection $1 / 2^{\prime \prime}$ with a specific gravity of 1.0 . |  |  |  |

## Support Spacing vs. Specific Gravity

| Specific Gravity | 3.00 | 2.00 | 1.50 | 1.25 | 1.00 | 0.75 | Gas/Air |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Multiplier | 0.76 | 0.84 | 0.90 | 0.95 | 1.00 | 1.07 | 1.40 |

Example: $6^{\prime \prime}$ pipe @ $150^{\circ}$ F with 1.5 specific gravity fluid,maximum support spacing $=23.9 \times 0.90=21.5 \mathrm{ft}$.

## Piping Span Adjustment Factors With Unsupported Fitting at Change in Direction

## Piping Span Adjustment Factors With Supported Fitting at Change in Direction

|  | Span Type | Factor |
| :---: | :---: | :---: |
| a | Continuous interior or fixed end spans | 1.00 |
| b | Second span from simple supported end or unsupported fitting | 0.80 |
| $c+d$ | Sum of unsupported spans at fitting | $\leq 0.75$ * |
| e | Simple supported end span | 0.67 |
| * For example: If continuous support span is $10 \mathrm{ft} ., \mathrm{c}+\mathrm{d}$ must not exceed 7.5 ft . (c $=3 \mathrm{ft}$. and $d=4.5 \mathrm{ft}$. would satisfy this condition). |  |  |

Span Type
Span at supported fitting or span adjacent to a
simple supported end
Simple supported end span

## Thermal Expansion

The effects of thermal gradients on piping systems may be significant and should be considered in every piping system stress analysis. Pipe line movements due to thermal expansion or contraction may cause high stresses or even buckle a pipe line if improperly restrained. Several piping system designs are used to manage thermal expansion and contraction in above ground piping systems. They are listed below according to economic preference:

1. Use of inherent flexibility in directional changes
2. Restraining axial movements and guiding to prevent buckling
3. Use expansion loops to absorb thermal movements
4. Use mechanical expansion joints to absorb thermal movements

To perform a thermal analysis the following information is required:

1. Isometric layout of piping system
2. Physical and material properties of pipe
3. Design temperatures
4. Installation temperature (final tie-in temperature)
5. Terminal equipment load limits
6. Support movements

A comprehensive review of temperature effects on fiberglass pipe may be found in Fiber Glass Systems' Engineering and Piping Design Guide.

| Change in <br> Temperature <br> ${ }^{\circ} \mathrm{F}$ | Pipe Change <br> In Length <br> (In/100 Ft) |
| :---: | :---: |
| 25 | 0.29 |
| 50 | 0.58 |
| 75 | 0.86 |
| 100 | 1.15 |
| 125 | 1.44 |
| 150 | 1.73 |
| 175 | 2.02 |
| 200 | 2.30 |

Restrained Thermal End Loads and Guide Spacing

| Size <br> (In) | Operating Temperature ${ }^{\circ} \mathrm{F}$ (Based on Installation Temperature of $75^{\circ} \mathrm{F}$ ) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 125 |  | 150 |  | 175 |  | 200 |  | 225 |  |
|  | Guide Spacing (Ft) | Thermal End Load (Lbs) | Guide Spacing (Ft) | Thermal End Load (Lbs) | Guide Spacing (Ft) | Thermal End Load (Lbs) | Guide Spacing (Ft) | Thermal End Load (Lbs) | Guide Spacing (Ft) | Thermal End Loads (Lbs) |
| 11/2 | 8.2 | 982 | 6.6 | 1,440 | 5.6 | 1,862 | 4.9 | 2,255 | 4.4 | 2,609 |
| 2 | 10.5 | 1,046 | 8.4 | 1,533 | 7.1 | 1,983 | 6.2 | 2,401 | 5.6 | 2,779 |
| 3 | 15.6 | 1,564 | 12.6 | 2,292 | 10.6 | 2,963 | 9.3 | 3,589 | 8.4 | 4,153 |
| 4 | 20.2 | 2,024 | 16.3 | 2,966 | 13.8 | 3,835 | 12.0 | 4,645 | 10.8 | 5,374 |
| 6 | 29.9 | 3,590 | 24.0 | 5,262 | 20.4 | 6,804 | 17.8 | 8,240 | 16.0 | 9,535 |
| 8 | 39.0 | 5,463 | 31.4 | 8,007 | 26.6 | 10,354 | 23.2 | 12,539 | 20.9 | 14,510 |
| 10 | 48.6 | 7,793 | 39.1 | 11,421 | 33.2 | 14,768 | 29.0 | 17,886 | 26.0 | 20,696 |
| 12 | 57.7 | 10,406 | 46.5 | 15,251 | 39.4 | 19,721 | 34.4 | 23,883 | 30.9 | 27,637 |
| 14 | 63.4 | 11,441 | 51.1 | 16,768 | 43.3 | 21,682 | 37.8 | 26,528 | 34.0 | 30,385 |


| Elbow Strength |  |  |  |
| :---: | :---: | :---: | :---: |
| Allowable Bending Moment 90 ${ }^{\circ}$ Elbow |  |  |  |
| Nominal <br> Pipe Size <br> $(\mathrm{In})$ | Allowable <br> Moment <br> $(\mathrm{Ft} \bullet \mathrm{Lbs})$ | Nominal <br> Pipe Size <br> $(\mathrm{In})$ | Allowable <br> Moment <br> $(\mathrm{Ft} \bullet \mathrm{Lbs})$ |
| $11 / 2$ | 150 | 8 | 2,850 |
| 2 | 225 | 10 | 4,500 |
| 3 | 475 | 12 | 6,500 |
| 4 | 650 | 14 | 10,000 |
| 6 | 1,650 |  |  |



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## CENTRICAST"' RB-1520 Piping System

## General Specifications

## SECTION 1 - Scope

This section covers the use of fiberglass reinforced plastic (FRP) pipe for chemical process and chemical handling applications up to $250^{\circ} \mathrm{F}$ and up to 150 psig pressure.

The piping shall be furnished and installed complete with all fittings, joining materials, supports, specials, and other necessary appurtenances.

## SECTION 2 - General Conditions

2.01 Coordination - Material furnished and work performed under this section shall be coordinated with related work and equipment specified under other sections.

| Valves | Section |
| :--- | :--- |
| Supports | Section |
| Equipment | Section |

2.02 Governing Standards - Except as modified or supplemented herein, all materials and construction methods shall comply with the applicable provisions of the following specifications and be tested using the following standards:

## Standard Specifications

| ASTM <br> D2997 | Standard Specification for Centrifugal Cast <br> "Fiberglass" (Glass-Fiber-Reinforced Thermosetting) <br> Resin Pipe |
| :--- | :--- |
| AWWA <br> 45 | Fiberglass Pipe Design |
| ASTM <br> D5685 | Standard Specification for "Fiberglass" (Glass- <br> Fiber-Reinforced-Thermosetting Resin) Pressure <br> Pipe Fittings |
| ASTM <br> D4024 | Standard Specification for Reinforced Thermo- <br> setting Resin (RTR) Flanges |

## Standard Test Methods

| ASTM <br> D2992 | Standard Practice for Obtaining Hydrostatic or <br> Pressure Design Basis for "Fiberglass" (Glass-Fiber- <br> Reinforced Thermosetting Resin) Pipe |
| :--- | :--- |
| ASTM <br> D1599 | Standard Test method for Short-Time Hydraulic <br> Failure Pressure of Plastic Pipe, Tubing and <br> Fittings |
| ASTM <br> D2105 | Standard Test Method for Longitudinal Tensile <br> Properties of "Fiberglass"" (Glass-Fiber-Reinforced <br> Thermosetting Resin) Pipe and Tube |
| ASTM <br> D2412 | Standard Test Method for Determination of Ex- <br> ternal Loading Characteristics of Plastic Pipe by <br> Parallel-Plate Loading |
| ASME <br> B31.3 | Process Piping |


| 2.03 | ASTM D2997 Designation Codes |  |
| :---: | :---: | :---: |
|  | $11 / 2 "-4 "$ | RTRP-21CW-4556 |
|  | $6 "$ | RTRP-21CW-4555 |
|  | 8 " | RTRP-21CW-4554 |
|  | 10"-12" | RTRP-21CW-4553 |
|  | 14" | RTRP-21CW-4552 |

Mechanical properties cell classifications shown are minimums.
2.04 Operating Conditions- In addition to the above minimum design requirements, the system shall meet the following minimum operating conditions:
a. Operating Pressure
b. Operating Temperature
c. Fluid Conveyed
d. Test Pressure
2.05 Quality Assurance - Pipe manufacturer's quality program shall be in compliance with ISO 9001.
2.06 Delivery, Storage and Handling - Pipe and fittings shall be protected from damage due to impact and point loading. Pipe shall be properly supported to avoid damage due to flexural strains. The contractor shall not allow dirt, debris, or other extraneous materials to get into pipe and fittings. All factory machined areas shall be protected from sunlight until installed.
2.07 Acceptable Manufacturers - NOV Fiber Glass Systems -918-245-6651 or approved equal.

## SECTION 3 - Materials and Construction

$3.01 \quad 11 / 2 "-14$ " Pipe The pipe shall be manufactured by the centrifugal casting process using premium grade amine cured epoxy thermosetting resin to impregnate woven glass filaments. Pipe shall be heat cured and the degree of cure shall be confirmed using a Differential Scanning Calorimeter. All pipe shall have a $100 \%$ resin corrosion barrier and the cured thickness shall be 50 mils nominal.

All pipe shall have a resin-rich reinforced 10 mil nominal exterior layer.

The pipe shall have a minimum design pressure rating of 150 psig at $225^{\circ} \mathrm{F}$ following ASTM D2992, Procedure B.

\author{

Minimum Reinforced Wall Thickness <br> | $11 / 2 "$ | 0.120 inches |
| :--- | :--- |
| $2 "-4 "$ | 0.100 inches |
| $6 "$ | 0.120 inches |
| $8 "$ | 0.140 inches |
| $10 "$ | 0.160 inches |
| $12 "-14 "$ | 0.180 inches |

}
3.02 Flanges and Fittings - All fittings shall be manufactured either by compression molding or contact molding. Fitting joints shall be either adhesive bonded socket or flanged. Flanges shall have ANSI B16.5 Class 150 bolt hold patterns.
3.03 Adhesive - Adhesive shall be manufacturer's standard for the piping system specified. All adhesive bonded joints shall be cured according to the manufacturer's instructions for maximum strength and corrosion resistance.
3.04 Gaskets - Gaskets shall be 3/16" thick, 60-70 durometer full-face type suitable for the service shown on the drawings and as recommended in the manufacturer's standard installation procedures.
3.05 Bolts, Nuts and Washers - ASTM F593, 304 stainless steel hex head bolts shall be supplied. Two each SAE size washers shall be supplied on all nuts and bolts.
3.06 Acceptable Products Centricast RB-1520 as manufactured by NOV Fiber Glass Systems or approved equal.

## SECTION 4 - Installation and Testing

4.01 Training and Certification - All joints installed or constructed in the field shall be assembled by employees of the contractor who have been trained by the pipe manufacturer. The pipe manufacturer or their authorized representative shall train the contractor's employees in the proper joining and assembly procedures required for the project, including hands-on participation by the contractor's employees. Each bonder shall fabricate one pipe-to-pipe and one pipe-to-fitting joint that shall pass the minimum pressure test for the application as stated in Section 2.04.d without leaking.

Only bonders who have successfully completed the pressure test shall bond pipe and fittings.

Certification by the manufacturer shall be in compliance with ASME B31.3, Section A328.2.
4.02 Pipe Installation Pipe shall be installed as specified and indicated on the drawings and in accordance with the manufacturer's current published installation procedures.
4.03 Testing - A hydrostatic pressure test shall be conducted on the completed piping system. The piping shall be subjected to a steady pressure at $11 / 2$ times the design operating pressure as stated in Section 2.04d. The pressure shall be held on the system for a minimum of one hour and the line inspected for leaks.

The test pressure should not exceed $11 / 2$ times the maximum rated operating pressure for the lowest rated element in the system.

The system shall be filled with water at the lowest point and air bled off from all the highest points. Systems shall be brought up to test pressure slowly to prevent water hammer or over pressurization.

All pipe joints shall be water tight. All joints that are found to leak by observation or during testing shall be repaired by the contractor and retested.

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## Centricast ${ }^{\circledR}$ RB-2530 Product Data

Applications

- Acids - Solvents
- Caustics
- Salts
- Chemical Process Solutions

Materials and Construction

All pipe is manufactured with glass fabrics and a highly resilient formulation of aromatic amine cured epoxy resin. A 100 mil integral corrosion barrier of pure resin provides excellent corrosion resistance. The pipe's proprietary resin formulation provides the toughness for many corrosive slurries. A 10 mil resin-rich reinforced external corrosion barrier proves excellent corrosion resistance and protection from ultraviolet (UV) radiation. Fiber Glass Systems warrants CENTRICAST RB-2530 pipe and fittings against UV degradation of physical properties and chemical resistance for 15 years.

Pipe is available in 1" through 14" diameters with pressure ratings up to 150 psig, with higher pressure ratings in smaller sizes. Centricast RB-2530 comes in 20' nominal or exact lengths from 18.0-20.4 feet long.

Fittings
Fittings are manufactured with the same chemical/temperature capabilities as the pipe. Depending on the particular part and size, fittings will be compression molded, contact molded, hand fabricated or filament wound.

## Joining Systems

## Socket Joint

Adhesive bonded straight socket joint with positive stops. This is the standard for Centricast piping systems.


| Nominal Dimensional Data |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Pipe Size <br> (In) | I.D. |  | O.D. |  | Wall <br> Thickness |  | Reinforcement Thickness |  | Weight |  | Capacity |  |
|  | (In) | (mm) | (ln) | (mm) | (In) | (mm) | (In) | (mm) | (Lbs/Ft) | (kg/m) | (Gal/Ft) | ( $\mathrm{F} \mathrm{t}^{3} / \mathrm{Ft}$ ) |
| 1 | 0.92 | 23.2 | 1.315 | 33.4 | 0.20 | 5.1 | 0.09 | 2.3 | 0.45 | 0.66 | 0.03 | 0.005 |
| $11 / 2$ | 1.40 | 35.6 | 1.900 | 48.3 | 0.25 | 6.4 | 0.14 | 3.6 | 0.82 | 1.23 | 0.08 | 0.011 |
| 2 | 1.88 | 47.6 | 2.375 | 60.3 | 0.25 | 6.4 | 0.14 | 3.6 | 1.06 | 1.58 | 0.14 | 0.019 |
| 3 | 3.00 | 76.2 | 3.500 | 88.9 | 0.25 | 6.4 | 0.14 | 3.6 | 1.62 | 2.42 | 0.37 | 0.049 |
| 4 | 3.94 | 100.1 | 4.500 | 114.0 | 0.28 | 7.1 | 0.17 | 4.3 | 2.36 | 3.51 | 0.63 | 0.085 |
| 6 | 6.07 | 154.0 | 6.625 | 168.0 | 0.28 | 7.1 | 0.17 | 4.3 | 3.55 | 5.28 | 1.50 | 0.201 |
| 8 | 8.03 | 204.0 | 8.625 | 219.0 | 0.30 | 7.6 | 0.19 | 4.8 | 4.99 | 7.43 | 2.63 | 0.351 |
| 10 | 10.10 | 256.0 | 10.750 | 273.0 | 0.33 | 8.4 | 0.22 | 5.6 | 6.87 | 10.2 | 4.15 | 0.555 |
| 12 | 12.10 | 307.0 | 12.750 | 324.0 | 0.33 | 8.4 | 0.22 | 5.6 | 8.19 | 12.2 | 5.96 | 0.797 |
| 14 | 13.30 | 339.0 | 14.000 | 356.0 | 0.33 | 8.4 | 0.22 | 5.6 | 9.01 | 13.4 | 7.26 | 0.971 |
| Tolerances or maximum/minimum limits can be obtained from NOV Fiber Glass Systems. |  |  |  |  |  |  |  |  |  |  |  |  |


| Properties of Pipe Sections Based on Minimum Reinforced Walls |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Size <br> (In) | Reinforcement <br> End Area( $\left(\mathbf{n}^{2}\right)$ | Reinforcement <br> Moment of Inertia $\left(\mathbf{I n}^{4}\right)$ | Reinforcement <br> Section Modulus $\left(\mathbf{I n}^{3}\right)$ | Nominal Wall <br> End Area $\left(\mathbf{I n}^{2}\right)$ |
| 1 | 0.35 | 0.07 | 0.10 | 0.70 |
| $11 / 2$ | 0.77 | 0.30 | 0.32 | 1.30 |
| 2 | 0.98 | 0.62 | 0.52 | 1.67 |
| 3 | 1.48 | 2.09 | 1.19 | 2.55 |
| 4 | 2.31 | 5.43 | 2.41 | 3.71 |
| 6 | 3.45 | 18.00 | 5.42 | 5.58 |
| 8 | 5.03 | 44.80 | 10.40 | 7.85 |
| 10 | 7.28 | 101.00 | 18.80 | 10.80 |
| 12 | 8.66 | 170.00 | 26.70 | 12.90 |
| 14 | 9.52 | 226.00 | 32.30 | 14.20 |

## Average Physical Properties

| Property | $\begin{gathered} 75^{\circ} \mathrm{F} / 24^{\circ} \mathrm{C} \\ 1^{\prime \prime} \end{gathered}$ |  | $\begin{gathered} 75^{\circ} \mathrm{F} / 24^{\circ} \mathrm{C} \\ 11 / 2^{\prime \prime}-14^{\prime \prime} \end{gathered}$ |  | $\begin{gathered} 225^{\circ} \mathrm{F} / 107^{\circ} \mathrm{C} \\ 1^{\prime \prime} \end{gathered}$ |  | $\begin{gathered} 225^{\circ} \mathrm{F} / 107^{\circ} \mathrm{C} \\ 11 / 2^{\prime \prime}-14^{\prime \prime} \end{gathered}$ |  | $\begin{gathered} 250^{\circ} \mathrm{F} / 121^{\circ} \mathrm{C} \\ 1 " \end{gathered}$ |  | $\begin{gathered} 250^{\circ} \mathrm{F} / 121^{\circ} \mathrm{C} \\ 11 / 2^{\prime \prime}-14^{\prime \prime} \end{gathered}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | psi | MPa | psi | MPa | psi | MPa | psi | MPa | psi | MPa | psi | MPa |
| Axial Tensile - ASTM D2105 |  |  |  |  |  |  |  |  |  |  |  |  |
| Ultimate Stress | 18,000 | 120 | 22,000 | 150 | 15,000 | 100 | 18,000 | 120 | 14,000 | 100 | 17,000 | 110 |
| Design Stress | 4,500 | 31 | 5,500 | 38 | 3,750 | 26 | 4,500 | 31 | 3.500 | 24 | 4,250 | 29 |
| Modulus of Elasticity | - | - | $2.5 \times 10^{6}$ | 17,000 | - | - | $2.1 \times 10^{6}$ | 14,000 | - | - | $1.9 \times 10^{6}$ | 13,000 |
| Poisson's Ratio $V$ |  |  |  |  |  |  | 15 |  |  |  | 15 |  |
| Axial Compression - ASTM D695 |  |  |  |  |  |  |  |  |  |  |  |  |
| Ultimate Stress | 19,600 | 140 | 35,000 | 240 | 10,000 | 70 | 19,000 | 130 | 7.000 | 50 | 13,000 | 90 |
| Design Stress | $4,900$ | 34 | 8,750 | $60$ | $2,500$ | 17 | $4,750$ | $33$ | $1,750$ | $12$ | $3,250$ | $22$ |
| Modulus of Elasticity | $1.3 \times 10^{6}$ | 9,000 | $2.5 \times 10^{6}$ | 17,000 | $1.1 \times 10^{6}$ | 8,000 | $2.1 \times 10^{6}$ | 14,000 | $1.0 \times 0^{6}$ | 7,000 | $1.9 \times 10^{6}$ | 13,000 |
| Beam Bending - ASTM D2925 |  |  |  |  |  |  |  |  |  |  |  |  |
| Ultimate Stress | 28,000 | 190 | 42,000 | 290 | 23,000 | 160 | 35,000 | 240 | 21,000 | 140 | 32,000 | 220 |
| Design Stress ${ }^{(1)}$ | 3,500 | 24 | 5,250 | 36 | 2,875 | 20 | 4,375 | 30 | 2,625 | 18 | 4,000 | 28 |
| Modulus of Elasticity (Long Term) | $5.6 \times 10^{6}$ | 4,000 | $3.7 \times 10^{6}$ | 26,000 | $4.7 \times 10^{6}$ | 3,200 | $3.1 \times 10^{6}$ | 21,000 | $4.4 \times 10^{6}$ | 3,000 | $2.9 \times 10^{6}$ | 20,000 |
| Hydrostatic Burst - ASTM D1599 |  |  |  |  |  |  |  |  |  |  |  |  |
| Ultimate Hoop Tensile Stress | 30,000 | 210 | 30,000 | 210 | 25,000 | 170 | 25,000 | 170 | 23,000 | 160 | 23,000 | 160 |
| Hoop Tensile Modulus of Elasticity | - | - | $2.8 \times 10^{6}$ | 19,000 | - | - | $2.3 \times 10^{6}$ | 16,000 | - | - | $2.2 \times 10^{6}$ | 15,000 |

## Hydrostatic Design - ASTM

D2992,
$\begin{array}{lllll}\text { Procedure B-Hoop Tensile Stress } & 16,090 & 110 & 16,090 & 110\end{array}$
Static 50 Year @ $75^{\circ} \mathrm{F}$
${ }^{(1)}$ Stress and modulus values can be interpolated between temperatures shown.

| Thermal Expansion Coefficient - ASTM D696 | Non-Insulated Pipe: Insulated Pipe: | $\begin{aligned} & \hline 11.0 \times 10^{-6} \\ & 12.0 \times 10^{-6} \end{aligned}$ | $\begin{aligned} & \mathrm{In} / \mathrm{In} / /{ }^{\circ} \mathrm{F} \cdot 19.9 \times 10^{6} \mathrm{~mm} / \mathrm{mm} /{ }^{\circ} \mathrm{C} \\ & \mathrm{In} / \mathrm{ln} /{ }^{\circ} \mathrm{F} \cdot 21.7 \times 10^{6} \mathrm{~mm} / \mathrm{mm} /{ }^{\circ} \mathrm{C} \end{aligned}$ |  |
| :---: | :---: | :---: | :---: | :---: |
| Thermal Conductivity | 0.07 BTU/hr-ft- ${ }^{\circ}$ |  |  | $0.4 \mathrm{~W} / \mathrm{m}-{ }^{\circ} \mathrm{C}$ |
| Specific Gravity - ASTM D792 | 1.47 |  |  |  |
| Hazen-Williams Coefficient | 150 |  |  |  |
| Absolute Surface Roughness | 0.00021 Inch |  |  | 0.0053 mm |
| Manning's Roughness Coefficient, n | 0.009 |  |  |  |

## Testing:

See NOV Fiber Glass Systems' Socket Joint Installation Handbook.

When possible, the piping system should be hydrostatically tested prior to beginning service. Care should be taken when testing to avoid water hammer. All anchors, guides and supports must be in place prior to testing the line.

Test pressure should not be more than $11 / 2$ times the working pressure of the piping system and never exceed $11 / 2$ times the rated operating pressure of the lowest rated component in the system.

| Pressure Ratings for Uninsulated Piping Systems ${ }^{(1)(2)}$ |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Nominal | Maximum InternalPressure @ $225^{\circ} \mathrm{F}$ (psig) |  |  | Maximum External Pressure (psig) ${ }^{(6)}$ |  |  |
| Pipe Size (In) | Socket Pressure Fittings ${ }^{(3)}$ | Flanged Pressure Fittings ${ }^{(4)}$ | Other Pressure ${ }^{(5)}$ | $75^{\circ} \mathrm{F}$ | $150^{\circ} \mathrm{F}$ | $250{ }^{\circ} \mathrm{F}$ |
| 1 | 300 | 300 | - | 2,125 | 1,849 | 1,381 |
| $11 / 2$ | 300 | 300 | - | 2,065 | 1,797 | 1,342 |
| 2 | 300 | 150 | 125 | 1,170 | 1,014 | 763 |
| 3 | 275 | 150 | 125 | 335 | 290 | 219 |
| 4 | 150 | 150 | 100 | 225 | 195 | 147 |
| 6 | 150 | 150 | 100 | 62 | 54 | 40 |
| 8 | 150 | 150 | 100 | 45 | 39 | 29 |
| 10 | 150 | 150 | 75 | 35 | 30 | 23 |
| 12 | 150 | 150 | 75 | 23 | 20 | 15 |
| 14 | 125 | 150 | - | 16 | 14 | 10 |

ASTM D2997
Designation Codes:

| $1 "$ | RTRP-21CW-4356 |
| :---: | :---: |
| $11 / 2 "-4 "$ | RTRP-21CW-4456 |
| $6 "-8 "$ | RTRP-21CW-4455 |
| $10 "-12^{\prime \prime}$ | RTRP-21CW-4454 |
| $14 "$ | RTRP-21CW-4553 |

${ }^{(1)}$ Static pressure ratings, typically created with use of a gear turbine, centrifugal, or multiplex pump having 4 or more pistons or elevation head.
${ }^{(2)}$ Specially fabricated higher pressure fittings are available on request. Consult the factory for compressible gases. For insulated and/ or heat traced piping systems, use $100 \%$ of the uninsulated piping recommendations up to $200^{\circ} \mathrm{F}$ and reduce these ratings $50 \%$ for $200^{\circ} \mathrm{F}$ to $250^{\circ} \mathrm{F}$ operating temperatures. For uninsulated piping systems, reduce these ratings $30 \%$ for $225^{\circ} \mathrm{F}$ to $250^{\circ} \mathrm{F}$ operating temperatures. Heat cured
adhesive joints are highly recommended for all piping systems carrying fluids at temperatures above $120^{\circ} \mathrm{F}$.
${ }^{(3)}$ Socket elbows, tees, reducers, couplings, flanges and nipples joined with Weldfast ZC-275 adhesive.
${ }^{(4)}$ Flanged elbows, tees, reducers, couplings and nipples assembled at factory.
${ }^{(5)}$ Laterals, crosses, and saddles.
${ }^{(6)}$ Ratings shown are $50 \%$ of ultimate; 14.7 psi external pressure is equal to full vacuum.

Recommended Operating Ratings

|  | Axial Te Ma | Loads bs) | Axial Co Loads M | ressive (Lbs) ${ }^{(1)}$ | Bending Radius Min. | Torque Max. | Par | I Plate Load STM D2412 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Size <br> (In) | $\begin{aligned} & \text { Tem } \\ & 75^{\circ} \mathrm{F} \end{aligned}$ | $250^{\circ} F$ | $\begin{aligned} & \text { Temp } \\ & 75^{\circ} \mathrm{F} \end{aligned}$ | ture $250^{\circ} \mathrm{F}$ | (Ft) Entire Temp. Range | (Ft Lbs) Entire Temp. Range | Stiffness Factor ( $\mathrm{In}^{3} \mathrm{Lbs} / \mathrm{In}^{2}$ ) | Pipe Stiffness (psi) | Hoop Modulus x10 ${ }^{6}$ (psi) |
| 1 | 1,560 | 1,200 | 1,700 | 600 | 50 | 41 | 164 | 4,791 | 2.7 |
| $11 / 2$ | 4,260 | 3,300 | 6,770 | 2,500 | 56 | 132 | 617 | 6,080 | 2.7 |
| 2 | 5,410 | 4,200 | 8,600 | 3,200 | 70 | 216 | 617 | 2,969 | 2.7 |
| 3 | 8,130 | 6,300 | 12,930 | 4,800 | 103 | 497 | 617 | 874 | 2.7 |
| 4 | 12,720 | 9,800 | 20,230 | 7,500 | 132 | 1,000 | 1,105 | 731 | 2.7 |
| 6 | 18,960 | 14,700 | 30,160 | 11,200 | 195 | 2,260 | 1,228 | 245 | 3.0 |
| 8 | 27,690 | 21,400 | 44,060 | 16,400 | 253 | 4,330 | 1,715 | 153 | 3.0 |
| 10 | 40,030 | 30,900 | 63,680 | 23,700 | 316 | 7,820 | 3,106 | 143 | 3.5 |
| 12 | 47,630 | 36,800 | 75,780 | 28,100 | 374 | 11,100 | 3,106 | 85 | 3.5 |
| 14 | 52,380 | 40,500 | 83,340 | 31,000 | 411 | 13,500 | 3,106 | 64 | 3.5 |
| ${ }^{(1)}$ Compressive loads are for short columns only. |  |  |  |  |  |  |  |  |  |

## Water Hammer:

Care should be taken when designing an FRP piping system to eliminate sudden surges. Soft start pumps and slow actuating valves should be considered.

## Support

Proper pipe support spacing depends on the temperature and weight of the fluid in the pipe. The support spacing table is based on unrestrained continuous beam theory using the pipe bending modulus derived from long-term beam bending tests. The maximum spans lengths were developed to ensure a design that limits mid-span deflection to $1 / 2$ inch and dead weight bending to $1 / 8$ of the ultimate bending stress. Any additional loads on the piping system such as insulation, wind, seismic, etc. requires further consideration. Restrained (anchored) piping systems operating at elevated temperatures may result in guide spacing requirements that are shorter than unrestrained piping systems. In this case, the maximum guide spacing governs the support span requirements for the system. Pipe spans near elbows require special attention. Both supported and unsupported elbows are considered in the following tables and must be followed to properly design the piping system.

There are seven basic rules to follow when designing piping system supports:

1. Do not exceed the recommended support span.
2. Support heavy valves and in-line equipment independently.
3. Protect pipe from external abrasion at supports.
4. Avoid point contact loads.
5. Avoid excessive bending. This applies to handling, transporting, initial layout, and final installed position.
6. Avoid excessive vertical loading to minimize bending stresses on pipe and fittings.
7. Provide adequate axial and lateral restraint to ensure line stability during rapid changes in flow.

| Maximum Support Spacing for Uninsulated Pipe ${ }^{(1)}$ |  |  |  |
| :---: | :---: | :---: | :---: |
| Pipe Size (In.) | Continuous Spans of Pipe (Ft.) ${ }^{(2)}$ |  |  |
|  | $75^{\circ} \mathrm{F}$ | $150^{\circ} \mathrm{F}$ | $250{ }^{\circ} \mathrm{F}$ |
| 1 | 8.4 | 8.3 | 7.9 |
| $11 / 2$ | 16.6 | 16.4 | 15.6 |
| 2 | 18.3 | 18.0 | 17.2 |
| 3 | 20.7 | 20.4 | 19.5 |
| 4 | 23.3 | 22.9 | 21.9 |
| 6 | 26.0 | 25.7 | 24.5 |
| 8 | 28.8 | 28.4 | 27.1 |
| 10 | 31.6 | 31.1 | 29.8 |
| 12 | 33.2 | 32.7 | 31.2 |
| 14 | 34.1 | 33.6 | 32.0 |
| ${ }^{(1)}$ Consult factory for insulated pipe support spacing. <br> ${ }^{(2)}$ Maximum mid-span deflection $1 / 2$ " with a specific gravity of 1.0 . |  |  |  |

## Support Spacing vs. Specific Gravity

| Specific Gravity | 3.00 | 2.00 | 1.50 | 1.25 | 1.00 | 0.75 | Gas/Air |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Multiplier | 0.76 | 0.84 | 0.90 | 0.95 | 1.00 | 1.07 | 1.40 |

Example: $6^{\prime \prime}$ pipe @ $150^{\circ} \mathrm{F}$ with 1.5 specific gravity fluid, maximum support spacing $=25.7 \times 0.90=23.1 \mathrm{ft}$.

Adjustment Factors for Various Spans With Unsupported Fitting at Change in Direction

Adjustment Factors for Various Spans With Supported Fitting at Change in Direction



## Thermal Expansion

The effects of thermal gradients on piping systems may be significant and should be considered in every piping system stress analysis. Pipe line movements due to thermal expansion or contraction may cause high stresses or even buckle a pipe line if improperly restrained. Several piping system designs are used to manage thermal expansion and contraction in above ground piping systems. They are listed below according to economic preference:

1. Use of inherent flexibility in directional changes
2. Restraining axial movements and guiding to prevent buckling
3. Use expansion loops to absorb thermal movements
4. Use mechanical expansion joints to absorb thermal movements

To perform a thermal analysis the following information is required:

1. Isometric layout of piping system
2. Physical and material properties of pipe
3. Design temperatures
4. Installation temperature (final tie in temperature)
5. Terminal equipment load limits
6. Support movements

A comprehensive review of temperature effects on fiberglass pipe may be found in NOV Fiber Glass Systems' Engineering and Piping Design Guide.

| Change in <br> Temperature <br> ${ }^{\circ} \mathrm{F}$ | Pipe Change <br> in Length <br> (In/100 Ft) |
| :---: | :---: |
| 25 | 0.3 |
| 50 | 0.7 |
| 75 | 1.0 |
| 100 | 1.3 |
| 125 | 1.7 |
| 150 | 2.0 |
| 175 | 2.3 |
| 200 | 2.6 |


| Restrained Thermal End Loads and Guide Spacing |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Size <br> (In) | Operating Temperature ${ }^{\circ} \mathrm{F}$ (Based on Installation Temperature of $75^{\circ} \mathrm{F}$ ) |  |  |  |  |  |  |  |  |  |
|  | $100^{\circ} \mathrm{F}$ |  | $150^{\circ} \mathrm{F}$ |  | $175{ }^{\circ} \mathrm{F}$ |  | $200^{\circ} \mathrm{F}$ |  | $225^{\circ} \mathrm{F}$ |  |
|  | Guide Spacing (Ft) | Thermal End Load (Lbs) | Guide Spacing (Ft) | Thermal End Load (Lbs) | Guide Spacing (Ft) | Thermal End Load (Lbs) | Guide Spacing (Ft) | Thermal End Load (Lbs) | Guide Spacing (Ft) | Thermal End Loads (Lbs) |
| 1 | 3.9 | 128 | 2.3 | 383 | 2.0 | 510 | 1.8 | 638 | 1.6 | 765 |
| $11 / 2$ | 10.4 | 553 | 6.0 | 1,658 | 5.2 | 2,210 | 4.7 | 2,763 | 4.3 | 3,315 |
| 2 | 13.2 | 700 | 7.6 | 2,100 | 6.6 | 2,800 | 5.9 | 3,500 | 5.4 | 4,200 |
| 3 | 19.9 | 1,053 | 11.5 | 3,158 | 9.9 | 4,210 | 8.9 | 5,263 | 8.1 | 6,315 |
| 4 | 25.6 | 1,648 | 14.8 | 4,943 | 12.8 | 6,590 | 11.4 | 8,238 | 10.4 | 9,885 |
| 6 | 38.1 | 2,458 | 22.0 | 7,373 | 19.1 | 9,830 | 17.1 | 12,288 | 15.6 | 14,745 |
| 8 | 49.8 | 3,588 | 28.8 | 10,763 | 24.9 | 14,350 | 22.3 | 17,938 | 20.3 | 21,525 |
| 10 | 62.2 | 5,185 | 35.9 | 15,555 | 31.1 | 20,740 | 27.8 | 25,925 | 25.4 | 31,110 |
| 12 | 74.0 | 6,170 | 42.7 | 18,510 | 37.0 | 24,680 | 33.1 | 30,850 | 30.2 | 37,020 |
| 14 | 81.4 | 6,785 | 47.0 | 20,355 | 40.7 | 27,140 | 36.4 | 33,925 | 33.2 | 40,710 |


| Elbow Strength |  |  |  |
| :---: | :---: | :---: | :---: |
| Allowable Bending Moment -90 Elbow |  |  |  |
| Nominal Pipe <br> Size (In) | Allowable <br> Moment (Ft•Lbs) | Nominal Pipe <br> Size (In) | Allowable <br> Moment (Ft•Lbs) |
| 1 | 100 | 6 | 1,650 |
| $11 / 2$ | 150 | 8 | 2,850 |
| 2 | 225 | 10 | 4,500 |
| 3 | 475 | 12 | 6,500 |
| 4 | 650 | 14 | 10,000 |



QUALITY MANAGEMENT SYSTEM
CERTIFIED BY DNV
ISO 9001:2008 $=$
LITTLE ROCK, AR
SAND SPRINGS, OK
SUZHOU, CHINA
FIBER GLASS SYSTEMS


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## Section 1 -Scope

This section covers the use of fiberglass reinforced plastic (FRP) pipe for chemical process and chemical handling up to $250^{\circ} \mathrm{F}$ and up to 150 psig pressure.
The piping shall be furnished and installed complete with all fittings, joining materials, supports, specials, and other necessary appurtenances.

## Section 2-General Conditions

2.01 Coordination - Material furnished and work performed under this section shall be coordinated with related work and equipment specified under othersections.

| Valves | Section |  |
| :--- | :--- | :--- |
| Supports | Section | - |
| Equipment | Section |  |

2.02 Governing Standards - Except as modified or supplemented herein, all materials and construction methods shall comply with the applicable provisions of the following specifications and be tested using the following standards.

## Standard Specifications

| ASTM D2997 | Standard Specification for Centrifugal Cast <br> "Fiberglass" (Glass-Fiber-Reinforced Thermosetting) Resin Pipe |
| :--- | :--- |
| AWWA 45 | Fiberglass Pipe Design |
| ASTM D5685 | Standard Specification for "Fiberglass" (Glass-Fiber-Reinforced- <br> Thermosetting Resin) Pressure Plpe Fittings |
| ASTM D4024 | Standard Specification for Reinforced Thermosetting Resin (RTR) <br> Flanges |

## Standard Test Methods

| ASTM D2997 | Standard Practice for Obtaining Hydrostatic or Pressure Design <br> Basis for "Fiberglass" (Glass-Fiber-Reinforced Thermosetting Resin) <br> Pipe |
| :--- | :--- |
| ASTM D1599 | Standard Test method for Short-Time Hydraulic Failure Pressure of <br> Plastic Pipe, Tubing and Fittings |
| ASTM D2105 | Standard Test Method for Longitudinal Tensile Properties of <br> "Fiberglass" (Glass-Fiber-Reinforced Thermosetting Resin) Pipe and <br> Tube |
| ASTM D2412 | Standard Test Method for Determination of External Loading <br> Characteristics of Plastic Pipe by Parallel-Plate Loading |
| ASTM B31.3 | Process Piping |

### 2.03 ASTM D2997 Designation Codes

| $1^{\prime \prime}-11 / 2^{\prime \prime}$ | RTRP-21CW-4326 |
| :--- | :--- |
| $2 "-4 "$ | RTRP-21CW-4456 |
| $6^{\prime \prime}-8 "$ | RTRP-21CW-4455 |
| $10 "-12 "$ | RTRP-21CW-4454 |
| $14 "$ | RTRP-21CW-4553 |

Mechanical properties cell classifications shown are minimums
2.04 Operating Conditions - In addition to the above minimum design requirements, the system shall meet the following minimum operating conditions:
a. Operating Pressure
b. Operating Temperature
c. Fluid Conveyed
d. Test Pressure
2.05 Quality Assurance - Pipe manufacturer's quality program shall be in compliance with ISO 9001.
2.06 Delivery, Storage and Handling - Pipe and fittings shall be protected from damage due to impact and point loading. Pipe shall be properly supported to avoid damage due to flexural strains. The contractor shall not allow dirt, debris, or other extraneous materials to get into pipe and fittings. All factory machined areas shall be protected from sunlight until installed.
2.07 Acceptable Manufacturers - NOV Fiber Glass Systems (918) 245-6651 or approved equal.

## Section 3 - Materials and Construction

3.01 1"-14" Pipe - The pipe shall be manufactured by the centrifugal casting process using premium grade amine cured epoxy thermosetting resin to impregnate woven glass filaments. Pipe shall be heat cured and the degree of cure shall be confirmed using a Differential Scanning Calorimeter. All pipe shall have a $100 \%$ resin corrosion barrier and the cured thickness shall be 100 mils nominal.

All pipe shall have a resin-rich reinforced 10 mil nominal exterior layer.

The pipe shall have a minimum design pressure rating of 150 psig at $150^{\circ}$ F following ASTM D2992 Procedure B.

## Nominal Reinforced Wall Thickness

| $1 "$ | 0.090 inches |
| :--- | :--- |
| $11 / 2^{\prime \prime}-3^{\prime \prime}$ | 0.140 inches |
| $4^{\prime \prime}-6 "$ | 0.170 inches |
| $8^{\prime \prime}$ | 0.190 inches |
| $10 "-14 "$ | 0.220 inches |

3.02 Flanges and Fittings - All fittings shall be manufactured either by compression molding or contact molding. Fitting joints shall be either adhesive bonded socket or flanged. Flanges shall have ANSI B16.5 Class 150 bolt hole patterns.
3.03 Adhesive - Adhesive shall be manufacturer's standard for the piping system specified. All adhesive bonded joints shall be cured according to the manufacturer's instructions for maximum strength and corrosion resistance.
3.04 Gaskets - Gaskets shall be 3/16" thick, 60-70 durometer fullfact type suitable for the service shown on the drawings and as recommended in the manufacturer's standard installation procedures.
3.05 Bolts, Nuts and Washers - ASTM F593, 304 stainless steel hex head bolts shall be supplied. Two each SAE size washers shall be supplied on all nuts and bolts.
3.06 Acceptable Products - Centricast RB-2530 as manufactured by NOV Fiber Glass Systems or approved equal.

## Section 4 - Installation and Testing

4.01 Training and Certification - All joints installed or constructed in the field shall be assembled by employees of the contractor who have been trained by the pipe manufacturer. The pipe manufacturer or their authorized representative shall train the contractor's employees in the proper joining and assembly procedures required for the project, including hands-on participation by the contractor's employees. Each bonder shall fabricate one pipe-to-pipe and one pipe-to-fitting joint that shall pass the minimum pressure test for the application as stated in Section 2.04.d without leaking.

Only bonders who have successfully completed the pressure test shall bond pipe and fittings.

Certification by the manufacturer shall be in compliance with ASME B31.3, Section A328.2.
4.02 Pipe Installation - Pipe shall be installed as specified and indicated on the drawings and in accordance with the manufacturer's current published installation procedures.
4.03 Testing A hydrostatic pressure test shall be conducted on the completed piping system. The pipe shall be subjected to a steady pressure at $11 / 2$ times the design operating pressure as stated in Section 2.04d. The pressure shall be held on the system for a minimum of one hour and the line inspected for leaks.

The test pressure should not exceed $11 / 2$ times the maximum rated operating pressure for the lowest rated element in the system.

The system shall be filled with water at the lowest point and air bled off from all the highest points. Systems shall be brought up to test pressure slowly to prevent water hammer or over pressurization.

All pipe joints shall be water tight. All joints that are found to leak by observation or during testing shall be repaired by the contractor and retested.

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## Fiber Glass Systems

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## Centricast CL-1520® Product Data

Applications • Acids • Oxidizing Agents

- Salts • Chlorine Water


## Materials and Construction

All pipe is manufactured with glass fabrics and a highly resilient formulation of vinyl ester resin. A 50-mil integral corrosion barrier of pure resin provides excellent corrosion resistance. It is recommended for most chlorinated and/or acidic mixtures up to $175^{\circ} \mathrm{F}$ and other chemicals up to $200^{\circ} \mathrm{F}$. A 10-mil resinrich reinforced external corrosion barrier provides excellent corrosion resistance and protection from ultraviolet (UV) radiation. Fiber Glass Systems warrants Centricast CL-1520 pipe and fittings against UV degradation of physical properties and chemical resistance for 15 years.

Pipe is available in $11 / 2^{\prime \prime}$ through 14" diameters and is recommended for highly chlorinated or acidic mixtures up to $175^{\circ} \mathrm{F}$ and many other chemicals up to $200^{\circ} \mathrm{F}$. Centricast CL-1520 comes in 20' nominal or exact lengths from 18.0-20.4 feet long.

## Fittings

Fittings are manufactured with the same chemical/temperature capabilities as the pipe. Depending on the particular part and size, fittings will be compression molded, contact molded, hand fabricated or filament wound.

## Joining Systems

## Socket Joint

An adhesive bonded socket connection with positive stops in the fittings is standard and simplifies close tolerance piping installation. This joining system is easy to install and no special tools are required for field assembly.


| Nominal Dimensional Data |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Pipe Size in | I.D. |  | O.D. |  | Wall Thickness |  | Reinforcement Thickness |  | Weight |  | Capacity |  |
|  | in | mm | in | mm | in | mm | in | mm | lbs/ft | kg/m | gal/ft | $\mathrm{ft}^{3} / \mathrm{ft}$ |
| $11 / 2$ | 1.52 | 38.6 | 1.90 | 48.3 | 0.19 | 4.8 | 0.13 | 3.3 | 0.67 | 1.00 | 0.09 | 0.013 |
| 2 | 2.00 | 50.8 | 2.38 | 60.5 | 0.19 | 4.8 | 0.13 | 3.3 | 0.86 | 1.28 | 0.16 | 0.022 |
| 3 | 3.12 | 79.2 | 3.50 | 88.9 | 0.19 | 4.8 | 0.13 | 3.3 | 1.30 | 1.94 | 0.40 | 0.053 |
| 4 | 4.12 | 104.6 | 4.50 | 114.3 | 0.19 | 4.8 | 0.13 | 3.3 | 1.70 | 2.53 | 0.69 | 0.093 |
| 6 | 6.21 | 157.7 | 6.63 | 168.4 | 0.21 | 5.3 | 0.15 | 3.8 | 2.79 | 4.16 | 1.57 | 0.210 |
| 8 | 8.15 | 207.0 | 8.63 | 219.2 | 0.24 | 6.1 | 0.18 | 4.6 | 4.17 | 6.21 | 2.71 | 0.362 |
| 10 | 10.30 | 261.6 | 10.75 | 273.1 | 0.24 | 6.1 | 0.18 | 4.6 | 5.23 | 7.78 | 4.30 | 0.575 |
| 12 | 12.30 | 312.4 | 12.75 | 323.9 | 0.24 | 6.1 | 0.18 | 4.6 | 6.23 | 9.26 | 6.14 | 0.821 |
| 14 | 13.50 | 342.9 | 14.00 | 355.6 | 0.24 | 6.1 | 0.18 | 4.6 | 6.85 | 10.19 | 7.46 | 0.997 |
| Tolerances or maximum/minimum limits can be obtained from NOV Fiber Glass Systems. |  |  |  |  |  |  |  |  |  |  |  |  |


| Properties of Pipe Sections Based on Minimum Reinforced Walls |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Size in | Reinforcement End Area in ${ }^{2}$ | Reinforcement Moment of Inertia in ${ }^{4}$ | Reinforcement Section Modulus in ${ }^{3}$ | Nominal Wall End Area in ${ }^{2}$ |
| $11 / 2$ | 0.72 | 0.29 | 0.30 | 1.02 |
| 2 | 0.92 | 0.58 | 0.49 | 1.30 |
| 3 | 1.38 | 1.96 | 1.12 | 1.98 |
| 4 | 1.79 | 4.26 | 1.90 | 2.57 |
| 6 | 3.05 | 16.00 | 4.83 | 4.23 |
| 8 | 4.78 | 42.60 | 9.88 | 6.32 |
| 10 | 5.98 | 83.50 | 15.50 | 7.92 |
| 12 | 7.11 | 140.00 | 22.00 | 9.43 |
| 14 | 7.82 | 187.00 | 26.70 | 10.40 |

Average Physical Properties

| Property | $\begin{aligned} & 75^{\circ} \mathrm{F} \\ & \mathrm{psi} \end{aligned}$ | $\begin{aligned} & 24^{\circ} \mathrm{C} \\ & \mathrm{MPa} \end{aligned}$ | $\begin{gathered} 150^{\circ} \mathrm{F} \\ \mathrm{psi} \end{gathered}$ | $\begin{aligned} & 66^{\circ} \mathrm{C} \\ & \mathrm{MPa} \end{aligned}$ | $\begin{gathered} 175^{\circ} \mathrm{F} \\ \mathrm{psi} \end{gathered}$ | $\begin{aligned} & 180^{\circ} \mathrm{C} \\ & \mathrm{MPa} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Axial Tensile - ASTM D2105 <br> Ultimate Stress <br> Design Stress <br> Modulus of Elasticity | $\begin{gathered} 30,000 \\ 7,500 \\ 2.6 \times 10^{6} \end{gathered}$ | $\begin{gathered} 210 \\ 52 \\ 17,900 \end{gathered}$ | $\begin{gathered} 26,000 \\ 6,500 \\ 2.3 \times 10^{6} \end{gathered}$ | $\begin{gathered} 180 \\ 45 \\ 15,900 \end{gathered}$ | $\begin{gathered} 25,000 \\ 6,200 \\ 2.2 \times 10^{6} \end{gathered}$ | $\begin{gathered} 170 \\ 43 \\ 15,200 \end{gathered}$ |
| Poisson's Ratio $\nu$ | 0.15 |  |  |  |  |  |
| Axial Compression - ASTM D695 <br> Ultimate Stress <br> Design Stress <br> Modulus of Elasticity | $\begin{gathered} 32,000 \\ 8,000 \\ 3.1 \times 10^{6} \end{gathered}$ | $\begin{gathered} 220 \\ 55 \\ 21,400 \end{gathered}$ | $\begin{gathered} 30,000 \\ 7,500 \\ 2.7 \times 10^{6} \end{gathered}$ | $\begin{gathered} 200 \\ 52 \\ 18,600 \end{gathered}$ | $\begin{gathered} 22,000 \\ 5,550 \\ 2.6 \times 10^{6} \end{gathered}$ | $\begin{gathered} 150 \\ 38 \\ 17,900 \end{gathered}$ |
| Beam Bending - ASTM D2925 <br> Ultimate Stress <br> Design Stress ${ }^{(1)}$ <br> Modulus of Elasticity (Long Term) | $\begin{gathered} 40,000 \\ 5,000 \\ 3.3 \times 10^{6} \end{gathered}$ | $\begin{gathered} 280 \\ 34 \\ 22,800 \end{gathered}$ | $\begin{gathered} 35,000 \\ 4,375 \\ 2.9 \times 10^{6} \end{gathered}$ | $\begin{gathered} 240 \\ 30 \\ 20,000 \end{gathered}$ | $\begin{gathered} 33,000 \\ 4,125 \\ 2.8 \times 10^{6} \end{gathered}$ | $\begin{gathered} 230 \\ 28 \\ 19,300 \end{gathered}$ |
| Hydrostatic Burst - ASTM D1599 Ultimate Hoop Tensile Stress Hoop Tensile Modulus of Elasticity | $\begin{gathered} 30,000 \\ 2.4 \times 10^{6} \end{gathered}$ | $\begin{gathered} 200 \\ 17,000 \end{gathered}$ | $\begin{gathered} 26,000 \\ 2.1 \times 10^{6} \end{gathered}$ | $\begin{gathered} 180 \\ 14,500 \end{gathered}$ | $\begin{gathered} 25,000 \\ 2.0 \times 10^{6} \end{gathered}$ | $\begin{gathered} 170 \\ 13,800 \end{gathered}$ |
| Hydrostatic Design - ASTM D2992 <br> Procedure B-Hoop Tensile Stress <br> Static 50 Year @ $175^{\circ} \mathrm{F}$ |  |  |  |  |  |  |
| ${ }^{(1)}$ Stress and modulus values can be interpolated between temperatures shown. |  |  |  |  |  |  |


| Thermal Expansion Coefficient - ASTM D696 | Non-Insulated Pipe: $8.4 \times 10^{6}$ Insulated Pipe: $\quad 9.2 \times 10^{6}$ | $\mathrm{In} / \mathrm{In} /{ }^{\circ} \mathrm{F} \cdot 15.2 \times 10^{6} \mathrm{~mm} / \mathrm{mm} /{ }^{\circ} \mathrm{C}$ <br> $\mathrm{In} / \mathrm{In} /{ }^{\circ} \mathrm{F} \cdot 16.6 \times 10^{6} \mathrm{~mm} / \mathrm{mm} /{ }^{\circ} \mathrm{C}$ |
| :---: | :---: | :---: |
| Thermal Conductivity | 0.07 BTU/hr-ft- ${ }^{\circ} \mathrm{F}$ | $0.04 \mathrm{~W} / \mathrm{m}-{ }^{\circ} \mathrm{C}$ |
| Specific Gravity - ASTM D792 |  | 52 |
| Hazen-Williams Coefficient |  | 50 |
| Absolute Surface Roughness | 0.00021 in | 0.0053 mm |
| Manning's Roughness Coefficient, n | 0.009 |  |

## Testing:

See Fiber Glass Systems' Socket Joint Installation Handbook.
When possible, Fiber Glass Systems' piping systems should be hydrostatically tested prior to beginning service. Care should be taken when testing to avoid water hammer.

All anchors, guides and supports must be in place prior to testing the line.

Test pressure should not be more than $11 / 2$ times the working pressure of the piping system and never exceed $11 / 2$ times the rated operating pressure of the lowest rated component in the system.

| Pressure Ratings for Uninsulated Piping Systems ${ }^{(1)(2)}$ |  |  |  |  |  |  | ASTM D2997 Designation Codes: |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Nominal | Maximum InternalPressure @ $175^{\circ} \mathrm{F}$ psig |  |  | Maximum External Pressure $\mathrm{psig}^{\left({ }^{(6)}\right.}$ |  |  | $\frac{11 / 2^{\prime \prime}-4^{\prime \prime}}{6^{\prime \prime}}$ | RTRP-22BT-4556 |
| $\begin{aligned} & \text { Pipe } \\ & \text { Size } \\ & \text { in } \end{aligned}$ | Socket Pressure Fittings ${ }^{(3)}$ | Flanged <br> Pressure <br> Fittings ${ }^{(4)}$ | Other Pressure ${ }^{(5)}$ | $75^{\circ} \mathrm{F}$ | $150^{\circ} \mathrm{F}$ | $175^{\circ} \mathrm{F}$ |  | RTRP-22BT-4554 |
| $11 / 2$ | 300 | 300 | - | 650 | 579 | 491 |  | RTRP-22BT-4552 |
| 2 | 275 | 200 | 125 | 380 | 268 | 227 |  |  |
| 3 | 200 | 150 | 125 | 130 | 74 | 63 |  |  |
| 4 | 150 | 150 | 100 | 50 | 33 | 28 |  |  |
| 6 | 150 | 150 | 100 | 30 | 21 | 17 |  |  |
| 8 | 150 | 150 | 100 | 25 | 17 | 14 |  |  |
| 10 | 150 | 150 | 75 | 16 | 13 | 11 |  |  |
| 12 | 150 | 150 | 75 | 10 | 8 | 7 |  |  |
| 14 | 125 | 150 | - | 7 | 5 | 4 |  |  |

${ }^{(1)}$ Static pressure ratings, typically created with use of a gear turbine, centrifugal, or multiplex pump having 4 or more pistons or elevation head.
${ }^{(2)}$ Reduce pressure ratings by $30 \%$ for $175^{\circ} \mathrm{F}$ to $200^{\circ} \mathrm{F}$ operating temperatures. For compressible gases, insulated and/or heat traced piping systems, consult the factory for pressure ratings. Centricast CL-1520 pipe and vinyl ester fittings can be used in drainage and vent systems up to $200^{\circ} \mathrm{F}$. Heat cured adhesive joints are highly recommended for all piping systems carrying fluids at temperatures above $120^{\circ} \mathrm{F}$.
${ }^{(3)}$ Socket elbows, tees, reducers, couplings, flanges and nipples joined with Weldfast CL-200 adhesive. ${ }^{(4)}$ Flanged elbows, tees, reducers, couplings and nipples assembled at factory.
${ }^{(5)}$ Laterals, crosses, and saddles.
${ }^{(6)}$ Ratings shown are $50 \%$ of ultimate; 14.7 psi external pressure is equal to full vacuum.

Recommended Operating Ratings

| $\begin{aligned} & \text { Size } \\ & \text { in } \end{aligned}$ | Axial Tensile Loads Max. Ibs |  | Axial Compressive Loads Max. Ibs ${ }^{(1)}$ |  | Bending Radius Min. ft. Entire Temp. Range | Torque Max. ft/lbs Entire Temp. Range | Parallel Plate Loading ASTM D2412 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{aligned} & \text { Tem } \\ & 75^{\circ} \mathrm{F} \end{aligned}$ | ure $175^{\circ} F$ | $\begin{gathered} \text { Tem } \\ 75^{\circ} \mathrm{F} \end{gathered}$ | ture $175^{\circ} \mathrm{F}$ |  |  | Stiffness Factor ln $^{3}$ Lbs/ln ${ }^{2}$ | Pipe Stiffness psi | Hoop Modulus $\times 10^{6} \mathrm{psi}$ |
| $11 / 2$ | 5,400 | 4,500 | 5,800 | 4,000 | 52 | 125 | 366 | 3,545 | 2.0 |
| 2 | 6,900 | 5,700 | 7,300 | 5,000 | 65 | 203 | 366 | 1,738 | 2.0 |
| 3 | 10,300 | 8,600 | 11,000 | 7,600 | 96 | 466 | 458 | 642 | 2.5 |
| 4 | 13,400 | 11,200 | 14,300 | 9,800 | 124 | 790 | 458 | 294 | 2.5 |
| 6 | 22,900 | 19,100 | 24,400 | 16,800 | 182 | 2,013 | 788 | 156 | 2.8 |
| 8 | 35,800 | 29,800 | 38,200 | 26,300 | 237 | 4,115 | 1,264 | 113 | 2.6 |
| 10 | 44,800 | 37,400 | 47,800 | 32,900 | 296 | 6,473 | 1,458 | 66 | 3.0 |
| 12 | 53,300 | 44,400 | 56,900 | 39,100 | 351 | 9,178 | 1,652 | 45 | 3.4 |
| 14 | 58,600 | 48,800 | 62,500 | 43,000 | 385 | 11,108 | 1,652 | 34 | 3.4 |

Water Hammer:
Care should be taken when designing an FRP piping system to eliminate sudden surges. Soft start pumps and slow actuating valves should be considered

| Pipe Lengths Available* |  |
| :---: | :---: |
| Size in | Random Length ft |
| $1 \frac{1}{2}-14$ | 20 |
| *Pipe comes in random or exact lengths from <br> $18.0-20.4$ feet long. |  |

## Supports

Proper pipe support spacing depends on the temperature and weight of the fluid in the pipe. The support spacing table is based on unrestrained continuous beam theory using the pipe bending modulus derived from long-term beam bending tests. The maximum spans lengths were developed to ensure a design that limits mid-span deflection to $1 / 2$ inch and dead weight bending to $1 / 8$ of the ultimate bending stress. Any additional loads on the piping system such as insulation, wind, seismic, etc. requires further consideration. Restrained (anchored) piping systems operating at elevated temperatures may result in guide spacing requirements that are shorter than unrestrained piping systems. In this case, the maximum guide spacing governs the support span requirements for the system. Pipe spans near elbows require special attention. Both supported and unsupported elbows are considered in the following tables and must be followed to properly design the piping system

There are seven basic rules to follow when designing piping system supports:

1. Do not exceed the recommended support span.
2. Support heavy valves and in-line equipment independently.
3. Protect pipe from external abrasion at supports.
4. Avoid point contact loads.
5. Avoid excessive bending. This applies to handling, transporting, initial layout, and final installed position.
6. Avoid excessive vertical loading to minimize bending stresses on pipe and fittings.
7. Provide adequate axial and lateral restraint to ensure line stability during rapid changes in flow.

## Maximum Support Spacing for

 Uninsulated Pipe ${ }^{(1)}$| Pipe Size <br> in | Continuous Spans of Pipe (Ft.) ${ }^{(2)}$ |  |  |
| :---: | :---: | :---: | :---: |
|  | $\mathbf{7 5} \mathbf{F}$ | $\mathbf{1 5 0}^{\circ} \mathrm{F}$ | $\mathbf{1 7 5}{ }^{\circ} \mathbf{F}$ |
| $11 / 2$ | 16.4 | 15.8 | 15.7 |
| 2 | 17.6 | 17.0 | 16.9 |
| 3 | 19.9 | 19.2 | 19.1 |
| 4 | 21.4 | 20.7 | 20.5 |
| 6 | 24.7 | 23.9 | 23.7 |
| 8 | 27.7 | 26.8 | 26.5 |
| 10 | 29.4 | 28.5 | 28.2 |
| 12 | 30.8 | 29.8 | 29.5 |
| 14 | 31.6 | 30.6 | 30.3 |

## Support Spacing vs. Specific Gravity

| Specific Gravity | 3.00 | 2.00 | 1.50 | 1.25 | 1.00 | 0.75 | Gas/Air |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Multiplier | 0.76 | 0.84 | 0.90 | 0.95 | 1.00 | 1.07 | 1.40 |

Example: 6" pipe @ $150^{\circ} \mathrm{F}$ with 1.5 specific gravity fluid, maximum support spacing $=23.9 \times 0.90=21.5 \mathrm{ft}$.

Adjustment Factors for Various Spans With Unsupported Fitting at Change in Direction

Adjustment Factors for Various Spans With Supported Fitting at Change in Direction

|  | Span Type | Factor |
| :---: | :---: | :---: |
| a | Continuous interior or fixed end spans | 1.00 |
| b | Second span from supported end or unsupported fitting | 0.80 |
| $c+d$ | Sum of unsupported spans at fitting | $\leq 0.75$ * |
| e | Simple supported end span | 0.67 |
|  | *For example: If continuous supp $\mathrm{c}+\mathrm{d}$ must not exceed 7.5 ft ( $\mathrm{c}=3 \mathrm{ft}$ ft .) would satisfy this condition. |  |



## Thermal Expansion

The effects of thermal gradients on piping systems may be significant and should be considered in every piping system stress analysis. Pipe line movements due to thermal expansion or contraction may cause high stresses or even buckle a pipe line if improperly restrained. Several piping system designs are used to manage thermal expansion and contraction in above ground piping systems. They are listed below according to economic preference:

1. Use of inherent flexibility in directional changes
2. Restraining axial movements and guiding to prevent buckling
3. Use expansion loops to absorb thermal movements
4. Use mechanical expansion joints to absorb thermal movements

To perform a thermal analysis the following information is required:

1. Isometric layout of piping system
2. Physical and material properties of pipe
3. Design temperatures
4. Installation temperature (Final tie in temperature)
5. Terminal equipment load limits
6. Support movements

A comprehensive review of temperature effects on fiberglass pipe may be found in NOV Fiber Glass Systems' Engineering and Piping Design Guide.

| Change in <br> Temperature <br> ${ }^{\circ} \mathrm{F}$ | Pipe Change <br> In Length <br> in/100 Ft |
| :---: | :---: |
| 25 | 0.25 |
| 50 | 0.50 |
| 75 | 0.76 |
| 100 | 1.01 |
| 125 | 1.26 |
| 150 | 1.51 |
| 175 | 1.76 |
| 200 | 2.02 |

## Restrained Thermal End Loads and Guide Spacing

| $\begin{gathered} \text { Size } \\ \text { in } \end{gathered}$ | Operating Temperature ${ }^{\circ} \mathrm{F}$ (Based on Installation Temperature of $75^{\circ} \mathrm{F}$ ) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $100^{\circ} \mathrm{F}$ |  | $125^{\circ} \mathrm{F}$ |  | $150^{\circ} \mathrm{F}$ |  | $175^{\circ} \mathrm{F}$ |  | $200^{\circ} \mathrm{F}$ |  |
|  | Guide Spacing ft | Thermal End Load lbs | Guide Spacing ft | Thermal End Load lbs | Guide Spacing ft | Thermal End Load Ibs | Guide Spacing ft | Thermal End Load Ibs | Guide Spacing ft | Thermal End Loads lbs |
| $11 / 2$ | 11.2 | 492 | 7.9 | 938 | 6.5 | 1,347 | 5.6 | 1,729 | 5.0 | 1,663 |
| 2 | 14.2 | 624 | 10.0 | 1,189 | 8.2 | 1,708 | 7.1 | 2,193 | 6.3 | 2,109 |
| 3 | 21.2 | 937 | 15.0 | 1,785 | 12.3 | 2,564 | 10.6 | 3,292 | 9.5 | 3,166 |
| 4 | 27.5 | 1,215 | 19.5 | 2,315 | 15.9 | 3,325 | 13.8 | 4,269 | 12.3 | 4,105 |
| 6 | 40.8 | 2,077 | 28.8 | 3,958 | 23.5 | 5,685 | 20.4 | 7,299 | 18.2 | 7,018 |
| 8 | 53.2 | 3,251 | 37.6 | 6,195 | 30.7 | 8,897 | 26.6 | 11,423 | 23.8 | 10,984 |
| 10 | 66.6 | 4,069 | 47.1 | 7,754 | 38.4 | 11,136 | 33.3 | 14,297 | 29.8 | 13,748 |
| 12 | 79.2 | 4,839 | 56.0 | 9,221 | 45.7 | 13,243 | 39.6 | 17,003 | 35.4 | 16,349 |
| 14 | 87.0 | 5,320 | 61.5 | 10,138 | 50.2 | 14,559 | 43.5 | 18,694 | 38.9 | 17,975 |


| Elbow Strength |  |  |  |
| :---: | :---: | :---: | :---: |
| Allowable Bending Moment -90 ${ }^{\circ}$ Elbow |  |  |  |
| Nominal <br> Pipe Size <br> in | Allowable <br> Moment <br> ft/lbs | Nominal <br> Pipe Size <br> in | Allowable <br> Moment <br> ft/lbs |
| $11 / 2$ | 150 | 8 | 2,850 |
| 2 | 225 | 10 | 4,500 |
| 3 | 475 | 12 | 6,500 |
| 4 | 650 | 14 | 10,000 |
| 6 | 1,650 |  |  |



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## CENTRICAST"' CL-1520 Piping System

## Specification Guide

## SECTION 1 - Scope

This section covers the use of fiberglass reinforced plastic (FRP) pipe for chemical process and chemical handling applications up to $200^{\circ} \mathrm{F}$ and 150 psig steady pressure.

The piping system shall be furnished and installed complete with all fittings, joining materials, supports, specials, and other necessary appurtenances.

## SECTION 2-General Conditions

2.01 Coordination - Material furnished and work performed under this section shall be coordinated with related work and equipment specified under other sections.

| Valves | Section |
| :--- | :--- |
| Supports | Section |
| Equipment | Section |

2.02 Governing Standards - Except as modified or supplemented herein, all materials and construction methods shall comply with the applicable provisions of the following specifications and be tested using the following standards:

## Standard Specifications

| ASTM <br> D2997 | Standard Specification for Centrifugal Cast "Fi- <br> berglass" (Glass-Fiber-Reinforced Thermoset- <br> ting) Resin Pipe |
| :--- | :--- |
| AWWWA <br> M45 | Fiberglass Pipe Design |
| ASTM <br> D5685 | Standard Specification for "Fiberglass" (Glass- <br> Fiber-Reinforced-Thermosetting Resin) <br> sure Plpe Fittings |
| ASTM <br> D4024 | Standard Specification for Reinforced Thermo- <br> setting Resin (RTR) Flanges |

## Standard Test Methods

| ASTM <br> D2992 | Standard Practice for Obtaining Hydrostatic or <br> Pressure Design Basis for "Fiberglass" (Glass- <br> Fiber-Reinforced Thermosetting Resin) Pipe |
| :--- | :--- |
| ASTM <br> D1599 | Standard Test method for Short-Time Hydraulic <br> Failure Pressure of Plastic Pipe, Tubing and Fit- <br> tings |
| ASTM <br> D2105 | Standard Test Method for Longitudinal Tensile <br> Properties of "Fiberglass" (Glass-Fiber-Rein- <br> forced Thermosetting Resin) Pipe and Tube |
| ASTM <br> D2412 | Standard Test Method for Determination of Ex- <br> ternal Loading Characteristics of Plastic Pipe by <br> Parallel-Plate Loading |
| ASME <br> B31.3 | Process Piping |

2.03 ASTM D2997 Designation Codes:

| $11 / 2 "-4 "$ | RTRP-22BT-4556 |
| :--- | :--- |
| $6 " \prime$ | RTRP-22BT-4555 |
| 8" | RTRP-22BT-4554 |
| $10 "-12 "$ | RTRP-22BT-4553 |
| $14 "$ | RTRP-22BT-4552 |

Mechanical properties cell classifications shown are minimums.
2.04 Operating Conditions - In addition to the above listed minimum design requirements, the system shall meet the following minimum operating conditions:
a. Operating Pressure
b. Operating Temperature
c. Fluid Conveyed
d. Test Pressure
2.05 Quality Assurance - Pipe manufacturer's quality program shall be in compliance with ISO 9001.
2.06 Delivery, Storage, and Handling - Pipe and fittings shall be protected from damage due to impact and point loading. Pipe shall be properly supported to avoid damage due to flexural strains. The contractor shall not allow dirt, debris, or other extraneous materials to get into pipe and fittings. All factory machined areas shall be protected from sunlight until installed.
2.07 Acceptable Manufacturers - NOV Fiber Glass Systems, (918) 245-6651, or approved equal.

## SECTION 3 - Materials and Construction

$3.01 \quad 11 / 2^{"-14 "}$ Pipe - The pipe shall be manufactured by the centrifugal casting process using premium grade vinyl ester thermosetting resin to impregnate woven glass filaments. Pipe shall be heat cured and the cure shall be confirmed using a Differential Scanning Calorimeter. All pipe shall have a $100 \%$ resin corrosion barrier and the cured thickness shall be 50 mils nominal. All pipe shall have a resin rich reinforced 10 mil nominal exterior layer with UV (ultraviolet) inhibitor.

The pipe shall have a minimum design pressure rating of 150 psig @ $175^{\circ}$ F following ASTM D2992, Procedure B.

## Minimum Reinforced Wall Thickness

$$
\begin{array}{ll}
\hline 11 / 2 "-4 " & 0.130 \text { inches } \\
6 " & 0.150 \text { inches } \\
8 "-14 " & 0.180 \text { inches }
\end{array}
$$

3.02 Flanges and Fittings - All fittings shall be manufactured either by compression molding or contact molding. Fitting joints shall be either adhesive bonded socket or flanged. Flanges shall have ANSI B16.5 Class 150 bolt hole patterns.
3.03 Adhesive - Adhesive shall be manufacturer's standard for the piping system specified. All adhesive bonded joints shall be cured according to the manufacturer's instructions for maximum strength and corrosion resistance.
3.04 Gaskets - Gaskets shall be ${ }^{3} / 16$ " thick, 60-70 durometer full-face type suitable for the service shown on the drawings and as recommended in the manufacturer's standard installation procedures.
3.05 Bolts, Nuts and Washers - ASTM F593, 304 stainless steel hex head bolts shall be supplied. Two each SAE size washers shall be supplied on all nuts and bolts.
3.06 Acceptable Products - Centricast CL-1520 as manufactured by NOV Fiber Glass Systems or approved equal.

## SECTION 4 - Installation and Testing

4.01 Training and Certification - All joints installed or constructed in the field shall be assembled by employees of the contractor who have been trained by the pipe manufacturer. The pipe manufacturer or their authorized representative shall train the contractor's employees in the proper joining and assembly procedures required for the project, including hands-on participation by the contractor's employees. Each bonder shall fabricate one pipe-to-pipe and one pipe-to-fitting joint that shall pass the minimum pressure test for the application as stated in Section 2.04.d without leaking.

Only bonders who have successfully completed the pressure test shall bond pipe and fittings.

Certification by the manufacturer shall be in compliance with ASME B31.3 Section A328.2.
4.02 Pipe Installation - Pipe shall be installed as specified and indicated on the drawings and in accordance with the manufacturer's current published installation procedures.
4.03 Testing - A hydrostatic pressure test shall be conducted on the completed piping system. The pipe shall be subjected to a steady pressure at $11 / 2$ times the design operating pressure as stated in Section 2.04a. The pressure shall be held on the system for a minimum of 1 hour and the line inspected for leaks.

The test pressure should not exceed $11 / 2$ times the maximum rated operating pressure for the lowest rated element in the system.

The system shall be filled with water at the lowest point and air bled off from all the highest points. Systems shall be brought up to test pressure slowly to prevent water hammer or over pressurization.

All pipe joints shall be water tight. All joints that are found to leak by observation or during testing shall be repaired by the contractor and retested.

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## Centricast CL-2030® Product Data

## Applications <br> Materials and Construction

- Acids
- Oxidizing Agents
- Salts
- Chemical Process Solutions

All pipe manufactured is manufactured with glass fibers and a highly resilient formulation of vinyl ester resin. A 100-mil integral corrosion barrier of pure resin provides excellent corrosion resistance. It is recommended for most chlorinated and/or acidic mixtures up to $175^{\circ} \mathrm{F}$ and other chemicals up to $200^{\circ} \mathrm{F}$. A 10-mil resin-rich reinforced external corrosion barrier provides corrosion resistance and protection from ultraviolet (UV) radiation. Fiber Glass Systems warrants Centricast CL-2030 pipe and fittings against UV degradation of physical properties and chemical resistance for 15 years.

Pipe is available in 1" through 14" diameters with static pressure ratings up to 150 psig, with higher pressure ratings in smaller sizes. Centricast CL-2030 comes in 20' nominal or exact lengths from 18.0-20.4 feet long.

## Fittings

Fittings are manufactured with the same chemical/temperature capabilities as the pipe. Depending on the particular part and size, fittings will be compression molded, contact molded, hand fabricated or filament wound.

## Joining Systems

## Socket Joint

Adhesive bonded straight socket joint with positive stops. This is the standard for Centricast piping systems.


Nominal Dimensional Data

| Pipe Size in | I.D. |  | O.D. |  | Wall Thickness |  | Reinforcement Thickness |  | Weight |  | Capacity |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | in | mm | in | mm | in | mm | in | mm | lbs/ft | kg/m | gal/ft | cuft/ft |
| 1 | 0.94 | 23.7 | 1.32 | 33.4 | 0.19 | 4.8 | 0.080 | 2.0 | 0.45 | 0.68 | 0.04 | 0.005 |
| $11 / 2$ | 1.42 | 36.1 | 1.90 | 48.3 | 0.24 | 6.1 | 0.130 | 3.8 | 0.84 | 1.26 | 0.08 | 0.011 |
| 2 | 1.86 | 47.1 | 2.38 | 60.3 | 0.26 | 6.6 | 0.150 | 3.8 | 1.16 | 1.74 | 0.14 | 0.019 |
| 3 | 2.92 | 74.2 | 3.50 | 88.9 | 0.29 | 7.4 | 0.180 | 4.6 | 1.97 | 2.94 | 0.35 | 0.047 |
| 4 | 3.84 | 97.5 | 4.50 | 114.3 | 0.33 | 8.4 | 0.220 | 5.6 | 2.91 | 4.35 | 0.60 | 0.080 |
| 6 | 5.97 | 152.0 | 6.63 | 168.4 | 0.33 | 8.4 | 0.220 | 5.6 | 4.39 | 6.57 | 1.45 | 0.194 |
| 8 | 7.97 | 202.0 | 8.63 | 219.2 | 0.33 | 8.4 | 0.220 | 5.6 | 5.78 | 8.65 | 2.59 | 0.348 |
| 10 | 10.10 | 256.0 | 10.75 | 273.1 | 0.33 | 8.4 | 0.220 | 5.6 | 7.26 | 10.90 | 4.15 | 0.555 |
| 12 | 12.10 | 307.0 | 12.75 | 323.9 | 0.33 | 8.4 | 0.220 | 5.6 | 8.65 | 13.00 | 5.96 | 0.797 |
| 14 | 13.30 | 339.0 | 14.00 | 355.6 | 0.33 | 8.4 | 0.220 | 5.6 | 9.52 | 14.30 | 7.26 | 0.971 |

[^4]
## Pressure Ratings ${ }^{(1)(2)}$

| Nominal Pipe Size in | Maximum Internal Pressure @ 175 ${ }^{\circ} \mathrm{F}$ psig |  |  | Maximum External Pressure psig ${ }^{(6)}$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Socket Pressure Fittings ${ }^{(3)}$ | FIg'd Pressure Fittings ${ }^{(4)}$ | Other Pressure Fittings ${ }^{(5)}$ | $75^{\circ} \mathrm{F}$ | $150{ }^{\circ} \mathrm{F}$ | $175{ }^{\circ} \mathrm{F}$ |
| 1 | 300 | 300 | N/A | 1,975 | 1,679 | 1,383 |
| $11 / 2$ | 300 | 300 | N/A | 1,034 | 878 | 775 |
| 2 | 275 | 200 | 125 | 1,013 | 861 | 759 |
| 3 | 200 | 150 | 125 | 467 | 397 | 350 |
| 4 | 150 | 150 | 100 | 425 | 361 | 319 |
| 6 | 150 | 150 | 100 | 218 | 185 | 163 |
| 8 | 150 | 150 | 100 | 69 | 59 | 52 |
| 10 | 150 | 150 | 75 | 34 | 29 | 26 |
| 12 | 150 | 150 | 75 | 43 | 36 | 32 |
| 14 | 125 | 150 | 75 | 16 | 14 | 12 |

${ }^{(1)}$ Static pressure ratings, typically created with use of a gear pump, turbine pump, centrifugal pump, or multiplex pump having 4 or more pistons, or elevation head.
${ }^{(2)}$ Specially fabricated higher pressure fittings are available on request. For insulated and/or heat traced temperatures, reduce pressure ratings by $30 \%$ for $175^{\circ} \mathrm{F}$ to $200^{\circ} \mathrm{F}$ operating temperatures. For compressible gases, consult the factory for pressure ratings. Centricast CL-2030 pipe and vinyl ester fittings can be used in insulated drainage and vent systems up to $200^{\circ} \mathrm{F}$ operating temperatures. Heat cured joints are highly recommended for all piping systems carrying fluids at temperatures above $120^{\circ} \mathrm{F}$.
${ }^{(3)}$ Socket elbows, tees reducers, couplings, flanges and nipples joined with WELDFAST CL-200 adhesive.
${ }^{(4)}$ Flanged elbows, tees, reducers, couplings and nipples assembled at factory.
${ }^{(5)}$ Laterals and crosses.
${ }^{(6)}$ Ratings shown are $50 \%$ of ultimate; 14.7 psi external pressure is equal to full vacuum.

Recommended Operating Ratings

| $\begin{aligned} & \text { Size } \\ & \text { in } \end{aligned}$ | Axial Tensile Loads Max. Ibs |  | Axial Compressive Loads Max. Ibs ${ }^{(1)(2)}$ |  | Bending Radius Min. ft Entire Temp. Range | Torque Max. ft lbs Entire Temp. Range | Parallel Plate Loading ASTM D2412 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{array}{r} \mathrm{Te} \\ 75^{\circ} \mathrm{F} \end{array}$ | rature $175^{\circ} \mathrm{F}$ | $\begin{aligned} & \text { Tem } \\ & 75^{\circ} \mathrm{F} \end{aligned}$ | ature $175^{\circ} \mathrm{F}$ |  |  | Stiffness Factor $\mathrm{in}^{3} / \mathrm{lbs} / \mathrm{in}^{2}$ | Pipe Stiffness psi | Hoop Modulus $\times 10^{6}$ psi |
| 1 | 2,000 | 1,600 | 2,400 | 1,600 | 66 | 43 | 143 | 4,225 | 2.0 |
| $11 / 2$ | 4,300 | 3,500 | 5,000 | 3,500 | 95 | 132 | 457 | 4,504 | 2.0 |
| 2 | 5,800 | 4,700 | 8,400 | 5,800 | 65 | 229 | 563 | 2,742 | 2.0 |
| 3 | 10,300 | 8,400 | 15,000 | 10,300 | 96 | 618 | 1,215 | 1,783 | 2.5 |
| 4 | 16,300 | 13,300 | 23,700 | 16,300 | 124 | 1,260 | 2,218 | 1,519 | 2.5 |
| 6 | 24,300 | 19,900 | 35,400 | 24,300 | 182 | 2,860 | 2,218 | 453 | 2.5 |
| 8 | 32,000 | 26,100 | 46,500 | 32,000 | 237 | 4,960 | 2,662 | 241 | 3.0 |
| 10 | 40,000 | 32,800 | 58,200 | 40,000 | 296 | 7,820 | 2,662 | 122 | 3.0 |
| 12 | 47,600 | 39,000 | 69,300 | 47,600 | 351 | 11,100 | 2,662 | 73 | 3.0 |
| 14 | 52,400 | 42,900 | 76,200 | 52,400 | 385 | 13,500 | 2,662 | 55 | 3.0 |

## Testing:

See Fiber Glass Systems' Socket Joint Installation Handbook. When possible, NOV Fiber Glass Systems' piping systems should be hydrostatically tested prior to beginning service. Care should be taken when testing to avoid water hammer. All anchors, guides and supports must be in place prior to testing the line.

Test pressure should not be more than $11 / 2$ times the working pressure of the piping system and never exceed $11 / 2$ times the
rated operating pressure of the lowest rated component in the system. Do not hydrotest until all support, anchors, and guides are properly installed.

## Water Hammer:

Care should be taken when designing an FRP piping system to eliminate sudden surges. Soft start pumps and slow actuating valves should be considered.

## Average Physical Properties

| Property | $75^{\circ} \mathrm{F} / 24^{\circ} \mathrm{C}$ |  |  |  | $150^{\circ} \mathrm{F} / 66^{\circ} \mathrm{C}$ |  |  |  | $175{ }^{\circ} \mathrm{F} / 80^{\circ} \mathrm{C}$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1"-11/2" |  | 2"-14" |  | 1"-11/2" |  | 2"-14" |  | 1"-11/2" |  | 2"-14" |  |
|  | psi | MPa | psi | MPa | psi | MPa | psi | MPa | psi | MPa | psi | MPa |
| Axial Tensile - ASTM D2105 |  |  |  |  |  |  |  |  |  |  |  |  |
| Ultimate Stress | 22,000 | 150 | 22,000 | 150 | 19,000 | 130 | 19,900 | 130 | 18,000 | 120 | 18,000 | 120 |
| Design Stress | 5,500 | 38 | 5,500 | 38 | 4,750 | 33 | 4,750 | 33 | 4,500 | 31 | 4,500 | 31 |
| Modulus of Elasticity | $2.1 \times 10^{6}$ | 14,500 | $2.1 \times 10^{6}$ | 14,500 | $1.8 \times 10^{6}$ | 12,400 | $1.8 \times 10^{6}$ | 12,400 | $1.8 \times 10^{6}$ | 12,400 | $1.8 \times 10^{6}$ | 12,400 |
| Poisson's Ratio v | 0.15 |  |  |  | 0.15 |  |  |  | 0.15 |  |  |  |
| Axial Compression - ASTM D695 |  |  |  |  |  |  |  |  |  |  |  |  |
| Ultimate Stress <br> Design Stress <br> Modulus of Elasticity | 26,000 | 180 | 32,000 | 220 | 24,000 | 170 | 30,000 | 210 | 18,000 | 120 | 22,000 | 150 |
|  | 6,500 | 45 | 8,000 | 55 | 6,000 | 41 | 7,500 | 52 | 4,500 | 31 | 5,550 | 38 |
|  | $3.3 \times 10^{6}$ | 22,800 | $2.6 \times 10^{6}$ | 17,900 | $2.9 \times 10^{6}$ | 20,000 | $2.3 \times 10^{6}$ | 15,900 | $2.8 \times 10^{6}$ | 19,300 | $2.2 \times 10^{6}$ | 15,100 |
| Beam Bending - ASTM D2925 |  |  |  |  |  |  |  |  |  |  |  |  |
| Ultimate Stress | 22,000 | 150 | 40,000 | 280 | 19,000 | 130 | 35,000 | 240 | 18,000 | 120 | 33,000 | 230 |
| Design Stress ${ }^{(1)}$ | 2.750 | 19 | 5,000 | 34 | 2.375 | 16 | 4.375 | 30 | 2.250 | 16 | 4,125 | 28 |
| Modulus of Elasticity (Long Term) | $3.3 \times 10^{6}$ | 22,800 | $3.3 \times 10^{6}$ | 22,800 | $2.9 \times 10^{6}$ | 20,000 | $2.9 \times 10^{6}$ | 20,000 | $2.8 \times 10^{6}$ | 19,300 | $2.8 \times 10^{6}$ | 19,300 |
| Hydrostatic Burst - ASTM D1599 |  |  |  |  |  |  |  |  |  |  |  |  |
| Ultimate Hoop Tensile Stress | 25.000 | 170 | 30,000 | 210 | 21,000 | 140 | 26,000 | 180 | 20,000 | 140 | 25,000 | 170 |
| Hoop Tensile Modulus of Elasticity | $3.0 \times 10^{6}$ | 20,700 | $3.2 \times 10^{6}$ | 22,100 | $2.6 \times 10^{6}$ | 17,900 | $2.8 \times 10^{6}$ | 19,300 | $2.5 \times 10^{6}$ | 17,200 | $2.7 \times 10^{6}$ | 18,600 |
| Hydrostatic Design - ASTM D2992, Procedure B-Hoop Tensile Stress Static 50 Year @ $175^{\circ} \mathrm{F}$ | - | - | - | - | - | - | - | - | 8,600 | 60 | 8,600 | 60 |
| ${ }^{(1)}$ Beam bending design stress is one-eighth of ultimate to allow for combined stress. Stress and modulus values can be interpolated between temperatures shown. |  |  |  |  |  |  |  |  |  |  |  |  |


| Coefficient of Linear Thermal Expansion - ASTM D696 | Non-Insulated Pipe: $8.9 \times 10^{-6} \mathrm{in} / \mathrm{in} /{ }^{\circ} \mathrm{F}$ Insulated Pipe: $\quad 10.0 \times 10^{-6} \mathrm{in} / \mathrm{in} /{ }^{\circ} \mathrm{F}$ | $\begin{aligned} & 16.1 \times 10^{-6} \mathrm{~mm} / \mathrm{mm}^{\circ} \mathrm{C} \\ & 18.1 \times 10^{-6} \mathrm{~mm} / \mathrm{mm} /{ }^{\circ} \mathrm{C} \end{aligned}$ |
| :---: | :---: | :---: |
| Thermal Conductivity | 0.07 BTU/hr-ft- ${ }^{\circ} \mathrm{F}$ | $0.04 \mathrm{~W} / \mathrm{m}-{ }^{\circ} \mathrm{C}$ |
| Specific Gravity - ASTM D792 | 1.56 |  |
| Flow Factor - SF / Hazen-Williams Coefficient | 150 |  |
| Absolute Surface Roughness | 0.00021 in | 0.0053 mm |
| Manning's Roughness Coefficient, n | 0.009 |  |

Properties of Pipe Sections Based on Minimum Reinforced Walls

| Size <br> in | Reinforcement <br> End Area in |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| 1 | 0.31 | Reinforcement <br> Moment of Inertia in | Reinforcement <br> Section Modulus in | Nominal Wall <br> End Area in |
| $1 / 2$ | 0.72 | 0.06 | 0.09 | 0.67 |
| 2 | 1.05 | 0.28 | 0.30 | 1.25 |
| 3 | 1.88 | 0.65 | 0.55 | 1.73 |
| 4 | 2.96 | 2.59 | 1.48 | 2.92 |
| 6 | 4.43 | 6.79 | 3.02 | 4.32 |
| 8 | 5.81 | 22.70 | 6.86 | 6.53 |
| 10 | 7.28 | 51.30 | 11.90 | 8.60 |
| 12 | 8.66 | 100.00 | 18.80 | 10.80 |
| 14 | 9.52 | 226.00 | 26.70 | 12.90 |

ASTM D2997 Designation Codes

| $1 "-1 \frac{1}{2 \prime}$ | RTRP-22BS-3446 |
| :---: | :--- |
| $2 "-6 "$ | RTRP-22BS-4446 |
| $8 "$ | RTRP-22BS-4445 |
| $10 "-12 "$ | RTRP-22BS-4444 |
| $14 "$ | RTRP-22BS-4443 |

## Thermal Expansion

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To perform a thermal analysis, the following information is required:

1. Isometric layout of piping system
2. Physical and material properties of pipe
3. Design temperatures
4. Installation temperature (final tie-in temperature)
5. Terminal equipment load limits
6. Support movements

A comprehensive review of temperature effects on fiberglass pipe may be found in NOV Fiber Glass Systems' Engineering and Piping Design Guide.

| Unrestrained Thermal Expansion Uninsulated Pipe |  |
| :---: | :---: |
| Change in Temperature <br> ${ }^{\circ} \mathrm{F}$ | Pipe Change in Length <br> in/100 ft |
| 25 | 0.27 |
| 50 | 0.53 |
| 75 | 0.80 |
| 100 | 1.07 |
| 125 | 1.34 |
| 150 | 1.60 |
| 175 | 1.87 |
| 200 | 2.21 |


| Elbow Strength |  |  |  |
| :---: | :---: | :---: | :---: |
| Allowable Bending Moment $-90^{\circ}$ Elbow |  |  |  |
| Nominal <br> Pipe <br> Size in | Allowable <br> Moment <br> ft/lbs | Nominal <br> Pipe <br> Size in | Allowable <br> Moment <br> ft/lbs |
| 1 | 100 | 6 | 1,650 |
| $1 / 2$ | 150 | 8 | 2,850 |
| 2 | 225 | 10 | 4,500 |
| 3 | 475 | 12 | 6,500 |
| 4 | 650 | 14 | 10.000 |

Restrained Thermal End Loads and Guide Spacing

| Operating Temperature ${ }^{\circ} \mathrm{F}$ (Based on Installation Temperature of $75^{\circ} \mathrm{F}$ ) |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 100 |  | 125 |  | 150 |  | 175 |  | 200 |  |
| $\begin{aligned} & \text { Size } \\ & \text { in } \end{aligned}$ | Guide Spacing ft | Thermal End Load lbs | Guide Spacing ft | Thermal End Load lbs | Guide Spacing ft | Thermal End Load lbs | Guide Spacing ft | Thermal End Load lbs | Guide Spacing ft | Thermal End Load lbs |
| 1 | 7.2 | 248 | 5.1 | 473 | 4.2 | 675 | 3.6 | 869 | 3.2 | 776 |
| $11 / 2$ | 10.4 | 578 | 7.3 | 1,102 | 6.0 | 1,572 | 5.2 | 2,024 | 4.6 | 1,807 |
| 2 | 14.7 | 655 | 10.4 | 1,258 | 8.5 | 1,809 | 7.4 | 2,307 | 6.6 | 2,621 |
| 3 | 21.9 | 1,173 | 15.5 | 2,253 | 12.7 | 3,239 | 11.0 | 4,130 | 9.8 | 4,694 |
| 4 | 28.3 | 1,849 | 20.0 | 3,550 | 16.3 | 5,103 | 14.1 | 6,508 | 12.6 | 7,395 |
| 6 | 42.3 | 2,767 | 29.9 | 5,312 | 24.4 | 7,636 | 21.1 | 9,739 | 18.9 | 11,067 |
| 8 | 55.5 | 3,631 | 39.2 | 6,971 | 32.0 | 10,021 | 27.7 | 12,780 | 24.8 | 14,523 |
| 10 | 69.5 | 4,549 | 49.1 | 8,733 | 40.1 | 12,554 | 34.7 | 16,011 | 31.1 | 18,195 |
| 12 | 82.6 | 5,413 | 58.4 | 10,392 | 47.7 | 14,939 | 41.3 | 19,052 | 37.0 | 21,650 |
| 14 | 90.9 | 5,953 | 64.3 | 11,429 | 52.5 | 16,429 | 45.4 | 20,953 | 40.6 | 23,810 |

## Supports

Proper pipe support spacing depends on the temperature and weight of the fluid in the pipe. The support spacing table is based on unrestrained continuous beam theory using the pipe bending modulus derived from long-term beam bending tests. The maximum spans lengths were developed to ensure a design that limits mid-span deflection to $1 / 2$ inch and dead weight bending to ${ }^{1 / 8}$ of the ultimate bending stress. Any additional loads on the piping system such as insulation, wind, seismic, etc. requires further consideration. Restrained (anchored) piping systems operating at elevated temperatures may result in guide spacing requirements that are shorter than unrestrained piping systems. In this case, the maximum guide spacing governs the support span requirements for the system. Pipe spans near elbows require special attention. Both supported and unsupported elbows are considered in the following tables and must be followed to properly design the piping system.

There are seven basic rules to follow when designing piping system supports:

1. Do not exceed the recommended support span.
2. Support valves and heavy in-line equipment independently. This applies to both vertical and horizontal piping.
3. Protect pipe from external abrasion at supports.
4. Avoid point contact loads.
5. Avoid excessive bending. This applies to handling, transporting, initial layout, and final installed position.
6. Avoid excessive vertical run loading. Vertical loads should be supported sufficiently to minimize bending stresses at outlets or fittings.
7. Provide adequate axial and lateral restraint to ensure line stability during rapid changes in flow.

## Maximum Support Spacing for Uninsulated Pipe ${ }^{(1)}$

| Pipe <br> Size in | Continuous Spans of Pipe ft. ${ }^{(2)}$ |  |  |
| :---: | :---: | :---: | :---: |
|  | $\mathbf{1 5 0}^{\circ} \mathrm{F}$ | $\mathbf{1 7 5}{ }^{\circ} \mathbf{F}$ |  |
| 1 | 13.5 | 13.1 | 13.0 |
| $11 / 2$ | 16.4 | 15.9 | 15.8 |
| 2 | 17.9 | 17.3 | 17.2 |
| 3 | 21.0 | 20.4 | 20.2 |
| 4 | 23.7 | 22.9 | 22.7 |
| 6 | 26.7 | 25.8 | 25.6 |
| 8 | 28.8 | 27.9 | 27.7 |
| 10 | 30.7 | 29.7 | 29.4 |
| 12 | 32.2 | 31.1 | 30.9 |
| 14 | 33.0 | 31.9 | 31.7 |

${ }^{(1)}$ Consult factory for insulated pipe support spacing and
operating temperatures between $175^{\circ} \mathrm{F}$ and $200^{\circ} \mathrm{F}$.
${ }^{(2}$ Maximum mid-span deflection $1 / 2$ " with a specific gravity of 1.0

## Support Spacing vs. Specific Gravity

| Specific Gravity | 3.00 | 2.00 | 1.50 | 1.25 | 1.00 | 0.75 | Gas/Air |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Multiplier | 0.76 | 0.84 | 0.90 | 0.95 | 1.00 | 1.07 | 1.40 |

Example: 6" pipe @ $150^{\circ}$ F with 1.5 specific gravity fluid, maximum support spacing $=25.8 \times 0.90=23.2$

Adjustment Factors for Various Spans With Unsupported Fitting at Change in Direction

Adjustment Factors for Various Spans With Supported Fitting at Change in Direction




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## CENTRICAST'" CL-2030 Piping System

## Specification Guide

## SECTION 1 - Scope

This section covers the use of fiberglass reinforced plastic (FRP) pipe for chemical process and chemical handling up to $200^{\circ} \mathrm{F}$ and up to 150 psig pressure.

The piping shall be furnished and installed complete with all fittings, joining materials, supports, specials, and other necessary appurtenances.

## SECTION 2 - General Conditions

2.01 Coordination - Material furnished and work performed under this section shall be coordinated with related work and equipment specified under other sections.

| Valves | Section |
| :--- | :--- |
| Supports | Section |
| Equipment | Section |

2.02 Governing Standards - Except as modified or supplemented herein, all materials and construction methods shall comply with the applicable provisions of the following specifications and be tested using the following standards:

## Standard Specifications

| ASTM <br> D2997 | Standard Specification for Centrifugal Cast"Fi- <br> berglass" (Glass-Fiber-Reinforced Thermosetting) <br> Resin Pipe |
| :--- | :--- |
| AWWA <br> M45 | Fiberglass Pipe Design |
| ASTM <br> D5685 | Standard Specification for "Fiberglass" (Glass- <br> Fiber-Reinforced-Thermosetting Resin) Pressure <br> Pipe Fittings |
| ASTM <br> D4024 | Standard Specification for Reinforced Thermoset- <br> ting Resin (RTR) Flanges |

## Standard Test Methods

| ASTM <br> D2992 | Standard Practice for Obtaining Hydrostatic or <br> Pressure Design Basis for "Fiberglass" (Glass- <br> Fiber-Reinforced Thermosetting Resin) Pipe and <br> Fittings |
| :--- | :--- |
| ASTM <br> D1599 | Standard Test method for Short-Time Hydraulic <br> Failure Pressure of Plastic Pipe, Tubing and Fit- <br> tings |
| ASTM <br> D2105 | Standard Test Method for Longitudinal Tensile <br> Properties of "Fiberglass" (Glass-Fiber-Reinforced <br> Thermosetting Resin) Pipe and Tube |
| ASTM <br> D2412 | Standard Test Method for Determination of Ex- <br> ternal Loading Characteristics of Plastic Pipe by <br> Parallel-Plate Loading |
| ASME <br> B31.3 | Process Piping |

### 2.03 ASTM D2997 Designation Codes <br> 1"-11/2" RTRP-22BS-3446 <br> 2"-6" RTRP-22BS-4446 <br> 10"-12" RTRP-22BS-4444 <br> 14" RTRP-22BS-4443

Mechanical properties cell classifications shown are minimums.
2.04 Operating Conditions - In addition to the above minimum design requirements, the system shall meet the following minimum operating conditions:
a. Operating Pressure
b. Operating Temperature
c. Fluid Conveyed
d. Test Pressure
2.05 Quality Assurance - Pipe manufacturer's quality program shall be in compliance with ISO 9001.
2.06 Delivery, Storage and Handling - Pipe and fittings shall be protected from damage due to impact and point loading. Pipe shall be properly supported to avoid damage due to flexural strains. The contractor shall not allow dirt, debris, or other extraneous materials to get into pipe and fittings. All factory machined areas shall be protected from sunlight until installed.
2.07 Acceptable Manufacturers - NOV Fiber Glass Systems (918) 245-6651 or approved equal.

## SECTION 3 - Materials and Construction

3.01 1"-14" Pipe - The pipe shall be manufactured by the centrifugal casting process using premium grade vinyl ester thermosetting resin to impregnate woven glass filaments. Pipe shall be heat cured and the degree of cure shall be confirmed using a Differential Scanning Calorimeter. All pipe shall have a $100 \%$ resin corrosion barrier and the cured thickness shall be 100 mils nominal.

All pipe shall have a resin-rich reinforced 10 mil nominal exterior layer with UV (ultraviolet) inhibitor.

The pipe shall have a minimum design pressure rating of 150 psig at $175^{\circ} \mathrm{F}$ following ASTM D2992 Procedure B.

| Minimum Reinforced Wall Thickness |  |
| :---: | :---: |
| $1 "$ | 0.095 inches |
| $11 / 2 "$ | 0.120 inches |
| $2 "$ | 0.150 inches |
| $3 "$ | 0.180 inches |
| $4 "-14 "$ | 0.220 inches |

3.02 Flanges and Fittings - All fittings shall be manufactured either by compression molding or contact molding. Fitting joints shall be either adhesive bonded socket or flanged. Flanges shall have ANSI B16.5 Class 150 bolt hole patterns.
3.03 Adhesive - Adhesive shall be manufacturer's standard for the piping system specified. All adhesive bonded joints shall be cured according to the manufacturer's instructions for maximum strength and corrosion resistance.
3.04 Gaskets - Gaskets shall be ${ }^{3} / 16^{\prime \prime}$ thick, 60-70 durometer full-face type suitable for the service shown on the drawings and as recommended in the manufacturer's standard installation procedures.
3.05 Bolts, Nuts and Washers - ASTM F593, 304 stainless steel hex head bolts shall be supplied. Two each SAE size washers shall be supplied on all nuts and bolts.
3.06 Acceptable Products - Centricast CL-2030 as manufactured by NOV Fiber Glass Systems or approved equal.

## SECTION 4 - Installation and Testing

4.01 Training and Certification - All joints installed or constructed in the field shall be assembled by employees of the contractor who have been trained by the pipe manufacturer. The pipe manufacturer or their authorized representative shall train the contractor's employees in the proper joining and assembly procedures required for the project, including hands-on participation by the contractor's employees. Each bonder shall fabricate one pipe-to-pipe and one pipe-to-fitting joint that shall pass the minimum pressure test for the application as stated in Section 2.04.d without leaking.

Only bonders who have successfully completed the pressure test shall bond pipe and fittings.

Certification by the manufacturer shall be in compliance with ASME B31.3 Section A328.2.
4.02 Pipe Installation - Pipe shall be installed as specified and indicated on the drawings and in accordance with the manufacturer's current published installation procedures.
4.03 Testing - A hydrostatic pressure test shall be conducted on the completed piping system. The pipe shall be subjected to a steady pressure at $11 / 2$ times the design operating pressure as stated in Section 2.04a. The pressure shall be held on the system for a minimum of 1 hour and the line inspected for leaks.

The test pressure should not exceed $11 / 2$ times the maximum rated operating pressure for the lowest rated element in the system.

The system shall be filled with water at the lowest point and air bled off from all the highest points. Systems shall be brought up to test pressure slowly to prevent water hammer or over pressurization.

All pipe joints shall be water tight. All joints that are found to leak by observation or during testing shall be repaired by the contractor and retested.

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## Z-Core ${ }^{\circledR}$ Product Data

Applications<br>- Sulfuric Acid<br>- Hydrochloric Acid<br>- Solvents<br>- Caustics<br>- Process Drains

Materials and Construction

Z-Core pipe is a centrifugally cast fiberglass pipe with a 100 mil resin-rich liner and is available in 1" through 8 " diameters. The pipe is rated for temperatures to $275^{\circ} \mathrm{F}$ and for pressures to 150 psig (higher pressures available on request).

Z-Core has a resin-rich 10 mil reinforced corrosion barrier on the outside surface which provides superior resistance to exterior corrosion. The resin-rich exterior also offers protection against "fiber blooming" caused by ultraviolet radiation. Pipe and fittings are warranted against reduction of physical and corrosion ratings due to ultraviolet exposure for a period of 15 years.

## Fittings

Fittings are manufactured with the same chemical/temperature capabilities as the pipe. Depending on the particular part and size, fittings will be compression molded, contact molded, hand fabricated or filament wound.

Joining
Systems

## Socket Joint

Adhesive bonded straight socket joint with positive stops.
This is the standard for Centricast piping systems.


## Nominal Dimensional Data

| Pipe Size (In) | I.D. |  | O.D. |  | Wall <br> Thickness |  | Reinforcement Thickness |  | Weight |  | Capacity |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | (In) | (mm) | (In) | (mm) | (In) | (mm) | (In) | (mm) | (Lbs/Ft) | (kg/m) | (Gal/Ft) | ( $\mathrm{Ft} 3 / \mathrm{Ft}$ ) |
| 1 | 0.92 | 23.2 | 1.315 | 33.4 | 0.20 | 5.1 | 0.09 | 2.3 | 0.67 | 0.99 | 0.03 | 0.005 |
| $11 / 2$ | 1.40 | 35.6 | 1.900 | 48.3 | 0.25 | 6.4 | 0.14 | 3.6 | 1.24 | 1.84 | 0.08 | 0.011 |
| 2 | 1.88 | 47.6 | 2.375 | 60.3 | 0.25 | 6.4 | 0.14 | 3.6 | 1.59 | 2.36 | 0.14 | 0.019 |
| 3 | 3.00 | 76.2 | 3.500 | 88.9 | 0.25 | 6.4 | 0.14 | 3.6 | 2.43 | 3.62 | 0.37 | 0.049 |
| 4 | 3.94 | 100.1 | 4.500 | 114.3 | 0.28 | 7.1 | 0.17 | 4.3 | 3.54 | 5.26 | 0.63 | 0.085 |
| 6 | 5.88 | 149.2 | 6.625 | 168.3 | 0.38 | 9.5 | 0.27 | 6.7 | 7.02 | 10.43 | 1.41 | 0.189 |
| 8 | 7.79 | 197.7 | 8.625 | 219.1 | 0.42 | 10.7 | 0.31 | 7.9 | 10.32 | 15.34 | 2.48 | 0.331 |

[^5]| Properties of Pipe Sections Based on Minimum Reinforced Walls |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Size } \\ & \text { (In) } \end{aligned}$ | Reinforcement End Area( $\ln ^{2}$ ) | Reinforcement Moment of Inertia ( $\mathbf{I n}^{4}$ ) | Reinforcement Section Modulus ( $\mathrm{In}^{3}$ ) | Nominal Wall <br> End Area ( $\mathrm{In}^{2}$ ) |
| 1 | 0.35 | 0.07 | 0.10 | 0.70 |
| $11 / 2$ | 0.77 | 0.30 | 0.32 | 1.30 |
| 2 | 0.98 | 0.62 | 0.52 | 1.67 |
| 3 | 1.48 | 2.09 | 1.19 | 2.55 |
| 4 | 2.31 | 5.43 | 2.41 | 3.71 |
| 6 | 5.39 | 27.26 | 8.23 | 7.46 |
| 8 | 8.10 | 70.08 | 16.25 | 10.83 |

## Average Physical Properties

| Property | $75^{\circ} \mathrm{F} / 24^{\circ} \mathrm{C}$ |  |  |  | $250{ }^{\circ} \mathrm{F} / 121^{\circ} \mathrm{C}$ |  |  |  | $275{ }^{\circ} \mathrm{F} / 135^{\circ} \mathrm{C}$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $1 "$ |  | 11/2"-8" |  | 1" |  | 11/2"-8" |  | 1" |  | 11/2"-8" |  |
|  | psi | MPa | psi | MPa | psi | MPa | psi | MPa | psi | MPa | psi | MPa |
| Axial Tensile - ASTM D2105 Ultimate Stress Modulus of Elasticity | $23,000$ | 159 | $\begin{array}{r} 29,000 \\ 1.9 \times 10^{6} \end{array}$ | $\begin{array}{r} 200 \\ 13,100 \end{array}$ | $15,000$ | 100 | $\begin{array}{r} 19,000 \\ 1.6 \times 10^{6} \end{array}$ | $\begin{array}{r} 131 \\ 11,000 \end{array}$ | $13,500$ | 93 | $\begin{array}{r} 17,500 \\ 1.5 \times 10^{6} \end{array}$ | $\begin{array}{r} 121 \\ 10,300 \end{array}$ |
| Poisson's Ratio v | 0.15 |  |  |  | 0.15 |  |  |  | 0.15 |  |  |  |
| Axial Compression - ASTM D695 Ultimate Stress Modulus of Elasticity | $\begin{array}{r} 20,000 \\ 4.7 \times 10^{6} \end{array}$ | $\begin{array}{r} 138 \\ 32,400 \end{array}$ | $\begin{array}{r} 26,000 \\ 6.4 \times 10^{6} \end{array}$ | $\begin{array}{r} 179 \\ 44,126 \end{array}$ | $\begin{array}{r} 21,000 \\ 1.4 \times 10^{6} \end{array}$ | $\begin{array}{r} 145 \\ 9,653 \end{array}$ | $\begin{array}{r} 22,000 \\ 1.8 \times 10^{6} \end{array}$ | $\begin{array}{r} 152 \\ 12,411 \end{array}$ | $\begin{array}{r} 20,000 \\ 1.0 \times 10^{6} \end{array}$ | $\begin{array}{r} 138 \\ 6,895 \end{array}$ | $\begin{array}{r} 21,000 \\ 1.1 \times 10^{6} \end{array}$ | $\begin{array}{r} 145 \\ 7.860 \end{array}$ |
| Beam Bending - ASTM D2925 Ultimate Stress Modulus of Elasticity (Long Term) | $\begin{array}{r} 50,000 \\ 6.0 \times 10^{5} \end{array}$ | $\begin{array}{r} 345 \\ 4,137 \end{array}$ | $\begin{array}{r} 42,000 \\ 4.0 \times 10^{6} \end{array}$ | $\begin{array}{r} 290 \\ 27,579 \end{array}$ | $\begin{array}{r} 32,000 \\ 1.8 \times 10^{5} \end{array}$ | $\begin{array}{r} 221 \\ 1,241 \end{array}$ | $\begin{array}{r} 27,000 \\ 1.2 \times 10^{6} \end{array}$ | $\begin{array}{r} 186 \\ 8,274 \end{array}$ | $\begin{array}{r} 29,000 \\ 1.2 \times 10^{5} \end{array}$ | 200 827 | $\begin{array}{r} 25,000 \\ 8.0 \times 10^{5} \end{array}$ | $\begin{array}{r} 172 \\ 5,516 \end{array}$ |
| Hydrostatic Burst - ASTM D1599 Ultimate Hoop Tensile Stress Hoop Tensile Modulus of Elasticity | 28,000 | 193 | $\begin{array}{r} 11,000 \\ 2.1 \times 10^{6} \end{array}$ | $\begin{array}{r} 76 \\ 14,686 \end{array}$ |  | NA |  |  |  | NA |  |  |


| Thermal Expansion Coefficient - ASTM D696 | Non-Insulated Pipe: Insulated Pipe: | $\begin{array}{r} 9.2 \times 10^{-6} \mathrm{in} / \mathrm{in} /{ }^{\circ} \mathrm{F} \\ 1.04 \times 10^{-5} \mathrm{in} / \mathrm{in} /{ }^{\circ} \mathrm{F} \end{array}$ | $\begin{aligned} & 1.7 \times 10^{-5} \mathrm{~mm} / \mathrm{mm}^{\circ} \mathrm{C} \\ & 1.9 \times 10^{-5} \mathrm{~mm} / \mathrm{mm} /{ }^{\circ} \mathrm{C} \end{aligned}$ |
| :---: | :---: | :---: | :---: |
| Thermal Conductivity | $0.09 \mathrm{BTU} / \mathrm{ft}-\mathrm{hr}-{ }^{\circ} \mathrm{F}$ |  | $0.16 \mathrm{~W} / \mathrm{m}-{ }^{\circ} \mathrm{C}$ |
| Specific Gravity - ASTM D792 | 2.20 |  |  |
| Hazen-Williams Coefficient | 150 |  |  |
| Absolute Surface Roughness | 0.00021 in |  | 0.0053 mm |
| Manning's Roughness Coefficient, n | 0.009 |  |  |

## Testing:

## See Pipe Installation Handbook for Hydrostatic Testing and System Startup.

When possible, NOV Fiber Glass Systems piping systems should be hydrostatically tested prior to being put into service. Care should be taken when testing, as in actual service, to avoid water hammer. All anchors, guides and supports must be in place prior to testing the line.

Test pressure should not be more than $11 / 2$ times the working pressure of the piping system and never exceed $11 / 2$ times the rated pressure of the lowest rated component in the system.

## Steam Cleaning:

Z-CORE piping systems can be steam cleaned under the following conditions:

1. The piping must be open-ended to prevent pressure buildup.
2. A maximum steam pressure of 45 psig must not be exceeded. (Temperature not to exceed $275^{\circ}$ F.)
3. To prevent pipe sagging at the steam cleaning temperature, support spacing must be adjusted for $275^{\circ} \mathrm{F}$ service.

## Pressure Ratings ${ }^{(1)}$

| Pipe Size In | Max Internal Pressure @ 275 ${ }^{\circ} \mathrm{F}$ (psig) |  |  | Maximum External Pressure (psig) ${ }^{(5)}$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Socket Pressure Fittings ${ }^{(2)}$ | Fig'd Pressure Fittings ${ }^{(3)}$ | Other Pressure Fittings ${ }^{(4)}$ | $75^{\circ} \mathrm{F}$ | $200^{\circ} \mathrm{F}$ | $275{ }^{\circ} \mathrm{F}$ |
| 1 | 275 | 275 | NA | 2,125 | 1,700 | 1,381 |
| $11 / 2$ | 275 | 275 | 125 | 2,065 | 1,652 | 1,342 |
| 2 | 275 | 275 | 125 | 1,170 | 931 | 763 |
| 3 | 175 | 150 | 100 | 335 | 267 | 219 |
| 4 | 150 | 150 | 100 | 225 | 179 | 147 |
| 6 | 150 | 150 | 100 | 62 | 49 | 40 |
| 8 | 150 | 150 | 100 | 45 | 36 | 29 |

${ }^{(1)}$ Specially fabricated higher pressure fittings are available on request. Consult the factory for compressible gases. Heat cured joints are recommended for all piping systems carrying fluids at temperatures above $120^{\circ} \mathrm{F}$.
${ }^{(4)}$ Laterals and crosses.
${ }^{(5)}$ Ratings shown are $50 \%$ of ultimate; 14.7 psi external pressure is equal to full vacuum.
$N A=$ Not available at time of printing.
${ }^{(2)}$ Socket elbows, tees reducers, couplings, flanges and nipples joined with WELDFAST ZC-275 adhesive.
${ }^{(3)}$ Flanged elbows, tees, reducers, couplings and nipples assembled at factory.

ASTM D2997 Designation Codes:

| $1 "$ | RTRP-21CO-3406 |
| :---: | :--- |
| $11 / 2^{\prime \prime}-6 "$ | RTRP-21CO-1446 |
| $8 "$ | RTRP-21CO-1445 |

Recommended Operating Ratings

| $\begin{aligned} & \text { Size } \\ & \text { In } \end{aligned}$ | Axial Tensile Loads Max. (Lbs) |  | Axial Compressive <br> Loads Max. (Lbs) ${ }^{(1)}$ |  | Bending Radius Min. (Ft) Entire Temp. Range | Torque Max. (Ft Lbs) Entire Temp. Range | Parallel Plate Loading ASTM D2412 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Temperature |  | Temperature |  |  |  | Stiffness Factor $\ln ^{3} / \mathrm{Lbs} / \mathrm{In}^{2}$ | Pipe Stiffness (psi) | Hoop Modulus $\times 10^{6}$ (psi) |
| 1 | 1,990 | 1,200 | 1,730 | 1,700 | 50 | 41 | 170 | 4,968 | 2.8 |
| $11 / 2$ | 5,610 | 3,400 | 5,030 | 4,100 | 60 | 132 | 869 | 8,558 | 3.8 |
| 2 | 7,130 | 4,300 | 6,390 | 5,200 | 75 | 216 | 2,287 | 10,997 | 10.0 |
| 3 | 10,710 | 6,500 | 9,610 | 7,800 | 111 | 497 | 2,515 | 3,560 | 11.0 |
| 4 | 16,770 | 10,100 | 15,030 | 12,100 | 143 | 1,005 | 4,094 | 2,708 | 10.0 |
| 6 | 39,080 | 23,580 | 35,040 | 28,300 | 210 | 3,373 | 10,080 | 2,104 | 6.5 |
| 8 | 58,710 | 35,400 | 52,640 | 42,500 | 274 | 6,771 | 10,179 | 951 | 4.1 |
| ${ }^{(1)}$ Compressive loads are for short columns only. |  |  |  |  |  |  |  |  |  |

## Water Hammer:

Care should be taken when designing an FRP piping system to eliminate sudden surges. Soft start pumps and slow actuating valves should be considered.

| Pipe Lengths Available* |  |
| :---: | :---: |
| Size (In) | Random Length (Ft) |
| $1-8$ | 20 |
| *Pipe is offered in random lengths from <br> 18.0 to 20.4 feet long. |  |

## Supports

Proper pipe support spacing depends on the temperature and weight of the fluid in the pipe. The support spacing table is based on unrestrained continuous beam theory using the pipe bending modulus derived from long-term beam bending tests. The maximum spans lengths were developed to ensure a design that limits mid-span deflection to $1 / 2$ inch and dead weight bending to $1 / 8$ of the ultimate bending stress. Any additional loads on the piping system such as insulation, wind, seismic, etc. requires further consideration. Restrained (anchored) piping systems operating at elevated temperatures may result in guide spacing requirements that are shorter than unrestrained piping systems. In this case, the maximum guide spacing governs the support span requirements for the system. Pipe spans near elbows require special attention. Both supported and unsupported elbows are considered in the following tables and must be followed to properly design the piping system.

There are seven basic rules to follow when designing piping
5. Avoid excessive bending. This applies to handling, transporting, initial layout, and final installed position.
6. Avoid excessive vertical loading to minimize bending stresses on pipe and fittings.
7. Provide adequate axial and lateral restraint to ensure line stability during rapid changes in flow.

| Maximum Support Spacing for Uninsulated Pipe ${ }^{(1)}$ |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| (In.) | Continuous Spans of Pipe (Ft.) ${ }^{(2)}$ |  |  | Gas $75^{\circ} \mathrm{F}$ |
|  | $75^{\circ} \mathrm{F}$ | $250^{\circ} \mathrm{F}$ | $275{ }^{\circ} \mathrm{F}$ |  |
| 1 | 8.2 | 6.1 | 5.5 | 9.0 |
| $11 / 2$ | 16.3 | 12.1 | 10.9 | 18.2 |
| 2 | 17.7 | 13.1 | 11.9 | 20.4 |
| 3 | 20.3 | 15.0 | 13.6 | 24.9 |
| 4 | 22.9 | 16.9 | 15.3 | 28.8 |
| 6 | 28.4 | 21.0 | 19.0 | 36.2 |
| 8 | 31.7 | 23.5 | 21.2 | 41.8 |
| ${ }^{(1)}$ Consult factory for insulated pipe support spacing. <br> ${ }^{(2)}$ Maximum mid-span deflection $1 / 2^{\prime \prime}$ with a specific gravity of 1.0 |  |  |  |  | system supports:

1. Do not exceed the recommended support span.
2. Support heavy valves and in-line equipment independently.
3. Protect pipe from external abrasion at supports.
4. Avoid point contact loads.

## Support Spacing vs. Specific Gravity

| Specific Gravity | 2.00 | 1.50 | 1.25 | 1.00 | 0.75 |
| :--- | :--- | :--- | :--- | :--- | :--- |
| Multiplier | 0.80 | 0.93 | 0.96 | 1.00 | 1.04 |

Example: $6^{\prime \prime}$ pipe @ $250^{\circ} \mathrm{F}$ with 1.5 specific gravity fluid, maximum support spacing $=21 \times 0.93=19.5 \mathrm{ft}$.


Adjustment Factors for Various Spans With Supported Fitting at Change in Direction


## Thermal Expansion

The effects of thermal gradients on piping systems may be significant and should be considered in every piping system stress analysis. Pipe line movements due to thermal expansion or contraction may cause high stresses or even buckle a pipe line if improperly restrained. Several piping system designs are used to manage thermal expansion and contraction in above ground piping systems. They are listed below according to economic preference:

1. Use of inherent flexibility in directional changes
2. Restraining axial movements and guiding to prevent buckling
3. Use expansion loops to absorb thermal movements
4. Use mechanical expansion joints to absorb thermal movements

To perform a thermal analysis the following information is required:

1. Isometric layout of piping system
2. Physical and material properties of pipe
3. Design temperatures
4. Installation temperature (final tie in temperature)
5. Terminal equipment load limits
6. Support movements

A comprehensive review of temperature effects on fiberglass pipe may be found in NOV Fiber Glass Systems' Engineering and Piping Design Guide.

| Unrestrained Thermal Expansion Uninsulated Pipe ${ }^{(1)}$ <br> Change in Temperature <br> ${ }^{\circ}$ F |  |
| :---: | :---: |
| 25 | Pipe Change in Length <br> $(\mathbf{I n} / \mathbf{1 0 0 ~ F t )}$ |
| 50 | 0.28 |
| 75 | 0.55 |
| 100 | 0.83 |
| 125 | 1.10 |
| 150 | 1.38 |
| 175 | 1.66 |
| 200 | 1.93 |
| 225 | 2.21 |
| 250 | 2.48 |
| 275 | 2.76 |

## Restrained Thermal End Loads and Guide Spacing

| Size <br> (In) | Operating Temperature ${ }^{\circ} \mathrm{F}$ (Based on installation temperature of $75^{\circ} \mathrm{F}$ ) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 100 |  | 150 |  | 200 |  | 250 |  | 275 |  |
|  | Guide Spacing (Ft) | Thermal End Load (Lbs) | Guide Spacing <br> (Ft) | Thermal End Load (Lbs) | Guide Spacing (Ft) | Thermal End Load (Lbs) | Guide Spacing (Ft) | Thermal End Load (Lbs) | Guide Spacing (Ft) | Thermal End Load (Lbs) |
| 1 | 2.7 | 335 | 1.5 | 767 | 1.2 | 904 | 1.0 | 781 | 0.9 | 637 |
| $11 / 2$ | 8.5 | 1,026 | 4.9 | 2,388 | 3.8 | 2,813 | 3.2 | 2,243 | 3.0 | 1,567 |
| 2 | 10.8 | 1,302 | 6.2 | 3,032 | 4.8 | 3,572 | 4.1 | 2,849 | 3.8 | 1,990 |
| 3 | 16.2 | 1,958 | 9.4 | 4,558 | 7.3 | 5,370 | 6.1 | 4,283 | 5.7 | 2,991 |
| 4 | 20.9 | 3,064 | 12.1 | 7,133 | 9.4 | 8,404 | 7.9 | 6,702 | 7.4 | 4,681 |
| 6 | 30.7 | 7,141 | 17.7 | 16,626 | 13.7 | 19,589 | 11.6 | 15,622 | 10.9 | 10,910 |
| 8 | 40.1 | 10,728 | 23.2 | 24,976 | 18.0 | 29,428 | 15.2 | 23,468 | 14.2 | 16,390 |


| Allowable Bending Moment $\mathbf{9 0}^{\circ}$ Elbow |  |
| :---: | :---: |
| Pipe Size (In) | Allowable Moment (Ft /Lbs) |
| 1 | 100 |
| $11 / 2$ | 150 |
| 2 | 225 |
| 3 | 475 |
| 4 | 650 |
| 6 | 1,650 |
| 8 | 2,850 |


| QUALITY MANAGEMENT SYSTEM <br> CERTIFIED BY DNV <br> ISO 9001:2008 <br> LITTLE ROCK, AR <br> SAND SPRINGS, OK <br> SUZHOU, CHINA <br> FIBER GLASS SYSTEMS${ }^{-1}$ |
| :---: |

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## Specification Guide

## SECTION 1 - Scope

This section covers the use of fiberglass reinforced plastic (FRP) pipe for severe chemical process and chemical handling applications up to $275^{\circ} \mathrm{F}$ and 150 psig steady pressure.

The piping system shall be furnished and installed complete with all fittings, joining materials, supports, specials, and other necessary appurtenances.

## SECTION 2 - General Conditions

2.01 Coordination - Material furnished and work performed under this section shall be coordinated with related work and equipment specified under other sections.

| Valves | Section |
| :--- | :--- |
| Supports | Section |
| Equipment | Section |

2.02 Governing Standards - Except as modified or supplemented herein, all materials and construction methods shall comply with the applicable provisions of the following specifications and be tested using the following standards:

## Standard Specifications

| ASTM <br> D2997 | Standard Specification for Centrifugal Cast Pipe |
| :--- | :--- |
| ASTM <br> D5685 | Standard Specification for "Fiberglass" (Glass- <br> Fiber-Reinforced-Thermosetting Resin) Pressure <br> Pipe Fittings |
| ASTM <br> D4024 | Standard Specification for Reinforced Thermoset- <br> ting Resin (RTR) Flanges |

## Standard Test Methods

| ASTM <br> D2992 | Standard Practice for Obtaining Hydrostatic or <br> Pressure Design Basis for "Fiberglass" (Glass-Fi- <br> ber-Reinforced Thermosetting Resin) Pipe and Fit- <br> tings |
| :--- | :--- |
| ASTM <br> D1599 | Standard Test method for Short-Time Hydraulic <br> Failure Pressure of Plastic Pipe, Tubing and Fit- <br> tings |
| ASTM <br> D2105 | Standard Test Method for Longitudinal Tensile <br> Properties of "Fiberglass" (Glass-Fiber-Reinforced <br> Thermosetting Resin) Pipe and Tube |
| ASTM <br> D2412 | Standard Test Method for Determination of Exter- <br> nal Loading Characteristics of Plastic Pipe by Par- <br> allel-Plate Loading |
| ASME <br> B31.3 | Process Piping |

### 2.03 ASTM D2310 Designation Code 1"-8" RTRP-21CO

Mechanical properties cell classification shown are minimum.
2.04 Operating Conditions - In addition to the above listed minimum design requirements, the system shall meet the following minimum operating conditions:
a. Operating Pressure
b. Operating Temperature
c. Fluids Conveyed
d. Test Pressure
2.05 Quality Assurance - Pipe manufacturer's quality program shall be in compliance with ISO 9001.
2.06 Delivery, Storage, and Handling - Pipe and fittings shall be protected from damage due to impact and point loading. Pipe shall be properly supported to avoid damage due to flexural strains. The contractor shall not allow dirt, debris, or other extraneous materials to get into pipe and fittings. All factory-machined areas shall be protected from sunlight until installed.
2.07 Acceptable Manufacturers - NOV Fiber Glass Systems (918) 245-6651, or approved equal.

## SECTION 3 - Materials and Construction

3.01 1"-8" Pipe - The pipe shall be manufactured by the centrifugal casting process utilizing amine cured, premium grade epoxy thermosetting resin to impregnate woven continuous glass filaments. Pipe shall be shall be heat cured and the degree of cure shall be confirmed by determining the glass transition temperature.

All pipe shall have an integral corrosion barrier of pure resin with a nominal cured thickness of 100 mils.

All pipe shall have a resin rich, reinforced 10 mil nominal exterior layer with a UV (ultraviolet) inhibitor.

The pipe shall have a minimum design pressure of 150 psig @ $275^{\circ}$ F following ASTM D2992 Procedure B.

| Minimum Reinforced Wall Thickness: |  |
| :---: | :---: |
| $1 "$ | $0.09 "$ |
| $11 / 2 "-3 "$ | $0.14 "$ |
| $4 "$ | $0.17 "$ |
| $6 "$ | $0.27^{\prime \prime}$ |
| $8 "$ | $0.31 "$ |

3.02 Flanges and Fittings - All fittings shall be manufactured using the same type materials as the pipe. Fittings may be manufactured either by compression molding or contact molding methods.

Fittings shall be adhesive bonded socket joint or flanged.
Flanges shall have ANSI B16.5, Class 150 bolt hole patterns.
3.03 Adhesive - Adhesive shall be manufacturer's standard for the piping system specified. All adhesive bonded joints shall be cured according to the manufacturer's instructions for maximum structural strength and corrosion resistance.
3.04 Gaskets - Gaskets shall be $3 / 16^{\prime \prime}$ thick, 60-70 durometer full-face type suitable for the service shown on the drawings and as recommended in the manufacturer's standard installation procedures.
3.05 Bolts, Nuts, and Washers - ASTM F593, 304, stainless steel hex head bolts shall be supplied. Two each SAE size washers shall be supplied on all nut and bolts.
3.06 Acceptable Products - Z-CORE as manufactured by NOV Fiber Glass Systems or approved equal.

## SECTION 4 - Installation and Testing

4.01 Training and Certification - All joints installed or constructed in the field shall be assembled by employees of the contractor who have been trained by the pipe manufacturer. The pipe manufacturer or their authorized representative shall train the contractor's employees in the proper joining and assembly procedures required for the project, including handson training by the contractor's employees. Each bonder shall fabricate one pipe-to-pipe or one pipe-to-fitting joint that shall pass the minimum pressure test for the application as stated in Section 2.04.d without leaking.

Only bonders who have successfully completed the pressure test and are certified shall bond pipe and fittings.

Certification by the manufacturer shall be in compliance with ANSI B31.3 Section A328.2.
4.02 Pipe Installation - Pipe shall be installed as specified and indicated on the drawings.

The piping system shall be installed in accordance with the manufacturer's current published installation procedures.
4.03 Testing - A hydrostatic pressure test shall be conducted on the completed piping system. The pipe shall be subjected to a steady pressure at $11 / 2$ times the design operating pressure as stated in Section 2.04.d. The pressure shall be held on the system for a minimum of one hour and the line inspected for leaks.

Test pressure shall not exceed $11 / 2$ times the maximum rated pressure of the lowest rated element in the system.

The system shall be filled with water at the lowest point and air bled off from all the highest points. Systems shall be brought up to test pressure slowly to prevent water hammer or overpressurization.

All pipe joints shall be watertight. All joints that are found to leak by observation or during testing shall be repaired by the contractor and retested.

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| Applications |
| :--- |
| Materials and |
| Construction |

- Potable Water
- pH 2-13 Solutions
- Wastewater
- Brine Solutions
- Food Processing
- Cooling Water
- Chemical Processing
- Crude Oil \& Gas
- Saltwater Handling
- $\mathrm{CO}_{2}$

All pipe manufactured by filament winding process using vinyl ester thermosetting resin. F-Chem pipe can be provided with custom tailored vinyl ester resin systems, reinforced corrosion and abrasion resistant barriers, reinforced structural walls and joining techniques to meet specific project requirements. The pipe is available in $14^{\prime \prime}-72^{\prime \prime}$ diameters.

## Fittings

Fittings are manufactured with the same chemical/temperature capabilities as the pipe. Depending on the particular part and size, fittings will be contact molded, hand fabricated or filament wound.

## Joining Systems

## Bell \& Spigot

Matched-taper joint secured with epoxy adhesive. Self-locking feature resists movement, facilitating joining runs of pipe without awaiting adhesive
 cure.

## Butt \& Wrap

Plain end pipes or pipe and fittings butted together and wrapped with multiple layers of resin-saturated mat or woven roving.


## Flanged

Available for all piping systems and diameters; factory assembled or shipped loose for assembly in the field.


## F-CHEM LARGE DIAMETER FITTINGS



| Average Physical Properties |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Property | $\begin{gathered} 75^{\circ} \mathrm{F} \\ \mathrm{psi} \end{gathered}$ | $\begin{aligned} & 24^{\circ} \mathrm{C} \\ & \mathrm{MPa} \end{aligned}$ | $\begin{gathered} 175^{\circ} F \\ \mathrm{psi} \end{gathered}$ | $\begin{gathered} 79^{\circ} \mathrm{C} \\ \mathrm{MPa} \end{gathered}$ |
| Axial Tensile - ASTM D2105 Ultimate Stress Modulus of Elasticity ${ }^{(1)}$ | $\begin{gathered} 9,300 \\ 1.50 \times 10^{6} \end{gathered}$ | $\begin{array}{r} 64.1 \\ 10,342 \end{array}$ | $\begin{array}{r} 5,500 \\ 1.04 \times 6 \end{array}$ | $\begin{array}{r} 37.9 \\ 7,171 \end{array}$ |
| Poisson's Ratio $\nu_{\text {a/h }}$ ( $\nu_{\text {h/a }}$ ) | 0.33 (0.73) |  |  |  |
| Axial Compression - ASTM D695 Ultimate Stress Modulus of Elasticity | $\begin{gathered} 17,900 \\ 1.40 \times 10^{6} \end{gathered}$ | $\begin{aligned} & 123.0 \\ & 9,653 \end{aligned}$ | $\begin{aligned} & 14,700 \\ & 9.00 \times 10^{5} \end{aligned}$ | $\begin{array}{r} 101 \\ 6,205 \end{array}$ |
| Beam Bending - ASTM D2925 Ultimate Stress Modulus of Elasticity (Long Term) | $\begin{gathered} 14,500 \\ 1.99 \times 10^{6} \end{gathered}$ | $\begin{gathered} 100.0 \\ 13,721 \end{gathered}$ | $\begin{aligned} & 8,000 \\ & 1.14 \times 10^{6} \end{aligned}$ | $\begin{array}{r} 55.2 \\ 7,860 \end{array}$ |
| Hydrostatic Burst - ASTM D1599 Ultimate Hoop Tensile Stress | 40,000 | 276 | 40,000 | 276 |
| Hydrostatic Design - ASTM D2992, <br> Procedure B - Hoop Tensile Stress <br> Static 50 Year Life <br> 14,000 <br> 96.5 |  |  |  |  |
| ${ }^{(1)}$ Consult the factory for Modulus of Elasticity values between $75^{\circ} \mathrm{F}$ and $175^{\circ} \mathrm{F}$. |  |  |  |  |


| Thermal Expansion Coefficient - ASTM D696 (Insulated Pipe) | $10.5 \times 10^{-6} \mathrm{in} / \mathrm{in} /{ }^{\circ} \mathrm{F}$ | $18.9 \times 10^{-6} \mathrm{~mm} / \mathrm{mm} /{ }^{\circ} \mathrm{C}$ |
| :--- | :--- | :--- |
| Thermal Conductivity | $0.11 \mathrm{BTU} / \mathrm{hr}-\mathrm{ft}-{ }^{\circ} \mathrm{F}$ | $0.06 \mathrm{~W} / \mathrm{m}-{ }^{\circ} \mathrm{C}$ |
| Specific Gravity - ASTM D792 |  | 1.8 |
| Hazen-Williams Coefficient | 0.00021 Inch | 150 |
| Absolute Surface Roughness |  | 0.0053 mm |
| Manning's Roughness Coefficient, $\mathbf{n}$ |  | 0.009 |

## ASTM D2996 Designation Codes:

| $14 "-24 " "$ | RTRP-12EU-3111 |
| :--- | :---: |
| The scope of ASTM D2996 is <br> limited to 24" and smaller |  |
| ASTM D231 O Designation Codes |  |
| $30 "-72 "$ |  |

## National Specification Compliance:

Pipe is manufactured in compliance with ASTM D2996, ASTM D2310 and ASTM D2992.

The following national specifications are met or exceeded when specified:
Designed in accordance with AWWA M45
Can be manufactured with ANSI/NSF Std. No. 61 approved resin system for potable water usage.
ASTM D6041 fittings
ASME/ANSI B31.3 compliant installation and training.

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QUALITY MANAGEMENT SYSTEM
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## F-Chem ${ }^{\circledR}$ Piping System

## GENERAL SPECIFICATIONS

## SECTION 1 - Scope

This section covers the use of fiberglass reinforced plastic (FRP) pipe for chemical and water services.

The piping system shall be furnished and installed complete with all fittings, joining materials, supports, specials, and other necessary appurtenances.

## SECTION 2-General Conditions

2.01 Coordination - Material furnished and work performed under this section shall be coordinated with related work and equipment specified under other sections.

Valves
Supports
Equipment

Section
Section
Section $\qquad$
2.02 Governing Standards - Except as modified or supplemented herein, all materials and construction methods shall comply with the applicable provisions of the following specifications and be tested using the following standards:

## Standard Specifications

| ASTM <br> D2310 | Standard Classification for Machine-Made "Fi- <br> berglass" (Glass-Fiber-Reinforced Thermosetting) <br> Resin Pipe |
| :--- | :--- |
| AWWWA <br> M45 | Fiberglass Pipe Design |

## Standard Test Methods

| ASTM <br> D2992 | Standard Practice for Obtaining Hydrostatic or <br> Pressure Design Basis for "Fiberglass" (Glass-Fi- <br> ber-Reinforced Thermosetting Resin) Pipe |
| :--- | :--- |
| ASTM <br> D2996 | Standard Specification for Filament-Wound <br> "Fiberglass" (Glass-Fiber-Reinforced-Thermo- <br> setting Resin) Pipe |
| ASTM <br> 2925 | Standard Practice for Measuring Beam Deflection <br> of Reinforced Thermosetting Plastic Pipe Under <br> Full Bore Flow |
| ASTM <br> D1599 | Standard Test method for Short-Time Hydraulic <br> Failure Pressure of Plastic Pipe, Tubing and Fit- <br> tings |
| ASTM <br> D2105 | Standard Test Method for Longitudinal Tensile <br> Properties of "Fiberglass" (Glass-Fiber-Reinforced <br> Thermosetting Resin) Pipe and Tube |
| ASTM | Standard Test Method for Determination of Exter- <br> nal Loading Characteristics of Plastic Pipe by Par- <br> allel-Plate Loading |
| D2412 |  |

2.03 ASTM D2310 Designation Code - All pipe shall be labeled with a four (4) character cell classification based on the design conditions in Section 2.04.
2.04 Design Conditions - The specified product shall meet the following design/operating conditions:
a. Operating Pressure
b. Operating Temperature
c. Fluids Conveyed
d. Minimum Liner Thickness
e. Resin Type
2.05 Quality Assurance - Pipe manufacturer's quality program shall be in compliance with ISO 9001.
2.06 Delivery, Storage, and Handling - Pipe and fittings shall be protected from damage due to impact and point loading. Pipe shall be properly supported to avoid damage due to flexural strains. The contractor shall not allow dirt, debris, or other extraneous materials to get into pipe and fittings. All factory-machined areas shall be protected from sunlight until installed.
2.07 Acceptable Manufacturers - NOV Fiber Glass Systems (918) 245-6651, or approved equal.

## SECTION 3 - Materials and Construction

3.01 14"- 72" Pipe - The pipe shall be manufactured by the filament winding process utilizing the thermosetting resin listed in Section 2.04.e to impregnate strands of continuous glass filaments, which are wound around a mandrel at a $54^{3} / 4^{\circ}$ winding angle under controlled tension. Pipe cure shall be confirmed using a Differential Scanning Calorimeter (DSC) or Thermal Mechanical Analysis (TMA)

The Pipe corrosion barrier shall consist of a 10-mil layer of synthetic surfacing veil, a 10 mil glass veil, and additional layers of $11 / 2$ ounce chopped strand mat to reach the liner thickness listed in Section 2.04.d. The nominal resin content in the veil layers shall be $80 \%$. The minimum resin content in the $11 / 2$ ounce chopped strand mat layers shall be 60\%.
3.02 Flanges and Fittings - All fittings shall be manufactured using the same type materials and liner construction as the pipe. Fittings may be manufactured either by spray-up/ contact molding or mitered/spray-up methods. Compression molded fittings manufactured with the same resin as the pipe are acceptable.

Flanges shall have ANSI B16.1 Class 125 bolt hole patterns.
$3.03 \quad$ Joints - All joints shall be butt and wrap, tapered bell \& spigot, or flanged as specified on the project drawings. The joints shall be the manufacturer's standard thickness and shall utilize the same resin system as the piping system specified. All joints shall have a pressure rating equal to the pipe rating.
3.04 Gaskets - Gaskets shall be ${ }^{1 / 4} 4^{\prime \prime}$ thick, 60-70 durometer full-face type suitable for the service shown on the drawings and as recommended in the manufacturer's standard installation procedures.
3.05 Bolts, Nuts, and Washers - ASTM A307, Grade B, hex head bolts shall be supplied. Two each SAE size washers shall be supplied on all nut and bolt sets.
3.06 Buried Pipe - All buried pipe shall have a minimum ASTM D2412 pipe stiffness of 9 psi at $5 \%$ deflection and must be buried in accordance with the manufacturer's standard installation instructions.
3.07 Acceptable Products - F-CHEM as manufactured by NOV Fiber Glass Systems or approved equal.

## SECTION 4 - Installation and Testing

4.01 Training and Certification - All joints installed or constructed in the field shall be assembled by employees of the contractor who have been trained by the pipe manufacturer. The pipe manufacturer or their authorized representative shall train the contractor's employees in the proper joining and assembly procedures required for the project, including handson training by the contractor's employees. Each bonder shall fabricate one pipe-to-pipe or one pipe-to-fitting joint that shall pass the minimum pressure test for the application without leaking.

Only bonders who have successfully completed the pressure test and are certified shall bond pipe and fittings.

Certification by the manufacturer shall be in compliance with ASME B31.3, Section A328.2 for the type of joint being made.
4.02 Pipe Installation - Pipe shall be installed as specified and indicated on the drawings.

The piping system shall be installed in accordance with the manufacturer's current published installation procedures.
4.03 Testing - A hydrostatic pressure test shall be conducted on the completed piping system. The pipe shall be subjected to a steady pressure at $11 / 2$ times the design operating pressure as stated in Section 2.04a. The pressure shall be held on the system for a minimum of 1 hour and the line inspected for leaks.

Test pressure shall not exceed $11 / 2$ times the maximum rated pressure of the lowest rated element in the system.

The system shall be filled with water at the lowest point and air bled off from all the highest points. Systems shall be brought up to test pressure slowly to prevent water hammer or overpressurization.

All pipe joints shall be water tight. All joints that are found to leak by observation or during testing shall be repaired by the contractor and retested.

All the system high points shall be open when draining the system to prevent vacuum collapse of the pipe.


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| Uses and | - Chemical process piping |
| :--- | :--- |
| Applications | - $\quad$ Deoling water piping |
|  | - Drainage systems |
|  | - Jood processing plant piping |
|  | - Jet fuel ${ }^{(1)}$ and liquid petroleum piping |
|  | - Piping systems for alkalis and non-oxidizing chemicals |
|  | - Waste water and sewage systems |
|  | - General industrial service for moderately corrosive liquids |
| (1) This is not suitable for primary pipe conveying jet fuel that is secondarily contained. |  |

Listings
Mil-P-29206A for jet fuel and petroleum liquids
U.S. Federal Regulations 21CFR175.105 and 21CFR177.2280 for conveying foodstuffs when joined with Bondstrand RP6B epoxy adhesive.

## Performance

Pipe designs to 450 psi (3.1 MPa) using an 8000 psi ( 41.2 MPa ) hydrostatic design stress in accordance with ASTM D2992 (B).

Continuous operating temperatures to $250^{\circ} \mathrm{F}\left(121^{\circ} \mathrm{C}\right)$.

Excellent corrosion resistance over a wide temperature range. See most recent release of Bondstrand Corrosion Guide for specific applications.

Weighs $1 / 6$ th as much as Sch. 40 steel.
Does not require thrust blocks at ambient temperatures when properly installed in most soils.

Smooth inner liner (Hazen-Williams $C=150$ ) produces extremely low frictional loss for greater discharge and reduced pumping costs.

Low thermal conductivity (1/100th of steel) minimizes heat losses.
Individual system components may not have the same ratings as the pipe. Refer to the detailed product information for the specific components to determine the pressure rating for the system as a whole.

## Joining Systems

Quick-Lock straight/taper adhesive-bonded joint. 2"-6" pipe outside diameter is within tolerance for reliable bonding without shaving. Integral pipe stop in socket featured for predictable, precise laying lengths.

Flanges and flanged fittings.

## Composition



## Pipe

Filament-wound fiberglass-reinforced epoxy resin pipe with integral resin-rich reinforced liner of 20 mil ( 0.5 mm ) nominal thickness.

## Filament-wound fittings

Furnished with 50 mil ( 1.3 mm ) reinforced liner using same materials as the pipe.

| Tees | Flanges* |
| :--- | :--- |
| $90^{\circ}$ and $45^{\circ}$ elbows | Nipples and coupling |
| Crosses | Tapered body reducers |
| $45^{\circ}$ laterals | Saddles* |
| *No iner. |  |
| Molded fittings ${ }^{(1)}$ |  |
| Tees |  |
| $90^{\circ}$ and $45^{\circ}$ elbows |  |
| Reducing flanges |  |
| Plugs and end-caps |  |
| Reducer bushings |  |
| Blind flanges |  |
| (1) Available parts vary by diameter. |  |

## Flanged fittings

2-12 inch filament-wound flanged fittings match ANSI B16.1 and ANSI B16.5 bolt hole pattern and face-to-face dimensions for 150 lb flanges.

1-16 inch flanges match ANSI B16.1 and ANSI B16.5 bolt hole pattern for 150 lb flanges.

Other flange drilling patterns such as DIN, ISO, JIS, ANSI B16.5 300 lb . etc., available on special request.

## Thermosetting adhesives

PSX ${ }^{\text {TM }} \cdot 34$ two-part epoxy adhesive for general industrial service and for service in compliance with U.S. Federal Regulations 21CFR175.105 and 21CFR177.2280.

## Pipe Lengths

| Nominal <br> Pipe Size |
| :--- |
| in | mm $\left.\quad$| Random |
| :---: |
| Lengths | \right\rvert\,


| Typical Pipe <br> Dimensions | Nominal Pipe Size |  | Pipe I.D. |  | Nominal Wall Thickness* |  | Average Sectional Area** |  | Pipe Weight |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| and Weights | in | mm | in | mm | in | mm | in ${ }^{2}$ | $\mathrm{mm}^{2}$ | lb/tt | kg/m |
|  | 1 | 25 | 1.07 | 27 | . 140 | 3.6 | 0.50 | 323 | 0.4 | 0.6 |
|  | $11 / 2$ | 40 | 1.67 | 42 | . 140 | 3.6 | 0.80 | 516 | 0.7 | 1.0 |
|  | 2 | 50 | 2.10 | 53 | . 123 | 3.7 | 0.73 | 730 | 0.7 | 1.3 |
|  | 3 | 80 | 3.21 | 82 | . 126 | 3.7 | 1.07 | 1100 | 1.1 | 1.8 |
|  | 4 | 100 | 4.14 | 105 | . 151 | 3.8 | 1.78 | 1760 | 1.7 | 3.0 |
|  | 6 | 150 | 6.19 | 159 | . 181 | 4.6 | 3.22 | 2620 | 2.6 | 4.5 |
|  | 8 | 200 | 8.22 | 209 | . 226 | 5.7 | 5.83 | 3720 | 4.3 | 6.4 |
|  | 10 | 250 | 10.35 | 263 | . 226 | 5.7 | 7.31 | 4720 | 5.4 | 8.0 |
|  | 12 | 300 | 12.35 | 314 | . 226 | 5.7 | 8.69 | 5610 | 6.4 | 9.5 |
|  | 14 | 350 | 13.56 | 344 | . 250 | 6.4 | 10.32 | 6660 | 7.4 | 11.0 |
|  | 16 | 400 | 15.50 | 394 | . 269 | 6.8 | 13.33 | 8600 | 9.5 | 14.1 |

* Minimum wall thickness shall not be less than $87.5 \%$ of nominal wall thickness in accordance with ASTM D2996.
** Use these values for calculating longitudinal thrust.


## Typical Pipe Performance

| Nominal <br> Pipe Size |  | Internal <br> Pressure Rating* |  | Collapse <br> Pressure Rating** |  | Designation |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | psig | MPa | psig | MPa | per ASTM D2996 |
| 1 | 25 | 450 | 3.10 | 945 | 6.52 | RTRP-11FE-1112 |
| $1 / 2$ | 40 | 450 | 3.10 | 280 | 1.93 | RTRP-11FE-1114 |
| 2 | 50 | 450 | 3.10 | 260 | 1.80 | 11FW-2232 |
| 3 | 80 | 450 | 3.10 | 80 | 0.55 | 11FW-2232 |
| 4 | 100 | 450 | 3.10 | 70 | 0.48 | 11FW-2232 |
| 6 | 150 | 375 | 2.59 | 50 | 0.34 | 11FW-2232 |
| 8 | 200 | 250 | 1.72 | 30 | 0.21 | RTRP-11FE-1114 |
| 10 | 250 | 200 | 1.38 | 14 | 0.097 | RTRP-11FE-1114 |
| 12 | 300 | 170 | 1.17 | 8 | 0.055 | RTRP-11FE-1114 |
| 14 | 350 | 165 | 1.14 | 8 | 0.055 | RTRP-11FE-1115 |
| 16 | 400 | 165 | 1.14 | 8 | 0.055 | RTRP-11FE-1116 |

[^6]Fittings Pressure
Ratings

| Nominal Pipe Size |  | Elbows \& Tees |  |  |  | Tapered Body Reducers \& Flanges |  | Blind Flanges \& Bushed Saddles** |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Filament Wound |  | Molded |  |  |  |  |  |
| in | mm | psig | MPa | psig | MPa | psig | MPa | psig | MPa |
| 1 | 25 | 300 | 2.07 | - | - | 600 | 4.14 | 150 | 1.03 |
| $1 \frac{1}{2}$ | 40 | 300 | 2.07 | - | - | 550 | 3.79 | 150 | 1.03 |
| 2 | 50 | 375 | 2.59 | 300 | 2.07 | 450 | 3.10 | 150 | 1.03 |
| 3 | 80 | 325 | 2.24 | 225 | 1.55 | 350 | 2.41 | 150 | 1.03 |
| 4 | 100 | 300 | 2.07 | 175 | 1.21 | 350 | 2.41 | 150 | 1.03 |
| 6 | 150 | 225 | 1.55 | 150 | 1.03 | 250 | 1.72 | 150 | 1.03 |
| 8 | 200 | 225 | 1.55 | - | - | 225 | 1.55 | 150 | 1.03 |
| 10 | 250 | 200 | 1.38 | - | - | 175 | 1.21 | 150 | 1.03 |
| 12 | 300 | 175 | 1.21 | - | - | 150 | 1.03 | 150 | 1.03 |
| 14 | 350 | 150 | 1.03 | - | - | 150 | 1.03 | - | - |
| 16 | 400 | 150 | 1.03 | - | - | 150 | 1.03 | - | - |

1) Refer to for fittings dimensions.
** With 316 stainless steel outlet. Other outlet materials available on special order.

| Nominal Pipe <br> Size |  | Laterals |  | Crosses |  | Reducers <br> Bushings |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | psig | MPa | psig | MPa | psig | MPa |
| 1 | 25 | - | - | - | - | 50 | .35 |
| $11 / 2$ | 40 | - | - | - | - | 50 | .35 |
| 2 | 50 | 275 | 1.90 | 150 | 1.03 | 50 | .35 |
| 3 | 80 | 250 | 1.72 | 150 | 1.03 | 50 | .35 |
| 4 | 100 | 200 | 1.38 | 150 | 1.03 | 50 | .35 |
| 6 | 150 | 150 | 1.03 | 100 | 0.69 | 50 | .35 |
| 8 | 200 | 150 | 1.03 | 100 | 0.69 | 50 | .35 |
| 10 | 250 | 150 | 1.03 | 100 | 0.69 | 50 | .35 |
| 12 | 300 | 150 | 1.03 | 100 | 0.69 | 50 | .35 |
| 14 | 350 | 150 | 1.03 | 100 | 0.69 | 50 | .35 |
| 16 | 400 | 150 | 1.03 | 100 | 0.69 | 50 | .35 |

1) Reducer bushings bonded into flanges will have the same rating as the flange. Otherwise, rated as shown.


| Nominal <br> Pipe Size |  | Bending <br> Radius* $^{*}(\mathrm{R})$ |  | Maximum Allowable <br> Deflection** (H) |  | Turning <br> Angle |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | ft | m | ft | m | $\mathrm{(a)}$ |
| 1 | 25 | 45.2 | 13.8 | 24.9 | 7.6 | 127 |
| $1 \frac{1}{2}$ | 40 | 66.4 | 20.2 | 17.9 | 5.5 | 86 |
| 2 | 50 | 75 | 22.9 | 15.9 | 4.8 | 76 |
| 3 | 80 | 100 | 30.5 | 12.1 | 3.7 | 57 |
| 4 | 100 | 200 | 70.0 | 6.4 | 2.0 | 29 |
| 6 | 150 | 250 | 76.2 | 5.0 | 1.5 | 23 |
| 8 | 200 | 304 | 93 | 4.1 | 1.2 | 19 |
| 10 | 250 | 379 | 116 | 3.3 | 1.0 | 15 |
| 12 | 300 | 450 | 137 | 2.8 | 0.85 | 13 |
| 14 | 350 | 494 | 151 | 2.5 | 0.76 | 12 |
| 16 | 400 | 564 | 172 | 2.2 | 0.67 | 10 |

[^7]Typical Mechanical Properties

| Pipe Property | Units | $\begin{aligned} & 70^{\circ} \mathrm{F} \\ & 21^{\circ} \mathrm{C} \end{aligned}$ |  | $\begin{gathered} 200^{\circ} \mathrm{F} \\ 93^{\circ} \mathrm{C} \end{gathered}$ |  | ASTM <br> Method |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Nominal Pipe Size |  | $\begin{gathered} 1 ", 11 / 2^{\prime \prime} \\ 8^{\prime \prime}-16^{\prime \prime} \end{gathered}$ | 2"-6" | $\begin{aligned} & 1^{\prime \prime}, 1^{1 / 2}{ }^{\prime \prime} \\ & 8^{\prime \prime}-16^{\prime \prime} \end{aligned}$ | 2"-6" |  |
| Circumferential <br> Tensile stress at weeping | $\begin{gathered} 10^{3} \mathrm{psi} \\ \mathrm{MPa} \end{gathered}$ | $\begin{gathered} 24.00 \\ 165.00 \end{gathered}$ | $\begin{aligned} & 32.00 \\ & 22.00 \end{aligned}$ | - | - | D1599 |
| Tensile modulus | $\begin{gathered} 10^{6} \mathrm{psi} \\ \mathrm{GPa} \end{gathered}$ | $\begin{aligned} & 3.65 \\ & 25.20 \end{aligned}$ | $\begin{gathered} 4.20 \\ 29.00 \end{gathered}$ | $\begin{aligned} & 3.20 \\ & 22.10 \end{aligned}$ | $\begin{gathered} 3.70 \\ 25.50 \end{gathered}$ |  |
| Poisson's ratio |  | 0.56 | 0.26 | 0.70 | 0.32 | D2105 |
| Longitudinal Tensile strength | $\begin{gathered} 10^{3} \mathrm{psi} \\ \mathrm{MPa} \end{gathered}$ | $\begin{aligned} & 8.50 \\ & 58.60 \end{aligned}$ | $\begin{gathered} 16.00 \\ 110.00 \end{gathered}$ | $\begin{aligned} & 6.90 \\ & 47.60 \end{aligned}$ | $\begin{aligned} & 13.00 \\ & 90.00 \end{aligned}$ | D2105 |
| Tensile modulus <br> Poisson's ratio | $\begin{gathered} 10^{6} \mathrm{psi} \\ \mathrm{GPa} \end{gathered}$ | $\begin{gathered} 1.60 \\ 11.00 \\ 0.37 \end{gathered}$ | $\begin{gathered} 3.00 \\ 20.70 \\ 0.16 \end{gathered}$ | $\begin{aligned} & 1.24 \\ & 8.50 \\ & 0.41 \end{aligned}$ | $\begin{gathered} 2.40 \\ 16.50 \\ 0.20 \end{gathered}$ | $\begin{aligned} & \text { D2105 } \\ & \text { D2105 } \end{aligned}$ |
| Beam apparent <br> Elastic modulus | $\begin{gathered} 10^{6} \mathrm{psi} \\ \mathrm{GPa} \end{gathered}$ | $\begin{gathered} 1.70 \\ 11.70 \end{gathered}$ | $\begin{gathered} 2.40 \\ 16.60 \end{gathered}$ | $\begin{aligned} & 1.00 \\ & 6.90 \end{aligned}$ | $\begin{gathered} 1.77 \\ 12.20 \end{gathered}$ | D2925 |
| Hydrostatic design basis (cyclic) | $\begin{aligned} & 10^{3} \mathrm{psi} \\ & \mathrm{MPa} \end{aligned}$ | $\begin{gathered} 6.00 \\ 41.40^{1} \end{gathered}$ | $\begin{aligned} & 16.00^{1,2} \\ & 110.00 \end{aligned}$ | - |  | D2992 |
| Thermal conductivity <br> Pipe wall | $\begin{gathered} \mathrm{Btu} \cdot \mathrm{in} /\left(\mathrm{hr} \cdot \mathrm{ft}^{2} \cdot{ }^{\circ} \mathrm{F}\right) \\ \mathrm{W} / \mathrm{m} \cdot{ }^{\circ} \mathrm{C} \mathrm{C} \end{gathered}$ | $\begin{aligned} & 2.00 \\ & 0.29 \end{aligned}$ | $\begin{gathered} 1.70 \\ 10.25 \end{gathered}$ |  |  | C177 |
| Thermal expansion Linear | $\begin{gathered} 10-6 \mathrm{in} / \mathrm{in} /{ }^{\circ} \mathrm{F} \\ 10-{ }^{-6} \mathrm{~mm} / \mathrm{mm}^{\circ} \mathrm{C} \end{gathered}$ | $\begin{aligned} & 10.00 \\ & 18.00 \end{aligned}$ | $\begin{aligned} & 8.50 \\ & 15.30 \end{aligned}$ | - |  | D696 |
| Flow coefficient | Hazens-Wiliams | 150.00 | 150.00 | - | - | - |
| Absolute roughness | $\begin{aligned} & 10-6 \mathrm{ft} \\ & 10-6 \mathrm{~m} \end{aligned}$ | $\begin{gathered} 17.40 \\ 5.30 \end{gathered}$ | $\begin{gathered} 17.40 \\ 3.30 \end{gathered}$ |  |  | - |
| Specific gravity | - | 1.80 | 1.80 | - | - | D792 |
| Density | $\begin{aligned} & \mathrm{lb} / \mathrm{in}^{3} \\ & \mathrm{~g} / \mathrm{cm}^{3} \end{aligned}$ | $\begin{aligned} & 0.07 \\ & 1.80 \end{aligned}$ | $\begin{aligned} & 0.07 \\ & 1.80 \end{aligned}$ |  |  | - |


| Nominal <br> Pipe Size |  | Stiffiness <br> Factor* |  | Pipe <br> Stifiness |  | Beam Moment <br> of Inertia** |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | $\mathrm{Ib} / \mathrm{tt}$ | $\mathrm{N} / \mathrm{m}$ | psi | MPa | $\mathrm{in}^{4}$ | $10^{6} \mathrm{~mm}^{4}$ |
| 1 | 25 | 770 | 87 | 26400 | 182 | 0.09 | 0.037 |
| $11 / 2$ | 40 | 1610 | 182 | 17200 | 119 | 0.36 | 0.150 |
| 2 | 50 | 265 | 30 | 1350 | 9.3 | 0.46 | 0.191 |
| 3 | 80 | 285 | 32 | 550 | 3.80 | 1.57 | 0.653 |
| 4 | 100 | 500 | 56 | 335 | 2.30 | 4.13 | 1.72 |
| 6 | 150 | 925 | 104 | 200 | 1.40 | 16.5 | 6.87 |
| 8 | 200 | 1890 | 214 | 170 | 1.17 | 45.1 | 18.8 |
| 10 | 250 | 1890 | 214 | 86 | 0.59 | 88.6 | 36.9 |
| 12 | 300 | 1890 | 214 | 51 | 0.35 | 149.0 | 62.0 |
| 14 | 350 | 2230 | 252 | 46 | 0.32 | 208.0 | 86.6 |
| 16 | 400 | 3250 | 367 | 45 | 0.31 | 353.0 | 147.0 |

[^8]Buried
Installations

Thrust blocks
Most installations at ambient operating temperatures do not require thrust blocks. Consult FGS for information regarding blocking of buried pipelines for your specific application.

## Live loads

Bondstrand 2000 will carry H20 wheel loadings of at least $16,000 \mathrm{lb}(7250 \mathrm{~kg})$ per axle when properly bedded in compacted sand in stable soils and provided with at least $3 \mathrm{ft}(1 \mathrm{~m})$ of cover.

Earth loads on buried pipe

| Nominal Pipe Size |  | Maximum Earth Cover ${ }^{1}$ |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 100 psi | 0.69 MPa | 125 psi | 0.86 MPa | 150 psi | 1.03 MPa |
| in | mm | ft | m | ft | m | ft | m |
| 1 | 25 | 30 | 9 | 30 | 9 | 30 | 9 |
| $1^{1 / 2}$ | 40 | 30 | 9 | 30 | 9 | 30 | 9 |
| 2 | 50 | 30 | 9 | 30 | 9 | 30 | 9 |
| 3 | 80 | 30 | 9 | 30 | 9 | 30 | 9 |
| 4 | 100 | 30 | 9 | 30 | 9 | 30 | 9 |
| 6 | 150 | 30 | 9 | 24 | 7 | 23 | 7 |
| 8 | 200 | 23 | 7 | 22 | 6 | 21 | 6 |
| 10 | 250 | 23 | 7 | 21 | 6 | 19 | 5 |
| 12 | 300 | 23 | 7 | 21 | 6 | 18 | 5 |
| 14 | 350 | 23 | 7 | 21 | 6 | 17 | 5 |
| 16 | 400 | 23 | 7 | 20 | 6 | 16 | 5 |

1) Based on a $120 \mathrm{lb} / \mathrm{tt3}(1925 \mathrm{~kg} / \mathrm{m} 3)$ soil density and $1000 \mathrm{psi}(6.9 \mathrm{MPa})$ modulus of soil reaction.

Span Lengths

Recommended maximum support spacings for Bondstrand Series 2000 pipe at various operating temperatures. Values based on 0.5 -inch ( 12 mm ) deflection at midspan for fluid specific gravity $=1.0$.

| Nominal Pipe Size |  | Continuous Spans ft |  |  |  | Simple Spans ft |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | $100^{\circ} \mathrm{F}$ | $150^{\circ} \mathrm{F}$ | $200^{\circ} \mathrm{F}$ | $250{ }^{\circ} \mathrm{F}$ | $100^{\circ} \mathrm{F}$ | $150^{\circ} \mathrm{F}$ | $200^{\circ} \mathrm{F}$ | $250^{\circ} \mathrm{F}$ |
| 1 | 25 | 11.7 | 11.1 | 10.3 | 9.3 | 7.3 | 7.4 | 6.7 | 6.2 |
| $1^{1 / 2}$ | 40 | 13.8 | 13.0 | 12.1 | 11.0 | 9.2 | 8.7 | 8.1 | 7.3 |
| 2 | 50 | 14.3 | 13.5 | 12.6 | 11.4 | 9.5 | 9.0 | 8.4 | 7.6 |
| 3 | 80 | 16.2 | 15.4 | 14.3 | 12.9 | 10.8 | 10.2 | 9.5 | 8.6 |
| 4 | 100 | 18.5 | 17.5 | 16.3 | 14.7 | 12.3 | 11.7 | 10.9 | 9.8 |
| 6 | 150 | 20.7 | 19.6 | 18.2 | 16.5 | 13.8 | 13.1 | 12.1 | 11.0 |
| 8 | 200 | 22.9 | 21.7 | 20.2 | 18.2 | 15.3 | 14.5 | 13.5 | 12.2 |
| 10 | 250 | 24.3 | 23.0 | 21.4 | 19.3 | 16.2 | 15.3 | 14.3 | 12.9 |
| 12 | 300 | 25.5 | 24.1 | 22.4 | 20.3 | 17.0 | 16.1 | 15.0 | 13.5 |
| 14 | 350 | 26.5 | 25.0 | 23.3 | 21.1 | 17.6 | 16.7 | 15.5 | 14.0 |
| 16 | 400 | 28.2 | 26.7 | 24.9 | 22.5 | 18.9 | 17.8 | 16.6 | 15.0 |

[^9]Field Bondstrand 2000 piping systems are designed for hydrostatic field testing at $150 \%$ of rated operating pressure.
Testing

## Pipe Construction

## Standard Fittings

 ConstructionThe structural wall of fiberglass pipe shall have continuous glass fibers in a matrix of aromatic amine cured epoxy resin.

The integral, reinforced resin-rich liner shall consist of C-glass and a resin/hardener system identical to that of the structural wall, and shall have a 20 mil nominal thickness.

Pipe in 1 through 16 -inch sizes shall be rated for a minimum of 165 psig at $250^{\circ} \mathrm{F}$. In 1 through 6 -inch sizes the pipe shall have full vacuum capability at $70^{\circ} \mathrm{F}$, when installed above ground with a safety factor of $3: 1$.

Pipe shall be manufactured according to ASTM D2996 specification for filament- wound Reinforced Thermosetting Resin Pipe (RTRP). When classified under ASTM D2310, the pipe shall meet Type 1, Grade 1 and Class F (RTRP-11FE or W) cell limits in 1 through 16-inch nominal pipe sizes.

Filament-wound epoxy fiberglass pipe shall be translucent to allow for inspection of damage.
Pipe in 2 through 8-inch sizes shall be furnished in 30 or 40 -ft. length to minimize the number of field-bonded joints for rapid installation.

Fittings in 1 through 16-inch sizes shall be filament wound with a reinforced resin-rich liner of 50 mil minimum thickness and of the same glass and resin type as the pipe. Pipe, filamentwound fittings and adhesive shall, as an assembly, provide a continuous liner throughout the system.

Compression-molded fittings in 2, 3, 4 and 6-inch nominal sizes may also be allowed upon agreement between purchaser and manufacturer.

Contact-molded, spray-up or hand-layup fittings shall not be allowed. Pipe and fittings shall be joined using a straight spigot by socket with a $0.5^{\circ}$ taper angle and a pipe stop inside the socket to allow precise makeup.

## Workmanship

The pipe and fittings shall be free from all defects, including delaminations, indentations, pinholes, foreign inclusions, bubbles and resin-starved areas which, due to their nature, degree or extent, detrimentally affect the strength and serviceability of the pipe or fittings. The pipe and fittings shall be as uniform as commercially practicable in color, density and other physical properties.

## Testing

Samples of pipe and couplings shall be tested at random, based on standard quality control practices to determine conformance of the materials to American Society for Testing and Materials guidelines for testing fiberglass pipe products: ASTM D1599, D2105, D2925, D2992A or D2992B.

Test samples may be hydrostatically tested by the manufacturer to 1.5 times the pressure rating for signs of leakage.

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## Bondstrand"' 2000 Guide Specification

Scope

References, Quality Assurance

This specification defines the reinforced thermosetting resin (RTR) piping system to be used in those sections of Plant Piping-General Services calling for fiberglass piping systems.

References are made to other standards and tests which are a part of this section as modified Where conflict exists between the requirements of this specification and listed references, the specification shall prevail.

## Physical and

 Mechanical Properties| Pipe Property | Units | $\begin{aligned} & 70^{\circ} \mathrm{F} \\ & 21^{\circ} \mathrm{C} \end{aligned}$ |  | $\begin{gathered} 200^{\circ} \mathrm{F} \\ 93^{\circ} \mathrm{C} \end{gathered}$ |  | ASTM <br> Method |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Nominal Pipe Size |  | $\begin{aligned} & 1 ", 11 / 2^{\prime \prime} \\ & 8^{\prime \prime}-16^{\prime \prime} \end{aligned}$ | 2"-6" | $\begin{gathered} 1^{\prime \prime}, 1^{1} / 2^{\prime \prime} \\ 8^{\prime \prime}-16^{\prime \prime} \end{gathered}$ | 2"-6" |  |
| Circumferential <br> Tensile stress at weeping <br> Tensile modulus <br> Poisson's ratio | $\begin{gathered} 1^{3} \mathrm{psi} \\ \mathrm{MPa} \\ 10^{6} \mathrm{psi} \\ \mathrm{GPa} \end{gathered}$ | $\begin{gathered} 24.00 \\ 165.00 \\ 3.65 \\ 25.20 \\ 0.56 \end{gathered}$ | $\begin{gathered} 32.00 \\ 22.00 \\ 4.20 \\ 29.00 \\ 0.26 \end{gathered}$ | $\begin{gathered} 3.20 \\ 22.10 \\ 0.70 \end{gathered}$ | $\begin{gathered} 3.70 \\ 25.50 \\ 0.32 \end{gathered}$ | D1599 <br> D2105 |
| Longitudinal <br> Tensile strength <br> Tensile modulus | $10^{3} \mathrm{psi}$ MPa <br> $10^{6} \mathrm{psi}$ GPa | $\begin{gathered} 8.50 \\ 58.60 \\ 1.60 \\ 11.00 \end{gathered}$ | $\begin{gathered} 16.00 \\ 110.00 \\ 3.00 \\ 20.70 \end{gathered}$ | $\begin{gathered} 6.90 \\ 47.60 \\ 1.24 \\ 8.50 \end{gathered}$ | $\begin{gathered} 13.00 \\ 90.00 \\ 2.40 \\ 16.50 \end{gathered}$ | $\begin{aligned} & \text { D2105 } \\ & \text { D2105 } \end{aligned}$ |
| Poisson's ratio |  | 0.37 | 0.16 | 0.41 | 0.20 | D2105 |
| Beam apparent <br> Elastic modulus | $\begin{gathered} 10^{6} \mathrm{psi} \\ \mathrm{GPa} \end{gathered}$ | $\begin{gathered} 1.70 \\ 11.70 \end{gathered}$ | $\begin{gathered} 2.40 \\ 16.60 \end{gathered}$ | $\begin{aligned} & 1.00 \\ & 6.90 \end{aligned}$ | $\begin{gathered} 1.77 \\ 12.20 \end{gathered}$ | D2925 |
| Hydrostatic design basis (cyclic) | $\begin{aligned} & 10^{3} \mathrm{psi} \\ & \mathrm{MPa} \end{aligned}$ | $\begin{gathered} 6.00 \\ 41.40^{1} \end{gathered}$ | $\begin{aligned} & 16.00^{1,2} \\ & 110.00 \end{aligned}$ |  | - | D2992 |
| Thermal conductivity <br> Pipe wall | $\begin{gathered} \mathrm{Btu} \cdot \mathrm{in} /\left(\mathrm{hr}^{\mathrm{ftt}} \mathrm{ft}^{\circ} \mathrm{F}\right) \\ \mathrm{W} / \mathrm{m} \cdot{ }^{\circ} \mathrm{C} \end{gathered}$ | $\begin{aligned} & 2.00 \\ & 0.29 \end{aligned}$ | $\begin{gathered} 1.70 \\ 10.25 \end{gathered}$ | - | - | C177 |
| Thermal expansion Linear | $\begin{gathered} 10-6 \mathrm{in} / \mathrm{in} /{ }^{\circ} \mathrm{F} \\ 10-{ }^{6} \mathrm{~mm} / \mathrm{mm}^{\circ} \mathrm{C} \end{gathered}$ | $\begin{aligned} & 10.00 \\ & 18.00 \end{aligned}$ | $\begin{gathered} 8.50 \\ 15.30 \end{gathered}$ | - | - | D696 |
| Flow coefficient | Hazens-Wiliams | 150.00 | 150.00 | - | - | - |
| Absolute roughness | $\begin{aligned} & 10-6 \mathrm{ft} \\ & 10-6 \mathrm{~m} \end{aligned}$ | $\begin{gathered} 17.40 \\ 5.30 \end{gathered}$ | $\begin{gathered} 17.40 \\ 3.30 \end{gathered}$ |  | - | - |
| Specific gravity | - | 1.80 | 1.80 | - | - | D792 |
| Density | $\begin{aligned} & \mathrm{lb} / \mathrm{in}^{3} \\ & \mathrm{~g} / \mathrm{cm}^{3} \end{aligned}$ | $\begin{aligned} & 0.07 \\ & 1.80 \end{aligned}$ | $\begin{aligned} & 0.07 \\ & 1.80 \end{aligned}$ |  | - | - |

## Performance <br> Requirements

The pipe in sizes 1 " through 16" must comply with U.S. Federal Regulations 21CFR 175.105 and 21CFR 177.2280 for conveying foodstuffs when joined with RP6B epoxy adhesive. Pipe shall be listed under NSF Standard 61-Drinking Water System Components. Piping must meet or exceed the requirements of MIL-P-29206A and ASTM D5677-95 when used in aviation fuel service. Fittings will be manufactured according to ASTM D5685. Piping will be manufactured according to ASTM D2996 for RTRP. When classified under ASTM D2310, the pipe shall meet Type I, Grade I and Class F (RTRP-11FE) cell limits in 1 " through 16 " nominal pipe sizes.

## Materials Pipe Construction

Filament-wound fiberglass reinforced epoxy resin pipe shall be Bondstrand 2000 as manufactured by FGS, or approved equal. The integral reinforced corrosion barrier shall have a nominal 20 mil thickness, and be constructed with the same epoxy resin as the pipe structural wall. Non-reinforced liners, or corrosion barriers, shall not be allowed due to potential for fracturing during lower temperatures, transportation and installation.

## Structural wall

The pipe shall have the following nominal wall thickness:

## Pipe end preparation options

The piping manufacturer will provide $20^{\prime}$ or $40^{\prime}$ RL joints if the contractor requests them in sizes 2 " through 6 " to reduce field labor time in those sections of the system where longer lengths may be employed. Additionally, the pipe manufacturer will provide pipe joints with the spigot ends already prepared to reduce field labor time on all pipe sizes (2"-16").

## Pressure rating

Aromatic amine cured epoxy resin piping shall be rated for a minimum of 165 psi at $200^{\circ} \mathrm{F}$ in sizes through 16 ". Pressure ratings reduce linearly to $50 \%$ at $250^{\circ} \mathrm{F}$.

| Pipe Diameter | Nominal Wall Thickness |  |
| :---: | :---: | :---: |
| in | in | mm |
| 1 | .140 | 3.5 |
| $1 \frac{1}{2}$ | .140 | 3.5 |
| 2 | .123 | 3.1 |
| 3 | .126 | 3.2 |
| 4 | .151 | 3.8 |
| 6 | .181 | 4.6 |
| 8 | .226 | 5.7 |
| 10 | .226 | 5.7 |
| 12 | .226 | 5.7 |
| 14 | .250 | 6.4 |
| 16 | .269 | 6.8 |

## Fittings

It is important to maintain compatibility of fittings, piping and adhesives to ensure that the system performs as specified. Pipe, fittings and adhesive shall be supplied by the same manufacturer.

## Filament-wound fittings

Fittings in 1 " through 16 " sizes shall be filament-wound with a reinforced resin-rich liner of equal or greater thickness than the pipe liner and shall be manufactured with the same resin type as the pipe.

## Compression-molded fittings

Compression molded fittings in sizes $2^{\prime \prime}$ through $6^{\prime \prime}$ may be used in services at or below $200^{\circ} \mathrm{F}$. Where fast closure of valves may produce surges (water hammer), filament-wound fittings will be used.

Contact molded, spray up or hand lay-up fittings shall not be allowed.

## Testing

## Inspection and testing

Inspection and testing of the piping will be performed in accordance with the requirements of ASME B31.1. Hydrostatic testing of all installed piping shall be performed with water at $1 \frac{1}{2}$ times the design pressure of the lowest rated piping system component.

## Test and repair procedures

The RTRP manufacturer will provide test and repair procedures in the event field repairs are required.
Installation Installation procedures and techniques as well as system design criteria including burial, anchoring, guiding and supporting shall be in accordance with manufacturer's recommendations.

Piping system installers and fitters will be trained by a direct factory employee of the piping system manufacturer and certified by the trainer prior to system assembly in the field.

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## Bondstrand ${ }^{\text {TM }} 2400$ Series Product Data Glassfiber Reinforced Epoxy (GRE) pipe systems

## Applications

- Potable Water
- Cooling Water
- Produced Water
- Fire Water (FM Approved)
- Waste Water
- Salt Water
- Crude Oil \& Gas
- Brine Solutions
- Drainage
- Sewage
- $\mathrm{CO}_{2}$
- General Service for Mildly Corrosive Liquids


## Materials and Characteristics

Filament wound Glassfiber Reinforced epoxy (GRE) pipe with an integral Taper female x shaved spigot adhesive bonded joint or Key-Lock integral female x male mechanical joint.

- Laminate meets requirements of API Specification 15LR and ISO 14692
- Pipe wall design based on hydrostatic design basis (Procedure B) with a 0.5 service factor
- Maximum operating temperature: $200^{\circ} \mathrm{F}\left(93^{\circ} \mathrm{C}\right)$. Temperatures up to $250^{\circ} \mathrm{F}\left(121^{\circ} \mathrm{C}\right)$ are possible.

Please consult NOV Fiber Glass Systems

- Pipe sizes: 2-40 inch (50-1000 mm)
- Standard pressure rating up to 725 psi (50 bar). Higher pressure ratings are possible. Please consult NOV Fiber Glass Systems.
- ASTM D-2310 classification: RTRP-11AW for conductive pipe and RTRP-11FW for non-conductive pipe.
- Non-conductive pipe has a standard liner thickness of 0.5 mm . Conductive pipe has no liner.


## Joining Systems

## Fittings

Filament wound Glassfiber Reinforced epoxy (GRE) fittings with integral taper female bell ends. A wide range of fittings is available.

## Flanges

Filament wound GRE heavy duty and stub end flanges with integral taper female bell end are available. Standard flange drilling pattern per ASME B16.5 and B16.47A, Class 150 are available. Other drilling patterns, such as Class 300, DIN and JIS are available.

For dimensional data and standard configurations for fittings, refer to the respective fitting guides. Optionally, the system can be suppled conductive (Bondstrand 2400C) or with fireproofing (Bondstrand 2400FP).

## Pipe Lengths

From 2-6 inch (50-150 mm) 9 m random length
From 8-40 inch (200-1000 mm) 11.89 m random length
Note: Overall pipe length depends on size, end configuration and production location.

## Total Wall Thickness

| Pipe <br> Size |  | Pressure Class (bar) |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| inch | mm | 2410 | 2412 | 2414 | 2416 | 2420 | 2425 | 2432 | 2440 | 2450 |
| 2 | 50 | 2.3 | 2.3 | 2.3 | 2.3 | 2.3 | 2.3 | 2.3 | 2.8 | 3.3 |
| 3 | 80 | 2.3 | 2.3 | 2.3 | 2.3 | 2.3 | 2.7 | 3.1 | 3.9 | 4.7 |
| 4 | 100 | 2.3 | 2.3 | 2.3 | 2.5 | 2.7 | 3.3 | 3.9 | 4.9 | 5.9 |
| 6 | 150 | 2.5 | 2.7 | 3.0 | 3.4 | 3.8 | 4.6 | 5.6 | 7.0 | 8.7 |
| 8 | 200 | 3.1 | 3.2 | 3.7 | 4.2 | 4.8 | 5.8 | 7.2 | 9.1 | 11.2 |
| 10 | 250 | 3.5 | 3.9 | 4.5 | 5.1 | 5.8 | 7.2 | 8.8 | 11.2 | 13.8 |
| 12 | 300 | 3.9 | 4.5 | 5.3 | 6.0 | 6.8 | 8.4 | 10.4 | 13.4 | 16.6 |
| 14 | 350 | 4.1 | 4.8 | 5.7 | 6.6 | 7.4 | 9.2 | 11.4 | 14.5 | 18.2 |
| 16 | 400 | 4.5 | 5.5 | 6.4 | 7.4 | 8.4 | 10.5 | 12.9 | 15.6 |  |
| 18 | 450 | 4.9 | 6.0 | 7.0 | 8.1 | 9.2 | 11.5 | 14.2 | 18.2 |  |
| 20 | 500 | 5.4 | 6.6 | 7.7 | 8.9 | 10.1 | 12.7 | 15.7 | 20.1 |  |
| 24 | 600 | 6.3 | 7.7 | 9.3 | 10.6 | 12.1 | 15.1 | 18.8 | 24.0 |  |
| 28 | 700 | 7.4 | 9.1 | 10.8 | 12.6 | 14.3 | 17.9 | 22.3 |  |  |
| 30 | 750 | 7.9 | 9.7 | 11.6 | 13.5 | 15.3 | 19.1 | 23.9 |  |  |
| 32 | 800 | 8.4 | 10.3 | 12.3 | 14.3 | 16.3 | 20.4 | 25.5 |  |  |
| 36 | 900 | 9.3 | 11.5 | 13.7 | 16.1 | 18.2 | 22.8 | 28.5 |  |  |
| 40 | 1000 | 10.3 | 12.8 | 15.3 | 17.8 | 20.3 | 24.8 |  |  |  |

Note: (1) Pipe wall thickness measured according to NOV Fiber Glass Systems' procedure.
(2) Total pipe wall thickness includes 0.5 mm liner for non-conductive pipe.

External Pressure (Ultimate Collapse Pressure at $21^{\circ} \mathrm{C} / 70^{\circ} \mathrm{F}$ )

| Pipe <br> Size |  | Pressure Class (bar) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| inch | mm | 2410 | 2412 | 2414 | 2416 | 2420 | 2425 | 2432 | 2440 | 2450 |  |
| 2 | 50 | 18.6 | 18.6 | 18.6 | 18.6 | 18.6 | 18.6 | 18.6 | 37.7 | 66.3 |  |
| 3 | 80 | 5.3 | 5.3 | 5.3 | 5.3 | 5.3 | 9.5 | 15.5 | 33.7 | 61.7 |  |
| 4 | 100 | 2.5 | 2.5 | 2.5 | 3.4 | 4.6 | 9.2 | 16.3 | 34.3 | 61.7 |  |
| 6 | 150 | 1.0 | 1.3 | 2.0 | 3.0 | 4.5 | 8.4 | 15.9 | 32.1 | 62.5 |  |
| 8 | 200 | 1.0 | 1.1 | 1.8 | 2.8 | 4.4 | 8.0 | 15.9 | 32.8 | 61.4 |  |
| 10 | 250 | 0.8 | 1.1 | 1.8 | 2.7 | 4.1 | 8.1 | 15.2 | 31.7 | 61.8 |  |
| 12 | 300 | 0.7 | 1.1 | 1.8 | 2.7 | 4.0 | 7.9 | 15.2 | 32.7 | 61.7 |  |
| 14 | 350 | 0.6 | 1.0 | 1.7 | 2.8 | 4.0 | 7.9 | 15.3 | 32.2 | 61.9 |  |
| 16 | 400 | 0.5 | 1.0 | 1.7 | 2.7 | 4.0 | 8.1 | 15.1 | 26.7 |  |  |
| 18 | 450 | 0.5 | 1.0 | 1.7 | 2.7 | 4.0 | 8.0 | 15.2 | 31.9 |  |  |
| 20 | 500 | 0.5 | 1.0 | 1.7 | 2.7 | 3.9 | 8.0 | 15.1 | 31.6 |  |  |
| 24 | 600 | 0.5 | 1.0 | 1.8 | 2.7 | 4.0 | 7.9 | 15.3 |  |  |  |
| 28 | 700 | 0.5 | 0.9 | 1.6 | 2.6 | 3.8 | 7.6 | 14.6 |  |  |  |
| 30 | 750 | 0.5 | 0.9 | 1.6 | 2.6 | 3.8 | 7.5 | 14.7 |  |  |  |
| 32 | 800 | 0.5 | 0.9 | 1.6 | 2.6 | 3.9 | 7.6 | 14.7 |  |  |  |
| 36 | 900 | 0.5 | 0.9 | 1.6 | 2.6 | 3.8 | 7.5 | 14.6 |  |  |  |
| 40 | 1000 | 0.5 | 1.0 | 1.6 | 2.6 | 3.9 | 7.5 |  |  |  |  |


| Typical Mechanical Properties |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Pipe Property | Units | Value $21^{\circ} \mathrm{C}$ | Value $93^{\circ} \mathrm{C}$ | Method |
| Hydrostatic Design Basis | $\mathrm{N} / \mathrm{mm}^{2}$ | $161{ }^{(1)}$ | 121 | ASTM D2992, Proc. B (20 years) |
| Ultimate Hoop Stress at Weeping | $\mathrm{N} / \mathrm{mm}^{2}$ | 280 | 334 | ASTM D1599 |
| Circumferential |  |  |  |  |
| Hoop Tensile Strength | $\mathrm{N} / \mathrm{mm}^{2}$ | 380 | - | ASTM D2290 |
| Hoop Tensile Modulus | $\mathrm{N} / \mathrm{mm}^{2}$ | 26700 | 16300 | ASTM D2290 |
| Poisson's Ratio $\nu_{\text {na }}{ }^{(2)}$ | - | 0.61 | 0.80 | NOV FGS |
| Longitudinal |  |  |  |  |
| Axial Tensile Strength | $\mathrm{N} / \mathrm{mm}^{2}$ | 80 | 65 | ASTM D2105 |
| Axial Strength Modulus | $\mathrm{N} / \mathrm{mm}^{2}$ | 15500 | 8550 | ASTM D2105 |
| Poisson's Ratio $\nu_{\text {ah }}{ }^{(3)}$ |  | 0.35 | 0.42 | ASTM D2105 |
| Axial Bending Strength | $\mathrm{N} / \mathrm{mm}^{2}$ | 85 | - | NOV FGS |
| Axial Bending Modulus | $\mathrm{N} / \mathrm{mm}^{2}$ | 15500 | 9900 | ASTM D2925 |
| Shear Modulus | $\mathrm{N} / \mathrm{mm}^{2}$ | 12100 | 11500 | NOV FGS |
| Typical Physical Properties |  |  |  |  |
| Pipe Property | Units |  | Value | Method |
| Thermal Conductivity Pipe Wall | $\mathrm{W} / \mathrm{m}^{\circ} \mathrm{C}$ |  | 0.33 | NOV FGS |
| Thermal Expansion @ $21^{\circ} \mathrm{C}$ | $\mathrm{mm} / \mathrm{mm}^{\circ} \mathrm{C}$ |  | $18 \times 10^{-6}$ | ASTM D696 |
| Thermal Expansion @ 93 ${ }^{\circ} \mathrm{C}$ | $\mathrm{mm} / \mathrm{mm}^{\circ} \mathrm{C}$ |  | $24 \times 10^{-6}$ | ASTM D696 |
| Flow Efficient, Hazen Williams | - |  | 150 | - |
| Absolute Roughness | m |  | $5.3 \times 10^{-6}$ | - |
| Density | $\mathrm{kg} / \mathrm{m}^{3}$ |  | 1800 | - |
| Specific Gravity | - |  | 1.8 | ASTM D792 |
| Specific Heat | $\mathrm{J} / \mathrm{kg}^{\circ} \mathrm{C}$ |  | 910 | - |
| Grounding Resistance @ 500 Volt-Pipe | Ohm/m |  | $<1 \times 10^{-6}$ | ASTM D257 |
| Grounding Resistance @ 500 Volt-Ftg. | Ohm/ea |  | $<1 \times 10^{-6}$ | ASTM D257 |
| Shielding Capability | Volt |  | 100 | - |

[^10]${ }^{(2)} \nu_{\text {na }}=$ The ratio of axial strain to hoop strain resulting from stress in the hoop direction.
${ }^{(3)} \nu_{\text {ah }}=$ The ratio of hoop strain to axial strain resulting from stress in the axial direction.

Stiffness Factor per ASTM D2412 @21 ${ }^{\circ} \mathrm{C}\left(@ 70^{\circ} \mathrm{F}\right)$

| Pipe <br> Size |  | Pressure Class (bar) |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| inch | mm | $\begin{aligned} & 2410 \\ & \mathrm{lb} / \mathrm{in} \end{aligned}$ | $\begin{aligned} & 2412 \\ & \mathrm{lb} / \mathrm{in} \end{aligned}$ | $\begin{aligned} & 2414 \\ & \mathrm{lb} / \mathrm{in} \end{aligned}$ | $\begin{aligned} & 2416 \\ & \mathrm{lb} / \mathrm{in} \end{aligned}$ | $\begin{aligned} & 2420 \\ & \mathrm{lb} / \mathrm{in} \end{aligned}$ | $\begin{aligned} & 2425 \\ & \mathrm{lb} / \mathrm{in} \end{aligned}$ | $\begin{aligned} & 2432 \\ & \mathrm{lb} / \mathrm{in} \end{aligned}$ | $\begin{aligned} & 2440 \\ & \mathrm{lb} / \mathrm{in} \end{aligned}$ | $\begin{aligned} & 2450 \\ & \mathrm{lb} / \mathrm{in} \end{aligned}$ |
| 2 | 50 | 114 | 114 | 114 | 114 | 114 | 114 | 114 | 238 | 429 |
| 3 | 80 | 114 | 114 | 114 | 114 | 114 | 208 | 344 | 768 | 1448 |
| 4 | 100 | 114 | 114 | 114 | 156 | 208 | 429 | 768 | 1665 | 3078 |
| 6 | 150 | 156 | 208 | 305 | 477 | 702 | 1347 | 2593 | 5368 | 10777 |
| 8 | 200 | 344 | 385 | 640 | 990 | 1554 | 2910 | 5879 | 12432 | 23944 |
| 10 | 250 | 528 | 768 | 1251 | 1902 | 2910 | 5879 | 11176 | 23944 | 48089 |
| 12 | 300 | 768 | 1251 | 2162 | 3252 | 4887 | 9637 | 18965 | 41958 | 81568 |
| 14 | 350 | 912 | 1554 | 2748 | 4436 | 6421 | 12871 | 25312 | 54790 | 108384 |
| 16 | 400 | 1251 | 2443 | 4014 | 6421 | 9637 | 19545 | 37266 | 67294 |  |
| 18 | 450 | 1665 | 3252 | 5368 | 8580 | 12871 | 26015 | 50258 | 108384 |  |
| 20 | 500 | 2299 | 4436 | 7295 | 11585 | 17293 | 35491 | 68640 | 147168 |  |
| 24 | 600 | 3814 | 7295 | 13320 | 20138 | 30508 | 60828 | 119784 |  |  |
| 28 | 700 | 6421 | 12432 | 21358 | 34626 | 51367 | 102966 | 202495 |  |  |
| 30 | 750 | 7920 | 15220 | 26731 | 42941 | 63362 | 125772 | 250433 |  |  |
| 32 | 800 | 9537 | 18396 | 32114 | 51367 | 77093 | 154029 | 305397 |  |  |
| 36 | 900 | 13320 | 26015 | 44954 | 72785 | 108384 | 216750 | 429060 |  |  |
| 40 | 1000 | 17612 | 36371 | 63362 | 101200 | 151719 | 301810 |  |  |  |

Pipe Stiffness per ASTM D2412 @21 ${ }^{\circ} \mathrm{C}\left(@ 70^{\circ} \mathrm{F}\right)$

| Pipe <br> Size |  | Pressure Class (bar) |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| inch | mm | 2410 <br> psi | 2412 <br> psi | 2414 <br> psi | 2416 <br> psi | 2420 <br> psi | 2425 <br> psi | 2432 <br> psi | 2440 <br> psi | 2450 <br> psi |  |  |  |
| 2 | 50 | 602.8 | 602.8 | 602.8 | 602.8 | 602.8 | 602.8 | 602.8 | 1223.8 | 2149.5 |  |  |  |
| 3 | 80 | 171.6 | 171.6 | 171.6 | 171.6 | 171.6 | 308.9 | 502.7 | 1092.8 | 2003.0 |  |  |  |
| 4 | 100 | 81.9 | 81.9 | 81.9 | 111.7 | 147.8 | 299.7 | 527.7 | 1112.6 | 2001.4 |  |  |  |
| 6 | 150 | 33.0 | 43.7 | 63.8 | 98.8 | 144.5 | 273.2 | 516.2 | 1041.8 | 2028.4 |  |  |  |
| 8 | 200 | 32.0 | 35.8 | 59.1 | 90.8 | 141.3 | 260.9 | 516.8 | 1064.5 | 1991.9 |  |  |  |
| 10 | 250 | 24.7 | 35.8 | 57.9 | 87.4 | 132.7 | 263.9 | 492.9 | 1028.6 | 2003.6 |  |  |  |
| 12 | 300 | 21.2 | 34.3 | 58.9 | 88.0 | 131.2 | 254.9 | 492.4 | 1059.6 | 2000.5 |  |  |  |
| 14 | 350 | 19.0 | 32.2 | 56.6 | 90.6 | 130.3 | 257.2 | 496.5 | 1046.2 | 2008.4 |  |  |  |
| 16 | 400 | 17.5 | 33.9 | 55.3 | 87.9 | 130.9 | 261.4 | 489.5 | 866.6 |  |  |  |  |
| 18 | 450 | 17.4 | 33.7 | 55.3 | 87.8 | 130.7 | 260.1 | 493.4 | 1036.0 |  |  |  |  |
| 20 | 500 | 17.5 | 33.5 | 54.8 | 86.4 | 128.0 | 258.5 | 491.0 | 1025.3 |  |  |  |  |
| 24 | 600 | 16.8 | 31.9 | 57.8 | 86.8 | 130.6 | 256.4 | 495.5 |  |  |  |  |  |
| 28 | 700 | 16.0 | 30.7 | 52.4 | 84.4 | 124.3 | 245.4 | 473.7 |  |  |  |  |  |
| 30 | 750 | 16.0 | 30.6 | 53.3 | 85.1 | 124.6 | 243.7 | 476.3 |  |  |  |  |  |
| 32 | 800 | 16.1 | 30.5 | 52.8 | 83.9 | 124.9 | 245.9 | 478.5 |  |  |  |  |  |
| 36 | 900 | 15.6 | 30.3 | 51.9 | 83.5 | 123.4 | 243.1 | 472.3 |  |  |  |  |  |
| 40 | 1000 | 15.7 | 30.8 | 53.3 | 84.6 | 125.9 | 244.2 |  |  |  |  |  |  |

## Single Span Lengths

| Pipe <br> Size |  | Pressure Class (bar) |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |

Continuous Span Lengths

|  |  | Pressure Class (bar) |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| inch | mm | $\begin{gathered} 2410 \\ \mathrm{~m} \end{gathered}$ | $\begin{gathered} 2412 \\ \mathrm{~m} \end{gathered}$ | $\begin{gathered} 2414 \\ \mathrm{~m} \end{gathered}$ | $\begin{gathered} 2416 \\ \mathrm{~m} \end{gathered}$ | $\begin{gathered} 2420 \\ \mathrm{~m} \end{gathered}$ | $\begin{gathered} 2425 \\ \mathrm{~m} \end{gathered}$ | $\begin{gathered} 2432 \\ \mathrm{~m} \end{gathered}$ | $\begin{gathered} 2440 \\ \mathrm{~m} \end{gathered}$ | $\begin{gathered} 2450 \\ \mathrm{~m} \end{gathered}$ |
| 2 | 50 | 4.2 | 4.2 | 4.2 | 4.2 | 4.2 | 4.2 | 4.2 | 4.5 | 4.7 |
| 3 | 80 | 4.8 | 4.8 | 4.8 | 4.8 | 4.8 | 5.0 | 5.2 | 5.5 | 5.8 |
| 4 | 100 | 5.1 | 5.1 | 5.1 | 5.2 | 5.4 | 5.7 | 5.9 | 6.3 | 6.5 |
| 6 | 150 | 5.8 | 6.0 | 6.2 | 6.4 | 6.6 | 6.9 | 7.3 | 7.7 | 8.1 |
| 8 | 200 | 6.7 | 6.7 | 7.0 | 7.3 | 7.5 | 7.9 | 8.3 | 8.8 | 9.2 |
| 10 | 250 | 7.3 | 7.6 | 7.9 | 8.1 | 8.4 | 8.9 | 9.3 | 9.8 | 10.3 |
| 12 | 300 | 7.9 | 8.2 | 8.6 | 8.9 | 9.2 | 9.7 | 10.2 | 10.8 | 11.3 |
| 14 | 350 | 8.2 | 8.6 | 9.0 | 9.3 | 9.6 | 10.1 | 10.7 | 11.3 | 11.8 |
| 16 | 400 | 8.7 | 9.2 | 9.6 | 9.9 | 10.3 | 10.8 | 11.4 | 11.9 |  |
| 18 | 450 | 9.2 | 9.7 | 10.1 | 10.4 | 10.8 | 11.4 | 11.9 | 12.6 |  |
| 20 | 500 | 9.7 | 10.2 | 10.6 | 11.0 | 11.3 | 12.0 | 12.6 | 13.3 |  |
| 24 | 600 | 10.6 | 11.1 | 11.7 | 12.0 | 12.4 | 13.1 | 13.8 | 14.6 |  |
| 28 | 700 | 11.6 | 12.2 | 12.7 | 13.2 | 13.6 | 14.4 | 15.1 |  |  |
| 30 | 750 | 12.0 | 12.6 | 13.2 | 13.7 | 14.1 | 14.9 | 15.7 |  |  |
| 32 | 800 | 12.4 | 13.0 | 13.6 | 14.1 | 14.6 | 15.4 | 16.2 |  |  |
| 36 | 900 | 13.1 | 13.8 | 14.4 | 15.0 | 15.4 | 16.3 | 17.2 |  |  |
| 40 | 1000 | 13.8 | 14.6 | 15.2 | 15.8 | 16.3 | 17.2 |  |  |  |

Note: Span lengths are at $21^{\circ} \mathrm{C}\left(70^{\circ} \mathrm{F}\right)$.

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## Bondstrand'" Series 3000 Fiberglass Pipe for General Industrial Service

Uses and<br>Applications

- Boiler feed water
- Bridge, roof and floor drains
- Brine and brackish water
- Chemical process piping
- Cooling water
- Demineralized water
- Electroplating
- Fuel oil piping
- General service piping
- Mild chemicals
- Municipal waste
- Oilfield gathering, transmission lines
- Power plant, steel mill and industrial plant piping
- Sewer lines and sewer force mains
- Source and recycle water
- Sump discharge
- Vent lines
- Water mains
- Water treatment


## Performance

Working pressure to 450 psig depending on pipe size.
Operating surge pressure to 1.25 times rated operating pressure.
No thrust blocks are required at rated system pressure for most buried piping configurations and most soil conditions.

Temperatures to $150^{\circ} \mathrm{F}\left(66^{\circ} \mathrm{C}\right)$ maximum.
Full vacuum capabilities when buried and properly backfilled. For above ground use, refer to collapse pressures listed below under pipe pressure performance.
Recommended burial depth: 3 to 25 feet.
Recommended for water, waste water ( pH 1 to 8.5), moderately corrosive liquids and mild chemicals. Consult corrosion guide or Applications Engineering for recommendations for your particular application.
Individual system components may not have the same ratings as the pipe. Refer to the detailed product information for the specific components to determine the pressure rating for the system as a whole.

## Composition

## Pipe

Filament-wound fiberglass reinforced epoxy pipe with integral epoxy liner and exterior coating.

| Pipe Size |  | ASTM Designation |  |
| :---: | :---: | :---: | :---: |
| in | mm | D2310 | D2996 |
| $2-6$ | $50-150$ | RTRP 11FX | RTRP 11FX-5420 |
| $8-16$ | $200-400$ | RTRP 11FW | RTRP 11FW1-3210 |

## Fittings

2 to 6 inch
Compression-molded fiberglass reinforced epoxy elbows and tees
Filament-wound and/or mitered crosses, wyes, laterals and reducers
8 to 16 inch
Filament-wound fiberglass reinforced epoxy elbows Filament-wound and/or mitered crosses, wyes, and laterals
Contact-molded reducers

## Flanges

Flange rings:
Molded or filament-wound fiberglass
Stub ends:
Molded or centrifugally cast fiberglass

## Blind flanges

Compression-molded fiberglass or epoxy-coated cast iron or steel.

## Adhesive

Two-part epoxy adhesive for field fabrication. (Consult NOV Fiber Glass Systems for specifications.)

## Joining Systems <br> 2 to 16 inch

Bell and spigot taper/taper adhesive-bonded joint.

Other lengths available on request.

Typical Pipe Dimensions and Weights

| Nominal <br> Pipe Size |  | Outside <br> Diameter ${ }^{(1)}$ |  | Inside Diameter |  | Wall Thickness |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Total | Structural |  |
| in | mm |  |  | in | mm | in | mm | in | mm | in | mm |
| 2 | 50 | 2.38 | 60 |  |  | 2.22 | 56 | 0.080 | 2.9 | 0.069 | 1.7 |
| 3 | 80 | 3.50 | 89 | 3.33 | 85 | 0.085 | 2.1 | 0.074 | 1.9 |
| 4 | 100 | 4.51 | 115 | 4.34 | 110 | 0.087 | 2.2 | 0.077 | 1.9 |
| 6 | 150 | 6.64 | 169 | 6.40 | 163 | 0.120 | 3.0 | 0.114 | 2.9 |
| 8 | 200 | 8.60 | 218 | 8.30 | 211 | 0.150 | 3.8 | 0.113 | 2.9 |
| 10 | 250 | 10.77 | 274 | 10.42 | 265 | 0.175 | 4.4 | 0.141 | 3.6 |
| 12 | 300 | 12.70 | 323 | 12.30 | 312 | 0.200 | 5.1 | 0.170 | 4.3 |
| 14 | 350 | 14.44 | 367 | 14.01 | 356 | 0.215 | 5.5 | 0.187 | 4.8 |
| 16 | 400 | 16.50 | 419 | 16.03 | 407 | 0.235 | 6.0 | 0.210 | 5.3 |

${ }^{(1)}$ Typical outside diameters of 2 through 12 inch pipe are within API, ASTM and ANSI fiberglass and steel pipe dimensions.

| Nominal <br> Pipe Size |  | Taper <br> Angle | Taper Length |  | Pipe Weight |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | $\mathbf{m m}$ | deg | in | $\mathbf{m m}$ | lb/ft | kg/m |
| 2 | 50 | 1.75 | 1.5 | 38 | 0.5 | 0.75 |
| 3 | 80 | 1.75 | 1.7 | 43 | 0.7 | 1.05 |
| 4 | 100 | 1.75 | 1.9 | 48 | 1.0 | 1.50 |
| 6 | 150 | 1.75 | 2.8 | 71 | 1.9 | 2.85 |
| 8 | 200 | 2.00 | 2.6 | 66 | 3.1 | 4.60 |
| 10 | 250 | 2.00 | 3.1 | 79 | 4.5 | 6.70 |
| 12 | 300 | 2.00 | 3.6 | 91 | 6.1 | 9.10 |
| 14 | 350 | 2.00 | 4.2 | 107 | 7.5 | 11.15 |
| 16 | 400 | 2.00 | 4.7 | 119 | 9.4 | 14.00 |

Typical Pipe Performance

| Nominal Pipe Size |  | Static Pressure Rating at $150^{\circ} \mathrm{F}$ |  | Ultimate Internal Pressure ${ }^{(1)}$ |  | Ultimate Collapse Pressure ${ }^{(2)}$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $80^{\circ} \mathrm{F}$ | $27^{\circ} \mathrm{C}$ |  |  | $150^{\circ} \mathrm{F}$ | $99^{\circ} \mathrm{C}$ |
| in | mm |  |  | psig | bar | psig | bar | psig | bar | psig | bar |
| 2 | 50 | 450 | 31 | 3,200 | 221 | 145 | 10.0 | 125 | 8.6 |
| 3 | 80 | 400 | 28 | 2,400 | 166 | 50 | 3.4 | 45 | 3.1 |
| 4 | 100 | 325 | 22 | 2,000 | 138 | 40 | 2.8 | 35 | 2.4 |
| 6 | 150 | 300 | 20 | 2,000 | 138 | 35 | 2.4 | 30 | 2.1 |
| 8 | 200 | 150 | 10 | 900 | 62 | 25 | 1.7 | 21 | 1.4 |
| 10 | 250 | 150 | 10 | 900 | 62 | 18 | 1.2 | 12 | 0.8 |
| 12 | 300 | 150 | 10 | 900 | 62 | 12 | 0.8 | 9 | 0.6 |
| 14 | 350 | 150 | 10 | 900 | 62 | 10 | 0.7 | 7.5 | 0.5 |
| 16 | 400 | 150 | 10 | 900 | 62 | 10 | 0.7 | 7.5 | 0.5 |

[^11]Fittings Pressure Ratings ${ }^{(3)}$

| Nominal <br> Pipe Size |  | Elbows ${ }^{(1)}$ |  |  | Tees |  | Flanges ${ }^{(2)}$ |  | Blind Flanges |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | psig | bar | psig | bar | psig | bar | psig | bar |  |
| 2 | 50 | 450 | 31 | 350 | 24 | 450 | 31 | 450 | 31 |  |
| 3 | 80 | 400 | 28 | 300 | 21 | 400 | 28 | 400 | 28 |  |
| 4 | 100 | 325 | 22 | 225 | 16 | 325 | 22 | 325 | 22 |  |
| 6 | 150 | 300 | 21 | 200 | 14 | 300 | 21 | 300 | 21 |  |
| 8 | 200 | 150 | 10 | 150 | 10 | 150 | 10 | 150 | 10 |  |
| 10 | 250 | 150 | 10 | 150 | 10 | 150 | 10 | 150 | 10 |  |
| 12 | 300 | 150 | 10 | 150 | 10 | 150 | 10 | 150 | 10 |  |
| 14 | 350 | 150 | 10 | 150 | 10 | 150 | 10 | 150 | 10 |  |
| 16 | 400 | 150 | 10 | 150 | 10 | 150 | 10 | 150 | 10 |  |


| Nominal <br> Pipe Size |  | Adapters |  | Laterals, Wyes <br> and Crosses |  | Saddles |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | psig | bar | psig | bar | psig | bar |
| 2 | 50 | 450 | 30 | 200 | 13 | 300 | 20 |
| 3 | 80 | 375 | 25 | 200 | 13 | 300 | 20 |
| 4 | 100 | 300 | 20 | 200 | 13 | 200 | 13 |
| 6 | 150 | 300 | 20 | 200 | 13 | 150 | 10 |
| 8 | 200 | 150 | 10 | 150 | 10 | 150 | 10 |
| 10 | 250 | - | - | 150 | 10 | 100 | 8 |
| 12 | 300 | - | - | 150 | 10 | 75 | 5 |
| 14 | 350 | - | - | 150 | 10 | 50 | 3 |
| 16 | 400 | - | - | 150 | 10 | 50 | 3 |

${ }^{(1)}$ Ratings shown are for $90^{\circ}$ and $45^{\circ}$ elbows. Ratings in 8 to 16 inch sizes are also applicable to elbows of other angles.
${ }^{(2)}$ ANSI B16.5 CL150 psig bolt hole pattern
${ }^{(3)}$ Ratings at $150^{\circ} \mathrm{F}$

Typical Physical Properties

| Pipe Property | Units | Value | ASTM |
| :---: | :---: | :---: | :---: |
| Thermal conductivity | $\begin{gathered} \mathrm{Btu}-\mathrm{in} /\left(\mathrm{h} \cdot \mathrm{ft}^{2} \cdot{ }^{\circ} \mathrm{F}\right) \\ \mathrm{W} / \mathrm{m} \cdot{ }^{\circ} \mathrm{C} \end{gathered}$ | $\begin{gathered} 1.7 \\ 0.25 \end{gathered}$ | C177 |
| Coefficient of thermal expansion (linear) <br> ( $77^{\circ} \mathrm{F}$ to $210^{\circ} \mathrm{F}$ ) <br> ( $25^{\circ} \mathrm{C}$ to $65^{\circ} \mathrm{C}$ ) | $\begin{gathered} 10^{-6} \mathrm{in} / \mathrm{in} /{ }^{\circ} \mathrm{F} \\ 10^{-6} \mathrm{~cm} / \mathrm{cm} /{ }^{\circ} \mathrm{C} \end{gathered}$ | $\begin{gathered} 8.5 \text { to } 12 \\ 15.3 \text { to } 21.6 \end{gathered}$ | $\begin{aligned} & \text { D696 } \\ & \text { E228 } \end{aligned}$ |
| Flow coefficient | Hazen-Williams | 150.0 | - |
| Absolute roughness | $\begin{aligned} & 10^{-6} \mathrm{ft} \\ & 10^{-6} \mathrm{~m} \end{aligned}$ | $\begin{aligned} & 50.0 \\ & 15.0 \end{aligned}$ | - |
| Specific gravity | - | 1.81 | D792 |

## Typical Mechanical Properties

| Pipe Property ${ }^{(1)}$ | Units | Value ${ }^{(1)}$ |  | ASTM |
| :---: | :---: | :---: | :---: | :---: |
|  |  | 2-6 in | 8-16 in |  |
| Tensile strength Longitudinal Circumferential | $\begin{gathered} 10^{3} \mathrm{psi} \\ \mathrm{MPa} \\ 10^{3} \mathrm{psi} \\ \mathrm{MPa} \end{gathered}$ | $\begin{array}{r} 35.0 \\ 240.0 \\ 70.0 \\ 480.0 \end{array}$ | $\begin{gathered} 20.0 \\ 138.0 \\ 40.0 \\ 275.0 \end{gathered}$ | $\begin{aligned} & \text { D2105 } \\ & \text { D1599 } \end{aligned}$ |
| Tensile modulus Longitudinal <br> Circumferential | $\begin{gathered} 10^{6} \mathrm{psi} \\ \mathrm{GPa} \\ 10^{6} \mathrm{psi} \\ \mathrm{GPa} \end{gathered}$ | $\begin{array}{r} 2.7 \\ 18.6 \\ 4.2 \\ 29.0 \end{array}$ | $\begin{gathered} 1.5 \\ 10.3 \\ 2.3 \\ 15.9 \end{gathered}$ | D2105 |
| Compressive strength Longitudinal | $\begin{gathered} 10^{3} \mathrm{psi} \\ \mathrm{MPa} \end{gathered}$ | $\begin{array}{r} 35.0 \\ 240.0 \end{array}$ | $\begin{gathered} 20.0 \\ 138.0 \end{gathered}$ | - |
| Compressive modulus Longitudinal | $10^{6} \mathrm{psi}$ GPa | $\begin{array}{r} 2.7 \\ 18.6 \end{array}$ | $\begin{gathered} 1.5 \\ 10.3 \end{gathered}$ | - |
| Long-Term Hydrostatic Design Basis ${ }^{(3)}$ <br> Static, Hoop Stress 95\% LCL 20-year Life @ $150^{\circ} \mathrm{F} / 65^{\circ} \mathrm{C}$ <br> Cyclic, Hoop Stress 95\% LCL 20 -year Life @ $75^{\circ} \mathrm{F} / 24^{\circ} \mathrm{C}$ | $\begin{gathered} 10^{3} \mathrm{psi} \\ \mathrm{MPa} \\ 10^{3} \mathrm{psi} \\ \mathrm{MPa} \end{gathered}$ | $\begin{gathered} 18.9 \\ 130.3 \\ 6.4 \\ 44.1 \end{gathered}$ | $\begin{gathered} 18.9 \\ 130.3 \end{gathered}$ $-$ | D2992 Procedure B <br> D2992 Procedure A |
| Poisson's Ratio ${ }^{(2)}$ $\nu_{y x}$ | - | $\begin{aligned} & 0.17 \\ & 0.15 \end{aligned}$ | $\begin{aligned} & 0.17 \\ & 0.15 \end{aligned}$ | - |

${ }^{(1)}$ Based on structural wall thickness, at room temperature unless noted.
${ }^{(2)}$ The first subscript denotes the direction of applied stress and the second subscript the measured strain contraction. $x$ denotes longitudinal direction.
y denotes circumferential direction.
${ }^{(3)}$ Test fixtures were end type (full end thrust on samples).

| Nominal Pipe Size |  | Change in Length Due to Pressure ${ }^{(1)}$ |  | Stiffness Factor ${ }^{(2)}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | in/100 ft/100 psi | mm/10m/10 bar | $\mathrm{lb} \cdot \mathrm{in}^{3} / \mathrm{in}^{2}$ | $\mathrm{N} \cdot \mathrm{m}$ |
| 2 | 50 | 0.271 | 3.27 | 45 | 5.1 |
| 3 | 80 | 0.379 | 4.58 | 75 | 8.5 |
| 4 | 100 | 0.482 | 5.82 | 60 | 6.8 |
| 6 | 150 | 0.477 | 5.76 | 275 | 31.1 |
| 8 | 200 | 1.085 | 13.11 | 500 | 56.5 |
| 10 | 250 | 1.088 | 13.15 | 750 | 85.0 |
| 12 | 300 | 1.069 | 12.92 | 1,250 | 140.0 |
| 14 | 350 | 1.107 | 13.38 | 1,600 | 180.0 |
| 16 | 400 | 1.130 | 13.65 | 2,000 | 225.0 |

[^12]
## Support Spacing

(Values are based on a $1 / 2$ inch ( 12 mm ) deflection at mid span.) ${ }^{(4)}$

| Nominal Pipe Size |  | Single Span ${ }^{(1)}$ |  |  |  |  |  | Continuous Span ${ }^{(2)}$ |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Gases |  | $1.00{ }^{(3)}$ |  | $1.3^{(3)}$ |  | Gases |  | 1.00 |  | $1.3{ }^{(3)}$ |  |
| in | mm | ft | m | ft | m | ft | m | ft | m | ft | m | ft | m |
| 2 | 50 | 13.9 | 4.2 | 9.9 | 3.0 | 9.4 | 2.9 | 16.5 | 5.0 | 11.8 | 3.6 | 11.2 | 3.4 |
| 3 | 80 | 17.5 | 5.3 | 11.2 | 3.4 | 10.6 | 3.2 | 20.8 | 6.3 | 13.3 | 4.1 | 12.6 | 3.8 |
| 4 | 100 | 19.5 | 6.0 | 12.1 | 3.7 | 11.4 | 3.5 | 23.2 | 7.1 | 14.3 | 4.4 | 13.6 | 4.1 |
| 6 | 150 | 24.2 | 7.4 | 14.4 | 4.4 | 13.7 | 4.2 | 28.8 | 8.8 | 17.2 | 5.2 | 16.3 | 5.0 |
| 8 | 200 | 23.1 | 7.0 | 13.6 | 4.1 | 12.8 | 3.9 | 27.5 | 8.4 | 16.2 | 4.9 | 15.2 | 4.6 |
| 10 | 250 | 26.1 | 8.0 | 15.1 | 4.6 | 14.2 | 4.3 | 31.0 | 9.5 | 17.9 | 5.5 | 16.9 | 5.1 |
| 12 | 300 | 28.4 | 8.7 | 16.2 | 4.9 | 15.3 | 4.7 | 33.8 | 10.3 | 19.3 | 5.9 | 18.2 | 5.5 |
| 14 | 350 | 30.1 | 9.3 | 17.4 | 5.3 | 16.4 | 5.0 | 36.1 | 11.0 | 20.7 | 6.3 | 19.5 | 5.9 |
| 16 | 400 | 32.5 | 9.9 | 18.4 | 5.6 | 17.4 | 5.3 | 38.7 | 11.8 | 21.9 | 6.7 | 20.6 | 6.3 |

${ }^{(1)}$ For fluid temperatures above $77^{\circ} \mathrm{F}\left(25^{\circ} \mathrm{C}\right)$ reduce span lengths 0.1 -inch/ ${ }^{\circ} \mathrm{F}\left(5 \mathrm{~mm} /{ }^{\circ} \mathrm{C}\right)$
${ }^{(2)}$ Beam fixed at both ends and uniformly distributed loads. Intermediate spans may be calculate by multiplying the single span length by 1.2.
${ }^{(3)}$ Fluid specific gravity.

| Bending Radius(1) |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Nominal <br> Pipe Size |  | Minimum <br> Bending Radius | Maximum <br> Deflection <br> per 39-ft <br> Joint | Minimum Length <br> Required <br> for 10 |  |  |
| in | mm | ft | m | deg | ft |  |
| 2 | 50 | 64 | 20 | 35 | 11 |  |
| 3 | 80 | 175 | 53 | 13 | 30 |  |
| 4 | 100 | 277 | 85 | 8 | 48 |  |
| 6 | 150 | 277 | 84 | 8 | 48 |  |
| 8 | 200 | 277 | 84 | 8 | 48 |  |
| 10 | 250 | 395 | 120 | 6 | 69 |  |
| 12 | 300 | 497 | 152 | 4 | 87 |  |
| 14 | 350 | 649 | 198 | 3 | 113 |  |
| 16 | 400 | 846 | 258 | 3 | 148 |  |

(1) At rated pressure. Sharper bends may create excessive stress concentrations. Do not bend pipe until adhesive has cured.

## Guide Specification

## Pipe Construction

Pipe-The structural wall of fiberglass pipe in 2 through 16 inch nominal pipe sizes shall be constructed of continuous glass fibers wound in a matrix of anhydride cured epoxy resin in a dual angle pattern that takes optimum advantage of the tensile strength of the filaments. Pipe produced by filament-winding shall have a smooth outer surface with an outside diametral tolerance not exceeding $\pm 1.0 \%$. The pipe shall incorporate an integral liner with a nominal thickness of $0.025 \pm 0.005$ inches for 2 through 16 inch nominal sizes. The pipe shall be manufactured in accordance with ASTM Standard D2996 for filament-wound reinforced thermosetting resin pipe (RTRP). When classified under ASTM Standard D2310, the pipe shall be Type 1, Grade 1, and Class F for 2 through 16 inch nominal pipe sizes.

Pipe shall be provided in standard lengths up to 40 feet, and shall be available in 60 ft . lengths on special request to minimize the number of field joints for rapid installation.

Pressure rating-Pipe in 2 through 16 inch sizes shall be rated for a minimum internal pressure of 150 psig at $150^{\circ} \mathrm{F}$.

## Fittings Construction

Fittings in 8 through 16 inch nominal sizes shall be filament wound and incorporate a resin-rich liner of equal or greater thickness than the pipe liner and shall be constructed of the same glass and resin type for corrosion and abrasion resistance equal to that of the pipe. Fittings in 2 through 6 inch nominal sizes may be compression molded from glass and resins similar to those used in the pipe. Sprayed-up fittings shall not be permitted.

Pipe and fittings shall be joined using bell and spigot taper/taper adhesive-bonded joints or mechanical screw-on type joints.

## Physical and Mechanical Requirements

Values for physical and mechanical properties shall be no less than $95 \%$ of those shown tabulated above under Typical Physical Properties and Typical Mechanical Properties.

## Workmanship

The pipe and fittings shall be free from all defects, including delamination, indentations, pinholes, foreign inclusions, bubbles and resin-starved areas which, due to their nature, degree or extent, detrimentally affect the strength and serviceability of the pipe or fittings. Pigments or dyes may be used in the resin as long as the product is sufficiently translucent to verify the structural integrity of the structural wall. The pipe and fittings shall be as uniform as commercially practicable in color, density and other physical properties.

## Testing

Quality control testing-Samples of pipe and fittings shall be tested at random based on standard quality control practices to determine conformance of the materials to the following ASTM guidelines for testing fiberglass pipe products: ASTM D1599, D2105, D2925, D2992A or D2992B. Test samples may be hydrostatically tested by the manufacturer to 1.5 times the pressure rating for signs of leakage.

## Marking

Each component shall be marked to show the following:
Manufacturer's name and address
Nominal pipe size
Hydrostatic test pressure (if so ordered)
Date and shift of manufacture (pipe only)

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Asia Pacific No. 7A, Tuas Avenue 3 Jurong, Singapore 639407 Phone: 6568616118

Middle East P.O. Box 17324 Dubai, UAE Phone: 97148813566

## Bondstrand"' Series 3000A Fiberglass Pipe for General Industrial Service

Uses and<br>Applications

- Alcohol solutions
- Boiler feed water
- Bridge, roof and floor drains
- Brine and brackish water
- Chemical process piping
- Cooling water
- Demineralized water
- Fuel oil piping
- General service piping
- Mild chemicals
- Municipal waste
- Oilfield piping
- Potable water - NSF 61 Listed
- Power plant, steel mill and industrial plant piping
- Sewer lines and sewer force mains
- Source and recycle water
- Sump discharge
- Vent lines
- Water mains
- Water treatment

Working pressure to 450 psig depending on pipe size.
No thrust blocks are required at rated system pressure for most buried piping configurations and most soil conditions.
Temperatures to $210^{\circ} \mathrm{F}\left(99^{\circ} \mathrm{C}\right)$ maximum.
For above ground use, refer to collapse pressures listed below under pipe pressure performance.
Recommended burial depth: 3 to 25 feet.
Recommended for water, waste water ( pH 1 to 12), moderately corrosive liquids and mild chemicals. Consult corrosion guide or Applications Engineering for recommendations for your particular application.

Individual system components may not have the same ratings as the pipe. Refer to the detailed product information for the specific components to determine the pressure rating for the system as a whole.

## Composition

## Pipe

Filament-wound fiberglass reinforced epoxy pipe with integral epoxy liner and exterior coating.

| Pipe Size |  | ASTM Designation |  |
| :---: | :---: | :---: | :---: |
| in | mm | D2310 | D2996 |
| $2-6$ | $50-150$ | RTRP-11FU | RTRP-11FU1-6430 |
| $8-16$ | $200-400$ | RTRP-11FU | RTRP-11FU1-3220 |

## Fittings

2 to 6 inch
Compression-molded fiberglass reinforced epoxy elbows and tees
Filament-wound and/or mitered crosses, wyes, laterals and reducers
8 to 16 inch
Filament-wound fiberglass reinforced epoxy elbows. Filament-wound and/or mitered crosses, tees, wyes, and laterals.
Contact-molded reducers

## Flanges

Flange rings:
Molded or filament-wound fiberglass
Stub Ends:
Molded or centrifugally cast fiberglass

## Blind Flanges

Compression-molded fiberglass
Two-part epoxy adhesive for field fabrication. (Consult NOV Fiber Glass Systems for specifications.)

## Joining Systems <br> 2 to 16 inch <br> Bell and spigot taper/taper.

## Pipe Lengths

Standard 20 and 39 ft . random lengths.
Other lengths available on request.

| Nominal Pipe Size |  | Outside Diameter ${ }^{(1)}$ |  | Inside Diameter |  | Wall Thickness |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Total | Structural |  |
| in | mm |  |  | in | mm | in | mm | in | mm | in | mm |
| 2 | 50 | 2.38 | 60 |  |  | 2.22 | 56 | 0.080 | 2.0 | 0.069 | 1.7 |
| 3 | 80 | 3.50 | 89 | 3.33 | 85 | 0.085 | 2.2 | 0.074 | 1.9 |
| 4 | 100 | 4.51 | 115 | 4.34 | 110 | 0.087 | 2.2 | 0.077 | 1.9 |
| 6 | 150 | 6.64 | 169 | 6.40 | 162 | 0.120 | 3.0 | 0.114 | 2.9 |
| 8 | 200 | 8.60 | 218 | 8.30 | 211 | 0.150 | 3.8 | 0.113 | 2.9 |
| 10 | 250 | 10.77 | 274 | 10.42 | 265 | 0.175 | 4.4 | 0.141 | 3.6 |
| 12 | 300 | 12.70 | 323 | 12.30 | 312 | 0.200 | 5.1 | 0.170 | 4.3 |
| 14 | 350 | 14.44 | 367 | 14.01 | 356 | 0.215 | 5.5 | 0.187 | 4.8 |
| 16 | 400 | 16.50 | 419 | 16.03 | 407 | 0.235 | 6.0 | 0.210 | 5.3 |

${ }^{(1)}$ Typical outside diameters of 2 through 12 inch pipe are within API, ASTM and ANSI fiberglass and steel pipe dimensions.

| Nominal <br> Pipe Size |  | Taper <br> Angle | Taper Length |  | Pipe Weight |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | $\mathbf{m m}$ | Degree | in | $\mathbf{m m}$ | lb/ft | kg/m |
| 2 | 50 | 1.75 | 1.5 | 38 | 0.50 | 0.75 |
| 3 | 80 | 1.75 | 1.7 | 43 | 0.70 | 1.05 |
| 4 | 100 | 1.75 | 1.9 | 48 | 1.00 | 1.50 |
| 6 | 150 | 1.75 | 2.8 | 71 | 1.90 | 2.85 |
| 8 | 200 | 2.00 | 2.6 | 66 | 3.10 | 4.60 |
| 10 | 250 | 2.00 | 3.1 | 79 | 4.50 | 6.70 |
| 12 | 300 | 2.00 | 3.6 | 91 | 6.10 | 9.10 |
| 14 | 350 | 2.00 | 4.2 | 107 | 7.50 | 11.15 |
| 16 | 400 | 2.00 | 4.7 | 119 | 9.40 | 14.00 |

## Typical Pipe Performance

| Nominal Pipe Size |  | Static Pressure ${ }^{(3)}$ Rating at $150^{\circ} \mathrm{F}$ |  | Ultimate Internal Pressure ${ }^{(1)}$ |  | Ultimate Collapse Pressure ${ }^{(2)}$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 80 ${ }^{\circ} \mathrm{F}$ | $27^{\circ} \mathrm{C}$ |  |  | 210F | $99^{\circ} \mathrm{C}$ |
| in | mm |  |  | psig | bar | psig | bar | psig | bar | psig | bar |
| 2 | 50 | 450 | 31 | 2,160 | 149 | 165 | 11.4 | 151 | 10.4 |
| 3 | 80 | 400 | 28 | 1,579 | 109 | 66 | 4.6 | 60 | 4.2 |
| 4 | 100 | 325 | 22 | 1,258 | 87 | 34 | 2.3 | 31 | 2.1 |
| 6 | 150 | 300 | 21 | 1,275 | 88 | 35 | 2.4 | 32 | 2.2 |
| 8 | 200 | 150 | 10 | 605 | 42 | 16 | 1.1 | 14 | 1.0 |
| 10 | 250 | 150 | 10 | 678 | 47 | 16 | 1.1 | 14 | 1.0 |
| 12 | 300 | 150 | 10 | 741 | 51 | 17 | 1.2 | 15 | 1.1 |
| 14 | 350 | 150 | 10 | 739 | 51 | 15 | 1.0 | 14 | 1.0 |
| 16 | 400 | 150 | 10 | 749 | 52 | 14 | 1.0 | 13 | 0.9 |

[^13]Fittings Pressure Ratings ${ }^{(3)}$

| Nominal <br> Pipe Size |  | Elbows |  | Tees |  | Flanges ${ }^{(2)}$ |  | Blind Flanges |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | psig | bar | psig | bar | psig | bar | psig | bar |
| 2 | 50 | 450 | 31 | 350 | 24 | 450 | 31 | 450 | 31 |
| 3 | 80 | 400 | 28 | 300 | 21 | 400 | 28 | 400 | 28 |
| 4 | 100 | 325 | 22 | 225 | 16 | 325 | 22 | 325 | 22 |
| 6 | 150 | 300 | 21 | 200 | 14 | 300 | 21 | 300 | 21 |
| 8 | 200 | 200 | 14 | 150 | 10 | 200 | 14 | 200 | 14 |
| 10 | 250 | 200 | 14 | 150 | 10 | 200 | 14 | 200 | 14 |
| 12 | 300 | 200 | 14 | 150 | 10 | 200 | 14 | 200 | 14 |
| 14 | 350 | 200 | 14 | 150 | 10 | 200 | 14 | 200 | 14 |
| 16 | 400 | 200 | 14 | 150 | 10 | 200 | 14 | 200 | 14 |


| Nominal <br> Pipe Size |  | Adapters |  | Laterals, Wyes <br> and Crosses |  | Saddles |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | psig | bar | psig | bar | psig | bar |
| 2 | 50 | 450 | 30 | 200 | 13 | 300 | 20 |
| 3 | 80 | 375 | 25 | 200 | 13 | 300 | 20 |
| 4 | 100 | 300 | 20 | 200 | 13 | 200 | 13 |
| 6 | 150 | 300 | 20 | 200 | 13 | 150 | 10 |
| 8 | 200 | 150 | 10 | 150 | 10 | 150 | 10 |
| 10 | 250 | - | - | 150 | 10 | 100 | 8 |
| 12 | 300 | - | - | 150 | 10 | 75 | 5 |
| 14 | 350 | - | - | 150 | 10 | 50 | 3 |
| 16 | 400 | - | - | 150 | 10 | 50 | 3 |

${ }^{(1)}$ Ratings shown are for $90^{\circ}$ and $45^{\circ}$ elbows in 2 to 16 inch sizes. Ratings in 8 to 16 inch sizes are also applicable to elbows of other angles.
${ }^{(2)}$ ANSI B16.5 Class 150 psig bolt pattern.
${ }^{(3)}$ At $210^{\circ} \mathrm{F}$, derate $2^{\prime \prime}-6$ " sizes by a factor of 0.73 and 8 " $-16^{\prime \prime}$ sizes by a factor of 0.63 . Linearly interpolate derating factors for temperatures between $150^{\circ} \mathrm{F}$ and $210^{\circ} \mathrm{F}$.

Typical Physical Properties (Biaxial Reinforcement Structure Wall)

| Pipe Property | Units | Value | ASTM |
| :--- | :---: | :---: | :---: |
| Thermal conductivity | $\mathrm{Btu}-\mathrm{in} /\left(\mathrm{h} \cdot \mathrm{ft}^{2} \cdot{ }^{\circ} \mathrm{F}\right)$ <br> $\mathrm{W} / \mathrm{m} \cdot{ }^{\circ} \mathrm{C}$ | 1.7 <br> Coefficient of thermal expansion linear <br> $\left(2-16\right.$ inch $-77^{\circ} \mathrm{F}$ to $\left.210^{\circ} \mathrm{F}\right)$ | $10^{-6} \mathrm{in} / \mathrm{in} /{ }^{\circ} \mathrm{F}$ <br> $10^{-6} \mathrm{~cm} / \mathrm{cm} /{ }^{\circ} \mathrm{C}$ |
|  | Hazen-Williams | 10 to 13 | 18 to 24 |

Typical Mechanical Properties

| Pipe Property ${ }^{(1)}$ | Units | Value |  | ASTM |
| :---: | :---: | :---: | :---: | :---: |
|  |  | 2-6 in | 8-16 in |  |
| Tensile Strength Longitudinal Circumferential | $\begin{gathered} 10^{3} \mathrm{psi} \\ \mathrm{MPa} \\ 10^{3} \mathrm{psi} \\ \mathrm{MPa} \end{gathered}$ | $\begin{gathered} 35 \\ 240 \\ 70 \\ 483 \end{gathered}$ | $\begin{gathered} 20 \\ 138 \\ 40 \\ 276 \end{gathered}$ | $\begin{aligned} & \text { D2105 } \\ & \text { D1599 }{ }^{(4)} \end{aligned}$ |
| Tensile Modulus Longitudinal Circumferential | $\begin{gathered} 10^{6} \mathrm{psi} \\ \mathrm{GPa} \\ 10^{6} \mathrm{psi} \\ \mathrm{GPa} \end{gathered}$ | $\begin{aligned} & 3.0 \\ & 21 \\ & 4.2 \\ & 29 \end{aligned}$ | $\begin{aligned} & 2.7 \\ & 19 \\ & 3.6 \\ & 25 \end{aligned}$ | D2105 |
| Compressive Strength Longitudinal | $10^{3} \mathrm{psi}$ MPa | $\begin{array}{r} 25 \\ 169 \end{array}$ | $\begin{gathered} 20 \\ 138 \end{gathered}$ | - |
| Compressive Modulus Longitudinal | $10^{6} \mathrm{psi}$ GPa | $\begin{aligned} & 2.6 \\ & 18 \end{aligned}$ | $\begin{gathered} 1.5 \\ 10.3 \end{gathered}$ | - |
| Long-Term Hydrostatic Design Basis ${ }^{(3)}$ <br> Static, Hoop Stress 95\% LCL 20-year Life @ $150^{\circ} \mathrm{F} / 65^{\circ} \mathrm{C}$ <br> Cyclic, Hoop Stress 95\% LCL 20-year Life @ $75^{\circ} \mathrm{F} / 24^{\circ} \mathrm{C}$ | $\begin{gathered} 10^{3} \mathrm{psi} \\ \mathrm{MPa} \\ 10^{3} \mathrm{psi} \\ \mathrm{MPa} \end{gathered}$ | $\begin{gathered} 14.2 \\ 98.1 \\ 6.9 \\ 47.4 \end{gathered}$ | $\begin{gathered} 14.2 \\ 98.1 \\ 6.9 \\ 47.4 \end{gathered}$ | D2992 Procedure B <br> D2992 Procedure A |
| Poisson's Ratio ${ }^{(2)}$ <br> $\nu_{\text {yx }}$ $\nu_{\text {xy }}$ | - | $\begin{aligned} & 0.17 \\ & 0.15 \end{aligned}$ | $\begin{aligned} & 0.17 \\ & 0.15 \end{aligned}$ | - |

${ }^{(1)}$ Based on structural wall thickness, at room temperature unless noted.
${ }^{(2)}$ The first subscript denotes the direction of applied stress and the second subscript the measured strain contraction $x$ denotes longitudinal direction. y denotes circumferential direction.
${ }^{(3)}$ Test fixtures were free end type (full end thrust on samples)

| Nominal Pipe Size |  | Change in Length Due to Pressure ${ }^{(1)}$ |  | Stiffness Factor ${ }^{(2)}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | in/100 ft/100 psi | mm/10m/10 bar | $\mathrm{lb} \cdot \mathrm{in}^{3} / \mathrm{in}^{2}$ | $\mathrm{N} \cdot \mathrm{m}$ |
| 2 | 50 | 0.236 | 3.27 | 76 | 8.5 |
| 3 | 80 | 0.331 | 4.58 | 96 | 10.9 |
| 4 | 100 | 0.420 | 5.82 | 105 | 11.9 |
| 6 | 150 | 0.416 | 5.76 | 350 | 39.5 |
| 8 | 200 | 0.597 | 7.21 | 401 | 45.3 |
| 10 | 250 | 0.599 | 7.24 | 766 | 86.5 |
| 12 | 300 | 0.588 | 7.11 | 1,303 | 147.2 |
| 14 | 350 | 0.609 | 7.36 | 1,722 | 194.5 |
| 16 | 400 | 0.622 | 7.51 | 2,408 | 272.1 |

[^14]
## Support Spacing

(Values are based on a $1 / 2$ inch ( 12 mm ) deflection at mid span.) ${ }^{(4)}$

| Nominal Pipe Size |  | Single Span ${ }^{(1)}$ |  |  |  |  |  | Continuous Span ${ }^{(2)}$ |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Gases |  | $1.00{ }^{(3)}$ |  | $1.3{ }^{(3)}$ |  | Gases |  | $1.00{ }^{(3)}$ |  | $1.3{ }^{(3)}$ |  |
| in | mm | ft | m | ft | m | ft | m | ft | m | ft | m | ft | m |
| 2 | 50 | 14.2 | 4.3 | 10.1 | 3.1 | 9.6 | 2.9 | 21.2 | 6.5 | 15.1 | 4.6 | 14.3 | 4.4 |
| 3 | 80 | 17.8 | 5.4 | 11.4 | 3.5 | 10.8 | 3.3 | 26.7 | 8.1 | 17.1 | 5.2 | 16.1 | 4.9 |
| 4 | 100 | 19.9 | 6.1 | 12.3 | 3.7 | 11.6 | 3.5 | 29.8 | 9.1 | 18.4 | 5.6 | 17.4 | 5.43 |
| 6 | 150 | 24.6 | 7.5 | 14.6 | 4.5 | 13.9 | 4.2 | 36.8 | 11.2 | 21.9 | 6.7 | 20. | 6.3 |
| 8 | 200 | 27.9 | 8.5 | 16.4 | 5.0 | 15.5 | 4.7 | 41.8 | 12.7 | 24.6 | 7.5 | 23.1 | 7.0 |
| 10 | 250 | 31.4 | 9.6 | 18.1 | 5.5 | 17.1 | 5.2 | 46.9 | 14.3 | 27.1 | 8.2 | 25.5 | 7.8 |
| 12 | 300 | 34.0 | 10.4 | 19.4 | 5.9 | 18.3 | 5.6 | 50.9 | 15.5 | 29.0 | 8.8 | 27.3 | 8.3 |
| 14 | 350 | 36.2 | 11.0 | 20.7 | 6.3 | 19.5 | 5.9 | 54.2 | 16.5 | 31.0 | 9.5 | 29.2 | 8.9 |
| 16 | 400 | 38.7 | 11.8 | 21.9 | 6.7 | 20.6 | 6.3 | 57.9 | 17.6 | 32.8 | 10.0 | 30.9 | 9.4 |

${ }^{(1)}$ For fluid temperatures above $77^{\circ} \mathrm{F}\left(25^{\circ} \mathrm{C}\right)$ reduce span lengths 0.1 -inch/ ${ }^{\circ} \mathrm{F}\left(5 \mathrm{~mm} /{ }^{\circ} \mathrm{C}\right)$
${ }^{(2)}$ Beam fixed at both ends and uniformly distributed loads. Intermediate spans may be calculate by multiplying the single span length by 1.2.
${ }^{(3)}$ Fluid specific gravity.

| Bending Radius |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Nominal Pipe Size |  | Minimum <br> Bending Radius |  | Maximum Deflection per 39-ft Joint | Minimum Length <br> Required <br> for $10^{\circ}$ Change |  |
| in | mm | ft | m | deg | ft | m |
| 2 | 50 | 64 | 20 | 35 | 11 | 3 |
| 3 | 80 | 175 | 53 | 13 | 30 | 9 |
| 4 | 100 | 277 | 85 | 8 | 48 | 15 |
| 6 | 150 | 266 | 81 | 8 | 46 | 14 |
| 8 | 200 | 498 | 152 | 4 | 87 | 26 |
| 10 | 250 | 710 | 216 | 3 | 124 | 38 |
| 12 | 300 | 895 | 273 | 2 | 156 | 48 |
| 14 | 350 | 1,169 | 356 | 2 | 204 | 62 |
| 16 | 400 | 1,523 | 464 | 1 | 266 | 81 |

[^15]
## Guide Specification

Pipe-The structural wall of fiberglass pipe in 2 through 16 inch nominal pipe sizes shall be constructed of continuous glass fibers wound in a matrix of aromatic amine cured epoxy resin in a dual angle pattern that takes optimum advantage of the tensile strength of the filaments. Pipe produced by filament-winding shall have a smooth outer surface with an outside diametric tolerance not exceeding $\pm 1.0 \%$. The pipe shall incorporate an integral liner with a nominal thickness of 0.005 , to 0.010 inches for 2 through 6-inch nominal sizes, and $0.025, \pm 0.005$ inches for 8 through 16 inch nominal sizes. The pipe shall be manufactured in accordance with ASTM Standard D2996 for filament-wound reinforced thermosetting resin pipe (RTRP). When classified under ASTM Standard D2310, the pipe shall be Type 1, Grade 1, and Class F for 2 through 16 inch nominal pipe sizes.
Pipe shall be provided in standard lengths up to 40 feet, and shall be available in 60 ft lengths on special request to minimize the number of field joints for rapid installation.
Pressure Rating-Pipe in 2 through 16 inch sizes shall be rated for a minimum internal pressure of 150 psig at $150^{\circ} \mathrm{F}$ and capable of $210^{\circ} \mathrm{F}$ service conditions in accordance with the derating factor. In 2 through 6 inch sizes the pipe shall have a full vacuum capability at $80^{\circ} \mathrm{F}$ when installed above ground.

## Fittings Construction

Fittings in 8 through 16 inch nominal sizes shall be filament wound and incorporate a resin-rich liner of equal or greater thickness than the pipe liner and shall be constructed of the same glass and resin type for corrosion and abrasion resistance equal to that of the pipe. Fittings in 2 through 6 inch nominal sizes may be compression molded from glass and resins similar to those used in the pipe. Contact molded, sprayed up or hand laid up fittings shall not be permitted.
Pipe and fittings shall be joined using bell and spigot taper/taper joints bonded with epoxy adhesive.

## Physical and Mechanical Requirements

Measured values for physical andmechanical properties shall be within $\pm 15 \%$ of those showntabulated above under Typical Physical Properties and Typical Mechanical Properties.

## Workmanship

The pipe and fittings shall be free from all defects, including delamination, indentations, pinholes, foreign inclusions, bubbles and resin-starved areas which, due to their nature, degree or extent, detrimentally affect the strength and serviceability of the pipe or fittings. Pigments or dyes may be used in the resin as long as the product is sufficiently translucent to verify the structural integrity of the structural wall. The pipe and fittings shall be as uniform as commercially practicable in color, density and other physical properties.

## Testing

Quality control testing-Samples of pipe and fittings shall be tested at random based on standard quality control practices to determine conformance of the materials to the following ASTM guidelines for testing fiberglass pipe products: ASTM D1599, D2105, D2925, D2992A or D2992B. Test samples may be hydrostatically tested by the manufacturer to 1.5 times the pressure rating for signs of leakage.

## Marking

```
Each component shall be marked to show the following:
Manufacturer's name and address
Nominal pipe size
Hydrostatic test pressure (if so ordered)
Date and shift of manufacture (pipe only)
```

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## Uses and Applications

- Boiler feed water
- Brine and brackish water
- Chemical process piping
- Cooling water
- Demineralized water
- Electroplating
- Fire mains
- Industrial plant piping
- Municipal waste
- Oilfield gathering, transmission lines
- Power plant and steel mill piping
- Sewer lines and sewer force mains
- Source and recycle water
- Sump discharge
- Vent lines
- Water mains
- Water treatment


## Performance

Pipe and fittings are rated at 200 psig.
Operating plus surge pressures to 1.25 times rated operating pressure occurring three times or less per 24-hour period.

Temperatures to $150^{\circ} \mathrm{F}\left(66^{\circ} \mathrm{C}\right)$ maximum. Sub-zero temperatures will not affect the physical properties.
Full vacuum capabilities when buried and properly backfilled. For above ground use, refer to collapse pressures listed below under pipe pressure Typical Pipe Performance.
Recommended burial depth: 3 to 25 feet.
Recommended for water, waste water ( pH 1 to 8.5), and mild chemicals. Consult Chemical Resistance Guide or contact NOV Fiber Glass Systems for recommendations for your particular application.

Individual system components may not have the same ratings as the pipe. Refer to the detailed product information for the specific components to determine the pressure rating for the system as a whole.

## Composition Pipe

Filament-wound fiberglass reinforced epoxy pipe with integral epoxy liner and exterior coating.

| Pipe Size |  | ASTM Designation |  |
| :---: | :---: | :---: | :---: |
| in | mm | D2310 | D2996 |
| $8-16$ | $200-400$ | RTRP 11FW | RTRP 11FW1-3210 |

## Fittings

8 to 16 inch:
Filament-wound fiberglass reinforced epoxy elbows
Mitered tees, crosses, wyes, and laterals

## Flanges

Molded or filament-wound fiberglass flange rings
Molded or centrifugally cast fiberglass stub ends

## Blind flanges

Compression-molded fiberglass or epoxy-coated cast iron or steel.

## Adhesive

Two-part epoxy adhesive.

| Joining Systems | 8 through 16 inch: |
| :--- | :--- |
|  | Bell and spigot taper/taper adhesive-bonded joint. |

## Pipe Lengths

Standard 20 and 39 ft . random lengths.
Other lengths available on request.

## Fittings

Elbows:
$8-16$ inch: $90^{\circ}, 60^{\circ}, 45^{\circ}, 30^{\circ}, 22 \frac{1}{2} 2^{\circ}, 11 \frac{1}{4} 4^{\circ}$
Tees, Flanges, Blind Flanges
Concentric Reducers, Reducer Bushings, Sleeve Couplings
For fittings dimensions, refer to the most recent release of product data sheets.

| Nominal <br> Pipe Size |  | Outside Diameter ${ }^{(1)}$ |  | Inside Diameter |  | Wall Thickness |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Total | Structural |  |
| in | mm |  |  | in | mm | in | mm | in | mm | in | mm |
| 8 | 200 | 8.60 | 219 |  |  | 8.30 | 211 | 0.150 | 3.8 | 0.125 | 3.2 |
| 10 | 250 | 10.77 | 273 | 10.42 | 264 | 0.175 | 4.4 | 0.145 | 3.7 |
| 12 | 300 | 12.70 | 324 | 12.30 | 312 | 0.200 | 5.1 | 0.175 | 4.4 |
| 14 | 350 | 14.44 | 367 | 14.01 | 356 | 0.215 | 5.5 | 0.185 | 4.7 |
| 16 | 400 | 16.50 | 419 | 16.03 | 407 | 0.235 | 6.0 | 0.205 | 5.2 |

${ }^{(1)}$ Typical outside diameters of 8 through 12 inch pipe are within API, ASTM and ANSI fiberglass and steel pipe dimensions.

| Nominal <br> Pipe Size |  | Taper <br> Angle | Taper <br> Length |  | Pipe <br> Weight |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | $\mathbf{m m}$ | deg | in | $\mathbf{m m}$ | $\mathbf{l b} / \mathbf{f t}$ | $\mathbf{k g} / \mathbf{m}$ |
| 8 | 200 | 2.00 | 2.6 | 66 | 3.1 | 4.60 |
| 10 | 250 | 2.00 | 3.1 | 79 | 4.5 | 6.70 |
| 12 | 300 | 2.00 | 3.6 | 91 | 6.1 | 9.10 |
| 14 | 350 | 2.00 | 4.2 | 107 | 7.5 | 11.15 |
| 16 | 400 | 2.00 | 4.7 | 119 | 9.4 | 14.00 |

## Typical Pipe Performance

| Nominal Pipe Size |  | Static Pressure Rating at $150^{\circ} \mathrm{F}$ |  | Ultimate Internal Pressure ${ }^{(1)}$ |  | Ultimate Collapse Pressure ${ }^{(2)}$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 80 ${ }^{\circ}$ | $27^{\circ} \mathrm{C}$ |  |  | 150F | $65.6^{\circ} \mathrm{C}$ |
| in | mm |  |  | psig | bar | psig | bar | psig | bar | psig | bar |
| 8 | 200 | 200 | 14 | 1200 | 83 | 25 | 1.7 | 21 | 1.4 |
| 10 | 250 | 200 | 14 | 1200 | 83 | 18 | 1.2 | 12 | 0.8 |
| 12 | 300 | 200 | 14 | 1200 | 83 | 12 | 0.8 | 9 | 0.6 |
| 14 | 350 | 200 | 14 | 1200 | 83 | 10 | 0.7 | 7.5 | 0.5 |
| 16 | 400 | 200 | 14 | 1200 | 83 | 10 | 0.7 | 7.5 | 0.5 |

${ }^{(1)}$ Quality control minimum, biaxially loading.
${ }^{(2)}$ For vacuum service above ground in sizes 10 inches and above consult NOV Fiber Glass Systems.

## Fittings Pressure Ratings

| Nominal <br> Pipe Size |  | Elbows and <br> Tees |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | psig | bar |  | psig | bar | psind <br> Flanges |  |
| 8 | 200 | 200 | 14 | 200 | 14 | 200 | 14 |  |
| 10 | 250 | 200 | 14 | 200 | 14 | 200 | 14 |  |
| 12 | 300 | 200 | 14 | 200 | 14 | 200 | 14 |  |
| 14 | 350 | 200 | 14 | 200 | 14 | 200 | 14 |  |
| 16 | 400 | 200 | 14 | 200 | 14 | 200 | 14 |  |

[^16]Typical Physical Properties

| Pipe Property | Units | Value | ASTM |
| :---: | :---: | :---: | :---: |
| Thermal conductivity | $\begin{gathered} \text { Btu-in } /\left(\mathrm{h} \cdot \mathrm{ft}^{2 \cdot} \cdot{ }^{\circ} \mathrm{F}\right) \\ \mathrm{W} / \mathrm{m} \cdot{ }^{\circ} \mathrm{C} \end{gathered}$ | $\begin{gathered} 1.7 \\ 0.25 \end{gathered}$ | C177 |
| Coefficient of thermal expansion (linear) (8-16 inch) | $\begin{gathered} 10^{-6} \mathrm{in} / \mathrm{in} /{ }^{\circ} \mathrm{F} \\ 10^{-6} \mathrm{~cm} / \mathrm{cm} /{ }^{\circ} \mathrm{C} \end{gathered}$ | $\begin{aligned} & 12.0 \\ & 21.6 \end{aligned}$ | $\begin{aligned} & \text { D696 } \\ & \text { D228 } \end{aligned}$ |
| Flow coefficient | Hazen-Williams | 150.0 | - |
| Absolute roughness | $\begin{aligned} & 10^{-6} \mathrm{ft} \\ & 10^{-6} \mathrm{~m} \end{aligned}$ | $\begin{aligned} & 50.0 \\ & 15.0 \end{aligned}$ | - |
| Specific gravity | - | 1.81 | D792 |

## Typical Mechanical Properties

| Pipe Property ${ }^{(1)}$ | Units | Value ${ }^{(1)}$ | ASTM |
| :---: | :---: | :---: | :---: |
| Tensile strength Longitudinal Circumferential | $\begin{gathered} 10^{3} \mathrm{psi} \\ \mathrm{MPa} \\ 10^{3} \mathrm{psi} \\ \mathrm{MPa} \end{gathered}$ | $\begin{array}{r} 35.0 \\ 240.0 \\ 70.0 \\ 480.0 \end{array}$ | $\begin{aligned} & \text { D2105 } \\ & \text { D1599 } \end{aligned}$ |
| Tensile modulus Longitudinal Circumferential | $\begin{gathered} 10^{6} \mathrm{psi} \\ \mathrm{GPa} \\ 10^{6} \mathrm{psi} \\ \mathrm{GPa} \end{gathered}$ | $\begin{array}{r} 2.7 \\ 18.6 \\ 4.2 \\ 29.0 \end{array}$ | D2105 |
| Compressive strength Longitudinal | $\begin{aligned} & 10^{3} \mathrm{psi} \\ & \mathrm{MPa} \end{aligned}$ | $\begin{array}{r} 35.0 \\ 240.0 \end{array}$ | - |
| Compressive modulus Longitudinal | $\begin{gathered} 10^{6} \mathrm{psi} \\ \mathrm{GPa} \end{gathered}$ | $\begin{array}{r} 2.7 \\ 18.6 \end{array}$ | - |
| Long-Term Hydrostatic Design Basis ${ }^{(3)}$ <br> Static, Hoop Stress $95 \%$ LCL 20 -year Life @ $150^{\circ} \mathrm{F} / 65^{\circ} \mathrm{C}$ Cyclic, Hoop Stress $95 \%$ LCL 20 -year Life @ $75^{\circ} \mathrm{F} / 24^{\circ} \mathrm{C}$ | $\begin{gathered} 10^{3} \mathrm{psi} \\ \mathrm{MPa} \\ 10^{3} \mathrm{psi} \\ \mathrm{MPa} \end{gathered}$ | $\begin{gathered} 18.9 \\ 130.3 \\ 6.4 \\ 44.1 \end{gathered}$ | D2992 Procedure B <br> D2992 Procedure A |
| Poisson's Ratio ${ }^{(2)}$ $v_{y x}$ $v_{x y}$ | - | $\begin{aligned} & 0.17 \\ & 0.15 \end{aligned}$ | - |

(1) Based on structural wall thickness, at room temperature unless noted.
(2) The first subscript denotes the direction of applied stress and the second subscript the measured strain contraction. $x$ denotes longitudinal direction
y denotes circumferential direction
${ }^{(3)}$ Test fixtures were free-end type (full end thrust on samples).

| Nominal Pipe Size |  | Change in Length Due to Pressure ${ }^{(1)}$ |  | Stiffness Factor ${ }^{(2)}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | in/100 ft/100 psi | mm/30.5m/6.9bar | $\mathrm{lb} \cdot \mathrm{in}^{3} / \mathrm{in}^{2}$ | $\mathrm{N} \cdot \mathrm{m}$ |
| 8 | 200 | 0.565 | 6.82 | 500 | 56.5 |
| 10 | 250 | 0.612 | 7.39 | 750 | 84.7 |
| 12 | 300 | 0.599 | 7.24 | 1,250 | 141.2 |
| 14 | 350 | 0.646 | 7.81 | 1,600 | 180.8 |
| 16 | 400 | 0.668 | 8.07 | 2,000 | 226.0 |

[^17]
## Support Spacing

(Values are based on a $1 / 2$ inch ( 12 mm ) deflection at mid span.)

| Nominal Pipe Size |  | Single Span ${ }^{(1)}$ |  |  |  |  |  | Continuous Span ${ }^{(2)}$ |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Gases |  | $1.00{ }^{(3)}$ |  | 1.25 |  | Gases |  | 1.00 |  | 1.25 |  |
| in | mm | ft | m | ft | m | ft | m | ft | m | ft | m | ft | m |
| 8 | 200 | 26.8 | 8.2 | 15.7 | 4.8 | 14.8 | 4.5 | 40.0 | 12.2 | 23.5 | 7.2 | 22.0 | 6.7 |
| 10 | 250 | 30.2 | 9.2 | 17.4 | 5.3 | 16.4 | 5.0 | 45.2 | 13.8 | 26.1 | 8.0 | 24.6 | 7.5 |
| 12 | 300 | 32.9 | 10.0 | 18.8 | 5.7 | 17.7 | 5.4 | 49.3 | 15.0 | 28.1 | 8.6 | 26.5 | 8.1 |
| 14 | 350 | 35.2 | 10.7 | 20.1 | 6.1 | 18.9 | 5.8 | 52.6 | 16.0 | 30.1 | 9.2 | 28.3 | 8.6 |
| 16 | 400 | 37.7 | 11.5 | 21.4 | 6.5 | 20.1 | 6.1 | 56.4 | 17.2 | 31.9 | 9.7 | 30.1 | 9.2 |

${ }^{(1)}$ For fluid temperatures above $77^{\circ} \mathrm{F}\left(25^{\circ} \mathrm{C}\right)$ reduce span lengths 0.1 -inch/ ${ }^{\circ} \mathrm{F}\left(5 \mathrm{~mm} /{ }^{\circ} \mathrm{C}\right)$
${ }^{(2)}$ Beam fixed at both ends and uniformly distributed loads. Intermediate spans may be calculate by multiplying the single span length by 1.2
${ }^{(3)}$ Fluid specific gravity

Bending Radius

| Nominal <br> Pipe Size |  | Minimum <br> Bending Radius |  | Maximum <br> Deflection <br> per 39-ft <br> Joint | Minimum Length <br> Required <br> for 10 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | ft | m | deg | ft | $\mathbf{m}$ |
| 8 | 200 | 209 | 64 | 11 | 37 | 11 |
| 10 | 250 | 281 | 86 | 8 | 49 | 15 |
| 12 | 300 | 343 | 105 | 7 | 60 | 18 |
| 14 | 350 | 418 | 127 | 5 | 73 | 22 |
| 16 | 400 | 507 | 155 | 4 | 89 | 27 |

${ }^{(1)}$ At rated pressure. Sharper bends may create excessive stress concentrations. Do not bend pipe until adhesive has cured

This specification covers approval, performance, materials and physical properties requirements for general industrial service piping in 8 through 16 inch nominal pipe sizes at operating temperatures to $150^{\circ} \mathrm{F}$.

## Performance

 RequirementsPipe, fittings and other components furnished under this specification shall be rated for service to 200 psig at $150^{\circ} \mathrm{F}$. All components shall be rated at or above the design pressure of the system. When classified in accordance with ASTM standards, the pipe shall meet the following cell limits:

| Nominal <br> Pipe Size |  | ASTM Designation |  |
| :---: | :---: | :---: | :---: |
| in | mm | D2310 | D2996 |
| $8-16$ | $200-400$ | RTRP 11FW | RTRP 11FW1-3210 |

## Materials

Liner-All filament-wound pipe shall incorporate an integral liner with a nominal thickness of 0.025 $\pm 0.005$ inches for 8 through 16 inch nominal sizes. The resin system used in the liner shall be a chemically resistant thermosetting epoxy resin suitable for the intended service.
Structural wall—Pipe shall be filament wound using continuous glass fiber reinforcements with a resin-compatible finish and a chemically resistant thermosetting epoxy resin. The glass filaments shall be wound in a dual-angle pattern that takes optimum advantage of the tensile strength of the filaments. The glass fiber content of the reinforced wall shall not be less than $60 \%$ by weight. Pigments or dies may be used in the resin as long as the product remains translucent.

External surface-The pipe shall have a typical 0.005 -inch thick resin-rich coating with organic fibrous reinforcement. This protection must be provided for both above and below-ground pipe installations. All external surfaces must be resistant to anticipated corrosion imposed by the service and the environment.
Fittings-Fittings supplied under this specification shall be filament-wound, compression molded, centrifugally cast, or manufactured from mitered pipe sections. The glass fiber content of the structural portion of compression-molded and filament-wound fittings shall not be less than $55 \%$ by weight.

## Joining Methods

Adhesive-Bonded Bell and Spigot-Both tapered bell and tapered spigot shall have matching taper angles and shall be joined by bonding with an epoxy adhesive. The nominal taper angle shall be $2^{\circ}$ on 8 through 16 inch nominal pipe sizes. The adhesive shall be a two part epoxy supplied as a kit with all necessary application materials.
Flanges-Flanges shall be two-piece van Stone type provided with raised grooves on the sealing surface. Fiberglass-reinforced compression-molded or centrifugally cast stub ends are to be adhesive bonded to the pipe or fitting.

Pipe Construction Pipe—Pipe shall be manufactured to steel pipe outside diameters in 8 through 12 inch nominal pipe sizes and should be based on nominal inside diameters in 14 inch sizes and above. Outside diameter tolerances shall not exceed $\pm 1.0 \%$. Pipe shall be provided in 40 feet random lengths ( 34 through 42 ft . unless otherwise specified. Up to $10 \%$ shorts may be included in any shipment unless otherwise agreed upon in writing between purchaser and manufacturer.
Wall thickness—The total wall thickness of pipe furnished to this specification shall not at any point less than 87.5 percent of the nominal thickness. Nominal wall thickness shall have dimensions as given in the manufacturer's published literature.
Fittings and flanges-Fittings and flanges shall have dimensions as given in the manufacturer's published literature. Flanges shall be drilled to match ANSI B16.5, Class 150 unless specified otherwise in the purchase order.

## Physical and Mechanical Requirements

Values for physical and mechanical properties shall be no less than $95 \%$ of those shown tabulated above under Typical Physical Properties and Typical Mechanical Properties.

## Workmanship

The pipe and fittings shall be free from all defects, including delamination, indentations, pinholes, foreign inclusions, bubbles and resin-starved areas which, due to their nature, degree or extent, detrimentally affect the strength and serviceability of the pipe or fittings. Pigments or dyes may be used in the resin as long as the product is sufficiently translucent to verify the structural integrity of the structural wall. The pipe and fittings shall be as uniform as commercially practicable in color, density and other physical properties.

## Testing

Quality control testing-Samples of pipe and fittings shall be tested at random based on standard quality control practices to determine conformance of the materials to the following tests: weight, taper angle, short-term rupture strength, cyclic pressure performance, ring crush strength and degree of cure. Each item shall be visually inspected for workmanship.
Proof testing—All components shall be hydrostatically tested by the manufacturer to 1.5 times the pressure rating for signs of leakage or porosity.

## Marking

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# Bondstrand"' Series 3200A Fiberglass Pipe (General Industrial Service) (For sizes 2 through 6 inch, use Series 3000A pipe and fittings products) 

Uses and
Applications

- Boiler feed water
- Brine and brackish water
- Chemical process piping
- Cooling water
- Demineralized water
- Electroplating
- Industrial plant piping
- Municipal waste
- Oilfield piping
- Potable Water - NSF 61 Listed
- Power plant and steel mill piping
- Sewer lines and sewer force mains
- Source and recycle water
- Sump discharge
- Vent lines
- Water mains
- Water treatment


## Performance

Pipe and fittings are rated at 200 psig.
Operating plus surge pressures to 1.25 times rated operating pressure occurring three times or less per 24-hour period.
No thrust blocks are required at rated system pressure for most buried piping configurations and most soil conditions. For above ground use, consult NOV Fiber Glass Systems.

Temperatures to $210^{\circ} \mathrm{F}\left(99^{\circ} \mathrm{C}\right)$ maximum. Sub-zero temperatures will not affect the physical properties. Water in pipe must not be allowed to freeze.
Vacuum to -14.7 psig when buried and properly backfilled. For above ground use, refer to collapse pressures listed below under pipe pressure Typical Pipe Performance.

Recommended burial depth: 3 to 25 feet.
Recommended for water, waste water ( pH 1 to 12), and mild chemicals. Consult Bondstrand Corrosion Guide or contact NOV Fiber Glass Systems for recommendations for your particular application.

Individual system components may not have the same ratings as the pipe. Refer to the detailed product information for the specific components to determine the pressure rating for the system as a whole.

## Composition

## Pipe

Filament-wound fiberglass reinforced epoxy pipe with integral epoxy liner and exterior coating

| Pipe Size |  | ASTM Designation |  |
| :---: | :---: | :---: | :---: |
| in | mm | D2310 | D2996 |
| $8-16$ | $200-400$ | RTRP 11FU | RTRP 11FU1-6430 |

## Fittings

8 to 16 inch
Filament-wound fiberglass reinforced epoxy elbows
Mitered tees, crosses, wyes, and laterals

## Flanges

Flange rings - Filament-wound fiberglass
Stub ends - Centrifugally cast fiberglass

## Blind flanges

Reference Cl3050 for fittings dimensions

## Adhesive

NOV Fiber Glass Systems two-part epoxy adhesive for field fabrication.

| Joining Systems | 8 to 16 -inch: |
| :--- | :--- |
|  | Bell and spigot taper/taper adhesive-bonded joint. |

Pipe Lengths
Standard 20 and 39 foot random lengths.
Other lengths available on request.

| Nominal Pipe Size |  | Outside Diameter ${ }^{(1)}$ |  | Inside Diameter |  | Wall Thickness |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Total | Structural |  |
| in | mm |  |  | in | mm | in | mm | in | mm | in | mm |
| 8 | 200 | 8.60 | 219 |  |  | 8.30 | 211 | 0.150 | 3.8 | 0.125 | 3.2 |
| 10 | 250 | 10.77 | 273 | 10.42 | 264 | 0.175 | 4.4 | 0.145 | 3.7 |
| 12 | 300 | 12.70 | 324 | 12.30 | 312 | 0.200 | 5.1 | 0.175 | 4.4 |
| 14 | 350 | 14.44 | 367 | 14.01 | 356 | 0.215 | 5.5 | 0.185 | 4.7 |
| 16 | 400 | 16.50 | 419 | 16.03 | 407 | 0.235 | 6.0 | 0.205 | 5.2 |

${ }^{(1)}$ Typical outside diameters of 8 through 12 inch pipe are within API, ASTM and ANSI fiberglass and steel pipe dimensions.

| Nominal <br> Pipe Size |  | Taper <br> Angle | Taper <br> Length |  | Pipe Weight |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | $\mathbf{m m}$ | deg | in | $\mathbf{m m}$ | $\mathbf{l b} / \mathbf{f t}$ | $\mathbf{k g} / \mathbf{m}$ |
| 8 | 200 | 2.00 | 2.6 | 66 | 3.10 | 4.60 |
| 10 | 250 | 2.00 | 3.1 | 79 | 4.50 | 6.70 |
| 12 | 300 | 2.00 | 3.6 | 91 | 6.10 | 9.10 |
| 14 | 350 | 2.00 | 4.2 | 107 | 7.50 | 11.15 |
| 16 | 400 | 2.00 | 4.7 | 119 | 9.40 | 14.00 |

Typical Pipe Performance

| Nominal Pipe Size |  | Static Pressure <br> Rating at $150^{\circ} F^{(3)}$ |  | Ultimate Internal Pressure ${ }^{(1)}$ |  | Ultimate Collapse Pressure ${ }^{(2)}$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $80^{\circ} \mathrm{F}$ | $27^{\circ} \mathrm{C}$ |  |  | $210^{\circ} \mathrm{F}$ | $99^{\circ} \mathrm{C}$ |
| in | mm |  |  | psig | bar | psig | bar | psig | bar | psig | bar |
| 8 | 200 | 200 | 14 | 1074 | 74 | 21 | 1.5 | 18 | 1.2 |
| 10 | 250 | 200 | 14 | 994 | 69 | 17 | 1.2 | 14 | 1.0 |
| 12 | 300 | 200 | 14 | 1017 | 70 | 18 | 1.2 | 15 | 1.1 |
| 14 | 350 | 200 | 14 | 945 | 65 | 15 | 1.0 | 12 | 0.8 |
| 16 | 400 | 200 | 14 | 916 | 63 | 13 | 0.9 | 11 | 0.8 |

${ }^{(1)}$ Quality control minimum, biaxial loading
${ }^{(2)}$ For vacuum service above ground consult NOV Fiber Glass Systems.
${ }^{(3)} \mathrm{At} 210^{\circ} \mathrm{F}$ derate the pipe by a factor of 0.73 , linearly interpolate derating factors for temperatures between $150^{\circ} \mathrm{F}$ and $210^{\circ} \mathrm{F}$.

Fittings Pressure Ratings ${ }^{(3)}$

| Nominal <br> Pipe Size |  | Elbows and <br> Tees $^{(1)}$ |  | Flanges $^{(2)}$ |  | Blind <br> Flanges |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | psig | bar | psig | bar | psig | bar |
| 8 | 200 | 200 | 14 | 200 | 14 | 200 | 14 |
| 10 | 250 | 200 | 14 | 200 | 14 | 200 | 14 |
| 12 | 300 | 200 | 14 | 200 | 14 | 200 | 14 |
| 14 | 350 | 200 | 14 | 200 | 14 | 200 | 14 |
| 16 | 400 | 200 | 14 | 200 | 14 | 200 | 14 |

${ }^{(1)}$ Ratings shown are for $90^{\circ}$ and $45^{\circ}$ elbows. Ratings in 8 to 16 inch sizes are also applicable to elbows of other angles.
${ }^{(2)}$ ANSI B16.5 150 psig bolt pattern
${ }^{(3)}$ At $210^{\circ} \mathrm{F}$ derate the pipe by a factor of 0.73 , linearly interpolate derating factors for temperatures between $150^{\circ} \mathrm{F}$ and $210^{\circ} \mathrm{F}$.

## Typical Physical Properties

| Pipe Property | Units | Value | ASTM |
| :---: | :---: | :---: | :---: |
| Thermal conductivity | $\begin{gathered} \mathrm{Btu}-\mathrm{in} /\left(\mathrm{h} \cdot \mathrm{ft}^{2 \cdot} \cdot{ }^{\circ} \mathrm{F}\right) \\ \mathrm{W} / \mathrm{m} \cdot{ }^{\circ} \mathrm{C} \end{gathered}$ | $\begin{gathered} 1.7 \\ 0.25 \end{gathered}$ | C177 |
| Coefficient of thermal expansion (linear) (8-16 inch) | $\begin{gathered} 10^{-6} \mathrm{in} / \mathrm{in} /{ }^{\circ} \mathrm{F} \\ 10^{-6} \mathrm{~cm} / \mathrm{cm} /{ }^{\circ} \mathrm{C} \end{gathered}$ | 10 to 13 <br> 18 to 24 | $\begin{aligned} & \text { D696 } \\ & \text { E228 } \end{aligned}$ |
| Flow coefficient | Hazen-Williams | 150.0 | - |
| Absolute roughness | $\begin{aligned} & 10^{-6} \mathrm{ft} \\ & 10^{-6} \mathrm{~m} \end{aligned}$ | $\begin{aligned} & 50.0 \\ & 15.0 \end{aligned}$ | - |
| Specific gravity | - | 1.81 | D792 |

Typical Mechanical Properties

| Pipe Property ${ }^{(1)}$ | Units | Value | ASTM |
| :---: | :---: | :---: | :---: |
| Tensile strength Longitudinal Circumferential | $\begin{gathered} 10^{3} \mathrm{psi} \\ \mathrm{MPa} \\ 10^{3} \mathrm{psi} \\ \mathrm{MPa} \end{gathered}$ | $\begin{gathered} 35 \\ 240 \\ 70 \\ 483 \end{gathered}$ | $\begin{aligned} & \text { D2105 } \\ & \text { D1599 } \end{aligned}$ |
| Tensile modulus Longitudinal Circumferential | $10^{6} \mathrm{psi}$ GPa $10^{6} \mathrm{psi}$ GPa | $\begin{aligned} & 2.7 \\ & 21 \\ & 4.2 \\ & 29 \end{aligned}$ | D2105 |
| Compressive strength Longitudinal | $10^{3} \mathrm{psi}$ $\mathrm{MPa}$ | $\begin{gathered} 25 \\ 169 \end{gathered}$ | - |
| Compressive modulus Longitudinal | $\begin{gathered} 10^{6} \mathrm{psi} \\ \mathrm{GPa} \end{gathered}$ | $\begin{gathered} 2.7 \\ 18 \end{gathered}$ | - |
| Long-Term Hydrostatic Design Basis ${ }^{(3)}$ <br> Static, Hoop Stress 95\% LCL 20-year Life @ $150^{\circ} \mathrm{F} / 65^{\circ} \mathrm{C}$ <br> Cyclic, Hoop Stress 95\% LCL 20 -year Life @ $75^{\circ} \mathrm{F} / 24^{\circ} \mathrm{C}$ | $\begin{gathered} 10^{3} \mathrm{psi} \\ \mathrm{MPa} \\ 10^{3} \mathrm{psi} \\ \mathrm{MPa} \end{gathered}$ | $\begin{gathered} 14.2 \\ 98.1 \\ 6.9 \\ 47.4 \end{gathered}$ | D2992 Procedure B <br> D2992 Procedure A |
| Poisson's Ratio ${ }^{(2)}$ $\nu_{y x} \nu_{x y} \nu_{x y}$ | - | $\begin{aligned} & 0.17 \\ & 0.15 \end{aligned}$ | - |

${ }^{(1)}$ Based on structural wall thickness.
(2) The first subscript denotes the direction of applied stress and the second subscript the measured strain contraction. x denotes longitudinal direction. y denotes circumferential direction
${ }^{(3)}$ Test fixtures were free end type (full end thrust on samples)

| Nominal <br> Pipe Size |  | Change in Length <br> Due to Pressure ${ }^{(1)}$ |  | Stiffness <br> Factor $^{(2)}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | $\mathrm{in} / 100 \mathrm{ft} / 100 \mathrm{psi}$ | $\mathrm{mm} / 10 \mathrm{~m} / \mathbf{1 0} \mathrm{bar}$ | $\mathrm{lb} \cdot \mathrm{in}^{3} / \mathrm{in}^{2}$ | $\mathrm{~N} \cdot \mathrm{~m}$ |
| 8 | 200 | 0.565 | 6.8 | 582 | 65.7 |
| 10 | 250 | 0.612 | 7.4 | 908 | 102.6 |
| 12 | 300 | 0.599 | 7.2 | 1,596 | 180.3 |
| 14 | 350 | 0.646 | 7.8 | 1,886 | 213.0 |
| 16 | 400 | 0.668 | 8.1 | 2,566 | 289.9 |

${ }^{(1)}$ In an unrestrained system due to pressure effects alone.
${ }^{(2)}$ At 5\% deflection.

## Support Spacing

(Values are based on a $1 / 2$-inch ( 12 mm ) deflection at mid span.)

| Nominal <br> Pipe Size |  | Single Span ${ }^{(1)}$ |  |  |  |  |  | Continuous Span ${ }^{(2)}$ |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Gases |  | $1.00{ }^{(3)}$ |  | 1.3 |  | Gases |  | 1.00 |  | 1.3 |  |
| in | mm | ft | m | ft | m | ft | m | ft | m | ft | m | ft | m |
| 8 | 200 | 27.9 | 8.5 | 16.4 | 5.0 | 15.5 | 4.7 | 41.8 | 12.7 | 24.6 | 7.5 | 23.1 | 7.0 |
| 10 | 250 | 31.4 | 9.8 | 18.1 | 5.5 | 17.1 | 5.2 | 46.9 | 14.3 | 27.1 | 8.2 | 25.5 | 7.8 |
| 12 | 300 | 34.0 | 10.4 | 19.4 | 5.9 | 18.3 | 5.6 | 50.9 | 15.5 | 29.0 | 8.8 | 27.3 | 8.3 |
| 14 | 350 | 36.2 | 11.0 | 20.7 | 6.3 | 19.5 | 5.9 | 54.2 | 16.5 | 31.0 | 9.5 | 29.2 | 8.9 |
| 16 | 400 | 38.7 | 11.8 | 21.9 | 6.7 | 20.6 | 6.3 | 57.9 | 17.6 | 32.8 | 10.0 | 30.9 | 9.4 |

${ }^{(1)}$ For fluid temperatures above $77^{\circ} \mathrm{F}\left(25^{\circ} \mathrm{C}\right)$ reduce span lengths 0.1 -inch/ ${ }^{\circ} \mathrm{F}\left(5 \mathrm{~mm} /{ }^{\circ} \mathrm{C}\right)$
${ }^{(2)}$ Beam fixed at both ends and uniformly distributed loads. Intermediate spans may be calculate by multiplying the single span length by 1.2 .
${ }^{(3)}$ Fluid specific gravity.

Bending Radius

| Nominal <br> Pipe Size |  | Minimum <br> Bending Radius |  | Maximum <br> Deflection <br> per 39-ft <br> Joint | Minimum Length <br> Required <br> for $10^{\circ}$ Change |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | ft | m | deg | ft | m |
| 8 | 200 | 209 | 64 | 11 | 37 | 11 |
| 10 | 250 | 281 | 86 | 8 | 49 | 15 |
| 12 | 300 | 343 | 105 | 7 | 60 | 18 |
| 14 | 350 | 418 | 127 | 5 | 73 | 22 |
| 16 | 400 | 507 | 155 | 4 | 89 | 27 |

[^19]
## Guide Specification

This specification covers approval, performance, materials and physical properties requirements for general industrial service piping in 8 through 16 inch nominal pipe sizes at operating temperatures to $210^{\circ} \mathrm{F}$.

## Performance Requirements

Pipe, fittings and other components furnished under this specification shall be rated for service to 200 psig at $150^{\circ} \mathrm{F}$ and capable of $210^{\circ} \mathrm{F}$ service conditions in accordance with the derating factor. All components shall be rated at or above the design pressure of the system.

| Nominal <br> Pipe Size |  | ASTM Designation |  |
| :---: | :---: | :---: | :---: |
| in | mm | D2310 | D2996 |
| $8-16$ | $200-400$ | RTRP 11FU | RTRP 11FU-6430 |

## Materials

Liner-All filament-wound pipe shall incorporate an integral liner with a nominal thickness of 0.025 $\pm 0.005$ inches for 8 through 16 inch nominal sizes. The resin system used in the liner shall be a chemically resistant thermosetting epoxy resin suitable for the intended service.

Structural Wall—Pipe shall be filament wound using continuous glass fiber reinforcements with a resin-compatible finish and a chemically resistant thermosetting epoxy resin. The glass filaments shall be wound in a dual-angle pattern that takes optimum advantage of the tensile strength of the filaments. The glass fiber content of the reinforced wall shall not be less than $60 \%$ by weight. Pigments or dies may be used in the resin as long as the product remains translucent.

External Surface-The pipe shall have a typical 0.005 inch thick resin-rich coating with organic fibrous reinforcement. This protection must be provided for both above and below-ground pipe installations. All external surfaces must be resistant to anticipated corrosion imposed by the service and the environment.

Fittings-Fittings supplied under this specification shall be filament-wound, compression molded, centrifugally cast, or manufactured from mitered pipe sections. The glass fiber content of the structural portion of compression-molded and filament-wound fittings shall not be less than $55 \%$ by weight.

Adhesive-Bonded Bell and Spigot—Both tapered bell and tapered spigot shall have matching taper angles and shall be joined by bonding with an epoxy adhesive. The nominal taper angle shall be $2^{\circ}$ on 8 through 16 inch nominal pipe sizes. The adhesive shall be a two-part epoxy supplied as a kit with all necessary application materials.
Flanges-Flanges shall be two-piece Van Stone type provided with raised grooves on the sealing surface. Fiberglass-reinforced, compression-molded or centrifugally cast stub ends are to be adhesive bonded to the pipe or fitting.
Adapters or Crossovers-The following adapters or crossovers shall be available on request:
Grooved end (8 inch nominal pipe sizes)
Cast iron pipe end (8 through 16 inch nominal pipe sizes)

## Pipe Construction

Pipe-Pipe shall be manufactured to steel pipe outside diameters in 8 through 12 inch nominal pipe sizes and should be based on nominal inside diameters in 14 inch sizes and above. Outside diameter tolerances shall not exceed $\pm 1.0 \%$. Pipe shall be provided in 40 feet random lengths ( 34 through 42 ft ) unless otherwise specified. Up to 10 percent shorts may be included in any shipment unless otherwise agreed upon in writing between purchaser and manufacturer.
Wall Thickness-The total wall thickness of pipe furnished to this specification shall not at any point be greater than 120 percent nor less than 87.5 percent of the nominal thickness. Nominal wall thickness shall have dimensions as given in the manufacturer's published literature.

Fittings and Flanges-Fittings and flanges shall have dimensions as given in the manufacturer's published literature. Flanges shall be drilled to match ANSI 816.5, Class 150 unless specified otherwise in the purchase order.

## Physical and Mechanical Requirements

Valuesforphysical andmechanical properties shall be within $15 \%$ ofthose showntabulated above under Typical Physical Properties and Typical Mechanical Properties.

## Workmanship

The pipe and fittings shall be free from all defects, including delamination, indentations, pinholes, foreign inclusions, bubbles and resin-starved areas which, due to their nature, degree or extent, detrimentally affect the strength and serviceability of the pipe or fittings. Pigments or dyes may be used in the resin as long as the product is sufficiently translucent to verify the structural integrity of the structural wall. The pipe and fittings shall be as uniform as commercially practicable in color, density and other physical properties.

## Testing

Quality Control Testing-Samples of pipe and fittings shall be tested at random based on standard quality control practices to determine conformance of the materials to the following tests: weight, taper angle, short-term rupture strength, cyclic pressure performance, ring crush strength, Barcol hardness and degree of cure. Each item shall be visually inspected for workmanship.

Proof Testing-All components may be required to be hydrostatically tested by the manufacturer to 1.5 times the pressure rating for signs of leakage or porosity.

## Marking

Each component shall be marked to show the following:
Manufacturer's name and address
Nominal pipe size
Pressure class
Hydrostatic test pressure (if so ordered)
UL Listing Mark (if so ordered)
ULC Listing Mark (if so ordered)
Date and shift of manufacture (pipe only)

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## Bondstrand Series 3300 Fiberglass Pipe (General Industrial Service) <br> (For sizes 2 through 6 inch, use Series 3000 pipe and fittings products)



## Composition

Pipe
Filament-wound fiberglass reinforced epoxy pipe with integral epoxy liner and exterior coating.

| Nominal Pipe Size |  | ASTM Designation |  |
| :---: | :---: | :---: | :---: |
| in | mm | D2310 | D2996 |
| $8-16$ | $200-400$ | RTRP 11FW | RTRP 11FW1-3210 |

## Fittings

8 to 16 inch: Filament-wound fiberglass reinforced epoxy elbows

Mitered tees, crosses, wyes, and laterals

## Flanges

Filament-wound fiberglass flange rings
Filament wound fiberglass stub ends
Blind flanges
Compression-molded fiberglass or epoxy-coated cast iron or steel.
Adhesive
Two-part epoxy adhesive

## Joining Systems

8 to 16 inch
Bell and spigot taper/taper adhesive-bonded joint.

## Pipe Lengths

Standard 20 and 39 ft . random lengths.
Other lengths available on request.

## Fittings

Elbows:

| $8-16$ inch | $90^{\circ}$ | $60^{\circ}$ | $45^{\circ}$ | $30^{\circ}$ | $22^{1} 2^{\circ}$ | $11114^{\circ}$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |

Tees Flanges Blind flanges
Concentric reducers Reducer bushings Sleeve couplings
For fittings dimensions, refer to the most recent release of product data sheets.

## Typical Pipe Dimensions and Weights

| Nominal Pipe Size |  | Outside <br> Diameter |  | Inside Diameter |  | Wall Thickness |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Total | Structural |  |
| in | mm |  |  | in | mm | in | mm | in | mm | in | mm |
| 8 | 200 | 8.64 | 219 |  |  | 8.30 | 211 | 0.170 | 4.3 | 0.140 | 3.6 |
| 10 | 250 | 10.85 | 273 | 10.42 | 264 | 0.215 | 5.5 | 0.185 | 4.7 |
| 12 | 300 | 12.78 | 324 | 12.30 | 312 | 0.240 | 6.1 | 0.210 | 5.3 |
| 14 | 350 | 14.53 | 367 | 14.00 | 356 | 0.265 | 6.7 | 0.235 | 6.0 |
| 16 | 400 | 16.65 | 419 | 16.03 | 407 | 0.310 | 7.9 | 0.282 | 7.2 |


| Nominal <br> Pipe Size |  | Taper <br> Angle | Taper Length |  | Pipe Weight |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | $\mathbf{m m}$ | deg | in | $\mathbf{m m}$ | $\mathbf{l b} / \mathbf{f t}$ | $\mathbf{k g} / \mathbf{m}$ |
| 8 | 200 | 2.00 | 2.6 | 66 | 3.1 | 4.60 |
| 10 | 250 | 2.00 | 3.1 | 79 | 4.5 | 6.70 |
| 12 | 300 | 2.00 | 3.6 | 91 | 6.1 | 9.10 |
| 14 | 350 | 2.00 | 5.4 | 137 | 8.8 | 13.00 |
| 16 | 400 | 2.00 | 6.1 | 155 | 11.4 | 16.90 |

## Typical Pipe Performance

| Nominal <br> Pipe Size |  | Static Pressure <br> Rating at $150^{\circ} \mathrm{F}$ |  | Ultimate Internal Pressure ${ }^{(1)}$ |  | Ultimate Collapse Pressure |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $80^{\circ} \mathrm{F}$ | $27^{\circ} \mathrm{C}$ |  |  | 150 ${ }^{\circ} \mathrm{F}$ | $65.6^{\circ} \mathrm{C}$ |
| in | mm |  |  | psig | bar | psig | bar | psig | bar | psig | bar |
| 8 | 200 | 300 | 20.7 | 1,800 | 124 | 29 | 2.0 | 19 | 1.3 |
| 10 | 250 | 300 | 20.7 | 1,800 | 124 | 33 | 2.3 | 22 | 1.5 |
| 12 | 300 | 300 | 20.7 | 1,800 | 124 | 30 | 2.1 | 20 | 1.4 |
| 14 | 350 | 300 | 20.7 | 1,800 | 124 | 28 | 2.0 | 19 | 1.3 |
| 16 | 400 | 300 | 20.7 | 1,800 | 124 | 33 | 2.3 | 21 | 1.5 |

${ }^{(1)}$ Quality control minimum, biaxially loaded.

## Typical Physical Properties

| Pipe Property | Units | Value | ASTM |
| :---: | :---: | :---: | :---: |
| Thermal conductivity | $\begin{gathered} \text { Btu-in } /\left(\mathrm{h} \cdot \mathrm{ft}^{2} \cdot{ }^{\circ} \mathrm{F}\right) \\ \mathrm{W} / \mathrm{m} \cdot{ }^{\circ} \mathrm{C} \end{gathered}$ | $\begin{gathered} 1.7 \\ 0.25 \end{gathered}$ | C177 |
| Coefficient of thermal expansion (linear) $8-16 \text { inch }$ | $\begin{gathered} 10^{-6} \mathrm{in} / \mathrm{in} /{ }^{\circ} \mathrm{F} \\ 10^{-6} \mathrm{~cm} / \mathrm{cm} /{ }^{\circ} \mathrm{C} \end{gathered}$ | $\begin{aligned} & 12.0 \\ & 21.6 \end{aligned}$ | $\begin{aligned} & \text { D696 } \\ & \text { E228 } \end{aligned}$ |
| Flow coefficient | Hazen-Williams | 150.0 | - |
| Absolute roughness | $\begin{aligned} & 10^{-6} \mathrm{ft} \\ & 10^{-6} \mathrm{~m} \end{aligned}$ | $\begin{aligned} & 50.0 \\ & 15.0 \end{aligned}$ | - |
| Specific gravity | - | 1.81 | D792 |

## Typical Mechanical Properties


(1) Based on structural wall thickness.
${ }^{(2)}$ The first subscript denotes the direction of applied stress and the second subscript the measured strain contraction. $x$ denotes longitudinal direction. $y$ denotes circumferential direction
${ }^{(3)}$ Test fixtures were free-end type (full end thrust)

| Nominal Pipe Size |  | Change in Length Due to Pressure ${ }^{(1)}$ |  | Stiffness <br> Factor ${ }^{(2)}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | in/100 ft/100 psi | mm/30.5 m/6.9 bar | $\mathrm{lb} \cdot \mathrm{in}^{3} / \mathrm{in}^{2}$ | $\mathrm{N} \cdot \mathrm{m}$ |
| 8 | 200 | 0.503 | 6.07 | 500 | 56.5 |
| 10 | 250 | 0.478 | 6.77 | 750 | 84.7 |
| 12 | 300 | 0.498 | 6.01 | 1,250 | 141.2 |
| 14 | 350 | 0.507 | 6.12 | 1,600 | 180.8 |
| 16 | 400 | 0.483 | 5.84 | 2,000 | 226.0 |

[^20]
## Support Spacing

(Values are based on a $1 / 2$ inch ( 12 mm ) deflection at mid span.)

| Nominal Pipe Size |  | Single Span ${ }^{(1)}$ |  |  |  |  |  | Continuous Span ${ }^{(2)}$ |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Gases |  | $1.00{ }^{(3)}$ |  | 1.25 |  | Gases |  | 1.00 |  | 1.25 |  |
| in | mm | ft | m | ft | m | ft | m | ft | m | ft | m | ft | m |
| 8 | 200 | 27.8 | 8.5 | 16.4 | 5.0 | 15.4 | 4.7 | 41.6 | 12.7 | 24.5 | 7.5 | 23.0 | 7.0 |
| 10 | 250 | 32.1 | 9.8 | 18.6 | 5.7 | 17.5 | 5.3 | 48.1 | 14.7 | 27.8 | 8.5 | 26.2 | 8.0 |
| 12 | 300 | 34.8 | 10.6 | 19.8 | 6.0 | 18.7 | 5.7 | 52.0 | 15.8 | 29.6 | 9.0 | 27.9 | 8.5 |
| 14 | 350 | 35.9 | 10.9 | 21.3 | 6.5 | 20.1 | 6.1 | 53.7 | 16.4 | 31.8 | 9.7 | 30.0 | 9.1 |
| 16 | 400 | 38.9 | 11.9 | 23.0 | 7.0 | 21.7 | 6.6 | 58.2 | 17.7 | 34.4 | 10.5 | 32.4 | 9.9 |

${ }^{(1)}$ For fluid temperatures above $77^{\circ} \mathrm{F}\left(25^{\circ} \mathrm{C}\right)$ reduce span lengths 0.1 -inch/ ${ }^{\circ} \mathrm{F}\left(5 \mathrm{~mm} /{ }^{\circ} \mathrm{C}\right)$
${ }^{(2)}$ Beam fixed at both ends and uniformly distributed loads. Intermediate spans may be calculate by multiplying the single span length by 1.2
${ }^{(3)}$ Fluid specific gravity.

| Bending Radius |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Nominal <br> Pipe Size |  | Minimum Bending Radius |  | Maximum Deflection per 39-ft Joint | Minimum Length <br> Required for $10^{\circ}$ Change |  |
| in | mm | ft | m | deg | ft | m |
| 8 | 200 | 293 | 89 | 8 | 51 | 16 |
| 10 | 250 | 364 | 111 | 6 | 63 | 19 |
| 12 | 300 | 472 | 144 | 5 | 82 | 25 |
| 14 | 350 | 570 | 174 | 4 | 100 | 30 |
| 16 | 400 | 626 | 191 | 4 | 109 | 33 |

${ }^{(1)}$ At rated pressure. Sharper bends may create excessive stress concentrations. Do not bend pipe until adhesive has cured.

This specification covers performance, materials and physical properties requirements for general industrial service piping in 8 through 16 inch nominal pipe sizes at operating temperatures to $150^{\circ} \mathrm{F}$.

## Performance Requirements

Pipe, fittings and other components furnished under this specification shall be rated for service to 300 psig at $150^{\circ} \mathrm{F}$. All components shall be rated at or above the design pressure of the system.
When classified in accordance with ASTM standards, the pipe shall meet the following cell limits:

| Nominal <br> Pipe Size |  | ASTM Designation |  |
| :---: | :---: | :---: | :---: |
| in | mm | D2310 | D2996 |
| $8-16$ | $200-400$ | RTRP 11FW | RTRP 11FW1-3210 |

## Materials

Liner-All filament-wound pipe shall incorporate an integral liner with a nominal thickness of 0.025 $\pm 0.005$. The resin system used in the liner shall be a chemically resistant thermosetting epoxy resin suitable for the intended service.

Structural wall—Pipe shall be filament wound using continuous glass fiber reinforcements with a resin-compatible finish and a chemically resistant thermosetting epoxy resin. The glass filaments shall be wound in a dual-angle pattern that takes optimum advantage of the tensile strength of the filaments. The glass fiber content of the reinforced wall shall not be less than $60 \%$ by weight. Pigments or dies may be used in the resin as long as the product remains translucent.
External surface-The pipe shall have a typical 0.005 -inch thick resin-rich coating with organic fibrous reinforcement. This protection must be provided for both above and below-ground pipe installations. All external surfaces must be resistant to anticipated corrosion imposed by the service and the environment.
Fittings—Fittings supplied under this specification shall be filament-wound, compression molded, centrifugally cast, or manufactured from mitered pipe sections. The glass fiber content of the structural portion of compression-molded and filament-wound fittings shall not be less than $55 \%$ by weight.

## Joining Methods

Adhesive-bonded bell and spigot-Both tapered bell and tapered spigot shall have matching taper angles and shall be joined by bonding with an epoxy adhesive. The nominal taper angle shall be $2^{\circ}$ on 8 through 16 inch nominal pipe sizes. The adhesive shall be a two part epoxy supplied as a kit with all necessary application materials.
Flanges-Flanges shall be two-piece van Stone type provided with raised grooves on the sealing surface. Fiberglass-reinforced compression-molded or centrifugally cast stub ends are to be adhesive bonded to the pipe or fitting.

## Pipe Construction

Pipe-Outside diameter tolerances shall not exceed $\pm 1.0 \%$. Pipe shall be provided in 40 -ft random lengths ( 34 through 42 ft ) unless otherwise specified. Up to 10 percent shorts may be included in any shipment unless otherwise agreed upon in writing between purchaser and manufacturer.

Wall thickness-The total wall thickness of pipe furnished to this specification shall not at any point be greater than 120 percent nor less than 87.5 percent of the nominal thickness. Nominal wall thickness shall have dimensions as given in the manufacturer's published literature.

Fittings and flanges-Fittings and flanges shall have dimensions as given in the manufacturer's published literature. Flanges shall be drilled to match ANSI B16.5, Class 150 unless specified otherwise in the purchase order.

## Physical and Mechanical Requirements

Values for physical and mechanical properties shall be no less than $95 \%$ of those shown tabulated above under Typical Physical Properties and Typical Mechanical Properties.

## Workmanship

The pipe and fittings shall be free from all defects, including delamination, indentations, pinholes, foreign inclusions, bubbles and resin-starved areas which, due to their nature, degree or extent, detrimentally affect the strength and serviceability of the pipe or fittings. Pigments or dyes may be used in the resin as long as the product is sufficiently translucent to verify the structural integrity of the structural wall. The pipe and fittings shall be as uniform as commercially practicable in color, density and other physical properties.

## Testing

Quality control testing-Samples of pipe and fittings shall be tested at random based on standard quality control practices to determine conformance of the materials to the following ASTM guidelines for testing fiberglass pipe products: ASTM D1599, D2105, D2925, D2992A or D2992B. Test samples may be hydrostatically tested by the manufacturer to 1.5 times the pressure rating for signs of leakage.

## Marking

Each component shall be marked to show the following:
Manufacturer's name and address
Nominal pipe size
Hydrostatic test pressure (if so ordered)
Date and shift of manufacture (pipe only)

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Europe
P.O. Box 6, 4190 CA

Geldermalsen, The Netherlands
Phone: 31345587587

Asia Pacific
No. 7A, Tuas Avenue 3 Jurong, Singapore 639407 Phone: 6568616118

## Middle East

 P.O. Box 17324 Dubai, UAE Phone: 97148813566
# Bondstrand"' Series 3300A Fiberglass Pipe (General Industrial Service) 

## (For sizes 2 through 6 inch, use Series 3000A pipe and fittings products.)

## Uses and <br> Applications

- Boiler feed water
- Brine and brackish water
- Chemical process piping
- Cooling water
- Demineralized water
- Electroplating
- Industrial plant piping
- Municipal waste
- Oilfield piping
- Power plant and steel mill piping
- Sewer lines and sewer force mains
- Source and recycle water
- Sump discharge
- Vent lines
- Water mains
- Water treatment


## Performance

Pipe and fittings are rated at 300 psig .
Operating plus surge pressures to 1.25 times rated operating pressure occurring three times or less per 24-hour period.
No thrust blocks are required at rated system pressure for most buried piping configurations and most soil conditions. For above ground use, consult NOV Fiber Glass Systems.
Temperatures to $210^{\circ} \mathrm{F}\left(99^{\circ} \mathrm{C}\right)$ maximum. Sub-zero temperatures will not affect the physical properties.
Full vacuum capabilities when buried and properly backfilled. For above ground use, refer to collapse pressures listed below under Typical Pipe Performance.
Recommended burial depth: 3 to 25 feet.
Recommended for water, waste water ( pH 1 to 12), moderately corrosive liquids and mild chemicals. Consult Corrosion Guide or Applications Engineering for recommendations for your particular application.
Individual system components may not have the same ratings as the pipe. Refer to the detailed product information for the specific components to determine the pressure rating for the system as a whole.

## Composition

## Pipe

Filament-wound fiberglass reinforced epoxy pipe with integral epoxy liner and exterior coating.

| Nominal Pipe Size |  | ASTM Designation |  |
| :---: | :---: | :---: | :---: |
| in | mm | D2310 | D2996 |
| $8-16$ | $200-400$ | RTRP 11FU | RTRP 11FU1-6430 |

## Fittings

8 to 16 inch:
Filament-wound fiberglass reinforced epoxy elbows.
Filament wound and/or mitered tees

## Flanges

Filament-wound fiberglass flange rings
Filament wound fiberglass stub ends

## Blind flanges

Compression-molded fiberglass or epoxy-coated cast iron or steel.

## Joining Systems

8 to 16 inch
Bell and spigot taper/taper adhesive-bonded joint.

## Pipe Lengths

Standard 39 foot random lengths.
Other lengths available on request.

## Typical Pipe Dimensions and Weights

| Nominal Pipe Size |  | Outside Diameter |  | Inside Diameter |  | Wall Thickness |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Total | Structural |  |
| in | mm |  |  | in | mm | in | mm | in | mm | in | mm |
| 8 | 200 | 8.65 | 220 |  |  | 8.30 | 211 | 0.170 | 4.3 | 0.140 | 3.6 |
| 10 | 250 | 10.85 | 276 | 10.41 | 264 | 0.215 | 5.5 | 0.185 | 4.7 |
| 12 | 300 | 12.80 | 323 | 12.30 | 312 | 0.240 | 6.1 | 0.210 | 5.3 |
| 14 | 350 | 14.55 | 370 | 14.01 | 356 | 0.270 | 6.8 | 0.240 | 6.1 |
| 16 | 400 | 16.63 | 422 | 16.01 | 407 | 0.310 | 7.9 | 0.282 | 7.2 |


| Nominal <br> Pipe Size |  | Taper <br> Angle | Taper Length |  | Pipe Weight |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | $\mathbf{m m}$ | deg | in | $\mathbf{m m}$ | lb/ft | $\mathbf{k g} / \mathbf{m}$ |
| 8 | 200 | 2.00 | 2.6 | 66 | 3.1 | 4.60 |
| 10 | 250 | 2.00 | 3.1 | 79 | 4.5 | 6.70 |
| 12 | 300 | 2.00 | 3.6 | 91 | 6.1 | 9.10 |
| 14 | 350 | 2.00 | 4.2 | 107 | 8.8 | 11.15 |
| 16 | 400 | 2.00 | 4.7 | 119 | 11.4 | 14.00 |

Typical Pipe Performance

| Nominal Pipe Size |  | Static Pressure Rating at $150^{\circ}{ }^{(1)}$ |  | Ultimate Internal Pressure ${ }^{(2)}$ |  | Ultimate Collapse Pressure |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $80^{\circ} \mathrm{F}$ | $27^{\circ} \mathrm{C}$ |  |  | 210% | $99^{\circ} \mathrm{C}$ |
| in | mm |  |  | psig | bar | psig | bar | psig | bar | psig | bar |
| 8 | 200 | 300 | 20.7 | 1,200 | 82.8 | 29 | 2.02 | 25 | 1.7 |
| 10 | 250 | 300 | 20.7 | 1,264 | 87.1 | 34 | 2.37 | 29 | 2.0 |
| 12 | 300 | 300 | 20.7 | 1,215 | 83.8 | 31 | 2.10 | 26 | 1.8 |
| 14 | 350 | 300 | 20.7 | 1,221 | 84.2 | 31 | 2.14 | 26 | 1.8 |
| 16 | 400 | 300 | 20.7 | 1,256 | 86.6 | 34 | 2.32 | 28 | 2.0 |

${ }^{(1)}$ At $210^{\circ} \mathrm{F}$, derate pipe by a factor of 0.73 , linearly interpolate derating factors for temperatures between $150^{\circ} \mathrm{F}$ and $210^{\circ} \mathrm{F}$.
${ }^{(2)}$ Quality control minimum biaxial loading

Fittings Pressure Ratings ${ }^{(3)}$

| Nominal <br> Pipe Size |  | Elbows and Tees ${ }^{(1)}$ |  | Flanges $^{(2)}$ |  | Blind Flanges |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | psig | bar | psig | bar | psig | bar |
| 8 | 200 | 300 | 21 | 300 | 21 | 300 | 21 |
| 10 | 250 | 300 | 21 | 300 | 21 | 300 | 21 |
| 12 | 300 | 300 | 21 | 300 | 21 | 300 | 21 |
| 14 | 350 | 300 | 21 | 300 | 21 | 300 | 21 |
| 16 | 400 | 300 | 21 | 300 | 21 | 300 | 21 |

${ }^{(1)}$ Ratings shown are $90^{\circ}$ and $45^{\circ}$ elbows. Ratings in 8 through 16 inch sizes are also applicable to elbows of other angles.
${ }^{(2)}$ ANSI B16.5, 150 psig bolt pattern.
${ }^{(3)}$ At $210^{\circ} \mathrm{F}$, derate by a factor of 0.73 , linearly interpolate derating factors for temperatures between $150^{\circ} \mathrm{F}$ and $210^{\circ} \mathrm{F}$.

## Typical Physical Properties

| Pipe Property | Units | Value | ASTM |
| :---: | :---: | :---: | :---: |
| Thermal conductivity | $\begin{gathered} \mathrm{Btu}-\mathrm{in} /\left(\mathrm{h} \cdot \mathrm{ft}^{2} \cdot{ }^{\circ} \mathrm{F}\right) \\ \mathrm{W} / \mathrm{m} \cdot{ }^{\circ} \mathrm{C} \end{gathered}$ | $\begin{gathered} 1.7 \\ 0.25 \end{gathered}$ | C177 |
| Coefficient of thermal expansion (linear) $\begin{gathered} 77^{\circ} \mathrm{F} \text { to } 210^{\circ} \mathrm{F} \\ 25^{\circ} \mathrm{C} \text { to } 98.9^{\circ} \mathrm{C} \end{gathered}$ | $\begin{gathered} 10-6 \mathrm{in} / \mathrm{in} /{ }^{\circ} \mathrm{F} \\ 10-{ }^{6} \mathrm{~cm} / \mathrm{cm} /{ }^{\circ} \mathrm{C} \end{gathered}$ | 10 To 13 <br> 18 to 24 | $\begin{aligned} & \text { D696 } \\ & \text { E228 } \end{aligned}$ |
| Flow coefficient | Hazen-Williams | 150 | - |
| Absolute roughness | $\begin{aligned} & 10^{-6} \mathrm{ft} \\ & 10^{-6} \mathrm{~m} \end{aligned}$ | $\begin{aligned} & 50 \\ & 15 \end{aligned}$ | - |
| Specific gravity | - | 1.81 | D792 |

## Typical Mechanical Properties

| Pipe Property ${ }^{(1)}$ | Units | Value | ASTM |
| :---: | :---: | :---: | :---: |
| Tensile strength Longitudinal Circumferential | $\begin{gathered} 10^{3} \mathrm{psi} \\ \mathrm{MPa} \\ 10^{3} \mathrm{psi} \\ \mathrm{MPa} \end{gathered}$ | $\begin{gathered} 35 \\ 240 \\ 70 \\ 483 \end{gathered}$ | $\begin{aligned} & \text { D2105 } \\ & \text { D1599 } \end{aligned}$ |
| Tensile modulus Longitudinal <br> Circumferential | $10^{6} \mathrm{psi}$ GPa $10^{6} \mathrm{psi}$ GPa | $\begin{aligned} & 2.7 \\ & 21 \\ & 4.2 \\ & 29 \end{aligned}$ | D2105 |
| Compressive strength Longitudinal | $\begin{gathered} 10^{3} \mathrm{psi} \\ \mathrm{MPa} \end{gathered}$ | $\begin{gathered} 25 \\ 169 \end{gathered}$ | - |
| Compressive modulus Longitudinal | $10^{6} \mathrm{psi}$ GPa | $\begin{gathered} 2.7 \\ 18 \end{gathered}$ | - |
| Long-Term Hydrostatic Design Basis ${ }^{(3)}$ <br> Static, Hoop Stress 95\% LCL 20-year Life @ $150^{\circ} \mathrm{F} / 65^{\circ} \mathrm{C}$ <br> Cyclic, Hoop Stress <br> 95\% LCL 20 -year Life @ $75^{\circ} \mathrm{F} / 24^{\circ} \mathrm{C}$ | $\begin{gathered} 10^{3} \mathrm{psi} \\ \mathrm{MPa} \\ 10^{3} \mathrm{psi} \\ \mathrm{MPa} \end{gathered}$ | $\begin{gathered} 14.2 \\ 98.1 \\ 6.9 \\ 47.4 \end{gathered}$ | D2992 Procedure B <br> D2992 Procedure A |
| Poisson's Ratio ${ }^{(2)}$ $V_{y x}$ $V_{x y}$ | - | $\begin{aligned} & 0.17 \\ & 0.15 \end{aligned}$ | - |

[^21]| Nominal Pipe Size |  | Change in Length Due to Pressure ${ }^{(1)}$ |  | Stiffness Factor ${ }^{(2)}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | in/100 ft/100 psi | mm/10m/10 bar | $\mathrm{lb} \cdot \mathrm{in}^{3} / \mathrm{in}^{2}$ | $\mathrm{N} \cdot \mathrm{m}$ |
| 8 | 200 | 0.503 | 6.1 | 817 | 92.3 |
| 10 | 250 | 0.477 | 5.8 | 1,886 | 213.0 |
| 12 | 300 | 0.498 | 6.0 | 2,758 | 311.6 |
| 14 | 350 | 0.496 | 6.0 | 4,117 | 465.2 |
| 16 | 400 | 0.483 | 5.8 | 6,679 | 754.6 |

${ }^{(1)}$ In an unrestrained system due to pressure effects alone.
${ }^{(2)}$ At $5 \%$ deflection.

## Support Spacing

(Values are based on a $1 / 2$ inch ( 12 mm ) deflection at mid span.)

| Nominal Pipe Size |  | Single Span ${ }^{(1)}$ |  |  |  |  |  | Continuous Span ${ }^{(2)}$ |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Gases |  | $1.0^{(3)}$ |  | 1.3 |  | Gases |  | 1.0 |  | 1.3 |  |
| in | mm | ft | m | ft | m | ft | m | ft | m | ft | m | ft | m |
| 8 | 200 | 29.0 | 8.8 | 17.1 | 5.2 | 16.0 | 4.9 | 43.4 | 13.2 | 25.5 | 7.8 | 24.0 | 7.3 |
| 10 | 250 | 33.2 | 10.1 | 19.2 | 5.8 | 18.1 | 5.5 | 49.6 | 15.1 | 28.6 | 8.7 | 27.0 | 8.2 |
| 12 | 300 | 36.1 | 11.0 | 20.6 | 6.3 | 19.4 | 5.9 | 53.9 | 16.4 | 30.8 | 9.4 | 29.0 | 8.8 |
| 14 | 350 | 37.0 | 11.3 | 21.9 | 6.7 | 20.6 | 6.3 | 55.3 | 16.8 | 32.8 | 10.0 | 30.9 | 9.4 |
| 16 | 400 | 39.6 | 12.1 | 23.5 | 7.1 | 22.1 | 6.7 | 59.3 | 18.1 | 35.1 | 10.7 | 33.0 | 10.1 |

${ }^{(1)}$ For fluid temperatures above $77^{\circ} \mathrm{F}\left(25^{\circ} \mathrm{C}\right)$, the span lengths decrease by $\left(0.1 \mathrm{in} /{ }^{\circ} \mathrm{F} / 5 \mathrm{~mm} /{ }^{\circ} \mathrm{C}\right)$.
${ }^{(2)}$ Beam fixed at both ends and uniformly distributed loads. Intermediate spans may be calculated by multiplying the single span length by 1.2.
${ }^{(3)}$ Fluid specific gravity.

## Bending Radius

| Nominal <br> Pipe Size |  | Minimum <br> Bending Radius <br> (1) |  | Maximum <br> Deflection <br> per 39-ft <br> Joint | Minimum Length <br> Required <br> for $10^{\circ}$ Change |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | ft | m | deg | ft | m |
| 8 | 200 | 309 | 94 | 7 | 54 | 16 |
| 10 | 250 | 423 | 129 | 5 | 74 | 23 |
| 12 | 300 | 488 | 149 | 4 | 85 | 26 |
| 14 | 350 | 631 | 192 | 3 | 110 | 34 |
| 16 | 400 | 764 | 233 | 3 | 133 | 41 |

${ }^{(1)}$ At rated pressure. Sharper bends may create excessive stress concentrations. Do not bend pipe until adhesive has cured.

## Guide Specification

This specification covers approval, performance, materials and physical properties requirements for fire protection piping and general industrial service piping in 8 through 16 inch nominal pipe sizes at operating temperatures to $210^{\circ} \mathrm{F}$.

## Performance Requirements

Pipe, fittings and other components furnished under this specification shall be rated for service to 300 psig at $150^{\circ} \mathrm{F}$ and capable of $210^{\circ} \mathrm{F}$ service conditions in accordance with the pressure derating factor. All components shall be rated at or above the design pressure of the system.
When classified in accordance with ASTM standards, the pipe shall meet the following cell limits:

| Nominal <br> Pipe Size |  | ASTM Designation |  |
| :---: | :---: | :---: | :---: |
| in | mm | D2310 | D2996 |
| $8-16$ | $200-400$ | RTRP 11FU | RTRP 11FU1-6430 |

## Materials

Liner-All filament-wound pipe shall incorporate an integral liner with a nominal thickness of 0.025 $\pm 0.005$. The resin system used in the liner shall be a chemically resistant thermosetting epoxy resin suitable for the intended service.

Structural wall—Pipe shall be filament wound using continuous glass fiber reinforcements with a resin-compatible finish and a chemically resistant thermosetting epoxy resin. The glass filaments shall be wound in a dual-angle pattern that takes optimum advantage of the tensile strength of the filaments. The glass fiber content of the reinforced wall shall not be less than $60 \%$ by weight. Pigments or dies may be used in the resin as long as the product remains translucent.

External surface-The pipe shall have a typical 0.005 -inch thick resin-rich coating with organic fibrous reinforcement. This protection must be provided for both above and below-ground pipe installations. All external surfaces must be resistant to anticipated corrosion imposed by the service and the environment.

Fittings—Fittings supplied under this specification shall be filament-wound, compression molded, centrifugally cast, or manufactured from mitered pipe sections. The glass fiber content of the structural portion of compression-molded and filament-wound fittings shall not be less than $55 \%$ by weight.

## Joining Methods

Adhesive Bonded Bell and Spigot—Both tapered bell and tapered spigot shall have matching taper angles and shall be joined by bonding with an epoxy adhesive. The nominal taper angle shall be $2^{\circ}$. The adhesive shall be a two part epoxy supplied as a kit with all necessary application materials.

Flanges—Flanges shall be two-piece Van Stone type provided with raised grooves on the sealing surface. Fiberglass-reinforced compression-molded or centrifugally cast stub ends are to be adhesive bonded to the pipe or fitting.

## Pipe Construction

Pipe-Outside diameter tolerances shall not exceed $\pm 1.0 \%$. Pipe shall be provided in 40 feet random lengths ( 34 through 42 ft ) unless otherwise specified. Up to 10 percent shorts may be included in any shipment unless otherwise agreed upon in writing between purchaser and manufacturer.

Wall thickness-The total wall thickness of pipe furnished to this specification shall not at any point be greater than 120 percent nor less than 87.5 percent of the nominal thickness. Nominal wall thickness shall have dimensions as given in the manufacturer's published literature.

Fittings and Flanges-Fittings and flanges shall have dimensions as given in the manufacturer's published literature. Flanges shall be drilled to match ANSI B16.5, Class 150 unless specified otherwise in the purchase order.

## Physical and Mechanical Requirements

Values for physical and mechanical properties shall be no less than $\pm 15 \%$ of those shown tabulated above under Typical Physical Properties and Typical Mechanical Properties.

## Workmanship

The pipe and fittings shall be free from all defects, including delamination, indentations, pinholes, foreign inclusions, bubbles and resin-starved areas which, due to their nature, degree or extent, detrimentally affect the strength and serviceability of the pipe or fittings. The pipe and fittings shall be as uniform as commercially practicable in color, density and other physical properties.

## Testing

Quality Control Testing-Samples of pipe and fittings shall be tested at random based on standard quality control practices to determine conformance of the materials to the following tests: weight, taper angle, short-term rupture strength, cyclic pressure performance, ring crush strength, Barcol hardness and degree of cure. Each item shall be visually inspected for workmanship.

Components may be hydrostatically tested by the manufacturer to 1.5 times the pressure rating for signs of leakage or porosity at a frequency agreed upon between the manufacturer and the purchaser.

## Marking

Each component shall be marked to show the following:
Manufacturer's name and address
Nominal pipe size
Hydrostatic test pressure (if so ordered)
Date and shift of manufacture (pipe only)

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## Bondstrand"' 4000 Product Data

## Uses and <br> Applications

- Acid drains
- Chemical process piping
- Corrosive slurries
- Food processing
- Geothermal
- Nonoxidizing chemicals and acids


## Listings

Meets USFDA requirements for food processing piping under Federal Regulations 21CFR175.105 and 21CFR177.2280 when bonded using Bondstrand PSX ${ }^{\top M} \bullet 34$ adhesive.

## Performance

Working pressure from 150 to 300 psig ( 1.0 to 2.0 MPa ) depending on pipe size.
Operating temperatures to $250^{\circ} \mathrm{F}\left(120^{\circ} \mathrm{C}\right)$, depending on fluid. Subzero temperatures will not adversely affect mechanical properties.

Excellent corrosion resistance over a wide temperature range. See most recent release of Bondstrand Corrosion Guide for specific applications.

Does not require thrust blocks at ambient temperatures when properly installed in most soils.

Smooth inner liner (Hazen-Williams $C=150$ ) produces extremely low frictional loss for greater discharge and reduced pumping costs.
Individual system components may not have the same ratings as the pipe. Refer to the detailed product information for the specific components to determine the pressure rating for the system as a whole.

## Composition

Pipe
Filament-wound fiberglass reinforced epoxy pipe with nominal 0.050 -inch ( 1.3 mm ) resin-rich reinforced liner.

| Nominal <br> Pipe Size |  | ASTM Designation |
| :---: | :---: | :---: |
| in | mm | D2996 |
| $2-3$ | $20-75$ | RTRP 11FE-2111 |
| $4-6$ | $100-150$ | RTRP 11FE-2112 |
| $8-16$ | $200-400$ | RTRP 11FE-2113 |

## Joining Systems



## Filament-wound fittings

Furnished with reinforced liner using same materials as pipe.

| Tees | $90^{\circ}$ and |  |  |
| :--- | :--- | :---: | :---: |
| Crosses | Nipple |  |  |
| $45^{\circ}$ laterals | Taper |  |  |
| Saddles (no liner) | Threa |  |  |
| Victaulic adapters (2 to 6 inch) |  |  |  |
|  |  |  |  |
| Molded fittings (General Service only) |  |  |  |
| Tees $\quad 90^{\circ}$ and $45^{\circ}$ elbows |  |  |  |
| Reducing flanges Reducer bushings |  |  |  |
| Endcaps $\quad$ Plugs |  |  |  |
| Flanges |  |  |  |

2 to 16 -inch flanges match ANSI B16.5 bolt hole pattern for Cl 150 lb flanges.
Other flange drilling patterns such as DIN, ISO, JIS, ANSI B16.5 CI 300, etc. available on special request.

## Flanged fittings

2 to 12-inch filament-wound flanged fittings match ANSI B16.1 and ANSI B16.5 bolt hole pattern and laying length dimensions. ANSI $90^{\circ}$ elbows must be specified as being either 'long' or 'short' when ordering.

## Thermosetting adhesives

Bondstrand type PSX"' • 34 two-part epoxy adhesive for field fabrication.

## Pipe Lengths

| Nominal <br> Pipe Size |  | Random Length |  |
| :---: | :---: | :---: | :---: |
| in | mm | ft | m |
| $2-6$ | $50-150$ | 20 or 30 | 6 or 9 |
| 8 | 200 | 20 or 30 | 6 or 9 |
| $10-16$ | $250-400$ | 20,30 or 40 | 6,9 or 12 |

Typical Pipe
Dimensions and Weights

| Nominal <br> Pipe Size |  | Pipe <br> I.D. |  | Nominal Wall <br> Thickness <br>  <br> $(1)$ |  | Average <br> Sectional Area |  | Pipe <br> Weight |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | in | mm | in | mm | in | mm | $\mathrm{lb} / \mathrm{ft}$ | $\mathrm{kg} / \mathrm{m}$ |
| 2 | 50 | 2.10 | 53 | .15 | 3.9 | 0.52 | 335 | 0.8 | 1.2 |
| 3 | 80 | 3.21 | 82 | .16 | 4.0 | 0.81 | 525 | 1.1 | 1.7 |
| 4 | 100 | 4.14 | 105 | .20 | 5.4 | 1.38 | 890 | 1.9 | 2.8 |
| 6 | 150 | 6.19 | 157 | .20 | 5.4 | 2.63 | 1700 | 2.8 | 4.2 |
| 8 | 200 | 8.22 | 209 | .23 | 5.7 | 5.83 | 3760 | 4.1 | 6.1 |
| 10 | 250 | 10.35 | 263 | .23 | 5.7 | 7.31 | 4720 | 5.1 | 7.7 |
| 12 | 300 | 12.35 | 314 | .23 | 5.7 | 8.69 | 5610 | 6.1 | 9.1 |
| 14 | 350 | 13.56 | 344 | .25 | 6.4 | 10.40 | 6710 | 7.4 | 11.0 |
| 16 | 400 | 15.50 | 394 | .29 | 7.3 | 13.40 | 8650 | 9.6 | 14.0 |

1) The minimum wall thickness shall not be less than $87.5 \%$ of nominal wall thickness in accordance with ASTM D2996.
2) Use these values for calculating longitudinal thrust.

## Pressure Ratings

| Nominal <br> Pipe Size |  | Internal <br> Pressure Rating |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | psig | Ultimate Collapse <br> Pressure |  |  |
| 2 | 50 | 450 | 3.10 | 212 | 1.46 |
| 3 | 80 | 320 | 2.21 | 68 | 0.47 |
| 4 | 100 | 350 | 2.41 | 82 | 0.56 |
| 6 | 150 | 249 | 1.72 | 74 | 0.17 |
| 8 | 200 | 220 | 1.52 | 16 | 0.11 |
| 10 | 250 | 175 | 1.21 | 8 | 0.06 |
| 12 | 300 | 150 | 1.03 | 5 | 0.03 |
| 14 | 350 | 150 | 1.03 | 5 | 0.03 |
| 16 | 400 | 150 | 1.03 | 6 | 0.04 |

1) At $200^{\circ} \mathrm{F}\left(93^{\circ} \mathrm{C}\right)$ using Bondstrand type $P S X^{\mathrm{m}} \cdot 34$ adhesive. For sustained service above $200^{\circ} \mathrm{F}$, reduce rating linearly from tabulated $200^{\circ} \mathrm{F}$ values to $50 \%$ of those values at $250^{\circ} \mathrm{F}\left(121^{\circ} \mathrm{C}\right)$. Above $250^{\circ} \mathrm{F}$, reduce ratings linearly to 0 at $300^{\circ} \mathrm{F}\left(149^{\circ} \mathrm{C}\right)$.
2) At $70^{\circ} \mathrm{F}\left(21^{\circ} \mathrm{C}\right)$. Reduce linearly to $90 \%$ at $150^{\circ} \mathrm{F}\left(66^{\circ} \mathrm{C}\right), 80 \%$ at $200^{\circ} \mathrm{F}$ and $65 \%$ at $230^{\circ} \mathrm{F}\left(110^{\circ} \mathrm{C}\right)$.

Fittings Pressure Ratings

| Nominal <br> Pipe Size |  | Filament-Wound <br> Elbows \& Tees |  | Molded <br> Elbows \& Tees |  | Tapered Body <br> Reducers \& Flanges |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | psig | MPa | psig | MPa | psig | MPa |
| 2 | 50 | 375 | 2.59 | 300 | 2.07 | 450 | 3.10 |
| 3 | 80 | 325 | 2.24 | 225 | 1.55 | 350 | 2.41 |
| 4 | 100 | 300 | 2.07 | 175 | 1.21 | 350 | 2.41 |
| 6 | 150 | 225 | 1.55 | 150 | 1.03 | 250 | 1.72 |
| 8 | 200 | 225 | 1.55 | - | - | 225 | 1.55 |
| 10 | 250 | 200 | 1.38 | - | - | 175 | 1.21 |
| 12 | 300 | 175 | 1.21 | - | - | 150 | 1.03 |
| 14 | 350 | 150 | 1.03 | - | - | 150 | 1.03 |
| 16 | 400 | 150 | 1.03 | - | - | 150 | 1.03 |


| Nominal <br> Pipe Size |  | Laterals |  | Crosses |  | Blind Flanges <br> \& Saddles |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | psig | MPa | psig | MPa | psig | MPa |
| 2 | 50 | 275 | 1.90 | 150 | 1.03 | 150 | 1.03 |
| 3 | 80 | 250 | 1.72 | 150 | 1.03 | 150 | 1.03 |
| 4 | 100 | 200 | 1.38 | 150 | 1.03 | 150 | 1.03 |
| 6 | 150 | 150 | 1.03 | 100 | 0.69 | 150 | 1.03 |
| 8 | 200 | 150 | 1.03 | 100 | 0.69 | 150 | 1.03 |
| 10 | 250 | 150 | 1.03 | 100 | 0.69 | 150 | 1.03 |
| 12 | 300 | 150 | 1.03 | 100 | 0.69 | 150 | 1.03 |
| 14 | 350 | 150 | 1.03 | - | - | 150 | 1.03 |
| 16 | 400 | 150 | 1.03 | - | - | 150 | 1.03 |

1) All pressure ratings valid from room temperature to $225^{\circ} \mathrm{F}\left(107^{\circ} \mathrm{C}\right)$ using FGS epoxy adhesives. For service above $225^{\circ} \mathrm{F}$, reduce the ratings shown linearly by $50 \%$ from $225^{\circ} \mathrm{F}$ to $250^{\circ} \mathrm{F}\left(121^{\circ} \mathrm{C}\right)$.

## Typical Physical Properties

## Typical Physical Properties

| Pipe Property | Units | Value | ASTM |
| :---: | :---: | :---: | :---: |
|  |  | 2 "-16" |  |
| Thermal conductivity | $\begin{gathered} \mathrm{Btu}-\mathrm{in} /\left(\mathrm{h} \cdot \mathrm{ft}^{2} \cdot{ }^{\circ} \mathrm{F}\right) \\ \mathrm{W} / \mathrm{m} \cdot{ }^{\circ} \mathrm{C} \end{gathered}$ | $\begin{aligned} & 2.23 \\ & 0.33 \end{aligned}$ | C177 |
| ```Coefficient of thermal expansion (linear) (2-16 inch) 77}\mp@subsup{}{}{\circ}\textrm{F}\mathrm{ to }15\mp@subsup{0}{}{\circ}\textrm{F (25*'C to 65 ' C)``` | $\begin{gathered} 10^{-6} \mathrm{in} / \mathrm{in} /{ }^{\circ} \mathrm{F} \\ 10^{-6} \mathrm{~cm} / \mathrm{cm} /{ }^{\circ} \mathrm{C} \end{gathered}$ | $\begin{aligned} & 10.00 \\ & 18.00 \end{aligned}$ | D696 |
| Flow coefficient | Hazen-Williams | 150.00 | - |
| Absolute roughness | $\begin{aligned} & 10^{-6} \mathrm{ft} \\ & 10^{-6} \mathrm{~m} \end{aligned}$ | $\begin{gathered} 17.40 \\ 5.30 \end{gathered}$ | - |
| Specific gravity | - | 1.80 | D792 |
| Density | $\mathrm{lb} / \mathrm{in}^{3}$ | 0.07 |  |

## Typical Mechanical Properties

Typical Mechanical Properties

| Pipe Property ${ }^{(1)}$ | Units | Value | ASTM |
| :---: | :---: | :---: | :---: |
|  |  | 2" - 16" |  |
| Tensile strength Longitudinal Circumferential | $\begin{gathered} 10^{3} \mathrm{psi} \\ \mathrm{MPa} \\ 10^{3} \mathrm{psi} \\ \mathrm{MPa} \end{gathered}$ | $\begin{gathered} 20.0 \\ 138.0 \\ 40.0 \\ 275.0 \end{gathered}$ | $\begin{aligned} & \text { D2105 } \\ & \text { D1599 } \end{aligned}$ |
| Tensile modulus Longitudinal Circumferential | $\begin{gathered} 10^{6} \mathrm{psi} \\ \mathrm{GPa} \\ 10^{6} \mathrm{psi} \\ \mathrm{GPa} \end{gathered}$ | $\begin{gathered} 1.5 \\ 10.3 \\ 2.3 \\ 15.9 \end{gathered}$ | D2105 |
| Compressive strength Longitudinal | $10^{3} \mathrm{psi}$ MPa | $\begin{gathered} 20.0 \\ 138.0 \end{gathered}$ | - |
| Compressive modulus Longitudinal | $10^{6} \mathrm{psi}$ GPa | $\begin{gathered} 1.5 \\ 10.3 \end{gathered}$ | - |
| Long-term hydrostatic ${ }^{(3)}$ Design basis <br> Static, Hoop Stress <br> LCL 20 Year Life @150아 $\left(65^{\circ} \mathrm{C}\right)$ <br> Cyclic, Hoop Stress <br> LCL 20 Year Life @ $150^{\circ} \mathrm{F}\left(65^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 10^{3} \mathrm{psi} \\ \mathrm{MPa} \\ 10^{3} \mathrm{psi} \\ \mathrm{MPa} \end{gathered}$ | $\begin{gathered} 18.9 \\ 130.3 \\ - \end{gathered}$ | $\begin{aligned} & \text { D2992(B) } \\ & \text { D2992(A) } \end{aligned}$ |
| Poisson's Ratio ${ }^{(2)}$ $v_{y x}$ $v_{x y}$ $v_{x y}$ | - | $\begin{aligned} & 0.19 \\ & 0.11 \end{aligned}$ | - |

${ }^{(1)}$ Based on structural wall thickness, at room temperature unless noted.
${ }^{(2)}$ The first subscript denotes the direction of applied stress and the second that of measured contraction $x$ denotes longitudinal direction. y denotes circumferential direction.
${ }^{(3)}$ Test fixtures were end type (full end thrust on samples).

| Nominal <br> Pipe Size |  | Stiffness <br> Factor $^{(1)}$ |  | Pipe <br> Stiffness |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | $\mathrm{Ib} \bullet$ in | $\mathrm{N} \bullet \mathrm{m}$ | psi | Beam Moment <br> of Inertia |  |  |
| 2 | 50 | 371 | 42 | 1677 | 11.6 | 0.49 | 0.20 |
| 3 | 80 | 371 | 42 | 602 | 3.5 | 1.68 | 0.69 |
| 4 | 100 | 894 | 101 | 676 | 4.6 | 4.84 | 2.01 |
| 6 | 150 | 894 | 101 | 176 | 1.2 | 15.9 | 6.61 |
| 8 | 200 | 1288 | 146.0 | 114 | 0.78 | 40.10 | 16.70 |
| 10 | 250 | 1288 | 146.0 | 68 | 0.40 | 78.60 | 32.70 |
| 12 | 300 | 1288 | 146.0 | 35 | 0.24 | 132.00 | 55.00 |
| 14 | 350 | 1759 | 199.0 | 36 | 0.25 | 194.00 | 80.90 |
| 16 | 400 | 2761 | 312.0 | 38 | 0.26 | 338.00 | 141.00 |

1) Per ASTM D2412.
2) Use these values to calculate permissible spans.

Bending Radius


| Nominal <br> Pipe Size |  | Bending Radius(1) <br> (R) |  | Maximum <br> Allowable <br> Deflection, $\mathrm{H}^{*}$ |  | Turning <br> Angle <br> (a) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | ft | m | ft | m | deg |
| 2 | 50 | 83 | 25 | 14.1 | 4.5 | 69 |
| 3 | 80 | 123 | 37 | 10.1 | 3.1 | 47 |
| 4 | 100 | 158 | 48 | 7.9 | 2.4 | 36 |
| 6 | 150 | 233 | 71 | 5.4 | 1.6 | 25 |
| 8 | 200 | 304 | 93.0 | 4.1 | 1.3 | 19 |
| 10 | 250 | 379 | 116.0 | 3.3 | 1.0 | 15 |
| 12 | 300 | 450 | 137.0 | 2.8 | 0.85 | 13 |
| 14 | 350 | 494 | 151.0 | 2.5 | 0.76 | 12 |
| 16 | 400 | 564 | 172.0 | 2.2 | 0.67 | 10 |

* For 100-ft (30m) Bending Length.

1) Do not bend pipe until adhesive has cured. At rated pressure sharper bends may create excessive stress concentrations.

Thrust blocks: most properly bedded installations do not require thrust blocks at ambient operating temperatures. Consult FGS for information regarding blocking of buried pipelines for your specific application.
Live loads: when properly bedded in compacted sand in stable soils and provided with at least $3 \mathrm{ft}(1 \mathrm{~m})$ of cover, Bondstrand 4000 will carry H 20 wheel loadings of at least $16,000 \mathrm{lb}(7250 \mathrm{~kg})$ per axle.

## Span Lengths

Recommended maximum support spacings for Bondstrand Series 4000 pipe at various operating temperatures. Values based on 0.5 -inch ( 12 mm ) deflection at midspan for fluid specific gravity $=1.0$.

| $\begin{array}{c}\text { Nominal } \\ \text { Pipe Size }\end{array}$ |  | $\begin{array}{c}\text { Continuous Spans } \\ \mathrm{ft}\end{array}$ |  |  |  |  | Single Spans |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ft |  |  |  |  |  |  |  |  |  |  |  |$]$

1) Span recommendations include no provision for weights (fittings, valves, flanges, etc.) or thrusts (branches, turns, etc.).
2) Span recommendations are calculated for a maximum long-term deflection of $1 / 2$ inch to ensure good appearance and adequate drainage.
3)-Continuous spans are defined as interior (not end) spans that are uniform in length and free from structural rotation at the supports. Single spans are supported only at the ends and are hinged or free to rotate at the supports.

Bondstrand 4000 piping systems are designed for hydrostatic testing at $150 \%$ of rated operating pressure. Pneumatic testing is not recommended.

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# Bondstrand ${ }^{\circledR}$ Series 4000 Fiberglass Pipe and Fittings for General Industrial Service 

Bondstrand Series 4000 pipe and fittings are available in $1 "-16$ " diameters. The specification defines the reinforced thermosetting resin (RTR) piping system to be used in those sections of plant piping, general services, calling for fiberglass piping systems.

## References, Quality Assurance

References are made to other standards and tests which are a part of this section as modified. Where conflict exists between the requirements of this specification and listed references, the specification shall prevail.

## Physical and Mechanical Properties

| Pipe Property | Units | $\begin{gathered} 70^{\circ} \mathrm{F} \\ \left(21^{\circ} \mathrm{C}\right) \end{gathered}$ | $\begin{aligned} & 200^{\circ} \mathrm{F} \\ & \left(93^{\circ} \mathrm{C}\right) \end{aligned}$ | ASTM Method |
| :---: | :---: | :---: | :---: | :---: |
| Circumferential Tensile Stress at Weeping | $\begin{gathered} 10^{3} \mathrm{psi} \\ \mathrm{MPa} \end{gathered}$ | $\begin{gathered} 18.50 \\ 128.00 \end{gathered}$ |  | D1599 |
| Tensile Modulus | $10^{6} \mathrm{psi}$ GPa | $\begin{gathered} 3.65 \\ 25.20 \end{gathered}$ | $\begin{gathered} 3.20 \\ 22.10 \end{gathered}$ |  |
| Poisson's Ratio |  | 0.56 | 0.68 | D2105 |
| Longitudinal Tensile Strength | $\begin{gathered} 10^{3} \mathrm{psi} \\ \mathrm{MPa} \end{gathered}$ | $\begin{gathered} 8.50 \\ 58.60 \end{gathered}$ | $\begin{gathered} 6.90 \\ 47.60 \end{gathered}$ | D2105 |
| Tensile Modulus | $10^{6} \mathrm{psi}$ GPa | $\begin{gathered} 1.60 \\ 11.10 \end{gathered}$ | $\begin{aligned} & 1.24 \\ & 8.60 \end{aligned}$ | D2105 |
| Poisson's Ratio |  | 0.37 | 0.41 | D2105 |
| Beam Apparent-Elastic Modulus | $\begin{gathered} 10^{6} \mathrm{si} \\ \mathrm{GPa} \end{gathered}$ | $\begin{gathered} \hline 1.70 \\ 11.70 \end{gathered}$ | $\begin{aligned} & 1.08 \\ & 6.90 \end{aligned}$ | D2925 |
| Hydrostatic Design Basis (Cyclic) | $\begin{gathered} 10^{3} \mathrm{psi} \\ \mathrm{MPa} \end{gathered}$ | $\begin{gathered} 6.00 \\ 11.40 \end{gathered}$ |  | D2992 |
| Thermal Conductivity Pipe Wall | $\begin{gathered} \mathrm{Btu} \cdot \mathrm{in} /\left(\mathrm{hr} \cdot \mathrm{ft}^{2} \cdot{ }^{\circ} \mathrm{F}\right) \\ \mathrm{W} / \mathrm{m} \cdot \mathrm{C} \end{gathered}$ | $\begin{aligned} & 1.70 \\ & 0.25 \end{aligned}$ |  | C177 |
| Thermal Expansion Linear | $\begin{gathered} 10^{-6} \mathrm{in} / \mathrm{in} /{ }^{\circ} \mathrm{F} \\ 10^{-6} \mathrm{~mm} / \mathrm{mm}^{\circ} \mathrm{C} \end{gathered}$ | $\begin{gathered} 8.50 \\ 15.30 \end{gathered}$ |  | D696 |
| Flow Coefficient | Hazen-Williams | 150.00 | - |  |
| Absolute Roughness | $10^{-6} \mathrm{ft}$ | $\begin{gathered} 17.40 \\ 5.30 \end{gathered}$ | - |  |
| Specific Gravity | - | 1.80 | - | D792 |
| Density | $\mathrm{lb} / \mathrm{in}^{3}$ | 0.07 | - |  |

## Performance Requirements

Pipe shall be manufactured according to ASTM D2996 Specification for RTRP. When classified under ASTM D2310, the pipe shall meet Type I, Grade I and Class F (RTRP 11FE) cell limits in 2" through 16" nominal pipe sizes.

The piping systems must meet USFDA requirements for food processing piping under Federal Regulations 21CFR 175.105 and 21CFR 177.242 when bonded with RP6B adhesive.

| Materials | Pipe Construction |
| :--- | :--- |
|  | Filament-wound fiberglass reinforced epoxy resin pipe shall be Bondstrand ${ }^{\circledR} 4000$ as manufactured by NOV |
|  | Fiber Glass Systems or approved equal. The integral reinforced corrosion barrier shall have a nominal 50-mil |
| thickness and be constructed with the same epoxy resin as the pipe structural wall. |  |

## Structural Wall

The pipe shall have the following nominal wall thickness.

| Diameter | Nominal <br> Wall <br> Thickness |  |
| :---: | :---: | :---: |
| in | in | mm |
| 2 | .123 | 3.1 |
| 3 | .126 | 3.2 |
| 4 | .151 | 3.8 |
| 6 | .181 | 4.6 |
| 8 | .226 | 5.7 |
| 10 | .226 | 5.7 |
| 12 | .226 | 5.7 |
| 14 | .250 | 6.4 |
| 16 | .269 | 6.8 |

## Pipe End Preparation Options

The piping manufacturer will provide $20^{\prime}$ or 30 " random length joints if the contractor requests them in sizes 2 " -6 " to reduce field labor time in those sections of the system where longer lengths may be employed. Additionally, the pipe manufacturer will provide pipe joints with the spigot ends already prepared for adhesive application to reduce field labor time on all pipe sizes (2"-16").

## Pressure Rating

Aromatic amine cured epoxy resin piping shall be rated for a minimum of 150 psi at $200^{\circ} \mathrm{F}$ in sizes through $16^{\prime \prime}$.

Fittings
It is important to maintain compatibility of fittings, piping and adhesives to ensure that the system performs as specified. Pipe, fittings and adhesive shall be supplied by the same manufacturer.

Filament wound fittings in 1 "-16" sizes shall be filament wound with a reinforced, resin-rich liner of equal or greater thickness than the pipe liner and shall be manufactured with the same resin type as the pipe.

Compression molded fittings in sizes 2"-6" may be used in some services; contact manufacturer. Where fast closure of valves may produce surges (water hammer), filament-wound fittings will be used. Contact molded, spray up or hand lay-up fittings shall not be allowed.

## Testing Inspection and testing of the piping will be performed in accordance with the requirements of ANSI B31.1. Hydrostatic testing of all installed piping shall be performed with water at a maximum of $1-1 / 2$ times the system design pressure or of the lowest rated piping system component, whichever is lower.

## Installation

Installation and techniques, as well as system design criteria including burial, anchoring, guiding and supporting, shall be in accordance with manufacturer's recommendations. Piping system installers and fitters will be trained by a direct factory employee of the piping system manufacturer and certified by the trainer prior to system assembly in the field.

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## Bondstrand"' 5000/5000C Product Data

## (Severely Corrosive Industrial Service and Oxidizing Acids

Uses and Applications

## Listings

- Acid drains
- Bleach processing
- Chemical process piping
- Chlorinated water
- Chlorine
- Corrosive slurries
- Food processing plant
- Organic chemicals
- Oxidizing chemicals and acids
- Phosphoric acid
- Water Treatment/Purification
- General industrial service for severely corrosive liquids


## Pipe

Filament-wound fiberglass-reinforced vinyl ester pipe with integral 0.050 -inch ( 1.3 mm ) resinrich reinforced liner.

| Nominal <br> Pipe Size |  | ASTM <br> Designation |
| :---: | :---: | :---: |
| in | mm | D2996 |
| $2-6$ | $50-150$ | RTRP 11FW-1012/11FE-1012 |
| $8-16$ | $200-400$ | RTRP 11FW-1013/11FE-1013 |

## Filament-wound fittings

Tees
$90^{\circ}$ and $45^{\circ}$ elbows
Crosses
Nipples and couplings
$45^{\circ}$ laterals
Tapered body reducers

## Molded fittings

Tees (2 to 6 inch only)
$90^{\circ}$ and $45^{\circ}$ elbows (2 to 6 inch only)
Reducing flanges
Plugs and end-caps

## Flanges

Filament-wound or molded flanges with ANSI B16.1 and ANSI B16.5 drilling Molded reducing and blind flanges

Thermosetting adhesives
RP105B two-part vinyl ester for 5000
RP106 two-part vinyl ester for 5000C

## Joining systems

Quick-Lock ${ }^{\circledR}$ straight/taper adhesive-bonded joint featuring integral pipe stop in bell for predictable, precise laying lengths.

Flanges and flanged fittings.

## Pipe Lengths

| Nominal <br> Pipe Size |  | Random <br> Lengths |  |
| :---: | :---: | :---: | :---: |
| in | mm | ft | m |
| $2-8$ | $50-150$ | 30 | 9 |
| $10-16$ | $200-400$ | 20 | 6 |

## Elbows

Tees
Flanges, blind flanges and reducing flanges
Plugs and end-caps
Crosses
Nipples and couplings $45^{\circ}$ laterals
Tapered body reducers
Tapered body reducers, tees and $90^{\circ}$ and $45^{\circ}$ elbows are available with any combination of Quick-Lock female and filament-wound or molded flange ends.

Laying lengths of filament-wound fittings with Quick-Lock ends match those of ANSI B16.9 steel buttwelding fittings. Flanged ends match ANSI B16.1 and B16.5 center-to-face and face-to-face dimensions.

Typical Pipe Dimensions and Weights

| Nominal Pipe Size ${ }^{(1)}$ |  | Pipe I.D. |  | Nominal Wall Thickness ${ }^{(2)}$ |  | Average Sectional Area ${ }^{(3)}$ |  | Pipe <br> Weight |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | in | mm | in | mm | in | $\mathrm{mm}^{2}$ | $\mathrm{lb} / \mathrm{ft}$ | kg/m |
| 2 | 50 | 2.10 | 53 | . 15 | 3.9 | 1.13 | 730 | 1.0 | 1.2 |
| 3 | 80 | 3.22 | 82 | . 16 | 4.0 | 1.70 | 1100 | 1.5 | 1.7 |
| 4 | 100 | 4.14 | 105 | . 20 | 5.1 | 2.73 | 1760 | 2.4 | 2.8 |
| 6 | 150 | 6.20 | 159 | . 20 | 5.1 | 4.06 | 2620 | 3.5 | 4.2 |
| 8 | 200 | 8.22 | 209 | . 226 | 5.7 | 5.83 | 3760 | 5.0 | 6.1 |
| 10 | 250 | 10.35 | 263 | . 226 | 5.7 | 7.31 | 4710 | 6.2 | 7.7 |
| 12 | 300 | 12.35 | 314 | . 226 | 5.7 | 8.69 | 5600 | 7.4 | 9.1 |
| 14 | 350 | 13.56 | 344 | . 250 | 6.4 | 10.85 | 7000 | 8.7 | 11.0 |
| 16 | 400 | 15.50 | 394 | . 286 | 7.3 | 14.18 | 9150 | 11.2 | 14.0 |

1) For availability of $1,11 / 2,14$ and 16 -inch ( $25,40,350$ and 400 mm ) sizes, consult your FGS representative.
2) Minimum wall thickness shall not be less than $87.5 \%$ of nominal wall thickness in accordance with ASTM D2996.
3) Use these values for calculating longitudinal thrust.

## Typical Pipe Performance

| Nominal <br> Pipe Size |  | Internal <br> Pressure Rating |  | Collapse <br> Pressure Rating <br>  <br> $(1)$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | psig | Mpa | psig | Mpa |
| 2 | 50 | 450 | 3.10 | 212 | 1.46 |
| 3 | 80 | 320 | 2.21 | 68 | 0.47 |
| 4 | 100 | 350 | 2.41 | 82 | 0.56 |
| 6 | 150 | 249 | 1.72 | 24 | 0.17 |
| 8 | 200 | 225 | 1.55 | 16 | 0.11 |
| 10 | 250 | 175 | 1.21 | 8 | 0.06 |
| 12 | 300 | 150 | 1.03 | 5 | 0.03 |
| 14 | 350 | 150 | 1.02 | 5 | 0.03 |
| 16 | 400 | 150 | 1.02 | 6 | 0.04 |

1) At $70^{\circ} \mathrm{F}\left(21^{\circ} \mathrm{C}\right)$. Reduce linearly to $84 \%$ at $140^{\circ} \mathrm{F}\left(60^{\circ} \mathrm{C}\right), 76 \%$ at $170^{\circ} \mathrm{F}$ and $50 \%$ at $200^{\circ} \mathrm{F}\left(93^{\circ} \mathrm{C}\right)$.

Fittings Pressure Ratings

| Nominal Pipe Size |  | Elbows \& Tees |  |  |  | Tapered Body Reducers \& Flanges |  | Blind Flanges \& Bushed Saddles |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Filament-Wound |  | Molded |  |  |  |  |  |
| in | mm | psig | MPa | psig | MPa | psig | MPa | psig | MPa |
| 2 | 50 | 300 | 2.07 | 200 | 1.38 | 450 | 3.10 | 150 | 1.03 |
| 3 | 80 | 275 | 1.89 | 150 | 1.03 | 350 | 2.41 | 150 | 1.03 |
| 4 | 100 | 200 | 1.38 | 150 | 1.03 | 350 | 2.41 | 150 | 1.03 |
| 6 | 150 | 175 | 1.21 | 150 | 1.03 | 250 | 1.72 | 150 | 1.03 |
| 8 | 200 | 225 | 1.03 | - | - | 225 | 1.55 | 150 | 1.03 |
| 10 | 250 | 150 | 1.03 | - | - | 175 | 1.21 | 150 | 1.03 |
| 12 | 300 | 150 | 1.03 | - | - | 150 | 1.03 | 150 | 1.03 |
| 14 | 350 | 150 | 1.03 | - | - | 150 | 1.03 | 150 | 1.03 |
| 16 | 400 | 150 | 1.03 | - | - | 150 | 1.03 | 150 | 1.03 |

1) Use Bondstrand Series 2000 epoxy saddles with 316 stainless steel outlet. Other outlet materials available on special order.

| Nominal <br> Pipe Size |  | Laterals |  | Crosses |  | Reducer <br> Bushing |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | psig | MPa | psig | MPa | psig | MPa |
| 2 | 50 | 275 | 1.90 | 150 | 1.03 | 50 | .35 |
| 3 | 80 | 250 | 1.72 | 150 | 1.03 | 50 | .35 |
| 4 | 100 | 200 | 1.38 | 150 | 1.03 | 50 | .35 |
| 6 | 150 | 150 | 1.03 | 100 | 0.69 | 50 | .35 |
| 8 | 200 | 150 | 1.03 | 100 | 0.69 | 50 | .35 |
| 10 | 250 | 150 | 1.03 | 100 | 0.69 | 50 | .35 |
| 12 | 300 | 150 | 1.03 | 100 | 0.69 | 50 | .35 |
| 14 | 350 | 150 | 1.03 | 100 | 0.69 | 50 | .35 |
| 16 | 400 | 150 | 1.03 | 100 | 0.69 | 50 | .35 |

1) Reducer bushings bonded into flanges will have the same rating as the flange. Otherwise, rated as shown.

## Typical

 Physical PropertiesTypical Physical Properties

| Pipe Property | Units | Value | ASTM |
| :--- | :---: | :---: | :---: |
| Thermal conductivity | $\mathrm{Btu}-\mathrm{in} /\left(\mathrm{h} \cdot \mathrm{ft}^{2}{ }^{\circ} \mathrm{F} \mathrm{F}\right)$ | 2.0 | C 177 |
| Coefficient of thermal |  |  |  |
| expansion (linear) | $\mathrm{W} / \mathrm{m} \cdot{ }^{\circ} \mathrm{C}$ | 0.28 |  |
| $(2-16$ inch $)$ |  |  |  |
| $77^{\circ} \mathrm{F}$ to $150^{\circ} \mathrm{F}$ | $10^{-6} \mathrm{in} / \mathrm{in} /{ }^{\circ} \mathrm{F}$ |  |  |
| $\left(25^{\circ} \mathrm{C}\right.$ to $\left.65^{\circ} \mathrm{C}\right)$ | $10^{-6} \mathrm{~cm} / \mathrm{cm} /{ }^{\circ} \mathrm{C}$ | 10 | 18 |
| Flow coefficient | Hazen-Williams | D696 |  |
| Absolute roughness | $10^{-6} \mathrm{ft}$ | 150.00 | - |
| Specific gravity | $10^{-6} \mathrm{~m}$ | 17.40 | - |
| Density | - | 5.30 | - |

## Typical Physical Properties

Typical Mechanical Properties

| Pipe Property ${ }^{(1)}$ | Units | Value | ASTM |
| :---: | :---: | :---: | :---: |
|  |  | 2"-16" |  |
| Tensile strength Longitudinal Circumferential | $\begin{gathered} 10^{3} \mathrm{psi} \\ \mathrm{MPa} \\ 10^{3} \mathrm{psi} \\ \mathrm{MPa} \end{gathered}$ | $\begin{gathered} 7.0 \\ 48.3 \\ 18.5 \\ 128.0 \end{gathered}$ | $\begin{aligned} & \text { D2105 } \\ & \text { D1599 } \end{aligned}$ |
| Tensile modulus Longitudinal <br> Circumferential | $10^{6} \mathrm{psi}$ GPa $10^{6} \mathrm{psi}$ GPa | $\begin{aligned} & 1.45 \\ & 10.1 \\ & 3.13 \\ & 21.6 \end{aligned}$ | D2105 |
| Compressive strength Longitudinal | $\begin{gathered} 10^{3} \mathrm{psi} \\ \mathrm{MPa} \end{gathered}$ | $\begin{gathered} 20.0 \\ 138.0 \end{gathered}$ | - |
| Compressive modulus Longitudinal | $10^{6} \mathrm{psi}$ GPa | $\begin{gathered} 1.5 \\ 10.3 \end{gathered}$ | - |
| Long-term hydrostatic ${ }^{(3)}$ Design basis <br> Static, Hoop Stress <br> LCL 20 Year Life @ $150^{\circ} \mathrm{F}\left(65^{\circ} \mathrm{C}\right)$ <br> Cyclic, Hoop Stress <br> LCL 20 Year Life @150 ${ }^{\circ}\left(65^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 10^{3} \mathrm{psi} \\ \mathrm{MPa} \\ 10^{3} \mathrm{psi} \\ \mathrm{MPa} \end{gathered}$ | $\begin{gathered} 12.8 \\ 88.2 \\ - \\ - \end{gathered}$ | $\begin{aligned} & \text { D2992(B) } \\ & \text { D2992(A) } \end{aligned}$ |
| Poisson's Ratio ${ }^{(2)}$ $\begin{aligned} & v_{y x} \\ & v_{x y} \end{aligned}$ | - | $\begin{aligned} & 0.19 \\ & 0.11 \end{aligned}$ | - |

${ }^{(1)}$ Based on structural wall thickness, at room temperature unless noted.
${ }^{(2)}$ The first subscript denotes the direction of applied stress and the second that of measured contraction
x denotes longitudinal direction.
y denotes circumferential direction.
${ }^{(3)}$ Test fixtures were end type (full end thrust on samples).

| Nominal <br> Pipe Size |  | Stiffness <br> Factor $^{(1)}$ |  | Pipe <br> Stiffness |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | Ib in | $\mathrm{N} \bullet \mathrm{m}$ | psi | MPa <br> Beam Moment <br> of Inertia(2) |  |  |
| 2 | 50 | 340 | 38.4 | 1540 | 10.6 | $\mathrm{in}^{4}$ | $10^{6} \mathrm{~mm}^{4}$ |
| 3 | 80 | 340 | 38.4 | 460 | 3.2 | 1.61 | 0.20 |
| 4 | 100 | 820 | 92.6 | 530 | 3.7 | 4.7 | 1.96 |
| 6 | 150 | 820 | 92.6 | 160 | 1.1 | 15.5 | 6.40 |
| 8 | 200 | 1180 | 133.3 | 105 | 0.72 | 39 | 16.3 |
| 10 | 250 | 1180 | 133.3 | 53 | 0.37 | 77 | 32 |
| 12 | 300 | 1180 | 133.3 | 31 | 0.23 | 129 | 54 |
| 14 | 350 | 1330 | 150.2 | 36 | 0.25 | 209 | 88 |
| 16 | 400 | 2190 | 247.4 | 38 | 0.26 | 368 | 154 |

1) Per ASTM D2412.
2) Use these values to calculate permissible spans.

| Bending Radius | Nominal Pipe Size |  | Bending Radius ${ }^{1}$ <br> (R) |  | Maximum Allowable ${ }^{(2)}$ <br> (H) |  | Turning Angle |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | in | mm | $\mathrm{lb} \cdot \mathrm{in}$ | $\mathrm{N} \cdot \mathrm{m}$ | ft | m | a |
|  | 2 | 50 | 69.4 | 21 | 17.5 | 5.3 | 84 |
|  | 3 | 80 | 101.1 | 31 | 12.1 | 3.7 | 57 |
|  | 4 | 100 | 129.9 | 40 | 9.5 | 2.9 | 44 |
|  | 6 | 150 | 191.8 | 58 | 6.5 | 1.9 | 30 |
|  | 8 | 200 | 250 | 76 | 5.0 | 1.5 | 23 |
|  | 10 | 250 | 312 | 95 | 4.0 | 1.2 | 18 |
|  | 12 | 300 | 370 | 113 | 3.4 | 1.0 | 15 |
|  | 14 | 350 | 410 | 125 | 3.2 | 0.9 | 14 |
|  | 16 | 400 | 410 | 143 | 2.7 | 0.8 | 12 |

1) Do not bend pipe until adhesive has cured. At rated pressure sharper bends may create excessive stress concentrations.
2) For $100-\mathrm{ft}(30 \mathrm{~m})$ bending length, S

## Buried Installations

## Live loads

Bondstrand 5000/5000C will carry H20 wheel loadings of at least $16.000 \mathrm{lb}(7250 \mathrm{~kg})$ per axle when properly bedded in compacted sand in stable soils and provided with at least $3 \mathrm{ft}(1 \mathrm{~m})$ of cover.

## Thrust blocks

Most properly bedded installations do not require thrust blocks. Consult FGS for recommendations for systems operating at elevated temperatures.

| Nominal <br> Pipe Size | Maximum Earth Cover ${ }^{1}$ |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 100 psi | 0.69 MPa | 125 psi | 0.86 MPa | 150 psi | 1.03 MPa |  |
| in | mm | ft | m | ft | m | ft | m |
| 2 | 50 | 30 | 9.14 | 30 | 9.14 | 30 | 9.14 |
| 3 | 80 | 30 | 9.14 | 30 | 9.14 | 30 | 9.14 |
| 4 | 100 | 30 | 9.14 | 30 | 9.14 | 30 | 9.14 |
| 6 | 150 | 30 | 9.14 | 24 | 7.32 | 23 | 7.01 |
| 8 | 200 | 23 | 7.01 | 22 | 6.71 | 21 | 6.40 |
| 10 | 250 | 23 | 7.01 | 21 | 6.40 | 19 | 5.79 |
| 12 | 300 | 23 | 7.01 | 21 | 6.40 | 18 | 5.49 |
| 14 | 350 | 23 | 7.01 | 21 | 6.40 | 17 | 5.18 |
| 16 | 400 | 23 | 7.01 | 20 | 6.10 | 16 | 4.88 |

1) Based on a $1201 \mathrm{~b} / \mathrm{tt} 3(1925 \mathrm{~kg} / \mathrm{m} 3)$ soil density and $1000 \mathrm{psi}(6.9 \mathrm{MPa})$ modulus of soil reaction.

## Span Lengths

Recommended maximum support spacings for Bondstrand 5000/5000C vinyl ester pipe at various operating temperatures. Values based on 0.5 -inch ( 12 mm ) deflection at midspan for fluid specific gravity $=1.0$. For fully continuous spans, values may be increased up to $20 \%$. Decrease values by $20 \%$ for single spans.

| Nominal <br> Pipe Size |  | Spans (ft) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | $100^{\circ} \mathrm{F}$ | $140^{\circ} \mathrm{F}$ | $170^{\circ} \mathrm{F}$ | $200^{\circ} \mathrm{F}$ |
| 2 | 50 | 12.1 | 10.8 | 9.4 | 7.5 |
| 3 | 80 | 13.7 | 12.3 | 10.7 | 8.6 |
| 4 | 100 | 16.1 | 14.5 | 12.6 | 10.0 |
| 6 | 150 | 18.1 | 16.1 | 14.2 | 11.2 |
| 8 | 200 | 20.1 | 18.1 | 15.5 | 12.6 |
| 10 | 250 | 21.4 | 19.2 | 16.6 | 13.5 |
| 12 | 300 | 22.3 | 20.2 | 17.5 | 13.9 |
| 14 | 350 | 23.1 | 20.7 | 18.1 | 14.4 |
| 16 | 400 | 24.3 | 21.6 | 18.9 | 15.0 |

1) Span recommendations are intended for normal horizontal piping support arrangements, but include no provision for weights (fittings, valves, flanges, etc) or thrusts (branches, turns, etc.).
2) Span recommendations are calculated for a maximum long-term deflection of $1 / 2$ inch to ensure good appearance and adequate drainage.

Bondstrand 5000/5000C piping systems are designed for hydrostatic field testing at $150 \%$ of rated operating pressure. Pneumatic testing is not recommended.

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## Bondstrand"' 5000/5000C Product Data

## (Severely Corrosive Industrial Service and Oxidizing Acids

Uses and Applications

## Listings

- Acid drains
- Bleach processing
- Chemical process piping
- Chlorinated water
- Chlorine
- Corrosive slurries
- Food processing plant
- Organic chemicals
- Oxidizing chemicals and acids
- Phosphoric acid
- Water Treatment/Purification
- General industrial service for severely corrosive liquids


## Pipe

Filament-wound fiberglass-reinforced vinyl ester pipe with integral 0.050 -inch ( 1.3 mm ) resinrich reinforced liner.

| Nominal <br> Pipe Size |  | ASTM <br> Designation |
| :---: | :---: | :---: |
| in | mm | D2996 |
| $2-6$ | $50-150$ | RTRP 11FW-1012/11FE-1012 |
| $8-16$ | $200-400$ | RTRP 11FW-1013/11FE-1013 |

## Filament-wound fittings

Tees
$90^{\circ}$ and $45^{\circ}$ elbows
Crosses
Nipples and couplings
$45^{\circ}$ laterals
Tapered body reducers

## Molded fittings

Tees (2 to 6 inch only)
$90^{\circ}$ and $45^{\circ}$ elbows (2 to 6 inch only)
Reducing flanges
Plugs and end-caps

## Flanges

Filament-wound or molded flanges with ANSI B16.1 and ANSI B16.5 drilling Molded reducing and blind flanges

Thermosetting adhesives
RP105B two-part vinyl ester for 5000
RP106 two-part vinyl ester for 5000C

## Joining systems

Quick-Lock ${ }^{\circledR}$ straight/taper adhesive-bonded joint featuring integral pipe stop in bell for predictable, precise laying lengths.

Flanges and flanged fittings.

## Pipe Lengths

| Nominal <br> Pipe Size |  | Random <br> Lengths |  |
| :---: | :---: | :---: | :---: |
| in | mm | ft | m |
| $2-8$ | $50-150$ | 30 | 9 |
| $10-16$ | $200-400$ | 20 | 6 |

## Elbows

Tees
Flanges, blind flanges and reducing flanges
Plugs and end-caps
Crosses
Nipples and couplings $45^{\circ}$ laterals
Tapered body reducers
Tapered body reducers, tees and $90^{\circ}$ and $45^{\circ}$ elbows are available with any combination of Quick-Lock female and filament-wound or molded flange ends.

Laying lengths of filament-wound fittings with Quick-Lock ends match those of ANSI B16.9 steel buttwelding fittings. Flanged ends match ANSI B16.1 and B16.5 center-to-face and face-to-face dimensions.

Typical Pipe Dimensions and Weights

| Nominal Pipe Size ${ }^{(1)}$ |  | Pipe I.D. |  | Nominal Wall Thickness ${ }^{(2)}$ |  | Average Sectional Area ${ }^{(3)}$ |  | Pipe <br> Weight |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | in | mm | in | mm | in | $\mathrm{mm}^{2}$ | $\mathrm{lb} / \mathrm{ft}$ | kg/m |
| 2 | 50 | 2.10 | 53 | . 15 | 3.9 | 1.13 | 730 | 1.0 | 1.2 |
| 3 | 80 | 3.22 | 82 | . 16 | 4.0 | 1.70 | 1100 | 1.5 | 1.7 |
| 4 | 100 | 4.14 | 105 | . 20 | 5.1 | 2.73 | 1760 | 2.4 | 2.8 |
| 6 | 150 | 6.20 | 159 | . 20 | 5.1 | 4.06 | 2620 | 3.5 | 4.2 |
| 8 | 200 | 8.22 | 209 | . 226 | 5.7 | 5.83 | 3760 | 5.0 | 6.1 |
| 10 | 250 | 10.35 | 263 | . 226 | 5.7 | 7.31 | 4710 | 6.2 | 7.7 |
| 12 | 300 | 12.35 | 314 | . 226 | 5.7 | 8.69 | 5600 | 7.4 | 9.1 |
| 14 | 350 | 13.56 | 344 | . 250 | 6.4 | 10.85 | 7000 | 8.7 | 11.0 |
| 16 | 400 | 15.50 | 394 | . 286 | 7.3 | 14.18 | 9150 | 11.2 | 14.0 |

1) For availability of $1,11 / 2,14$ and 16 -inch ( $25,40,350$ and 400 mm ) sizes, consult your FGS representative.
2) Minimum wall thickness shall not be less than $87.5 \%$ of nominal wall thickness in accordance with ASTM D2996.
3) Use these values for calculating longitudinal thrust.

## Typical Pipe Performance

| Nominal <br> Pipe Size |  | Internal <br> Pressure Rating |  | Collapse <br> Pressure Rating <br>  <br> $(1)$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | psig | Mpa | psig | Mpa |
| 2 | 50 | 450 | 3.10 | 212 | 1.46 |
| 3 | 80 | 320 | 2.21 | 68 | 0.47 |
| 4 | 100 | 350 | 2.41 | 82 | 0.56 |
| 6 | 150 | 249 | 1.72 | 24 | 0.17 |
| 8 | 200 | 225 | 1.55 | 16 | 0.11 |
| 10 | 250 | 175 | 1.21 | 8 | 0.06 |
| 12 | 300 | 150 | 1.03 | 5 | 0.03 |
| 14 | 350 | 150 | 1.02 | 5 | 0.03 |
| 16 | 400 | 150 | 1.02 | 6 | 0.04 |

1) At $70^{\circ} \mathrm{F}\left(21^{\circ} \mathrm{C}\right)$. Reduce linearly to $84 \%$ at $140^{\circ} \mathrm{F}\left(60^{\circ} \mathrm{C}\right), 76 \%$ at $170^{\circ} \mathrm{F}$ and $50 \%$ at $200^{\circ} \mathrm{F}\left(93^{\circ} \mathrm{C}\right)$.

Fittings Pressure Ratings

| Nominal Pipe Size |  | Elbows \& Tees |  |  |  | Tapered Body Reducers \& Flanges |  | Blind Flanges \& Bushed Saddles |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Filament-Wound |  | Molded |  |  |  |  |  |
| in | mm | psig | MPa | psig | MPa | psig | MPa | psig | MPa |
| 2 | 50 | 300 | 2.07 | 200 | 1.38 | 450 | 3.10 | 150 | 1.03 |
| 3 | 80 | 275 | 1.89 | 150 | 1.03 | 350 | 2.41 | 150 | 1.03 |
| 4 | 100 | 200 | 1.38 | 150 | 1.03 | 350 | 2.41 | 150 | 1.03 |
| 6 | 150 | 175 | 1.21 | 150 | 1.03 | 250 | 1.72 | 150 | 1.03 |
| 8 | 200 | 225 | 1.03 | - | - | 225 | 1.55 | 150 | 1.03 |
| 10 | 250 | 150 | 1.03 | - | - | 175 | 1.21 | 150 | 1.03 |
| 12 | 300 | 150 | 1.03 | - | - | 150 | 1.03 | 150 | 1.03 |
| 14 | 350 | 150 | 1.03 | - | - | 150 | 1.03 | 150 | 1.03 |
| 16 | 400 | 150 | 1.03 | - | - | 150 | 1.03 | 150 | 1.03 |

1) Use Bondstrand Series 2000 epoxy saddles with 316 stainless steel outlet. Other outlet materials available on special order.

| Nominal <br> Pipe Size |  | Laterals |  | Crosses |  | Reducer <br> Bushing |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | psig | MPa | psig | MPa | psig | MPa |
| 2 | 50 | 275 | 1.90 | 150 | 1.03 | 50 | .35 |
| 3 | 80 | 250 | 1.72 | 150 | 1.03 | 50 | .35 |
| 4 | 100 | 200 | 1.38 | 150 | 1.03 | 50 | .35 |
| 6 | 150 | 150 | 1.03 | 100 | 0.69 | 50 | .35 |
| 8 | 200 | 150 | 1.03 | 100 | 0.69 | 50 | .35 |
| 10 | 250 | 150 | 1.03 | 100 | 0.69 | 50 | .35 |
| 12 | 300 | 150 | 1.03 | 100 | 0.69 | 50 | .35 |
| 14 | 350 | 150 | 1.03 | 100 | 0.69 | 50 | .35 |
| 16 | 400 | 150 | 1.03 | 100 | 0.69 | 50 | .35 |

1) Reducer bushings bonded into flanges will have the same rating as the flange. Otherwise, rated as shown.

## Typical

 Physical PropertiesTypical Physical Properties

| Pipe Property | Units | Value | ASTM |
| :--- | :---: | :---: | :---: |
| Thermal conductivity | $\mathrm{Btu}-\mathrm{in} /\left(\mathrm{h} \cdot \mathrm{ft}^{2}{ }^{\circ} \mathrm{F} \mathrm{F}\right)$ | 2.0 | C 177 |
| Coefficient of thermal |  |  |  |
| expansion (linear) | $\mathrm{W} / \mathrm{m} \cdot{ }^{\circ} \mathrm{C}$ | 0.28 |  |
| $(2-16$ inch $)$ |  |  |  |
| $77^{\circ} \mathrm{F}$ to $150^{\circ} \mathrm{F}$ | $10^{-6} \mathrm{in} / \mathrm{in} /{ }^{\circ} \mathrm{F}$ |  |  |
| $\left(25^{\circ} \mathrm{C}\right.$ to $\left.65^{\circ} \mathrm{C}\right)$ | $10^{-6} \mathrm{~cm} / \mathrm{cm} /{ }^{\circ} \mathrm{C}$ | 10 | 18 |
| Flow coefficient | Hazen-Williams | D696 |  |
| Absolute roughness | $10^{-6} \mathrm{ft}$ | 150.00 | - |
| Specific gravity | $10^{-6} \mathrm{~m}$ | 17.40 | - |
| Density | - | 5.30 | - |

## Typical Physical Properties

Typical Mechanical Properties

| Pipe Property ${ }^{(1)}$ | Units | Value | ASTM |
| :---: | :---: | :---: | :---: |
|  |  | 2"-16" |  |
| Tensile strength Longitudinal Circumferential | $\begin{gathered} 10^{3} \mathrm{psi} \\ \mathrm{MPa} \\ 10^{3} \mathrm{psi} \\ \mathrm{MPa} \end{gathered}$ | $\begin{gathered} 7.0 \\ 48.3 \\ 18.5 \\ 128.0 \end{gathered}$ | $\begin{aligned} & \text { D2105 } \\ & \text { D1599 } \end{aligned}$ |
| Tensile modulus Longitudinal <br> Circumferential | $10^{6} \mathrm{psi}$ GPa $10^{6} \mathrm{psi}$ GPa | $\begin{aligned} & 1.45 \\ & 10.1 \\ & 3.13 \\ & 21.6 \end{aligned}$ | D2105 |
| Compressive strength Longitudinal | $\begin{gathered} 10^{3} \mathrm{psi} \\ \mathrm{MPa} \end{gathered}$ | $\begin{gathered} 20.0 \\ 138.0 \end{gathered}$ | - |
| Compressive modulus Longitudinal | $10^{6} \mathrm{psi}$ GPa | $\begin{gathered} 1.5 \\ 10.3 \end{gathered}$ | - |
| Long-term hydrostatic ${ }^{(3)}$ Design basis <br> Static, Hoop Stress <br> LCL 20 Year Life @ $150^{\circ} \mathrm{F}\left(65^{\circ} \mathrm{C}\right)$ <br> Cyclic, Hoop Stress <br> LCL 20 Year Life @150 ${ }^{\circ}\left(65^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 10^{3} \mathrm{psi} \\ \mathrm{MPa} \\ 10^{3} \mathrm{psi} \\ \mathrm{MPa} \end{gathered}$ | $\begin{gathered} 12.8 \\ 88.2 \\ - \\ - \end{gathered}$ | $\begin{aligned} & \text { D2992(B) } \\ & \text { D2992(A) } \end{aligned}$ |
| Poisson's Ratio ${ }^{(2)}$ $\begin{aligned} & v_{y x} \\ & v_{x y} \end{aligned}$ | - | $\begin{aligned} & 0.19 \\ & 0.11 \end{aligned}$ | - |

${ }^{(1)}$ Based on structural wall thickness, at room temperature unless noted.
${ }^{(2)}$ The first subscript denotes the direction of applied stress and the second that of measured contraction
x denotes longitudinal direction.
y denotes circumferential direction.
${ }^{(3)}$ Test fixtures were end type (full end thrust on samples).

| Nominal <br> Pipe Size |  | Stiffness <br> Factor $^{(1)}$ |  | Pipe <br> Stiffness |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | Ib in | $\mathrm{N} \bullet \mathrm{m}$ | psi | MPa <br> Beam Moment <br> of Inertia(2) |  |  |
| 2 | 50 | 340 | 38.4 | 1540 | 10.6 | $\mathrm{in}^{4}$ | $10^{6} \mathrm{~mm}^{4}$ |
| 3 | 80 | 340 | 38.4 | 460 | 3.2 | 1.61 | 0.20 |
| 4 | 100 | 820 | 92.6 | 530 | 3.7 | 4.7 | 1.96 |
| 6 | 150 | 820 | 92.6 | 160 | 1.1 | 15.5 | 6.40 |
| 8 | 200 | 1180 | 133.3 | 105 | 0.72 | 39 | 16.3 |
| 10 | 250 | 1180 | 133.3 | 53 | 0.37 | 77 | 32 |
| 12 | 300 | 1180 | 133.3 | 31 | 0.23 | 129 | 54 |
| 14 | 350 | 1330 | 150.2 | 36 | 0.25 | 209 | 88 |
| 16 | 400 | 2190 | 247.4 | 38 | 0.26 | 368 | 154 |

1) Per ASTM D2412.
2) Use these values to calculate permissible spans.

| Bending Radius | Nominal Pipe Size |  | Bending Radius ${ }^{1}$ <br> (R) |  | Maximum Allowable ${ }^{(2)}$ <br> (H) |  | Turning Angle |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | in | mm | $\mathrm{lb} \cdot \mathrm{in}$ | $\mathrm{N} \cdot \mathrm{m}$ | ft | m | a |
|  | 2 | 50 | 69.4 | 21 | 17.5 | 5.3 | 84 |
|  | 3 | 80 | 101.1 | 31 | 12.1 | 3.7 | 57 |
|  | 4 | 100 | 129.9 | 40 | 9.5 | 2.9 | 44 |
|  | 6 | 150 | 191.8 | 58 | 6.5 | 1.9 | 30 |
|  | 8 | 200 | 250 | 76 | 5.0 | 1.5 | 23 |
|  | 10 | 250 | 312 | 95 | 4.0 | 1.2 | 18 |
|  | 12 | 300 | 370 | 113 | 3.4 | 1.0 | 15 |
|  | 14 | 350 | 410 | 125 | 3.2 | 0.9 | 14 |
|  | 16 | 400 | 410 | 143 | 2.7 | 0.8 | 12 |

1) Do not bend pipe until adhesive has cured. At rated pressure sharper bends may create excessive stress concentrations.
2) For $100-\mathrm{ft}(30 \mathrm{~m})$ bending length, S

## Buried Installations

## Live loads

Bondstrand 5000/5000C will carry H20 wheel loadings of at least $16.000 \mathrm{lb}(7250 \mathrm{~kg})$ per axle when properly bedded in compacted sand in stable soils and provided with at least $3 \mathrm{ft}(1 \mathrm{~m})$ of cover.

## Thrust blocks

Most properly bedded installations do not require thrust blocks. Consult FGS for recommendations for systems operating at elevated temperatures.

| Nominal <br> Pipe Size | Maximum Earth Cover ${ }^{1}$ |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 100 psi | 0.69 MPa | 125 psi | 0.86 MPa | 150 psi | 1.03 MPa |  |
| in | mm | ft | m | ft | m | ft | m |
| 2 | 50 | 30 | 9.14 | 30 | 9.14 | 30 | 9.14 |
| 3 | 80 | 30 | 9.14 | 30 | 9.14 | 30 | 9.14 |
| 4 | 100 | 30 | 9.14 | 30 | 9.14 | 30 | 9.14 |
| 6 | 150 | 30 | 9.14 | 24 | 7.32 | 23 | 7.01 |
| 8 | 200 | 23 | 7.01 | 22 | 6.71 | 21 | 6.40 |
| 10 | 250 | 23 | 7.01 | 21 | 6.40 | 19 | 5.79 |
| 12 | 300 | 23 | 7.01 | 21 | 6.40 | 18 | 5.49 |
| 14 | 350 | 23 | 7.01 | 21 | 6.40 | 17 | 5.18 |
| 16 | 400 | 23 | 7.01 | 20 | 6.10 | 16 | 4.88 |

1) Based on a $1201 \mathrm{~b} / \mathrm{tt} 3(1925 \mathrm{~kg} / \mathrm{m} 3)$ soil density and $1000 \mathrm{psi}(6.9 \mathrm{MPa})$ modulus of soil reaction.

## Span Lengths

Recommended maximum support spacings for Bondstrand 5000/5000C vinyl ester pipe at various operating temperatures. Values based on 0.5 -inch ( 12 mm ) deflection at midspan for fluid specific gravity $=1.0$. For fully continuous spans, values may be increased up to $20 \%$. Decrease values by $20 \%$ for single spans.

| Nominal <br> Pipe Size |  | Spans (ft) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | $100^{\circ} \mathrm{F}$ | $140^{\circ} \mathrm{F}$ | $170^{\circ} \mathrm{F}$ | $200^{\circ} \mathrm{F}$ |
| 2 | 50 | 12.1 | 10.8 | 9.4 | 7.5 |
| 3 | 80 | 13.7 | 12.3 | 10.7 | 8.6 |
| 4 | 100 | 16.1 | 14.5 | 12.6 | 10.0 |
| 6 | 150 | 18.1 | 16.1 | 14.2 | 11.2 |
| 8 | 200 | 20.1 | 18.1 | 15.5 | 12.6 |
| 10 | 250 | 21.4 | 19.2 | 16.6 | 13.5 |
| 12 | 300 | 22.3 | 20.2 | 17.5 | 13.9 |
| 14 | 350 | 23.1 | 20.7 | 18.1 | 14.4 |
| 16 | 400 | 24.3 | 21.6 | 18.9 | 15.0 |

1) Span recommendations are intended for normal horizontal piping support arrangements, but include no provision for weights (fittings, valves, flanges, etc) or thrusts (branches, turns, etc.).
2) Span recommendations are calculated for a maximum long-term deflection of $1 / 2$ inch to ensure good appearance and adequate drainage.

Bondstrand 5000/5000C piping systems are designed for hydrostatic field testing at $150 \%$ of rated operating pressure. Pneumatic testing is not recommended.

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## Bondstrand ${ }^{\circledR}$ Guide Specification

Pipe Construction

The structural wall of fiberglass pipe in 2 through 16 inch sizes shall have continuous glass fibers wound at a $543 / 4$ helical angle in a matrix of premium vinyl ester resin.

The integral, reinforced resin-rich liner shall consist of Nexus veil and a resin-/hardener system identical to that of the structural wall, and shall have a 50-mil nominal thickness. Non-reinforced pure resin-type corrosion barriers (liners) shall not be allowed due to their potential for severe fracturing during transportation, installation and operation of the pipe.

Pipe in 2 through 16 inch sizes shall be rated for a minimum of 150 psig at $200^{\circ} \mathrm{F}$. In 2 through 8 inch sizes the pipe shall have full vacuum capability at $70^{\circ} \mathrm{F}$, when installed above ground with a safety factor of $3: 1$.

Pipe shall be manufactured according to ASTM D2996 specification for filamentwound Reinforced Thermosetting Resin Pipe (RTRP). When classified under ASTM ED2310, the pipe shall meet Type 1, Grade 2 and Class E (RTRP-12ED) cell limited in 2 through 16 inch nominal pipe sizes.

Filament-wound vinyl ester fiberglass pipe shall be gray.
Pipe in 2 through 8 inch sizes shall be furnished in 30 ft length to minimize the number of field-bonded joints for rapid installation.

## Standard Fittings

 ConstructionFittings in 2 through 16 inch sizes shall be filament wound with a reinforced resin-rich liner of equal or greater thickness than the pipe liner and of the same glass resin type as the pipe.

Compression-molded fittings in 2, 3, 4 and 6 inch nominal sizes may also be allowed upon agreement between purchaser and manufacturer.

Contact-molded, spray-up or hand lay-up fittings shall not be allowed. Pipe and Fittings shall be joined using a straight spigot by socket with a $0.5^{\circ}$ taper angle and a pipe stop inside the socket to allow precise makeup.

## Workmanship

The pipe and fittings shall be free from all defects, including delaminations, indentations, pinholes, foreign inclusions, bubbles and resin-starved areas which, due to their nature, degree or extent, detrimentally affect the strength and serviceability of the pipe or fittings. The pipe and fittings shall be as uniform as commercially practicable in color, density and other physical properties.

## Testing

Samples of pipe and couplings shall be tested at random, based on standard quality control practices to determine conformance of the materials to American Society for Testing of Materials guidelines for testing fiberglass pipe products: ASTM D1599, D2105, D2925, D2992A or D2992B.

Test samples may be hydrostatically tested by the manufacturer to 1.5 times the pressure rating for signs of leakage.

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# Bondstrand'" 7000 Antistatic Pipe Product Data <br> (For Industrial Service) 

Above ground jet fuel lines Double-contained jet fuel lines
General industrial service where static electrical charge build-up is possible or through hazardous areas (Class 1,Div. 1 and 2)

## Listings and Approvals

## Performance

## Composition

Pipe: Filament-wound fiberglass reinforced epoxy resin pipe with conductive filaments in the pipe wall.

Fittings: Wide range of filament-wound epoxy resin fittings reinforced with fiberglass strands and conductive veils employing Quick-Lock ${ }^{\circledR}$ adhesive joint or flanged ends.

Flanges: Filament-wound epoxy reinforced with fiberglass strands and conductive filaments.

Blind flanges: Injection molded non-conductive epoxy in 2 through 12-inch (50 to 300 mm ) sizes.

Grounding saddles: Filament-wound fiberglass with stainless steel grounding cable.

Adhesive: PSX•60 two-part thermosetting electrically conductive epoxy.

## Joining Systems

Quick-Lock straight/taper adhesive-bonded joint featuring integral pipe stop in bell for precise laying lengths.

One-piece flanges in hubbed (standard) and hubless (heavy duty) configuration. All pipe is shipped ready for assembly with Quick-Lock bell x shaved spigot.

Static Electricity Generation and Accumulation

Static electricity accumulation is most likely to be a problem in pipes conveying non conducting fluids at high velocities (less than 1000 pico-Siemens per meter). Measurable amounts of electricity can be generated in the fluid when the flow velocity exceeds $9 \mathrm{ft} /$ sec in fiberglass pipe and $20 \mathrm{ft} / \mathrm{sec}$ in metallic systems. Filtration units and valves typically experience the highest rate of static electricity accumulation when high flow rates occur. Charge densities are affected by the conductivity of the fluid,the pipe and the filter media. Depending on the media, flow through filters generally tends to give rise to charge densities 5 to 1000 times greater than flow through unrestricted pipes.

| Pipe Lengths | Bondstrand pipe is produced in different lengths depending on pipe size and location of manufacture. Pipe can be cut to specified lengths at the factory. Consult your FGS representative. | Nominal Pipe Size |  | Standard Length |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | in | mm | ft | m |
|  |  | 2-6 | 50-150 | 20-30 | 6-9 |
|  |  | 8 | 200 | 20-30 | 6-9 |
|  |  | 10-16 | 250-400 | 40 | 12 |

## Fittings and

Flanges
$90^{\circ}$ and $45^{\circ}$ elbows
Tees and reducing tees, reducers
Reducing saddles furnished with:

- Quick-Lock spigot outlet
- Flanged outlet
- Metallic bushing outlet


## $45^{\circ}$ laterals

## Crosses

Nipples and couplings
Flanges are produced with ANSI B16.5 Class 150 drilling. Other drill patterns as well as blank flanges are available.

Grounding saddles

## Typical Pipe Dimensions and Weight

| Nominal <br> Pipe Size |  | Pipe <br> Inside Diameter |  | Nominal Wall <br> Thickness |  | Shipping <br> Weight |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | in | mm | in | mm | $\mathrm{lb} / \mathrm{ft}$ | $\mathrm{kg} / \mathrm{m}$ |
| 2 | 50 | 2.09 | 53 | 0.16 | 4.1 | 1.0 | 1.5 |
| 3 | 80 | 3.22 | 82 | 0.16 | 4.1 | 1.5 | 2.3 |
| 4 | 100 | 4.14 | 105 | 0.20 | 5.2 | 2.4 | 3.5 |
| 6 | 150 | 6.26 | 159 | 0.20 | 5.2 | 3.5 | 5.2 |
| 8 | 200 | 8.22 | 209 | 0.25 | 6.5 | 5.0 | 7.4 |
| 10 | 250 | 10.35 | 263 | 0.32 | 8.1 | 6.2 | 9.3 |
| 12 | 300 | 12.35 | 314 | 0.38 | 9.6 | 7.4 | 11.0 |
| 14 | 350 | 13.56 | 344 | 0.41 | 10.5 | 8.7 | 14.7 |
| 16 | 400 | 15.50 | 394 | 0.47 | 11.9 | 11.2 | 19.0 |

Typical Pipe Performance

| Nominal <br> Pipe Size |  | Internal <br> Pressure Rating* |  | Ultimate <br> Collapse Pressure** |  | Designation <br> per ASTM D2996 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | psig | MPa | psig | MPa |  |
| 2 | 50 | 450 | 3.10 | 500 | 3.46 | RTRP-11FE-1112 |
| 3 | 80 | 425 | 2.93 | 400 | 2.76 | RTRP-11FE-1112 |
| 4 | 100 | 400 | 2.76 | 400 | 2.76 | RTRP-11FE-1113 |
| 6 | 150 | 300 | 2.07 | 163 | 1.12 | RTRP-11FE-1113 |
| 8 | 200 | 250 | 1.72 | 150 | 1.03 | RTRP-11FE-1114 |
| 10 | 250 | 200 | 1.38 | 150 | 1.03 | RTRP-11FE-1114 |
| 12 | 300 | 170 | 1.17 | 150 | 1.03 | RTRP-11FE-1114 |
| 14 | 350 | 165 | 1.14 | 150 | 1.03 | RTRP-11FE-1115 |
| 16 | 400 | 165 | 1.14 | 150 | 1.03 | RTRP-11FE-1116 |

[^22]Typical Mechanical Properties

| Typical Pipe Property | Units | $\begin{gathered} 70^{\circ} \mathrm{F} \\ \left(21^{\circ} \mathrm{C}\right) \end{gathered}$ | $\begin{aligned} & 200^{\circ} \mathrm{F} \\ & \left(93^{\circ} \mathrm{C}\right) \end{aligned}$ | ASTM <br> Method |
| :---: | :---: | :---: | :---: | :---: |
| Circumferential Tensile Stress at Weeping | $10^{3} \mathrm{psi}$ MPa | $\begin{gathered} 24.0 \\ 165.0 \end{gathered}$ |  | D1599 |
| Circumferential Tensile Modulus | $10^{6} \mathrm{psi}$ GPa | $\begin{aligned} & 3.65 \\ & 25.5 \end{aligned}$ | $\begin{aligned} & 3.20 \\ & 22.1 \end{aligned}$ |  |
| Circumferential Poisson's Ratio | - | 0.56 | 0.70 |  |
| Longitudinal Tensile Strength | $10^{3} \mathrm{psi}$ MPa | $\begin{aligned} & 8.50 \\ & 59.0 \end{aligned}$ | $\begin{aligned} & 6.90 \\ & 44.6 \end{aligned}$ | D2105 |
| Longitudinal Tensile Modulus | $10^{6} \mathrm{psi}$ GPa | $\begin{gathered} 1.6 \\ 11.0 \end{gathered}$ | $\begin{gathered} 1.24 \\ 8.5 \end{gathered}$ | D2105 |
| Longitudinal Poisson's Ratio | - | 0.37 | 0.41 |  |
| Hydrostatic Design Basis(cyclic) (at $150^{\circ} \mathrm{F}\left(66{ }^{\circ} \mathrm{C}\right)$ ) | $10^{3} \mathrm{psi}$ $\mathrm{MPa}$ | $\begin{gathered} 6.0 \\ 41.4 \end{gathered}$ |  | D2992(A) |
| Beam Apparent Elastic Modulus | $10^{6} \mathrm{psi}$ GPa | $\begin{gathered} 1.7 \\ 11.7 \end{gathered}$ | $\begin{aligned} & 1.0 \\ & 6.9 \end{aligned}$ | D2925 |
|  | Value |  |  |  |
| Flow Coefficient | Hazen Williams 150 |  |  |  |
| Thermal Conductivity Pipe Wall | BTU-in./(hr.ft. ${ }^{20}$ F) <br> W/M ${ }^{\circ} \mathrm{C}$ |  | $\begin{gathered} 2.3 \\ 0.33 \end{gathered}$ |  |
| Grounding Resistance at 1500 volts | $10^{6}$ ohms |  | 1.0 max. |  |
| Coefficient of Thermal Expansion,Linear | 10-6in./in. ${ }^{\circ}$ F $10-6 \mathrm{~mm} / \mathrm{mm} / 24^{\circ} \mathrm{C}$ |  | $\begin{aligned} & 10 \\ & 18 \end{aligned}$ | D696 |

${ }^{(1)}$ Based on structural wall thickness, at room temperature unless noted.
${ }^{(2)}$ The first subscript denotes the direction of applied stress
and the second that of measured contraction
$x$ denotes longitudinal direction.
y denotes circumferential direction.
${ }^{(3)}$ Test fixtures were end type (full end thrust on samples).
(4) Circumferentially loaded only.

Support Spacing

Recommended maximum support spacing for Bondstrand Series 7000 pipe at various operating temperatures. Values based on 0.5 inch ( 12 mm ) deflection at mid-span for fluid specific gravity $=1.0$.

| Nominal Pipe Size |  | Span in Feet ( m )* <br> Temperature in ${ }^{\circ} \mathrm{F}\left({ }^{\circ} \mathrm{C}\right)$ |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | 100 | (38) | 150 | (66) | 200 | (93) |
| 2 | 50 | 11.8 | 3.6 | 11.2 | 3.4 | 10.4 | 3.2 |
| 3 | 80 | 13.6 | 4.1 | 12.8 | 3.9 | 11.9 | 3.6 |
| 4 | 100 | 15.4 | 4.7 | 14.6 | 4.5 | 13.6 | 4.1 |
| 6 | 150 | 17.2 | 5.2 | 16.4 | 5.0 | 15.1 | 4.6 |
| 8 | 200 | 19.2 | 5.9 | 18.1 | 5.5 | 16.9 | 5.2 |
| 10 | 250 | 20.3 | 6.2 | 19.2 | 5.9 | 17.9 | 5.5 |
| 12 | 300 | 21.3 | 6.5 | 20.1 | 6.1 | 18.7 | 5.7 |
| 14 | 350 | 22.3 | 6.8 | 21.2 | 6.5 | 19.6 | 6.0 |
| 16 | 400 | 23.3 | 7.1 | 22.3 | 6.8 | 20.5 | 6.2 |

*Span recommendations are intended for normal horizontal piping support arrangements,a com
promise between continuous spans and simple spans, but include no provision for weight such as fittings, valves, flanges,etc. or thrust from branches and turns. Fully continuous spans may be installed with support spacing up to $20 \%$ greater than values shown for this deflection; for simple spans the support spacing should be reduced by $20 \%$ from tabulated values.

Typical Pipe Performance

| Nominal <br> Pipe Size |  | Stiffness <br> Factor* |  | Pipe <br> Stiffness |  | Beam Moment <br> of Inertia** |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | $\mathrm{lb} \cdot$ in | $\mathrm{N} \cdot \mathrm{m}$ | psi | MPa | $\mathrm{in}^{4}$ | $10^{6} \mathrm{~mm}^{4}$ |
| 2 | 50 | 620 | 70 | 2900 | 20.0 | 0.59 | 0.25 |
| 3 | 80 | 620 | 70 | 860 | 5.93 | 1.99 | 0.83 |
| 4 | 100 | 1360 | 154 | 890 | 6.14 | 5.50 | 2.29 |
| 6 | 150 | 1360 | 154 | 270 | 1.86 | 18.10 | 7.53 |
| 8 | 200 | 1890 | 214 | 170 | 1.17 | 45.10 | 18.80 |
| 10 | 250 | 1890 | 214 | 86 | 0.59 | 88.60 | 36.90 |
| 12 | 300 | 1890 | 214 | 51 | 0.35 | 149.00 | 62.00 |
| 14 | 350 | 2230 | 252 | 46 | 0.32 | 208.00 | 86.60 |
| 16 | 400 | 3250 | 367 | 45 | 0.31 | 353.00 | 147.00 |

* Per ASTM D2412
** Use these values to calculate permissible spans

Typical Physical Properties

| Typical Physical Properties |  |  |  |
| :---: | :---: | :---: | :---: |
| Pipe Property | Units | Value | ASTM |
| Thermal conductivity | $\begin{gathered} \mathrm{Btu}-\mathrm{in} /\left(\mathrm{h} \cdot \mathrm{ft}^{2} \cdot{ }^{\circ} \mathrm{F}\right) \\ \mathrm{W} / \mathrm{m} \cdot{ }^{\circ} \mathrm{C} \end{gathered}$ | $\begin{gathered} 2.3 \\ 0.33 \end{gathered}$ | FGS |
| $\begin{aligned} & \text { Coefficient of thermal } \\ & \text { expansion (linear) } \\ & (2-16 \text { inch) } \\ & 77^{\circ} \mathrm{F} \text { to } 150^{\circ} \mathrm{F} \\ & \left(25^{\circ} \mathrm{C} \text { to } 65^{\circ} \mathrm{C}\right) \end{aligned}$ | $\begin{gathered} 10^{-6} \mathrm{in} / \mathrm{in} /{ }^{\circ} \mathrm{F} \\ 10^{-6} \mathrm{~cm} / \mathrm{cm} /{ }^{\circ} \mathrm{C} \end{gathered}$ | $\begin{aligned} & 10.00 \\ & 18.00 \end{aligned}$ | FGS |
| Flow coefficient | Hazen-Williams | 150.00 | - |
| Absolute roughness | $\begin{aligned} & 10^{-6} \mathrm{ft} \\ & 10^{-6} \mathrm{~m} \end{aligned}$ | $\begin{gathered} 17.40 \\ 5.30 \end{gathered}$ | - |
| Specific gravity | - | 1.79 | D792 |
| Density | $\mathrm{lb} / \mathrm{in}^{3}$ | 0.07 |  |
| Grounding resistance <br> @ 1500 volts | $10^{6}$ ohms | 1.0* |  |
| Shielding capability | Volts | 100* |  |

*Maximum values when measured in accordance with Annexes 2 and 3 of proposed ASTM standard for marine antistatic pipe.

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## Bondstrand 7000 Specification Guide

This specification defines the reinforced thermosetting resin (RTR) piping system to be used in those services that may produce a dangerous build-up of static electrical charges. Such services include above-ground jet fuel lines, double contained jet fuel lines, and transmission of refined petroleum products, gases, or non-polar fluids at high velocities.

## References, <br> Quality Assurance

References are made to other standards and tests which are a part of this section as modified. Where conflict exists between the requirements of this specification and listed references, the specification shall prevail.

## Physical and <br> Mechanical Properties

| Typical Pipe Property | Units | $\begin{gathered} 70^{\circ} \mathrm{F} \\ \left(21^{\circ} \mathrm{C}\right) \end{gathered}$ | $\begin{aligned} & 200^{\circ} \mathrm{F} \\ & \left(93^{\circ} \mathrm{C}\right) \end{aligned}$ | ASTM Method |
| :---: | :---: | :---: | :---: | :---: |
| Circumferential Tensile Stress at Weeping | $10^{3} \mathrm{psi}$ MPa | $\begin{gathered} 24.0 \\ 165.0 \end{gathered}$ | - | D1599 |
| Circumferential Tensile Modulus | $10^{6} \mathrm{psi}$ GPa | $3.65$ | $\begin{aligned} & 3.20 \\ & 22.1 \end{aligned}$ |  |
| Circumferential Poisson's Ratio | - | 0.56 | 0.70 |  |
| Longitudinal Tensile Strength | $10^{3} \mathrm{psi}$ MPa | $\begin{aligned} & 8.50 \\ & 59.0 \end{aligned}$ | $\begin{aligned} & 6.90 \\ & 44.6 \end{aligned}$ | D2105 |
| Longitudinal Tensile Modulus | $10^{6} \mathrm{psi}$ GPa | $\begin{gathered} 1.6 \\ 11.0 \end{gathered}$ | $\begin{gathered} 1.24 \\ 8.5 \end{gathered}$ | D2105 |
| Longitudinal Poisson's Ratio | - | 0.37 | 0.41 |  |
| Hydrostatic Design Basis(cyclic) (at $150^{\circ} \mathrm{F}\left(66{ }^{\bullet} \mathrm{C}\right)$ ) | $10^{3} \mathrm{psi}$ MPa | $\begin{gathered} 6.0 \\ 41.4 \end{gathered}$ |  | D2992(A) |
| Beam Apparent Elastic Modulus | $10^{6} \mathrm{psi}$ GPa | $\begin{gathered} 1.7 \\ 11.7 \end{gathered}$ | $\begin{aligned} & 1.0 \\ & 6.9 \end{aligned}$ | D2925 |
|  | Value |  |  |  |
| Flow Coefficient | Hazen Williams 150 |  |  |  |
| Thermal Conductivity Pipe Wall | BTU-in./(hr.ft. ${ }^{20} \mathrm{~F}$ ) W/M ${ }^{\circ} \mathrm{C}$ |  | $\begin{gathered} 2.3 \\ 0.33 \end{gathered}$ |  |
| Grounding Resistance at 1500 volts | $10^{6}$ ohms |  | 1.0 max. |  |
| Coefficient of Thermal Expansion,Linear | 10-6in./in. ${ }^{\circ}$ F $10-6 \mathrm{~mm} / \mathrm{mm} / 24^{\circ} \mathrm{C}$ |  | $\begin{aligned} & 10 \\ & 18 \end{aligned}$ | D696 |

The pipe shall meet or exceed the requirements of MIL-P-29206A and ASTM 05677-95. Pipe dimensions must conform to Iron Pipe Size (IPS) outside diameters. In sizes 2" through 16" the piping must be rated for a minimum internal pressure rating of 165 psig at $200^{\circ} \mathrm{F}$. In $2^{\prime \prime}$ through 16 " sizes the pipe shall have full vacuum capabilities at $70^{\circ} \mathrm{F}$ when installed above ground.

Pipe shall be manufactured in accordance with ASTM 02996 Specifications for RTRP, with designations as follows:

| $2 ", 3 "$ | RTRP-11AE-1112 | $8 ", 10^{\prime \prime}, 12^{\prime \prime}$ | RTRP-11AE-1114 |
| :---: | :---: | :---: | :---: |
| $4 ", 6 "$ | RTRP-11AE-1113 | $14 "$ | RTRP-11AE-1115 |
|  |  | $16 "$ | RTRP-11AE-1116 |

## Materials

## Pipe Construction

The conductive filament wound fiberglass reinforced epoxy resin pipe shall be Bondstrand 7000 as manufactured by FGS Fiberglass Pipe Group or approved equal. The piping system will be made electrically continuous by using conductive filaments in the pipe wall,conductive adhesive in the bonded joints, and may be grounded by use of filament wound fiberglass saddles with stainless steel grounding cable. External or field installed techniques such as conductive wire or mesh, for achieving conductivity along the length of the pipe shall not be allowed.

## Structural wall

The pipe shall have the following nominal wall thickness:

Pipe end preparation options
The piping manufacturer will provide standard pipe joint lengths up to 30 feet RL in sizes 2 " through 8 " to reduce field labor assembly time The pipe manufacturer will prepare the bell end and the spigot end of each joint in the factory to reduce field labor assembly time.

| Nominal <br> Pipe Diameter | Nominal Wall <br> Thickness |  |
| :---: | :---: | :---: |
| in | in | mm |
| 2 | 0.16 | 4.1 |
| 3 | 0.16 | 4.1 |
| 4 | 0.20 | 5.2 |
| 6 | 0.20 | 5.2 |
| 8 | 0.25 | 6.3 |
| 10 | 0.32 | 8.1 |
| 12 | 0.38 | 9.6 |
| 14 | 0.41 | 10.4 |
| 16 | 0.47 | 11.9 |

## Fittings

It is important to maintain compatibility of fittings, piping and adhesives to ensure that the system performs as specified. Pipe, fittings and adhesive shall be supplied by the same manufacturer.

Fittings will be constructed with epoxy resin and conductive material, filament wound to specific dimensions. Flanges will be filament wound with epoxy resin and conductive filaments.

Spray up or hand lay-up fittings shall not be allowed.

## Testing

The RTRP manufacturer will provide test and repair procedures in the event field repairs are required. The installed piping shall be hydrostatically tested with water at $1 \frac{1}{2}$ times the design pressure of the lowest rated piping system component.

Hydrostatic and conductivity testing of buried systems will be completed prior to backfill.

## Installation

Installation procedures and techniques as well as system design criteria including burial, anchoring, guiding and supporting shall be in accordance with manufacturer's recommendations.

Piping system installers and fitters will be trained by a direct factory employee of the piping system manufacturer and certified by the trainer prior to system assembly in the field.

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## EPOXY FITTINGS NOMINAL DIMENSIONS

2"-16" Green Thread"' HP fittings are be used with both Green Thread HP and Red Thread"' HP piping. Refer to "Chemical Resistance Guide", Bulletin No. ENG5615, for chemical recommendations.

2"-16" Red Thread HP fittings may be used only on Red Thread HP piping.
$1 "-11 / 2$ " fittings are available in Green Thread HP products only. All fitting ratings are for $200^{\circ} \mathrm{F}\left(93^{\circ} \mathrm{C}\right)$. Red Thread fittings are serviceable up to $210^{\circ} \mathrm{F}\left(98.9^{\circ} \mathrm{C}\right)$ by applying a 0.92 de-rating factor. Green Thread fittings are serviceable up to $230^{\circ} \mathrm{F}\left(110^{\circ} \mathrm{C}\right)$ by applying a 0.76 de-rating factor.
$90^{\circ}$ ELBOWS ${ }^{(1)} 1 "-16 "$ parts are available in Green Thread HP only.


| Pipe Size | A | B | C | D | E <br> Bolt Hole Size | $\mathrm{O}^{(3)}$ | $\begin{gathered} \mathbf{X}^{(2)} \\ \mathbf{G T} \\ \text { Pipe } \end{gathered}$ | $\begin{gathered} \mathbf{X}^{(2)} \\ \mathbf{R T} \\ \text { Pipe } \end{gathered}$ | $\begin{aligned} & \text { Wt. } \\ & \text { BxB } \end{aligned}$ | $\begin{aligned} & \text { Wt. } \\ & \text { BxF } \end{aligned}$ | $\begin{aligned} & \text { Wt. } \\ & \text { FxF } \end{aligned}$ | Steady Pressure |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | in | in | in | in | in | in | in | in | lbs | lbs | lbs | psig |
| 1 | $23 / 4$ | $31 / 2$ | $3 / 4$ | $31 / 8$ | 5/8-4 holes | $41 / 4$ | 1 | - | 0.4 | 1.0 | 1.7 | 435 |
| 1 1/2 | $3 \mathrm{3} / 8$ | 4 | $3 / 4$ | 37/8 | 5/8-4 holes | 5 | $11 / 8$ | - | 0.6 | 1.5 | 2.4 | 435 |
| 2 | $33 / 8$ | $41 / 2$ | $3 / 4$ | $43 / 4$ | $3 / 4-4$ holes | 6 | $15 / 8$ | $15 / 8$ | 1.2 | 2.5 | 3.6 | 435 |
| 3 | $45 / 8$ | $51 / 2$ | $13 / 8$ | 6 | 3/4-4 holes | $71 / 2$ | $17 / 8$ | $13 / 4$ | 2.3 | 4.6 | 10.0 | 435 |
| 4 | $51 / 8$ | $61 / 2$ | $13 / 8$ | $71 / 2$ | $3 / 4-8$ holes | 9 | 2 | $15 / 8$ | 3.3 | 6.4 | 15.9 | 232 |
| 6 | $61 / 8$ | 8 | $11 / 2$ | $91 / 2$ | 7/8-8 holes | 11 | $21 / 4$ | $21 / 4$ | 7.2 | 11.8 | 15.9 | 232 |
| 8 | 11 5/8 | 9 | $13 / 4$ | $11^{3 / 4}$ | 7/8-8 holes | $131 / 2$ | 3 | $33 / 8$ | 10.9 | 15.4 | 19.9 | 232 |
| 10 | 13 | 11 | 2 | $141 / 4$ | 1-12 holes | 16 | $31 / 4$ | $31 / 2$ | 14.9 | 23.8 | 32.8 | 232 |
| 12 | 14 | 12 | $21 / 4$ | 17 | 1-12 holes | 19 | $33 / 8$ | $37 / 8$ | 22.6 | 38.3 | 54.0 | 232 |
| 14 | 19 | 14 | $21 / 2$ | $183 / 4$ | $11 / 8-12$ holes | $203 / 4$ | $53 / 8$ | $51 / 2$ | 26.5 | 45.0 | 65.0 | 232 |
| 16 | $201 / 4$ | 15 | $21 / 2$ | $211 / 4$ | 11/8-16 holes | $231 / 4$ | $51 / 2$ | $51 / 2$ | 45.0 | 65.0 | 108.0 | 232 |


| $\mathbf{m m}$ | $\mathbf{m m}$ | $\mathbf{m m}$ | $\mathbf{m m}$ | $\mathbf{m m}$ | $\mathbf{m m}$ | $\mathbf{m m}$ | $\mathbf{m m}$ | $\mathbf{m m}$ | $\mathbf{k g}$ | $\mathbf{k g}$ | $\mathbf{k g}$ | $\mathbf{b a r}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 25 | 70 | 89 | 19 | 79 | $16-4$ holes | 108 | 25 | - | 0.18 | 0.45 | 0.77 | 30 |
| 40 | 86 | 102 | 19 | 98 | $16-4$ holes | 127 | 29 | - | 0.27 | 0.68 | 1.09 | 30 |
| 50 | 86 | 114 | 19 | 121 | $19-4$ holes | 152 | 41 | 41 | 0.54 | 1.13 | 1.63 | 30 |
| 80 | 117 | 140 | 35 | 152 | $19-4$ holes | 190 | 48 | 44 | 1.04 | 2.09 | 4.54 | 30 |
| 100 | 130 | 165 | 35 | 190 | $19-8$ holes | 229 | 51 | 41 | 1.50 | 2.90 | 7.21 | 16 |
| 150 | 156 | 203 | 38 | 241 | $22-8$ holes | 279 | 57 | 57 | 3.27 | 5.35 | 7.21 | 16 |
| 200 | 295 | 229 | 44 | 298 | $22-8$ holes | 343 | 76 | 86 | 4.94 | 6.99 | 9.02 | 16 |
| 250 | 330 | 279 | 51 | 362 | $25-12$ holes | 406 | 83 | 89 | 6.76 | 10.80 | 14.88 | 16 |
| 300 | 356 | 305 | 57 | 432 | $25-12$ holes | 483 | 86 | 98 | 10.25 | 17.37 | 24.49 | 16 |
| 350 | 483 | 356 | 64 | 476 | $29-12$ holes | 527 | 137 | 140 | 12.02 | 20.41 | 29.48 | 16 |
| 400 | 514 | 381 | 64 | 540 | $29-16$ holes | 591 | 140 | 140 | 20.41 | 29.48 | 48.99 | 16 |

${ }^{(1)}$ "A" dimensions shown are for GREEN THREAD HP fittings. 1 " -6 " fittings are compression molded; 8 " -16 " fittings are filament wound. 1"-6" filament wound fittings are in Cl 1370.
${ }^{(2)}$ Nominal make-up dimension for drawing layout work only using non-threaded spigots. Do not use for assembly dimensions.
${ }^{(3)}$ Flanges should be joined to flat-faced flanges. When joining to raised-faced flange connections, consult installation or engineering manuals. Bolt torque, gasket thickness and hardness recommendations are in Manual INS6000


| Pipe Size | A | B | C | D | E <br> Bolt Hole Size | $\mathrm{O}^{(3)}$ | $\begin{gathered} \mathbf{X}^{(2)} \\ \mathbf{G T} \\ \text { Pipe } \end{gathered}$ | $\begin{aligned} & \mathrm{X}^{(2)} \\ & \mathrm{RT} \\ & \text { Pipe } \end{aligned}$ | $\begin{aligned} & \text { Wt. } \\ & \text { BxB } \end{aligned}$ | Wt. BxF | $\begin{aligned} & \text { Wt. } \\ & \text { FxF } \end{aligned}$ | Steady <br> Pressure |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in. | in. | in. | in. | in. | in. | in. | in. | in. | Ibs. | Ibs. | Ibs. | psig |
| 1 | $23 / 8$ | 2 | $3 / 4$ | $31 / 8$ | 5/8-4 holes | $41 / 4$ | 1 | - | 0.3 | 0.8 | 1.4 | 435 |
| $11 / 2$ | $27 / 8$ | $21 / 4$ | $3 / 4$ | $37 / 8$ | 5/8-4 holes | 5 | $11 / 8$ | - | 0.4 | 1.2 | 2.0 | 435 |
| 2 | $25 / 8$ | $21 / 2$ | $3 / 4$ | $43 / 4$ | $3 / 4-4$ holes | 6 | $15 / 8$ | $15 / 8$ | 0.9 | 1.9 | 2.8 | 435 |
| 3 | $33 / 4$ | 3 | $13 / 8$ | 6 | $3 / 4-4$ holes | $71 / 2$ | $17 / 8$ | $13 / 4$ | 1.6 | 3.5 | 7.9 | 435 |
| 4 | $37 / 8$ | 4 | $13 / 8$ | $71 / 2$ | $3 / 4-8$ holes | 9 | 2 | $15 / 8$ | 2.4 | 5.1 | 13.1 | 232 |
| 6 | $43 / 8$ | 5 | $11 / 2$ | $91 / 2$ | 7/8-8 holes | 11 | $21 / 4$ | $21 / 4$ | 4.8 | 8.4 | 12.5 | 232 |
| 8 | $81 / 8$ | $51 / 2$ | $13 / 4$ | $113 / 4$ | 7/8-8 holes | $131 / 2$ | 3 | $33 / 8$ | 6.9 | 11.9 | 16.8 | 232 |
| 10 | 8 5/8 | $61 / 2$ | 2 | $141 / 4$ | 1-12 holes | 16 | $31 / 4$ | $31 / 2$ | 8.9 | 18.5 | 28.2 | 232 |
| 12 | $91 / 2$ | $71 / 2$ | $21 / 4$ | 17 | 1-12 holes | 19 | $33 / 8$ | $37 / 8$ | 14.0 | 32.6 | 47.2 | 232 |
| 14 | $121 / 2$ | $71 / 2$ | $21 / 2$ | $183 / 4$ | $11 / 8-12$ holes | $203 / 4$ | $53 / 8$ | $51 / 2$ | 17.0 | 46.0 | 73.0 | 232 |
| 16 | $1311 / 4$ | 8 | $21 / 2$ | $211 / 4$ | $11 / 8-16$ holes | $231 / 4$ | $51 / 2$ | $51 / 2$ | 25.0 | 56.0 | 84.0 | 232 |


| $\mathbf{m m}$ | $\mathbf{m m}$ | $\mathbf{m m}$ | $\mathbf{m m}$ | $\mathbf{m m}$ | $\mathbf{m m}$ | $\mathbf{m m}$ | $\mathbf{m m}$ | $\mathbf{m m}$ | $\mathbf{k g}$ | $\mathbf{k g}$ | $\mathbf{k g}$ | $\mathbf{b a r}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 25 | 60 | 51 | 19 | 79 | $16-4$ holes | 108 | 25 | - | 0.14 | 0.36 | 0.64 | 30 |
| 40 | 73 | 57 | 19 | 98 | $16-4$ holes | 127 | 29 | - | 0.18 | 0.54 | 0.91 | 30 |
| 50 | 67 | 64 | 19 | 121 | $19-4$ holes | 152 | 41 | 41 | 0.41 | 0.86 | 1.27 | 30 |
| 80 | 95 | 76 | 35 | 152 | $19-4$ holes | 190 | 48 | 44 | 0.73 | 1.59 | 3.58 | 30 |
| 100 | 98 | 102 | 35 | 190 | $19-8$ holes | 229 | 51 | 41 | 1.09 | 2.31 | 5.94 | 16 |
| 150 | 111 | 127 | 38 | 241 | $22-8$ holes | 279 | 57 | 57 | 2.18 | 3.81 | 5.67 | 16 |
| 200 | 206 | 140 | 44 | 298 | $22-8$ holes | 343 | 76 | 86 | 3.11 | 5.40 | 7.62 | 16 |
| 250 | 219 | 165 | 51 | 362 | $25-12$ holes | 406 | 83 | 89 | 4.04 | 8.39 | 12.79 | 16 |
| 300 | 241 | 190 | 57 | 432 | $25-12$ holes | 483 | 86 | 98 | 6.35 | 14.78 | 21.41 | 16 |
| 350 | 318 | 191 | 64 | 476 | $29-12$ holes | 527 | 137 | 140 | 7.71 | 20.87 | 33.11 | 16 |
| 400 | 337 | 203 | 64 | 540 | $29-16$ holes | 591 | 140 | 140 | 11.3 | 25.40 | 38.10 | 16 |

(1) "A" dimensions shown are for GREEN THREAD HP fittings. 1 " -6 " fittings are compression molded; 8 "-16" fittings are filament wound. 1"-6" filament wound fittings are in Cl1370.
(2) Nominal make-up dimension for drawing layout work only using non-threaded spigots. Do not use for assembly dimensions.
(3) Flanges should be joined to flat-faced flanges. When joining to raised-faced flange connections, consult installation or engineering Manuals INS1000 \& ENG1000. Bolt torque, gasket thickness and hardness recommendations are in Manual INS1000.

TEES ${ }^{(1)} \mathbf{1 "}^{1 "}$-16" parts are available in Green Thread HP only.


| Pipe Size | A | B | C | D | E Bolt Hole Size | $\mathrm{O}^{(3)}$ | $\begin{gathered} \mathbf{X}^{(2)} \\ \text { GT } \\ \text { Pipe } \end{gathered}$ | $\begin{gathered} \mathbf{X}^{(2)} \\ \mathbf{R T} \\ \text { Pipe } \end{gathered}$ | $\begin{gathered} \text { Wt. } \\ \text { 3B } \end{gathered}$ | Wt. 1F | $\begin{aligned} & \text { Wt. } \\ & \text { 2F } \end{aligned}$ | $\begin{gathered} \text { Wt. } \\ \text { 3F } \end{gathered}$ | Steady Pressure |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in. | in. | in. | in. | in. | in. | in. | in. | in. | lbs. | lbs. | lbs. | lbs. | psig |
| 1 | $23 / 4$ | $31 / 2$ | $3 / 4$ | $31 / 8$ | 5/8-4 holes | $41 / 4$ | 1 | - | 0.5 | 1.1 | 1.8 | 2.5 | 435 |
| $11 / 2$ | $33 / 8$ | 4 | $3 / 4$ | $37 / 8$ | 5/8-4 holes | 5 | $11 / 8$ | - | 0.9 | 1.9 | 2.8 | 3.6 | 435 |
| 2 | $33 / 8$ | $41 / 2$ | $3 / 4$ | $43 / 4$ | $3 / 4-4$ holes | 6 | $15 / 8$ | $15 / 8$ | 1.9 | 3.1 | 4.8 | 5.5 | 435 |
| 3 | $45 / 8$ | $51 / 2$ | $13 / 8$ | 6 | $3 / 4-4$ holes | $71 / 2$ | $17 / 8$ | $13 / 4$ | 3.6 | 5.8 | 8.0 | 14.5 | 435 |
| 4 | $51 / 8$ | $61 / 2$ | $13 / 8$ | $71 / 2$ | $3 / 4-8$ holes | 9 | 2 | $15 / 8$ | 4.9 | 8.0 | 11.3 | 22.7 | 232 |
| 6 | $61 / 8$ | 8 | $11 / 2$ | $91 / 2$ | 7/8-8 holes | 11 | $21 / 4$ | $21 / 4$ | 10.1 | 14.3 | 19.0 | 22.3 | 232 |
| 8 | 11 5/8 | 9 | $13 / 4$ | $113 / 4$ | 7/8-8 holes | $131 / 2$ | 3 | $33 / 8$ | 16.1 | 20.4 | 24.6 | 28.9 | 232 |
| 10 | 13 | 11 | 2 | $141 / 4$ | 1-12 holes | 16 | $31 / 4$ | $31 / 2$ | 26.2 | 34.1 | 42.0 | 49.8 | 232 |
| 12 | 14 | 12 | $21 / 4$ | 17 | 1-12 holes | 19 | $33 / 8$ | $37 / 8$ | 31.8 | 47.1 | 62.5 | 77.8 | 232 |
| 14 | 19 | 14 | $21 / 2$ | $183 / 4$ | $11 / 8-12$ holes | $203 / 4$ | $53 / 8$ | $51 / 2$ | 52.0 | 75.5 | 99.5 | 127.0 | 232 |
| 16 | $201 / 4$ | 15 | $21 / 2$ | $211 / 4$ | $11 / 8$ - 16 holes | $231 / 4$ | $51 / 2$ | $51 / 2$ | 68.0 | 107.0 | 135.0 | 170.0 | 232 |


| $\mathbf{m m}$ | $\mathbf{m m}$ | $\mathbf{m m}$ | $\mathbf{m m}$ | $\mathbf{m m}$ | $\mathbf{m m}$ | $\mathbf{m m}$ | $\mathbf{m m}$ | $\mathbf{m m}$ | $\mathbf{k g}$ | $\mathbf{k g}$ | $\mathbf{k g}$ | $\mathbf{k g}$ | $\mathbf{b a r}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 25 | 70 | 89 | 19 | 79 | $16-4$ holes | 108 | 25 | - | 0.2 | 0.5 | 0.8 | 1.1 | 30 |
| 40 | 86 | 102 | 19 | 98 | $16-4$ holes | 127 | 29 | - | 0.4 | 0.9 | 1.3 | 1.6 | 30 |
| 50 | 86 | 114 | 19 | 121 | $19-4$ holes | 152 | 41 | 41 | 0.9 | 1.4 | 2.2 | 2.5 | 30 |
| 80 | 117 | 127 | 35 | 152 | $19-4$ holes | 190 | 48 | 44 | 1.6 | 2.6 | 3.6 | 6.6 | 30 |
| 100 | 130 | 165 | 35 | 190 | $19-8$ holes | 229 | 51 | 41 | 2.2 | 3.6 | 5.1 | 10.3 | 16 |
| 150 | 156 | 203 | 38 | 241 | $22-8$ holes | 279 | 57 | 57 | 4.6 | 6.5 | 8.6 | 10.1 | 16 |
| 200 | 295 | 229 | 44 | 298 | $22-8$ holes | 343 | 76 | 86 | 7.3 | 9.3 | 11.2 | 13.1 | 16 |
| 250 | 330 | 279 | 51 | 362 | $25-12$ holes | 406 | 83 | 89 | 11.9 | 15.5 | 19.1 | 22.6 | 16 |
| 300 | 356 | 305 | 57 | 432 | $25-12$ holes | 483 | 86 | 98 | 14.4 | 21.4 | 28.3 | 35.3 | 16 |
| 350 | 483 | 356 | 64 | 476 | $29-12$ holes | 527 | 137 | 140 | 23.6 | 34.2 | 45.1 | 57.6 | 16 |
| 400 | 514 | 381 | 64 | 540 | $29-16$ holes | 591 | 140 | 140 | 30.8 | 48.5 | 61.2 | 77.1 | 16 |

(1) "A" dimensions shown are for Green Thread HP fittings. 1"-6" fittings are compression molded; 8"-16" fittings are filament wound. 1"-6" filament wound fittings are in Cl 1370.
(2) Nominal make-up dimension for drawing layout work only using non-threaded spigots. Do not use for assembly dimensions.
(3) Flanges should be joined to flat-faced flanges. When joining to raised-faced flange connections, consult installation or engineering Manuals INS1000 \& ENG1000. Bolt torque, gasket thickness and hardness recommendations are in Manual INS1000.


FLANGES

| All flanges meet ANSI B16.5 Class 150 Bolt Hole Standards. The following flanges are available as standard parts: |  |  |
| :--- | :--- | :--- |
| Flanges: | $1 "-12^{\prime \prime}$ Green Thread HP | Compression Molded (M) or Filament Wound (FW) |
|  | $2^{\prime \prime}-6 " ~ R e d ~ T h r e a d ~ H P ~$ | Filament Wound (FW) |
|  | $14 "-16 "$ Red Thread or Green Thread HP | Filament Wound (FW) |
| Blind Flanges: | $1 "-12^{\prime \prime}$ Green Thread HP | Compression Molded (M) |
|  | $14 "-16 "$ Red Thread or Green Thread HP | Contact Molded (M) |


| Pipe Size | B | C | CC | D | E Bolt Hole Size | 0 | $\begin{gathered} \hline \mathbf{X}^{(1)} \text { for GT } \\ \text { Pipe } \end{gathered}$ |  | $\begin{gathered} \hline \mathbf{X}^{(1)} \text { for } R T \\ \text { Pipe } \\ \hline \end{gathered}$ |  | Bolt Torque ${ }^{(2)}$ |  | Weight Flange |  | Wt. Blind FIg. | Steady Pressure Rating |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  | M | FW | M | FW | Min. | Max. | M | FW |  | M | FW | Blind ${ }^{(3)}$ |
| in | in | in | in | in | in - no. |  | in | in | in | in | ft-lbs |  | Ibs | lbs | lbs | psig |  |  |
| 1 | $13 / 4$ | $3 / 4$ | $3 / 4$ | $31 / 8$ | 5/8-4 holes | $4^{1 / 4}$ | 1 | 1 | - | - | 20 | 25 | 0.6 | 0.6 | 0.8 | 435 | 435 | 300 |
| $1^{1 / 2}$ | $13 / 4$ | $3 / 4$ | $3 / 4$ | 37/8 | 5/8-4 holes | 5 | 1 | $1^{1 / 8}$ | - | - | 20 | 25 | 0.9 | 0.9 | 0.9 | 435 | 435 | 300 |
| 2 | $21 / 4$ | $3 / 4$ | $3 / 4$ | $4^{3 / 4}$ | $3 / 4-4$ holes | 6 | $15 / 8$ | $15 / 8$ | 1 5/8 | 1 5/8 | 25 | 30 | 1.3 | 1.3 | 1.3 | 435 | $435{ }^{(4)}$ | 300 |
| 3 | $25 / 8$ | $13 / 8$ | 1 | 6 | $3 / 4-4$ holes | $71 / 2$ | $1^{7 / 8}$ | $1^{7 / 8}$ | $13 / 4$ | $13 / 4$ | 25 | 30 | 2.6 | 3.4 | 3.0 | 435 | $300{ }^{(4)}$ | 300 |
| 4 | $25 / 8$ | $13 / 8$ | 1 | $71 / 2$ | $3 / 4-8$ holes | 9 | 2 | $2^{3 / 8}$ | $15 / 8$ | $15 / 8$ | 25 | 30 | 3.6 | 4.9 | 4.0 | 232 | $232{ }^{(4)}$ | 150 |
| 6 | 3 | $11 / 2$ | $1^{1 / 8}$ | $9^{1 / 2}$ | 7/8-8 holes | 11 | $21 / 2$ | $21 / 4$ | $21 / 4$ | $21 / 4$ | 25 | 30 | 4.4 | 6.5 | 6.6 | 232 | 232 ${ }^{4}$ | 150 |
| 8 | 4 | $1^{3 / 4}$ | $1^{1 / 8}$ | $11^{3 / 4}$ | 7/8-8 holes | $13^{1 / 2} 2$ | 23/8 | 2 $1 / 8$ | 27/8 | $25 / 8$ | 80 | 100 | 9.3 | 11.0 | 10.6 | 232 | 232 | 135 |
| 10 | $4^{3 / 4}$ | 2 | $1^{1 / 4}$ | $14^{1 / 4}$ | 1-12 holes | 16 | 37/8 | $31 / 8$ | $4^{1 / 8}$ | $33 / 8$ | 80 | 100 | 16.0 | 15.8 | 16.3 | 232 | 232 | 95 |
| 12 | 5 | $21 / 4$ | $11 / 4$ | 17 | 1-12 holes | 19 | 37/8 | 2 7 \% | 4 | $31 / 8$ | 80 | 100 | 24.0 | 25.8 | 24.0 | 232 | 232 | 65 |
| 14 | $31 / 8$ | $21 / 2$ | $1^{7 / 8}$ | $18^{3 / 4}$ | 11/8-12 holes | $20^{3 / 4}$ | - | 3 | - | 3 | 80 | 100 | - | 30.7 | 44.8 | - | 232 | 150 |
| 16 | $3^{1 / 8}$ | $2^{1 / 2}$ | $2^{1 / 4}$ | $21^{1 / 4}$ | 11/8-16 holes | $23^{1 / 4}$ | - | 3 | - | 3 | 80 | 100 | - | 37.0 | 67.3 | - | 232 | 150 |


| mm | mm | mm | mm | mm | mm | mm | mm ${ }^{(1)}$ | mm ${ }^{(1)}$ | $\mathrm{mm}^{(1)}$ | mm ${ }^{(1)}$ |  | $\mathrm{N}-\mathrm{m}^{(2)}$ | kg | kg | kg | bar | bar | bar |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 25 | 44 | 19 | 19 | 79 | $16 \mathrm{D}-4$ holes | 108 | 25 | 25 | - | - | 27 | 34 | 0.27 | 0.27 | 0.36 | 30 | 30 | 20.7 |
| 40 | 44 | 19 | 19 | 98 | $16 \mathrm{D}-4$ holes | 127 | 25 | 29 | - | - | 27 | 34 | 0.41 | 0.41 | 0.41 | 30 | 30 | 20.7 |
| 50 | 57 | 19 | 19 | 121 | 19D-4 holes | 152 | 41 | 41 | 41 | 41 | 34 | 41 | 0.59 | 0.59 | 0.59 | 30 | $30^{(4)}$ | 20.7 |
| 80 | 67 | 35 | 25 | 152 | 19D-4 holes | 191 | 48 | 48 | 44 | 44 | 34 | 41 | 1.18 | 1.54 | 1.36 | 30 | $21^{(4)}$ | 20.7 |
| 100 | 67 | 35 | 25 | 191 | 19D-8 holes | 229 | 51 | 60 | 41 | 41 | 34 | 41 | 1.63 | 2.22 | 1.81 | 16 | $16^{(4)}$ | 10.3 |
| 150 | 76 | 38 | 29 | 241 | $22 \mathrm{D}-8$ holes | 279 | 64 | 57 | 57 | 57 | 34 | 41 | 2.00 | 2.95 | 2.99 | 16 | $16^{(4)}$ | 10.3 |
| 200 | 102 | 44 | 29 | 298 | $22 \mathrm{D}-8$ holes | 343 | 60 | 54 | 73 | 67 | 41 | 135 | 4.22 | 4.99 | 4.81 | 16 | 16 | 9.3 |
| 250 | 121 | 51 | 32 | 362 | $25 \mathrm{D}-12$ holes | 406 | 98 | 79 | 105 | 86 | 108 | 135 | 7.26 | 7.17 | 7.39 | 16 | 16 | 6.5 |
| 300 | 127 | 57 | 32 | 432 | 25D-12 holes | 483 | 98 | 73 | 102 | 79 | 108 | 135 | 10.89 | 11.70 | 10.89 | 16 | 16 | 4.5 |
| 350 | 79 | 64 | 48 | 476 | $28 \mathrm{D}-12$ holes | 527 | - | 76 | - | 76 | 108 | 135 | - | 13.93 | 20.32 | - | 16 | 10.3 |
| 400 | 79 | 64 | 57 | 540 | $28 \mathrm{D}-16$ holes | 594 | - | 76 | - | 76 | 108 | 135 | - | 16.78 | 30.53 | - | 16 | 10.3 |


|  | 0 | $\subseteq$ | $\stackrel{ \pm}{\sim}$ | $\infty$ | $\underset{\infty}{\stackrel{N}{N}}$ | * |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\infty$ | ᄃ | $\infty$ | $\stackrel{ \pm}{ \pm}$ | $\stackrel{\text { ¢ }}{\text { ¢ }}$ | $\stackrel{ \pm}{+}$ |
|  | 免 | $\subseteq$ | $\sim$ | $\infty$ | * | $\bullet$ |


| ${ }^{(1)}$ Nominal make-up dimension for drawing layout work only using non-threaded spigots. Do not use for assembly dimension ${ }^{(2)}$ Flanges should be joined to flat-faced flanges. When joining to raised-faced flange connections, consult FGS installation or engineering Manuals INS1000 \& ENG1000. Bolt torque, gasket thickness and hardness recommendations are in Manual INS1000. | ${ }^{(3)}$ Steel back-up plates must be used to achieve pressure ratings equivalent to the pipe. | ${ }^{(4)}$ Heavy duty ANSI 16.5 Class 150 and 300 flanges rated to 450 psig ( 3.10 MPa ) are available. Dimensions are shown in the "Heavy Duty Flange Dimensions" table. The maximum bolt torque for $2 "-6$ " is 100 ft . lbs . |
| :---: | :---: | :---: |

ORIFICE FLANGES (2"-8" parts are available in Green Thread HP only)
Orifice Flange


Note: the 2" orifice flange has only one orifice

| Pipe Size | B | C | D | E <br> Bolt Hole Size | H | J | 0 | $\begin{aligned} & \mathbf{X}^{(1)} \\ & \mathbf{G T} \\ & \text { Pipe } \end{aligned}$ | $\begin{gathered} \mathbf{X}^{(1)} \\ \mathbf{R T} \\ \text { Pipe } \end{gathered}$ | Flange BoltTorque ${ }^{(2)}$ ft-lbs |  | Wt. | Steady <br> Pressure |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | in | in | in | in | in | in | in | in | in | To Seal | Max. | Ibs | psig |
| 2 | $41 / 4$ | 2 | $43 / 4$ | 3/4-4 holes | 1/2 NPT | 1 | 6 | $15 / 8$ | 1 5/8 | 25 | 30 | 3.6 | 435 |
| 3 | 5 | 2 | 6 | 3/4-4 holes | 1⁄2 NPT | 1 | $71 / 2$ | $17 / 8$ | $13 / 8$ | 25 | 30 | 5.3 | 435 |
| 4 | 5 | 2 | $71 / 2$ | 3/4-8 holes | 1⁄2 NPT | 1 | 9 | $15 / 8$ | 2 | 25 | 30 | 6.6 | 232 |
| 6 | 6 | 2 | $91 / 2$ | 7/8-8 holes | 1⁄2 NPT | 1 | 11 | $21 / 4$ | $21 / 4$ | 25 | 30 | 8.8 | 232 |
| 8 | $83 / 4$ | 2 | $113 / 4$ | 7/8-8 holes | $1 / 2$ NPT | 1 | $131 / 2$ | $31 / 8$ | $31 / 2$ | 30 | 100 | 14.5 | 232 |


| $\mathbf{m m}$ | $\mathbf{m m}$ | $\mathbf{m m}$ | $\mathbf{m m}$ | $\mathbf{m m}$ | $\mathbf{m m}$ | $\mathbf{m m}$ | $\mathbf{m m}$ | $\mathbf{m m}^{(1)}$ | $\mathbf{m m}^{(1)}$ | $\mathbf{N}-\mathbf{m}^{(2)}$ | $\mathbf{N}-\mathbf{m}^{(2)}$ | $\mathbf{k g}$ | $\mathbf{b a r}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 50 | 108 | 51 | 121 | $19-4$ holes | 12.7 NPT | 25 | 152 | 41 | 41 | 34 | 41 | 1.6 | 30 |
| 80 | 127 | 51 | 152 | $19-4$ holes | 12.7 NPT | 25 | 191 | 48 | 35 | 34 | 41 | 2.4 | 30 |
| 100 | 127 | 51 | 191 | $19-8$ holes | 12.7 NPT | 25 | 229 | 41 | 51 | 34 | 41 | 3.0 | 16 |
| 150 | 152 | 51 | 241 | $22-8$ holes | 12.7 NPT | 25 | 279 | 57 | 57 | 34 | 41 | 4.0 | 16 |
| 200 | 222 | 51 | 298 | $22-8$ holes | 12.7 NPT | 25 | 343 | 79 | 89 | 41 | 135 | 6.6 | 16 |

${ }^{(1)}$ Nominal make-up dimension for drawing layout work only using non-threaded spigots.
Do not use for assembly dimensions.
${ }^{(2)}$ Flanges should be joined to flat-faced flanges. When joining to raised-faced flange connections, consult installation or engineering Manuals INS1000 \& ENG1000. Gasket thickness and hardness recommendations are in Manual INS1000.

## STUB ENDS



| Nominal <br> Pipe Size | Pressure <br> Rating | Bolt <br> Torque | A | B | D | X | Wgt. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | psi | ft-lb | in | in | in | in | Ibs. |
| 2 | 250 | 66 | 2.75 | 0.27 | 3.91 | 2.13 | 0.5 |
| 3 | 200 | 66 | 2.88 | 0.28 | 5.16 | 2.26 | 0.7 |
| 4 | 150 | 66 | 2.88 | 0.28 | 6.66 | 2.10 | 1.0 |
| 6 | 150 | 111 | 3.88 | 0.39 | 8.53 | 3.69 | 2.4 |


| $\mathbf{m m}$ | bar | kg-mm | $\mathbf{m m}$ | $\mathbf{m m}$ | $\mathbf{m m}$ | $\mathbf{m m}$ | $\mathbf{k g}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 50 | 17 | 98 | 70 | 7 | 99 | 54 | 0.22 |
| 80 | 14 | 98 | 73 | 7 | 131 | 57 | 0.31 |
| 100 | 10 | 98 | 73 | 7 | 169 | 53 | 0.45 |
| 150 | 10 | 165 | 99 | 10 | 217 | 94 | 1.08 |

FLANGE RINGS

| ANSI B16.5 Class 150 | Nominal Pipe Size | A | B | E | Bolt Hole Size | No. of Holes | Wgt. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | in | in | in | in | in | \# | lbs. |
|  | 2 | 2.78 | 0.82 | 6.00 | $3 / 4$ | 4 | 1.10 |
|  | 3 | 3.90 | 1.10 | 7.50 | $3 / 4$ | 4 | 2.10 |
|  | 4 | 4.90 | 1.10 | 9.00 | $3 / 4$ | 8 | 2.90 |
|  | 6 | 7.26 | 1.25 | 11.00 | 7/8 | 8 | 3.80 |
|  | mm | mm | mm | mm | mm | \# | kg |
|  | 50 | 71 | 21 | 152 | 19 | 4 | 0.50 |
|  | 70 | 99 | 28 | 191 | 19 | 4 | 0.95 |
|  | 100 | 124 | 28 | 229 | 19 | 8 | 1.32 |
|  | 150 | 184 | 32 | 279 | 22 | 8 | 1.73 |

## NIPPLES

GT - Green Thread HP
RT - Red Thread HP
$\boxtimes$ - Standard Available Size


| Size | Close |  | 4" |  | 6" |  | 8" |  | 10" |  | 12" |  | 16" |  | 24" |  | 36" |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| In. | GT | RT | GT | RT | GT | RT | GT | RT | GT | RT | GT | RT | GT | RT | GT | RT | GT | RT |
| 1 | $21 / 2$ | - | - | - | X | - | X | - | - | - | - | - | - | - | - | - | - | - |
| $11 / 2$ | $31 / 8$ | - | - | - | X | - | X | - | - | - | - | - | - | - | - | - | - | - |
| 2 | $41 / 2$ | X | - | $\mathrm{X}^{3}$ | X | X | X | X | - | X | - | X | - | - | - | - | - | - |
| 3 | $51 / 8$ | $51 / 8$ | - | - | X | $\mathrm{X}^{4}$ | X | X | - | X | - | X | - | - | - | - | - | - |
| 4 | $53 / 8$ | $53 / 8$ | - | - | X | X | X | X | - | X | - | X | - | - | - | - | - | - |
| 6 | $61 / 8$ | $61 / 8$ | - | - | $X^{(4)}$ | $X^{(5)}$ | X | X | - | X | X | X | - | - | - | - | - | - |
| 8 | 8 5/8 | $93 / 8$ | - | - | - | - | - | - | - | - | X | X | X | X | - | X | - | - |
| 10 | $93 / 8$ | $93 / 8$ | - | - | - | - | - | - | - | - | X | X | X | X | - | X | - | X |
| 12 | $93 / 8$ | $101 / 4$ | - | - | - | - | - | - | - | - | X | X | X | X | - | X | - | X |
| 14 | - | X | - | - | - | - | - | - | - | - | - | - | X | X | - | X | - | X |
| 16 | - | - | - | - | - | - | - | - | - | - | - | - | X | X | - | X | - | $\square$ |

## SLEEVE COUPLINGS

Green Thread HP Couplings

| Pipe Size | A | B | $\mathbf{X}^{(1)}$ | Wt. | Steady Pressure |
| :---: | :---: | :---: | :---: | :---: | :---: |
| in. | in. | in. | in. | lbs. | psig |
| 1 | $23 / 4$ | $11 / 2$ | 1 | 0.1 | 435 |
| $11 / 2$ | $31 / 4$ | 2 | $11 / 8$ | 0.1 | 435 |
| 2 | $47 / 8$ | $25 / 8$ | $15 / 8$ | 0.4 | 435 |
| 3 | 5 | $33 / 4$ | 2 | 0.8 | 435 |
| 4 | 5 | $43 / 4$ | 2 | 0.9 | 232 |
| 6 | 7 | $67 / 8$ | $21 / 4$ | 1.9 | 232 |
| 8 | 10 | 9 | $31 / 8$ | 3.4 | 232 |
| 10 | 10 1/2 | 11 | $31 / 8$ | 5.2 | 232 |
| 12 | 11 | $131 / 8$ | $31 / 4$ | 7.5 | 232 |
| 14 | $121 / 2$ | 15 | $37 / 8$ | 11.2 | 232 |
| 16 | 13 | $171 / 8$ | $41 / 8$ | 16.0 | 232 |
| mm | mm | mm | mm ${ }^{(1)}$ | kg | bar |
| 25 | 70 | 38 | 25 | 0.05 | 30 |
| 40 | 83 | 52 | 29 | 0.05 | 30 |
| 50 | 124 | 67 | 41 | 0.18 | 30 |
| 80 | 127 | 95 | 51 | 0.36 | 30 |
| 100 | 127 | 121 | 51 | 0.41 | 16 |
| 150 | 178 | 175 | 57 | 0.86 | 16 |
| 200 | 254 | 229 | 79 | 1.54 | 16 |
| 250 | 268 | 279 | 79 | 2.36 | 16 |
| 300 | 279 | 333 | 83 | 3.40 | 16 |
| 350 | 318 | 381 | 98 | 5.08 | 16 |
| 400 | 330 | 435 | 105 | 7.26 | 16 |

${ }^{(3)}$ Actual length $41 / 4$
${ }^{(4)}$ Actual length $61 / 4 /$
${ }^{(5)}$ Actual length $61 / 8^{\prime \prime}$

## Red Thread HP Couplings

| Pipe <br> Size | A | B | $\mathbf{X}^{(1)}$ | Wt. | Steady Pressure |
| :---: | :---: | :---: | :---: | :---: | :---: |
| in. | in. | in. | in. | lbs. | psig |
| 1 | - | - | - | - | - |
| $11 / 2$ | - | - | - | - | - |
| 2 | 6 | $25 / 8$ | $15 / 8$ | 0.4 | 435 |
| 3 | 6 | $33 / 4$ | $17 / 8$ | 0.8 | 435 |
| 4 | 7 | $47 / 8$ | 2 | 1.4 | 435 |
| 6 | $83 / 8$ | $71 / 8$ | $23 / 4$ | 2.8 | 435 |
| 8 | 10 | 9 | $27 / 8$ | 3.3 | 232 |
| 10 | 10 1/2 | $111 / 8$ | $33 / 8$ | 4.7 | 232 |
| 12 | 11 | $131 / 8$ | $31 / 2$ | 6.8 | 232 |
| 14 | $121 / 2$ | 15 | 4 | 11.2 | 232 |
| 16 | 13 | $171 / 8$ | $41 / 8$ | 16.0 | 232 |


| $\mathbf{m m}$ | $\mathbf{m m}$ | $\mathbf{m m}$ | $\mathbf{m m}^{(1)}$ | $\mathbf{k g}$ | bar |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 25 | - | - | - | - | - |
| 40 | - | - | - | - | - |
| 50 | 152 | 67 | 41 | 0.18 | 30 |
| 80 | 152 | 95 | 48 | 0.36 | 30 |
| 100 | 178 | 124 | 51 | 0.64 | 30 |
| 150 | 213 | 181 | 70 | 1.27 | 30 |
| 200 | 254 | 229 | 73 | 1.50 | 16 |
| 250 | 268 | 283 | 86 | 2.13 | 16 |
| 300 | 279 | 333 | 89 | 3.08 | 16 |
| 350 | 318 | 381 | 102 | 5.08 | 16 |
| 400 | 330 | 435 | 105 | 7.26 | 16 |

ADAPTERS - 1 " and $11 / 2$ " parts are available in Green Thread only; 2 "- 8 " parts are available in Green Thread or Red Thread HP

| Bell X Male |  |  | $\square$ | $-x$ | ${ }^{(1)}$ Nominal make-up dimension for drawing layout work only using non-threaded spigots. Do not use for assembly dimensions. |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | NPT Thread |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Pipe Size | A | B | $\begin{aligned} & \mathbf{X}^{(1)} \\ & \mathbf{G T} \\ & \text { Pipe } \end{aligned}$ | $\begin{gathered} \mathbf{X}^{(1)} \\ \text { RT } \\ \text { Pipe } \end{gathered}$ | Wt. GT | Wg. RT | Steady Pressure | Pipe Size | A | B | $\begin{gathered} \mathbf{X}^{(1)} \\ \mathbf{G T} \\ \text { Pipe } \end{gathered}$ | $\begin{gathered} \mathbf{X}^{(1)} \\ \mathrm{RT} \\ \text { Pipe } \end{gathered}$ | Wt. GT | Wt. RT | Steady Pressure |
| in. | in. | in. | in. | in. | Ibs. | lbs. | psig | mm | mm | mm | mm | mm | kg | kg | bar |
| 1 | $31 / 2$ | 1 | 1 | - | 0.1 | - | 435 | 25 | 89 | 25 | 25 | - | 0.05 | - | 30 |
| $11 / 2$ | $33 / 4$ | $11 / 2$ | $11 / 8$ | - | 0.3 | - | 435 | 40 | 99 | 38 | 29 | - | 0.14 | - | 30 |
| 2 | $41 / 4$ | 2 | $15 / 8$ | $13 / 8$ | 0.4 | 0.3 | 435 | 50 | 108 | 51 | 41 | 35 | 0.18 | 0.14 | 30 |
| 3 | $51 / 2$ | 3 | $17 / 8$ | $13 / 8$ | 0.9 | 0.6 | 300 | 80 | 140 | 76 | 48 | 35 | 0.41 | 0.27 | 20.7 |
| 4 | $51 / 2$ | 4 | 2 | $15 / 8$ | 1.6 | 1.0 | 232 | 100 | 140 | 102 | 51 | 41 | 0.73 | 0.45 | 16 |
| 6 | 6 | 6 | $21 / 4$ | $21 / 4$ | 2.6 | 1.8 | 232 | 150 | 152 | 152 | 57 | 57 | 1.18 | 0.82 | 16 |
| 8 | $91 / 4$ | 8 | $31 / 8$ | $31 / 2$ | 7.2 | 6.6 | 232 | 200 | 235 | 203 | 79 | 89 | 3.27 | 2.99 | 16 |



| Pipe Size | A | B | $\begin{aligned} & \mathbf{X}^{(1)} \\ & \text { GT } \\ & \text { Pipe } \\ & \hline \end{aligned}$ | $\begin{gathered} \mathbf{X}^{(1)} \\ \mathbf{R T} \\ \text { Pipe } \\ \hline \end{gathered}$ | Wt. GT | Wt. RT | Steady Pressure | Pipe Size | A | B | $\begin{gathered} \mathbf{X}^{(1)} \\ \mathbf{G T} \\ \text { Pipe } \end{gathered}$ | $\begin{gathered} \mathbf{X}^{(1)} \\ \mathrm{RT} \\ \text { Pipe } \end{gathered}$ | Wt. GT | Wt. RT | Steady <br> Pressure |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in. | in. | in. | in. | in. | lbs. | Ibs. | psig | mm | mm | mm | mm | mm | kg | kg | bar |
| 1 | $25 / 8$ | 1 | - | - | 0.1 | - | 435 | 25 | 67 | 25 | - | - | 0.05 | - | 30 |
| $11 / 2$ | $23 / 4$ | $11 / 4$ | - | - | 0.3 | - | 435 | 40 | 70 | 38 | - | - | 0.14 | - | 30 |
| 2 | $35 / 8$ | 2 | - | - | 0.4 | 0.3 | 435 | 50 | 92 | 51 | - | - | 0.18 | 0.1 | 30 |
| 3 | $45 / 8$ | 3 | - | - | 0.9 | 0.6 | 300 | 80 | 117 | 76 | - | - | 0.41 | 0.2 | 20.7 |
| 4 | $47 / 8$ | 4 | - | - | 1.1 | 1.0 | 232 | 100 | 124 | 102 | - | - | 0.50 | 0.4 | 16 |
| 6 | $67 / 8$ | 6 | - | - | 2.6 | 2.0 | 232 | 150 | 175 | 152 | - | - | 1.18 | 0.9 | 16 |
| 8 | 8 | 8 | - | - | 5.6 | 4.9 | 232 | 200 | 203 | 203 | - | - | 2.54 | 2.2 | 16 |



| Pipe Size | A | B | $\begin{aligned} & \mathbf{X}^{(1)} \\ & \text { GT } \\ & \text { Pipe } \end{aligned}$ | $\begin{gathered} \mathbf{X}^{(1)} \\ \mathbf{R T} \\ \text { Pipe } \end{gathered}$ | Wt. GT | Wgt. RT | Steady Pressure | Pipe Size | A | B | $\begin{gathered} \mathbf{X}^{(1)} \\ \mathbf{G T} \\ \text { Pipe } \end{gathered}$ | $\begin{gathered} \mathbf{X}^{(1)} \\ \mathrm{RT} \\ \text { Pipe } \end{gathered}$ | Wt. GT | Wt. RT | Steady Pressure |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in. | in. | in. | in. | in. | lbs. | lbs. | psig | mm | mm | mm | mm | mm | kg | kg | bar |
| 1 | $25 / 8$ | - | 1 | - | 0.1 | - | 435 | 25 | 67 | - | 25 | - | 0.05 | - | 30 |
| $11 / 2$ | $23 / 4$ | - | $11 / 8$ | - | 0.3 | - | 435 | 40 | 70 | - | 29 | - | 0.14 | - | 30 |
| 2 | $31 / 2$ | - | $15 / 8$ | $13 / 8$ | 0.6 | 0.3 | 435 | 50 | 89 | - | 41 | 35 | 0.27 | 0.1 | 30 |
| 3 | $41 / 2$ | - | $17 / 8$ | $13 / 8$ | 0.6 | 0.5 | 300 | 80 | 114 | - | 48 | 35 | 0.27 | 0.2 | 20.7 |
| 4 | $41 / 2$ | - | 2 | $15 / 8$ | 0.6 | 0.5 | 232 | 100 | 114 | - | 51 | 41 | 0.27 | 0.2 | 16 |
| 6 | $51 / 2$ | - | $21 / 4$ | $21 / 4$ | 1.9 | 1.3 | 232 | 150 | 140 | - | 57 | 57 | 0.86 | 0.6 | 16 |
| 8 | 7 | - | $31 / 8$ | $31 / 2$ | 5.1 | 3.5 | 150 | 200 | 178 | - | 79 | 89 | 2.31 | 1.6 | 10.3 |

ADAPTERS - 1 " and $11 / 2^{\prime \prime}$ parts are available in Green Thread only; 2"-8" parts are available in Green Thread or Red Thread HP; 10" and 12" are available in Red Thread HP.

## Spigot X Female



| Pipe | A | B | $\begin{aligned} & \mathbf{X}^{(1)} \\ & \text { GT } \\ & \text { Pipe } \end{aligned}$ | $\begin{gathered} \mathbf{X}^{(1)} \\ \mathrm{RT} \\ \text { Pipe } \end{gathered}$ | Wt. GT | $\begin{aligned} & \text { Wt. } \\ & \text { RT } \end{aligned}$ | Steady Pressure | $\begin{aligned} & \text { Pipe } \\ & \text { Size } \end{aligned}$ | A | B | $\begin{gathered} \mathbf{X}^{(1)} \\ \mathbf{G T} \\ \text { Pipe } \end{gathered}$ | $\begin{gathered} \mathbf{X}^{(1)} \\ \mathrm{RT} \\ \text { Pipe } \end{gathered}$ | $\begin{aligned} & \text { Wt. } \\ & \text { GT } \end{aligned}$ | Wt. RT | Steady Pressure |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in. | in. | in. | in. | in. | lbs. | lbs. | psig | mm | mm | mm | mm | mm | kg | kg | bar |
| 1 | 3 5/8 | 1 | - | - | 0.2 | - | 435 | 25 | 92 | 25 | - | - | 0.09 | - | 30 |
| $11 / 2$ | 4 | $11 / 2$ | - | - | 0.3 | - | 435 | 40 | 102 | 38 | - | - | 0.14 | - | 30 |
| 2 | $37 / 8$ | 2 | - | - | 0.4 | 0.3 | 435 | 50 | 98 | 51 | - | - | 0.18 | 0.14 | 30 |
| 3 | $43 / 4$ | $31 / 8$ | - | - | 0.8 | 0.5 | 290 | 80 | 121 | 76 | - | - | 0.36 | 0.23 | 20.7 |
| 4 | $47 / 8$ | $41 / 8$ | - | - | 1.0 | . 6 | 232 | 100 | 124 | 102 | - | - | 0.45 | 0.27 | 16 |
| 6 | $63 / 4$ | 6 | - | - | 3.4 | 2.6 | 232 | 150 | 171 | 152 | - | - | 1.54 | 1.18 | 16 |
| 8 | 10 | 8 | - | - | 8.0 | 7.1 | 150 | 200 | 254 | 203 | - | - | 3.63 | 3.22 | 10 |



| Pipe Size | A | B | $\begin{aligned} & \mathbf{X}^{(1)} \\ & \text { GT } \\ & \text { Pipe } \end{aligned}$ | $\begin{gathered} \hline \mathbf{X}^{(1)} \\ \mathbf{R T} \\ \text { Pipe } \end{gathered}$ | Wt. GT | Wt. RT | Steady Pressure | Pipe Size | A | B | $\begin{gathered} \mathbf{X}^{(1)} \\ \mathbf{G T} \\ \text { Pipe } \end{gathered}$ | $\begin{gathered} \mathbf{X}^{(1)} \\ \mathbf{R T} \\ \text { Pipe } \end{gathered}$ | Wt. GT | Wt. RT | Steady <br> Pressure |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in. | in. | in. | in. | in. | Ibs. | Ibs. | psig | mm | mm | mm | mm | mm | kg | kg | bar |
| 1 | $31 / 2$ | 7/8 | 1 | - | 0.3 | - | 435 | 25 | 89 | 22 | 25 | - | 0.14 | - | 30 |
| $11 / 2$ | $37 / 8$ | 11/2 | $11 / 8$ | - | 0.5 | - | 435 | 40 | 98 | 38 | 29 | - | 0.23 | - | 30 |
| 2 | $41 / 4$ | 2 | $15 / 8$ | $13 / 8$ | 0.5 | 0.3 | 435 | 50 | 108 | 51 | 41 | 35 | 0.23 | 0.14 | 30 |
| 3 | 5 | 3 | $17 / 8$ | $13 / 8$ | 0.9 | 0.6 | 290 | 80 | 127 | 76 | 48 | 35 | 0.41 | 0.27 | 20.7 |
| 4 | 5 | 4 | 2 | $15 / 8$ | 1.0 | 0.8 | 232 | 100 | 127 | 102 | 51 | 41 | 0.45 | 0.63 | 16 |
| 6 | $55 / 8$ | 6 | $21 / 4$ | $21 / 4$ | 2.3 | 1.8 | 232 | 150 | 143 | 152 | 57 | 57 | 1.04 | 0.84 | 16 |
| 8 | $81 / 4$ | 8 | $31 / 8$ | $31 / 2$ | 5.8 | 4.9 | 232 | 200 | 210 | 203 | 79 | 89 | 2.63 | 2.22 | 16 |
| 10 | $81 / 4$ | $10^{1 / 8}$ | - | $33 / 4$ | - | 6.3 | 190 | 250 | 210 | 257 | - | 95 | - | 2.86 | 13.1 |



| Pipe Size | A | B | $\begin{gathered} \mathbf{X}^{(1)} \\ \mathbf{G T} \\ \text { Pipe } \\ \hline \end{gathered}$ | $\begin{gathered} \mathbf{X}^{(1)} \\ \mathbf{R T} \\ \text { Pipe } \\ \hline \end{gathered}$ | Wt. GT | Wt. RT | Steady Pressure | Pipe Size | A | B | $\begin{gathered} \mathbf{X}^{(1)} \\ \mathbf{G T} \\ \text { Pipe } \\ \hline \end{gathered}$ | $\begin{gathered} \mathbf{X}^{(1)} \\ \mathbf{R T} \\ \text { Pipe } \\ \hline \end{gathered}$ | Wt. GT | Wg. RT | Steady Pressure |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in. | in. | in. | in. | in. | Ibs. | Ibs. | psig | mm | mm | mm | mm | mm | kg | kg | bar |
| 1 | $23 / 4$ | 7/8 | - | - | 0.1 | - | 435 | 25 | 70 | 22 | - | - | 0.05 | - | 30 |
| $11 / 2$ | $31 / 8$ | $11 / 2$ | - | - | 0.2 | - | 435 | 40 | 79 | 38 | - | - | 0.09 | - | 30 |
| 2 | $35 / 8$ | 2 | - | - | 0.3 | 0.3 | 435 | 50 | 92 | 51 | - | - | 0.14 | 0.14 | 30 |
| 3 | $41 / 4$ | 3 | - | - | 0.9 | 0.6 | 290 | 80 | 127 | 76 | - | - | 0.41 | 0.27 | 20 |
| 4 | $41 / 2$ | 4 | - | - | 1.0 | 0.9 | 232 | 100 | 114 | 102 | - | - | 0.45 | 0.41 | 16 |
| 6 | 5 | 6 | - | - | 2.6 | 2.0 | 232 | 150 | 127 | 152 | - | - | 1.18 | 0.91 | 16 |
| 8 | 7 | 8 | - | - | 4.4 | 4.1 | 232 | 200 | 178 | 203 | - | - | 2.00 | 1.86 | 16 |
| 10 | 7 | 10 1/8 | - | - | - | 5.6 | 190 | 250 | 178 | 257 | - | - | - | 2.54 | 13.1 |
| 12 | 7 | 12 | - | - | - | 6.8 | 150 | 300 | 178 | 305 | - | - | - | 3.08 | 10.3 |

[^23]Bell $x$ Bell


| Pipe Size | A | $\begin{aligned} & \text { X }_{1}{ }^{(1)} \\ & \text { GT } \\ & \text { Pipe } \end{aligned}$ | $\begin{aligned} & \mathbf{X}_{2}{ }^{(1)} \\ & \mathbf{G T} \\ & \text { Pipe } \end{aligned}$ | $\begin{aligned} & \mathrm{X}_{1}{ }^{(1)} \\ & \mathrm{RT} \\ & \text { Pipe } \end{aligned}$ | $\begin{aligned} & \mathbf{X}_{2}{ }^{(1)} \\ & \mathbf{R T}^{1} \\ & \text { Pipe } \end{aligned}$ | Wt. | Steady Pressure | Pipe Size | A | $\begin{aligned} & \mathbf{X}^{(1)} \\ & \mathbf{G T} \\ & \text { Pipe } \end{aligned}$ | $\begin{aligned} & \mathrm{X}_{2}{ }^{(1)} \\ & \mathrm{GT} \\ & \text { Pipe } \end{aligned}$ | $\begin{aligned} & \mathrm{X}^{(1)} \\ & \mathrm{RT} \\ & \text { Pipe } \end{aligned}$ | $\begin{aligned} & \mathrm{X}^{(1)} \\ & \mathrm{RT} \\ & \text { Pipe } \end{aligned}$ | Wt. | Steady Pressure |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in. | in. | in. | in. | in. | in. | Ibs. | psig | mm | mm | mm | mm | mm | mm | kg | bar |
| 2x1 | $51 / 2$ | $15 / 8$ | 1 | $15 / 8$ | NA | 0.6 | 435 | 50x25 | 140 | 41 | 25 | 41 | NA | 0.27 | 30 |
| 2x1 $1 / 2$ | 5 | $15 / 8$ | $11 / 8$ | $15 / 8$ | NA | 0.6 | 435 | 50x40 | 127 | 41 | 29 | 41 | NA | 0.27 | 30 |
| $3 \times 1$ | $61 / 4$ | $17 / 8$ | 1 | $17 / 8$ | NA | 1.0 | 435 | 80X25 | 159 | 48 | 25 | 48 | NA | 0.45 | 30 |
| $3 \times 11 / 2$ | $61 / 4$ | $17 / 8$ | $11 / 8$ | $13 / 4$ | NA | 1.1 | 435 | 80x40 | 159 | 48 | 29 | 44 | NA | 0.50 | 30 |
| $3 \times 2$ | 6 | 17/8 | $11 / 8$ | $17 / 8$ | 15/8 | 1.1 | 435 | 80x50 | 152 | 48 | 29 | 48 | 41 | 0.50 | 30 |
| 4X1 1/2 | $73 / 8$ | 2 | $11 / 8$ | $15 / 8$ | NA | 1.8 | 232 | 100X40 | 187 | 51 | 29 | 41 | NA | 0.82 | 16 |
| $4 \times 2$ | 81/4 | 2 | 1 5/8 | $15 / 8$ | 1 5/8 | 2.0 | 232 | 100x50 | 210 | 51 | 41 | 41 | 41 | 0.91 | 16 |
| 4x3 | 7 | 2 | $17 / 8$ | $15 / 8$ | $17 / 8$ | 1.7 | 232 | 100x80 | 178 | 51 | 48 | 41 | 48 | 0.77 | 16 |
| 6x3 | 10 \%/8 | $27 / 8$ | $17 / 8$ | $27 / 8$ | $17 / 8$ | 4.3 | 232 | 150x80 | 276 | 73 | 48 | 73 | 48 | 1.95 | 16 |
| 6x4 | 9 | $21 / 4$ | 2 | $21 / 4$ | 1 5/8 | 3.4 | 232 | 150x100 | 229 | 57 | 51 | 57 | 41 | 1.54 | 16 |
| $8 \times 4$ | 14 | 3 | 2 | $33 / 8$ | $15 / 8$ | 6.7 | 232 | 200x100 | 356 | 76 | 51 | 86 | 41 | 3.04 | 16 |
| $8 \times 6$ | $151 / 4$ | 3 | $27 / 8$ | $33 / 8$ | $27 / 8$ | 7.3 | 232 | 200x150 | 387 | 76 | 73 | 86 | 73 | 3.31 | 16 |
| 10x6 | $151 / 4$ | $31 / 4$ | $27 / 8$ | $31 / 2$ | $25 / 8$ | 10.5 | 232 | 250x150 | 387 | 83 | 73 | 89 | 67 | 4.76 | 16 |
| 10x8 | $161 / 2$ | $31 / 4$ | 3 | $31 / 2$ | $33 / 8$ | 11.1 | 232 | 250x200 | 419 | 83 | 76 | 89 | 86 | 5.03 | 16 |
| 12x8 | $183 / 8$ | 3 3/8 | 3 | $37 / 8$ | $33 / 8$ | 17.0 | 232 | 300x200 | 467 | 86 | 76 | 98 | 86 | 7.71 | 16 |
| 12x10 | $173 / 4$ | $33 / 8$ | $31 / 4$ | $37 / 8$ | $31 / 2$ | 16.4 | 232 | $300 \times 250$ | 451 | 86 | 83 | 98 | 89 | 7.44 | 16 |
| 14×10 | 22 7/8 | $53 / 8$ | $31 / 4$ | $51 / 2$ | $31 / 2$ | 21.9 | 232 | $350 \times 250$ | 581 | 137 | 83 | 140 | 89 | 9.93 | 16 |
| 14x12 | $22^{3 / 4}$ | $53 / 8$ | $33 / 8$ | $51 / 2$ | $37 / 8$ | 21.8 | 232 | 350x300 | 578 | 137 | 86 | 140 | 98 | 9.89 | 16 |
| 16x12 | 25 | $51 / 2$ | $33 / 8$ | $51 / 2$ | $37 / 8$ | 27.7 | 232 | 400x300 | 635 | 140 | 86 | 140 | 98 | 12.56 | 16 |
| 16x14 | 28 | $71 / 4$ | 7 | $71 / 4$ | 7 | 31.1 | 232 | $400 \times 350$ | 711 | 184 | 178 | 184 | 178 | 14.11 | 16 |

NOTE: MULTI-STEP reducers are available through 16" sizes. Information is available on request.
${ }^{(1)}$ Nominal make-up dimension for drawing layout work only using non-threaded spigots. Do not use for assembly dimensions.
${ }^{(2)}$ Flanges should be joined to flat-faced flanges. When joining to raised-faced flange connections, consult installation or engineering manuals. Bolt torque, gasket thickness and hardness recommendations are in manual INS1000.
These comments also apply to the flanged concentric reducers on the following page.

## Flanged ${ }^{(2)}$



| Pipe Size | B | C | D | E <br> Bolt Hole Size | 0 | G | H | Bolt Hole Size | P | Wt. | Steady Pressure |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in. | in. | in. | in. | in. | in. | in. | in. | in. | in. | Ibs. | psig |
| $2 \times 1$ | 5 | $3 / 4$ | $43 / 4$ | $3 / 4-4$ holes | 6 | $3 / 4$ | $37 / 8$ | 5/8-4 holes | $41 / 4$ | 2.6 | 300 |
| $2 \times 11 / 2$ | 5 | $3 / 4$ | $43 / 4$ | $3 / 4-4$ holes | 6 | $3 / 4$ | $37 / 8$ | 5/8-4 holes | 5 | 2.6 | 300 |
| $3 \times 11 / 2$ | 6 | $13 / 8$ | 6 | $3 / 4-4$ holes | $71 / 2$ | $3 / 4$ | $43 / 4$ | $3 / 4-4$ holes | 5 | 4.4 | 190 |
| $3 \times 2$ | 6 | $13 / 8$ | 6 | $3 / 4-4$ holes | $71 / 2$ | $3 / 4$ | $43 / 4$ | $3 / 4-4$ holes | 6 | 4.4 | 190 |
| $4 \times 2$ | 7 | $13 / 8$ | $71 / 2$ | $3 / 4-8$ holes | 9 | $13 / 8$ | 6 | $3 / 4-4$ holes | 6 | 7.1 | 150 |
| $4 \times 3$ | 7 | $13 / 8$ | $71 / 2$ | $3 / 4-8$ holes | 9 | $13 / 8$ | 6 | $3 / 4-4$ holes | $71 / 2$ | 7.1 | 150 |
| 6x3 | 9 | $11 / 2$ | $91 / 2$ | 7/8-8 holes | 11 | $13 / 8$ | $71 / 2$ | $3 / 4-8$ holes | $71 / 2$ | 11.0 | 150 |
| $6 \times 4$ | 9 | $11 / 2$ | $91 / 2$ | 7/8-8 holes | 11 | $13 / 8$ | $71 / 2$ | $3 / 4-8$ holes | 9 | 11.0 | 150 |
| $8 \times 4$ | 11 | $13 / 4$ | $113 / 4$ | 7/8-8 holes | $131 / 2$ | $11 / 2$ | $91 / 2$ | 7/8-8 holes | 9 | 17.6 | 232 |
| $8 \times 6$ | 11 | $13 / 4$ | $113 / 4$ | 7/8-8 holes | $131 / 2$ | $11 / 2$ | $91 / 2$ | 7/8-8 holes | 11 | 17.6 | 232 |
| 10x6 | 12 | 2 | $141 / 4$ | 1-12 holes | 16 | $13 / 4$ | $113 / 4$ | 7/8-8 holes | 11 | 28.2 | 232 |
| 10x8 | 12 | 2 | $141 / 4$ | 1-12 holes | 16 | $13 / 4$ | $113 / 4$ | 7/8-8 holes | $131 / 2$ | 28.2 | 232 |
| 12x8 | 14 | $21 / 4$ | 17 | 1-12 holes | 19 | 2 | $141 / 4$ | 1-12 holes | $131 / 2$ | 43.0 | 232 |
| $12 \times 10$ | 14 | $21 / 4$ | 17 | 1-12 holes | 19 | 2 | $141 / 4$ | 1-12 holes | 16 | 43.0 | 232 |
| $14 \times 10$ | 16 | $21 / 2$ | $183 / 4$ | $11 / 8-12$ holes | $203 / 4$ | $21 / 4$ | 17 | 1-12 holes | 16 | 55.0 | 232 |
| $14 \times 12$ | 16 | $21 / 2$ | $183 / 4$ | $11 / 8-12$ holes | $20^{3 / 4}$ | $21 / 4$ | 17 | 1-12 holes | 19 | 55.0 | 232 |
| 16x12 | 18 | $21 / 2$ | $211 / 4$ | $11 / 8-16$ holes | $231 / 4$ | $21 / 2$ | $183 / 4$ | $11 / 8-12$ holes | 19 | 89.5 | 232 |
| 16x14 | 18 | $21 / 2$ | $211 / 4$ | $11 / 8-16$ holes | $231 / 4$ | $21 / 2$ | $183 / 4$ | 11/8-12 holes | $203 / 4$ | 89.5 | 232 |


| $\mathbf{m m}$ | $\mathbf{m m}$ | $\mathbf{m m}$ | $\mathbf{m m}$ | $\mathbf{m m}$ | $\mathbf{m m}$ | $\mathbf{m m}$ | $\mathbf{m m}$ | $\mathbf{m m}$ | $\mathbf{m m}$ | $\mathbf{k g}$ | $\mathbf{b a r}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $50 \times 25$ | 127 | 19 | 121 | $19-4$ holes | 152 | 19 | 98 | $16-4$ holes | 108 | 1.18 | 20.7 |
| $50 \times 40$ | 127 | 19 | 121 | $19-4$ holes | 152 | 19 | 98 | $16-4$ holes | 127 | 1.18 | 20.7 |
| $80 \times 40$ | 152 | 35 | 152 | $19-4$ holes | 191 | 19 | 121 | $19-4$ holes | 127 | 2.00 | 13.1 |
| $80 \times 50$ | 152 | 35 | 152 | $19-4$ holes | 191 | 19 | 121 | $19-4$ holes | 152 | 2.00 | 13.1 |
| $100 \times 50$ | 178 | 35 | 191 | $19-8$ holes | 229 | 35 | 152 | $19-4$ holes | 152 | 3.22 | 10.3 |
| $100 \times 80$ | 178 | 35 | 191 | $19-8$ holes | 229 | 35 | 152 | $19-4$ holes | 191 | 3.22 | 10.3 |
| $150 \times 80$ | 229 | 38 | 241 | $22-8$ holes | 279 | 35 | 191 | $19-8$ holes | 191 | 4.99 | 10.3 |
| $150 \times 100$ | 229 | 38 | 241 | $22-8$ holes | 279 | 35 | 191 | $19-8$ holes | 229 | 4.99 | 10.3 |
| $200 \times 100$ | 279 | 44 | 298 | $22-8$ holes | 343 | 38 | 241 | $22-8$ holes | 229 | 7.98 | 16 |
| $200 \times 150$ | 279 | 44 | 298 | $22-8$ holes | 343 | 38 | 241 | $22-8$ holes | 279 | 7.98 | 16 |
| $250 \times 150$ | 305 | 51 | 362 | $25-12$ holes | 406 | 44 | 298 | $22-8$ holes | 279 | 12.79 | 16 |
| $250 \times 200$ | 305 | 51 | 362 | $25-12$ holes | 406 | 44 | 298 | $22-8$ holes | 343 | 12.79 | 16 |
| $300 \times 200$ | 356 | 57 | 432 | $25-12$ holes | 483 | 51 | 362 | $25-12$ holes | 343 | 19.50 | 16 |
| $300 \times 250$ | 356 | 57 | 432 | $25-12$ holes | 483 | 51 | 362 | $25-12$ holes | 406 | 19.50 | 16 |
| $350 \times 250$ | 406 | 64 | 476 | $29-12$ holes | 527 | 57 | 432 | $25-12$ holes | 406 | 24.95 | 16 |
| $350 \times 300$ | 406 | 64 | 476 | $29-12$ holes | 527 | 57 | 432 | $25-12$ holes | 483 | 24.95 | 16 |
| $400 \times 305$ | 457 | 64 | 540 | $29-16$ holes | 591 | 64 | 476 | $29-12$ holes | 483 | 40.60 | 16 |
| $406 \times 350$ | 457 | 64 | 540 | $29-16$ holes | 591 | 64 | 476 | $29-12$ holes | 527 | 40.60 | 16 |



## Bell x Bell

| Pipe <br> Size | A | $\begin{gathered} \mathrm{X}_{1}{ }^{(1)} \\ \mathrm{GT} \\ \text { Pipe } \\ \hline \end{gathered}$ | $\begin{aligned} & \mathbf{X}^{(1)} \\ & \mathbf{G T}^{1} \\ & \text { Pipe } \end{aligned}$ | $\begin{aligned} & \mathrm{X}_{1}{ }^{11} \\ & \mathrm{RT} \\ & \text { Pipe } \end{aligned}$ | $\begin{gathered} \mathbf{X}^{(1)} \\ \mathbf{R T}^{(1)} \\ \text { Pipe } \\ \hline \end{gathered}$ | Wt. | Steady Pressure | Pipe | A | $\begin{aligned} & X^{(1)} \\ & \text { GT } \\ & \text { Pipe } \end{aligned}$ | $\begin{array}{\|l} \hline \mathbf{X}^{(1)} \\ \mathbf{G T} \\ \text { Pipe } \\ \hline \end{array}$ | $\begin{gathered} \mathrm{X}^{(1)} \\ \mathrm{RT} \\ \text { Pipe } \\ \hline \end{gathered}$ | $\begin{aligned} & \mathrm{X}^{(1)} \\ & \mathrm{RT}^{(1)} \\ & \text { Pipe } \\ & \hline \end{aligned}$ | Wt. | Steady Pressure |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in. | in. | in. | in. | in. | in. | Ibs. | psig | mm | mm | mm | mm | mm | mm | kg | bar |
| 2x1 | $51 / 2$ | 1 5/8 | 1 | 1 5/8 | NA | 0.6 | 435 | 50x25 | 140 | 41 | 25 | 41 | NA | 0.27 | 30 |
| 2x11/2 | $51 / 2$ | $15 / 8$ | $11 / 8$ | $15 / 8$ | NA | 0.6 | 435 | 50x40 | 140 | 41 | 29 | 41 | NA | 0.27 | 30 |
| $3 \times 1$ | $61 / 4$ | $17 / 8$ | 1 | $17 / 8$ | NA | 1.0 | 435 | 80X25 | 159 | 48 | 25 | 48 | NA | 0.45 | 30 |
| $3 \times 11 / 2$ | $61 / 4$ | $17 / 8$ | $11 / 8$ | $13 / 4$ | NA | 1.1 | 435 | 80x40 | 159 | 48 | 29 | 44 | NA | 0.50 | 30 |
| 3x2 | $71 / 8$ | 17/8 | $11 / 8$ | $17 / 8$ | 15/8 | 1.1 | 435 | 80x50 | 181 | 48 | 29 | 48 | 41 | 0.50 | 30 |
| $4 \times 11 / 2$ | $73 / 8$ | 2 | $11 / 8$ | $15 / 8$ | NA | 1.8 | 232 | 100×40 | 187 | 51 | 29 | 41 | NA | 0.82 | 16 |
| $4 \times 2$ | 81/4 | 2 | $15 / 8$ | $15 / 8$ | $15 / 8$ | 2.0 | 232 | 100x50 | 210 | 51 | 41 | 41 | 41 | 0.91 | 16 |
| 4x3 | 8 | 2 | $17 / 8$ | $15 / 8$ | $17 / 8$ | 1.7 | 232 | 100x80 | 203 | 51 | 48 | 41 | 48 | 0.77 | 16 |
| 6x3 | $107 / 8$ | $27 / 8$ | $17 / 8$ | $27 / 8$ | $17 / 8$ | 4.3 | 232 | 150x80 | 276 | 73 | 48 | 73 | 48 | 1.95 | 16 |
| 6x4 | $103 / 4$ | $21 / 4$ | 2 | $21 / 4$ | $15 / 8$ | 3.4 | 232 | 150x100 | 273 | 57 | 51 | 57 | 41 | 1.54 | 16 |
| $8 \times 4$ | 14 | 3 | 2 | $33 / 8$ | $15 / 8$ | 6.7 | 232 | 200x100 | 356 | 76 | 51 | 86 | 41 | 3.04 | 16 |
| 8x6 | $15^{1 / 4}$ | 3 | $27 / 8$ | $33 / 8$ | $27 / 8$ | 7.3 | 232 | 200x150 | 387 | 76 | 73 | 86 | 73 | 3.31 | 16 |
| 10x6 | $151 / 4$ | $31 / 4$ | $27 / 8$ | $31 / 2$ | 2 5/8 | 10.5 | 232 | 250x150 | 387 | 83 | 73 | 89 | 67 | 4.76 | 16 |
| 10x8 | $161 / 2$ | $31 / 4$ | 3 | $31 / 2$ | $33 / 8$ | 11.1 | 232 | 250x200 | 419 | 83 | 76 | 89 | 86 | 5.03 | 16 |
| 12x8 | 18 3/8 | 3 3/8 | 3 | $37 / 8$ | $33 / 8$ | 17.0 | 232 | 300x200 | 467 | 86 | 76 | 98 | 86 | 7.71 | 16 |
| 12x10 | $173 / 4$ | $33 / 8$ | $31 / 4$ | $37 / 8$ | $31 / 2$ | 16.4 | 232 | $300 \times 250$ | 451 | 86 | 83 | 98 | 89 | 7.44 | 16 |
| 14×10 | $227 / 8$ | $53 / 8$ | $31 / 4$ | $51 / 2$ | $31 / 2$ | 21.9 | 232 | 350x250 | 581 | 137 | 83 | 140 | 89 | 9.93 | 16 |
| 14x12 | $223 / 4$ | $53 / 8$ | $33 / 8$ | $51 / 2$ | $37 / 8$ | 21.8 | 232 | 350x300 | 578 | 137 | 86 | 140 | 98 | 9.89 | 16 |
| 16x12 | 25 | $51 / 2$ | $33 / 8$ | $51 / 2$ | $37 / 8$ | 27.7 | 232 | $400 \times 300$ | 635 | 140 | 86 | 140 | 98 | 12.56 | 16 |
| 16x14 | 28 | $71 / 4$ | 7 | $71 / 4$ | 7 | 31.1 | 232 | $400 \times 350$ | 711 | 184 | 178 | 184 | 178 | 14.11 | 16 |

NOTE: MULTI-STEP reducers are available through 16" sizes. Information is available on request.
${ }^{(1)}$ Nominal make-up dimension for drawing layout work only using non-threaded spigots. Do not use for assembly dimensions.
${ }^{(2)}$ Flanges should be joined to flat-faced flanges. When joining to raised-faced flange connections, consult installation or engineering manuals. Bolt torque, gasket thickness and hardness recommendations are in manual INS1000.
These comments also apply to the flanged concentric reducers on the following page.

ECCENTRIC REDUCERS (1"-16" parts are available in Green Thread HP only.)

Flanged ${ }^{(2)}$

| Pipe Size | B | C | D | E <br> Bolt Hole Size | 0 | G | H | Bolt Hole Size | P | Wt. | Steady Pressure |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in. | in. | in. | in. | in. | in. | in. | in. | in. | in. | Ibs. | psig |
| 2x1 | 5 | $3 / 4$ | $43 / 4$ | $3 / 4-4$ holes | 6 | $3 / 4$ | $37 / 8$ | 5/8-4 holes | $411 / 4$ | 2.6 | 300 |
| $2 \times 11 / 2$ | 5 | $3 / 4$ | $43 / 4$ | $3 / 4-4$ holes | 6 | $3 / 4$ | $37 / 8$ | 5/8-4 holes | 5 | 2.6 | 300 |
| $3 \times 1$ | 6 | $13 / 8$ | 6 | $3 / 4-4$ holes | $71 / 2$ | $3 / 4$ | $43 / 4$ | $3 / 4-4$ holes | 5 | 4.4 | 190 |
| $3 \times 11 / 2$ | 6 | $13 / 8$ | 6 | $3 / 4-4$ holes | $71 / 2$ | $3 / 4$ | $43 / 4$ | $3 / 4-4$ holes | 5 | 4.4 | 190 |
| $3 \times 2$ | 6 | $13 / 8$ | 6 | $3 / 4-4$ holes | $71 / 2$ | $3 / 4$ | $43 / 4$ | $3 / 4-4$ holes | 6 | 4.4 | 190 |
| $4 \times 11 / 2$ | 7 | $13 / 8$ | $71 / 2$ | $3 / 4-8$ holes | 9 | $13 / 8$ | 6 | $3 / 4-4$ holes | 6 | 7.1 | 150 |
| $4 \times 2$ | 7 | $13 / 8$ | $71 / 2$ | $3 / 4-8$ holes | 9 | $13 / 8$ | 6 | $3 / 4-4$ holes | 6 | 7.1 | 150 |
| $4 \times 3$ | 7 | $13 / 8$ | $71 / 2$ | $3 / 4-8$ holes | 9 | $13 / 8$ | 6 | $3 / 4-4$ holes | $71 / 2$ | 7.1 | 150 |
| 6x3 | 9 | $11 / 2$ | $911 / 2$ | 7/8-8 holes | 11 | $13 / 8$ | $71 / 2$ | $3 / 4-8$ holes | $71 / 2$ | 11.0 | 150 |
| 6x4 | 9 | $11 / 2$ | $911 / 2$ | 7/8-8 holes | 11 | $13 / 8$ | $71 / 2$ | $3 / 4-8$ holes | 9 | 11.0 | 150 |
| $8 \times 4$ | 11 | $13 / 4$ | $11^{3 / 4}$ | 7/8-8 holes | $131 / 2$ | $11 / 2$ | $91 / 2$ | 7/8-8 holes | 9 | 17.6 | 232 |
| $8 \times 6$ | 11 | $13 / 4$ | $11^{3 / 4}$ | 7/8-8 holes | $131 / 2$ | $11 / 2$ | $91 / 2$ | 7/8-8 holes | 11 | 17.6 | 232 |
| 10x6 | 12 | 2 | $141 / 4$ | 1-12 holes | 16 | $13 / 4$ | $11^{3 / 4}$ | 7/8-8 holes | 11 | 28.2 | 232 |
| 10x8 | 12 | 2 | $141 / 4$ | 1-12 holes | 16 | $13 / 4$ | $113 / 4$ | 7/8-8 holes | $131 / 2$ | 28.2 | 232 |
| 12x8 | 14 | $21 / 4$ | 17 | 1-12 holes | 19 | 2 | $141 / 4$ | 1-12 holes | $131 / 2$ | 43.0 | 232 |
| $12 \times 10$ | 14 | $21 / 4$ | 17 | 1-12 holes | 19 | 2 | $141 / 4$ | 1-12 holes | 16 | 43.0 | 232 |
| 14×10 | 16 | $21 / 2$ | 18 3/4 | $11 / 8-12$ holes | $203 / 4$ | $21 / 4$ | 17 | 1-12 holes | 16 | 55.0 | 232 |
| 14×12 | 16 | $21 / 2$ | $183 / 4$ | $11 / 8-12$ holes | $203 / 4$ | $21 / 4$ | 17 | 1-12 holes | 19 | 55.0 | 232 |
| 16x12 | 18 | $21 / 2$ | $211 / 4$ | $11 / 8-16$ holes | $231 / 4$ | $21 / 2$ | $183 / 4$ | $11 / 8-12$ holes | 19 | 89.5 | 232 |
| 16x14 | 18 | $21 / 2$ | 21 1/4 | $11 / 8$ - 16 holes | $231 / 4$ | $21 / 2$ | $183 / 4$ | 11/8-12 holes | $203 / 4$ | 89.5 | 232 |
| mm | mm | mm | mm | mm | mm | mm | mm | mm | mm | kg | bar |
| 50x25 | 127 | 19 | 121 | 19-4 holes | 152 | 19 | 98 | 16-4 holes | 108 | 1.18 | 20.7 |
| $50 \times 40$ | 127 | 19 | 121 | 19-4 holes | 152 | 19 | 98 | 16-4 holes | 127 | 1.18 | 20.7 |
| $80 \times 25$ | 375 | 35 | 152 | 19-4 holes | 191 | 19 | 121 | 19-4 holes | 127 | 2.00 | 13 |
| $80 \times 40$ | 152 | 35 | 152 | 19-4 holes | 191 | 19 | 121 | 19-4 holes | 127 | 2.00 | 13.1 |
| 80x50 | 152 | 35 | 152 | 19-4 holes | 191 | 19 | 121 | 19-4 holes | 152 | 2.00 | 13.1 |
| 100x40 | 391 | 35 | 191 | 19-8 holes | 229 | 35 | 152 | 19-4 holes | 152 | 3.20 | 10.0 |
| 100x50 | 178 | 35 | 191 | 19-8 holes | 229 | 35 | 152 | 19-4 holes | 152 | 3.22 | 10.3 |
| 100x80 | 178 | 35 | 191 | 19-8 holes | 229 | 35 | 152 | 19-4 holes | 191 | 3.22 | 10.3 |
| 150x80 | 229 | 38 | 241 | 22-8 holes | 279 | 35 | 191 | 19-8 holes | 191 | 4.99 | 10.3 |
| 150x100 | 229 | 38 | 241 | 22-8 holes | 279 | 35 | 191 | 19-8 holes | 229 | 4.99 | 10.3 |
| 200x100 | 279 | 44 | 298 | 22-8 holes | 343 | 38 | 241 | 22-8 holes | 229 | 7.98 | 16 |
| 200x150 | 279 | 44 | 298 | 22-8 holes | 343 | 38 | 241 | 22-8 holes | 279 | 7.98 | 16 |
| 250x150 | 305 | 51 | 362 | 25-12 holes | 406 | 44 | 298 | 22-8 holes | 279 | 12.79 | 16 |
| 250x200 | 305 | 51 | 362 | 25-12 holes | 406 | 44 | 298 | 22-8 holes | 343 | 12.79 | 16 |
| 300x200 | 356 | 57 | 432 | 25-12 holes | 483 | 51 | 362 | 25-12 holes | 343 | 19.50 | 16 |
| 300x250 | 356 | 57 | 432 | 25-12 holes | 483 | 51 | 362 | 25-12 holes | 406 | 19.50 | 16 |
| 350x250 | 406 | 64 | 476 | 29-12 holes | 527 | 57 | 432 | 25-12 holes | 406 | 24.95 | 16 |
| 350x300 | 406 | 64 | 476 | 29-12 holes | 527 | 57 | 432 | 25-12 holes | 483 | 24.95 | 16 |
| $400 \times 305$ | 457 | 64 | 540 | 29-16 holes | 591 | 64 | 476 | 29-12 holes | 483 | 40.60 | 16 |
| 406x350 | 457 | 64 | 540 | 29-16 holes | 591 | 64 | 476 | 29-12 holes | 527 | 40.60 | 16 |

## REDUCER BUSHING



Reducer Bushing

| Pipe Size | A | $\begin{aligned} & \mathbf{X}^{(1)} \\ & \mathbf{G T} \\ & \text { Pipe } \end{aligned}$ | $\begin{gathered} \mathbf{X}^{(1)} \\ \mathrm{RT} \\ \text { Pipe } \end{gathered}$ | Wt. | Steady <br> Pressure | Pipe Size | A | $\begin{gathered} \mathbf{X}^{(1)} \\ \mathbf{G T} \\ \text { Pipe } \end{gathered}$ | $\begin{gathered} \mathbf{X}^{(1)} \\ \mathrm{RT} \\ \text { Pipe } \end{gathered}$ | Wt. | Steady Pressure |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in. | in. | in. | in. | Ibs | psig | mm | mm | mm | mm | kg | bar |
| * | $11 / 8$ | - | - | 0.1 | 435 | * | 29 | - | - | 0.05 | 30 |
| ** | $13 / 8$ | 1 | - | 0.1 | 435 | ** | 35 | 25 | - | 0.05 | 30 |
| 2x1 | $21 / 4$ | 1 | - | 0.4 | 435 | 50x25 | 57 | 25 | - | 0.18 | 30 |
| 2x1 NPT | $13 / 4$ | - | - | 0.4 | 435 | 50x25 | 44 | - | - | 0.18 | 30 |
| $2 \times 11 / 4$ NPT | $13 / 4$ | - | - | 0.4 | 435 | 50x30 | 44 | - | - | 0.18 | 30 |
| $2 \times 11 / 2$ | 2 | $11 / 8$ | - | 0.1 | 435 | 50x40 | 51 | 29 | - | 0.05 | 30 |
| $2 \times 11 / 2$ NPT | $13 / 4$ | - | - | 0.1 | 435 | 50x40 | 44 | - | - | 0.05 | 30 |
| $3 \times 2$ | $21 / 4$ | $15 / 8$ | $15 / 8$ | 0.8 | 435 | 80x50 | 57 | 41 | 41 | 0.36 | 30 |
| $4 \times 3$ | $25 / 8$ | $17 / 8$ | $13 / 8$ | 1.0 | 232 | 100x80 | 67 | 48 | 35 | 0.45 | 16 |
| 6x4 | $31 / 8$ | 2 | $11 / 2$ | 3.9 | 232 | 150x100 | 79 | 51 | 38 | 1.77 | 16 |
| $8 \times 6$ | $31 / 4$ | 3 | $23 / 8$ | 6.8 | 232 | 200x150 | 83 | 76 | 60 | 3.08 | 16 |
| 10x8 | 4 | 2 5/8 | 3 | 9.9 | 232 | 250x200 | 102 | 67 | 76 | 4.49 | 16 |
| $12 \times 10$ | $41 / 2$ | 3 | $31 / 4$ | 11.8 | 232 | $300 \times 250$ | 114 | 76 | 83 | 5.35 | 16 |
| $14 \times 12$ | $51 / 2$ | $37 / 8$ | $41 / 8$ | 20.2 | 232 | $350 \times 300$ | 140 | 98 | 105 | 9.16 | 16 |
| 16x14 | 6 | $41 / 2$ | $41 / 2$ | 28.9 | 232 | $400 \times 350$ | 152 | 114 | 114 | 13.11 | 16 |

* $1 \times 1 / 4$ NPT, $1 \times 1 / 2$ NPT, $1 \times 3 / 4$ NPT, $11 / 2 x^{1 / 2}$ NPT, $11 / 2 x$ 3/4 NPT

NOTE: MULTI-STEP and ECCENTRIC reducers are available through 16 " sizes. Information available on request.
${ }^{(1)}$ Nominal make-up dimension for drawing layout work only using non-threaded spigots. Do not use for assembly dimensions.


## LATERALS

## 45은ateral Belled



| Pipe Size | A | F | $\begin{aligned} & \hline \mathbf{X}^{(1)} \\ & \text { GT } \\ & \text { Pipe } \end{aligned}$ | $\begin{gathered} \mathbf{X}^{(1)} \\ \mathrm{RT} \\ \text { Pipe } \\ \hline \end{gathered}$ | Wt. | Steady Pressure | Pipe Size | A | F | $\begin{aligned} & \mathbf{X}^{(1)} \\ & \text { GT } \\ & \text { Pipe } \end{aligned}$ | $\begin{gathered} \mathbf{X}^{(1)} \\ \mathrm{RT} \\ \text { Pipe } \\ \hline \end{gathered}$ | Wt. | Steady Pressure |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in. | in. | in. | in. | in. | Ibs. | psig | mm | mm | mm | mm | mm | kg | bar |
| 1 | $37 / 8$ | $21 / 2$ | 1 | - | 0.6 | 150 | 25 | 98 | 64 | 25 | - | 0.27 | 10.3 |
| $11 / 2$ | $51 / 4$ | $31 / 4$ | 1 | - | 1.3 | 150 | 40 | 133 | 83 | 25 | - | 0.59 | 10.3 |
| 2 | 6 5/8 | $23 / 4$ | $11 / 2$ | $11 / 2$ | 4.1 | 150 | 50 | 168 | 70 | 38 | 38 | 1.86 | 10.3 |
| 3 | $73 / 4$ | $41 / 4$ | $17 / 8$ | $13 / 4$ | 4.4 | 150 | 80 | 197 | 108 | 48 | 44 | 2.00 | 10.3 |
| 4 | 9 | $43 / 8$ | 2 | $15 / 8$ | 7.8 | 150 | 100 | 229 | 111 | 51 | 41 | 3.54 | 10.3 |
| 6 | $121 / 2$ | $53 / 4$ | $21 / 4$ | $21 / 4$ | 13.7 | 135 | 150 | 318 | 146 | 57 | 57 | 6.21 | 9.3 |
| 8 | $161 / 4$ | $73 / 8$ | $31 / 8$ | $31 / 2$ | 33.7 | 135 | 200 | 413 | 187 | 79 | 89 | 15.29 | 9.3 |
| 10 | 19 /8 | $83 / 4$ | $31 / 8$ | $33 / 8$ | 53.3 | 120 | 250 | 498 | 222 | 79 | 86 | 24.17 | 8.3 |
| 12 | $243 / 4$ | $11^{3 / 4}$ | $31 / 4$ | $31 / 2$ | 96.0 | 90 | 300 | 629 | 298 | 83 | 89 | 43.54 | 6.2 |
| 14 | $321 / 2$ | $153 / 4$ | $37 / 8$ | 4 | 154.2 | 75 | 350 | 826 | 400 | 98 | 102 | 69.94 | 5.2 |
| 16 | $353 / 4$ | $173 / 4$ | $41 / 8$ | $41 / 8$ | 222.6 | 75 | 400 | 908 | 451 | 105 | 105 | 101 | 5.2 |



450 Lateral Flanged ${ }^{(2)}$

| Pipe Size | B | C | D | E <br> Bolt Hole Size | F | 0 | Wt. | Steady Press. | Pipe Size | B | C | D | E <br> Bolt Hole Size | F | 0 | Wt. | Steady Press. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in. | in. | in. | in. | in. | in. | in. | lbs. | psig | mm | mm | mm | mm | mm | mm | mm | kg | bar |
| 1 | 6 | $3 / 4$ | $31 / 4$ | 5/8-4 holes | $41 / 2$ | $41 / 4$ | 2.8 | 150 | 25 | 152 | 19 | 83 | 16-4 holes | 114 | 108 | 1.27 | 10.3 |
| $11 / 2$ | $81 / 2$ | $3 / 4$ | $37 / 8$ | 5/8-4 holes | $51 / 2$ | 5 | 4.4 | 150 | 40 | 216 | 19 | 98 | 16-4 holes | 140 | 127 | 2.00 | 10.3 |
| 2 | $87 / 8$ | $3 / 4$ | $43 / 4$ | 3/4-4 holes | $63 / 8$ | 6 | 7.8 | 150 | 50 | 225 | 19 | 121 | 19-4 holes | 162 | 152 | 3.54 | 10.3 |
| 3 | $113 / 4$ | $13 / 8$ | 6 | 3/4-4 holes | 8 | $71 / 2$ | 13.4 | 150 | 80 | 298 | 35 | 152 | 19-4 holes | 203 | 191 | 6.08 | 10.3 |
| 4 | $12 \mathrm{l} / 8$ | $13 / 8$ | $71 / 2$ | 3/4-8 holes | $81 / 2$ | 9 | 19.2 | 150 | 100 | 327 | 35 | 191 | 19-8 holes | 216 | 229 | 8.71 | 10.3 |
| 6 | 18 | $11 / 2$ | $91 / 2$ | 7/8-8 holes | 11 | 11 | 35 | 135 | 150 | 457 | 38 | 241 | 22-8 holes | 279 | 279 | 15.9 | 9.3 |
| 8 | $213 / 4$ | $13 / 4$ | $113 / 4$ | 7/8-8 holes | 13 3/4 | $131 / 2$ | 65.3 | 135 | 200 | 552 | 44 | 298 | 22-8 holes | 349 | 343 | 29.6 | 9.3 |
| 10 | 26 5/8 | 2 | $141 / 4$ | 1-12 holes | 16 5/8 | 16 | 112 | 120 | 250 | 676 | 51 | 362 | 25-12 holes | 422 | 406 | 50.8 | 8.3 |
| 12 | 32 | $21 / 4$ | 17 | 1-12 holes | 20 | 19 | 172 | 90 | 300 | 813 | 57 | 432 | 25-12 holes | 508 | 483 | 78 | 6.2 |
| 14 | 36 | $21 / 2$ | 18 3/4 | 11/8-12 holes | 22 | $203 / 4$ | 209 | 75 | 350 | 914 | 64 | 476 | 29-12 holes | 559 | 527 | 94.6 | 5.2 |
| 16 | 40 | $21 / 2$ | 21 1/4 | 11⁄8-16 holes | 24 | $231 / 4$ | 267 | 75 | 400 | 1,016 | 64 | 540 | 29-16 holes | 610 | 594 | 121 | 5.2 |

${ }^{(1)}$ Nominal make-up dimension for drawing layout work only using non-threaded spigots. Do not use for assembly dimensions.
${ }^{(2)}$ Flanges should be joined to flat-faced flanges. When joining to raised-faced flange connections, consult installation or engineering Manuals INS1000 \& ENG1000. Bolt torque, gasket thickness and hardness recommendations are in Manual INS1000.

## Cross - Belled



| Pipe Size | A | $\overline{\mathbf{X}^{(1)}}$ <br> GT Pipe | $\overline{\mathbf{X}^{(1)}}$ <br> RT Pipe | Wt. | Steady Pressure | Pipe Size | A | $\begin{gathered} \mathbf{X}^{(1)} \\ \text { GT Pipe } \end{gathered}$ | $\overline{\mathbf{X}^{(1)}}$ <br> RT Pipe | Wt. | Steady Pressure |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in. | in. | in. | in. | Ibs. | psig | mm | mm | mm | mm | kg | bar |
| 1 | $23 / 4$ | 1 | - | 1.4 | 300 | 25 | 70 | 25 | - | 0.64 | 20.7 |
| $11 / 2$ | $33 / 8$ | $11 / 8$ | - | 2.0 | 300 | 40 | 86 | 29 | - | 0.91 | 20.7 |
| 2 | $33 / 8$ | $15 / 8$ | $11 / 2$ | 3.4 | 300 | 50 | 86 | 41 | 38 | 1.54 | 20.7 |
| 3 | $45 / 8$ | $17 / 8$ | $13 / 4$ | 8.5 | 190 | 80 | 117 | 48 | 44 | 3.86 | 13.1 |
| 4 | $51 / 8$ | 2 | 1 5/8 | 10.7 | 150 | 100 | 130 | 51 | 41 | 4.85 | 10.3 |
| 6 | $61 / 8$ | $21 / 4$ | $21 / 4$ | 17.3 | 150 | 150 | 156 | 57 | 57 | 7.85 | 10.3 |
| 8 | 11 5/8 | $31 / 8$ | $31 / 2$ | 30.8 | 150 | 200 | 295 | 79 | 89 | 13.97 | 10.3 |
| 10 | 13 1/8 | $31 / 4$ | $31 / 2$ | 42.7 | 150 | 250 | 333 | 83 | 89 | 19.37 | 10.3 |
| 12 | 14 | $33 / 8$ | $37 / 8$ | 73.2 | 150 | 300 | 356 | 86 | 98 | 33.20 | 10.3 |
| 14 | 16 | $37 / 8$ | 4 | 104 | 150 | 350 | 406 | 98 | 102 | 47.27 | 10.3 |
| 16 | $171 / 4$ | $41 / 8$ | $41 / 8$ | 143 | 150 | 400 | 438 | 105 | 105 | 64.86 | 10.3 |

Cross - Flanged ${ }^{(2)}$


| Pipe Size | B | C | D | E <br> Bolt Hole Size | 0 | Wt. | Steady Pressure | Pipe Size | B | C | D | E <br> Bolt Hole Size | 0 | Wt. | Steady Pressure |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in. | in. | in. | in. | in. | in. | Ibs. | psig | mm | mm | mm | mm | mm | mm | kg | bar |
| 1 | $311 / 2$ | $3 / 4$ | $31 / 8$ | $5 / 8-4$ holes | $41 / 4$ | 3.8 | 300 | 25 | 89 | 19 | 79 | 16-4 holes | 108 | 1.7 | 20.7 |
| $11 / 2$ | 4 | $3 / 4$ | $31 / 8$ | $5 / 8-4$ holes | 5 | 5.4 | 300 | 40 | 102 | 19 | 79 | 16-4 holes | 127 | 2.5 | 20.7 |
| 2 | $41 / 2$ | $3 / 4$ | $43 / 4$ | $3 / 4-4$ holes | 6 | 8.6 | 300 | 50 | 114 | 19 | 121 | 19-4 holes | 152 | 3.9 | 20.7 |
| 3 | $51 / 2$ | $13 / 8$ | 6 | $3 / 4-4$ holes | $71 / 2$ | 15.1 | 190 | 80 | 140 | 35 | 152 | $19-4$ holes | 191 | 6.8 | 13.1 |
| 4 | $61 / 2$ | $13 / 8$ | $71 / 2$ | $3 / 4-8$ holes | 9 | 22.8 | 150 | 100 | 165 | 35 | 191 | 19-8 holes | 229 | 10.3 | 10.3 |
| 6 | 8 | $11 / 2$ | $91 / 2$ | $7 / 8-8$ holes | 11 | 34.9 | 150 | 150 | 203 | 38 | 241 | $22-8$ holes | 279 | 15.8 | 10.3 |
| 8 | 9 | $13 / 4$ | $11^{3 / 4}$ | 7/8-8 holes | $131 / 2$ | 61.2 | 150 | 200 | 229 | 44 | 298 | 22-8 holes | 343 | 27.8 | 10.3 |
| 10 | 11 | 2 | $141 / 4$ | $1-12$ holes | 16 | 83.5 | 150 | 250 | 279 | 51 | 362 | 25-12 holes | 406 | 37.9 | 10.3 |
| 12 | 12 | $21 / 4$ | 17 | 1-12 holes | 19 | 145 | 150 | 300 | 305 | 57 | 432 | 25-12 holes | 483 | 65.8 | 10.3 |
| 14 | 14 | $21 / 2$ | $18^{3 / 4}$ | 11/8-12 holes | $203 / 4$ | 224 | 150 | 350 | 356 | 64 | 476 | 29-12 holes | 527 | 102 | 10.3 |
| 16 | 15 | $21 / 2$ | $211 / 4$ | $11 / 8-16$ holes | $231 / 4$ | 303 | 150 | 400 | 381 | 64 | 540 | 29-16 holes | 594 | 137 | 10.3 |

${ }^{(1)}$ Nominal make-up dimension for drawing layout work only using non-threaded spigots. Do not use for assembly dimensions.
${ }^{(2)}$ Flanges should be joined only to flat-faced flanges. When joining to raised-faced flange connections, consult installation or engineering Manuals INS1000 \& ENG1000. Bolt torque, gasket thickness and hardness recommendations are in Manual INS1000.

## SADDLES (Parts are available in Green Thread HP only.)



| Size | A | B | C Angle | $\begin{gathered} \mathbf{X}^{(1)} \\ \mathbf{G T} \\ \text { Pipe } \end{gathered}$ | $\begin{gathered} \mathbf{X X}^{(1)} \\ \mathrm{RT} \\ \text { Pipe } \\ \hline \end{gathered}$ | Wt. | Steady Pressure | Size | A | B | $\begin{gathered} \mathbf{X}^{(1)} \\ \text { GT } \\ \text { Pipe } \end{gathered}$ | $\begin{gathered} \hline X^{(1)} \\ \text { RT } \\ \text { Pipe } \end{gathered}$ | Wt. | Steady Pressure |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in. | in. | in. | Degree | in. | in. | lbs. | psig | mm | mm | mm | mm | mm | kg | bar |
| 2x1 | $27 / 8$ | 4 | 180 | 1 | - | 0.6 | 435 | 50x25 | 73 | 102 | 25 | - | 0.27 | 30 |
| $2 \times 11 / 2$ | $27 / 8$ | 4 | 180 | $11 / 8$ | - | 0.5 | 232 | $50 \times 40$ | 73 | 102 | 29 | - | 0.23 | 16 |
| $3 \times 1$ | $31 / 2$ | 6 | 180 | 1 | - | 1.5 | 300 | $80 \times 25$ | 89 | 152 | 25 | - | 0.68 | 20.7 |
| $3 \times 11 / 2$ | $31 / 2$ | 6 | 180 | $11 / 8$ | - | 0.9 | 232 | $80 \times 40$ | 89 | 152 | 29 | - | 0.41 | 16 |
| $3 \times 2$ | 4 | 6 | 180 | $15 / 8$ | $15 / 8$ | 1.4 | 232 | $80 \times 50$ | 102 | 152 | 41 | 41 | 0.64 | 16 |
| 4x1 | 4 | 6 | 180 | 1 | - | 1.4 | 232 | $100 \times 25$ | 102 | 152 | 25 | - | 0.64 | 16 |
| $4 \times 11 / 2$ | 4 | 6 | 180 | 11/8 | - | 1.5 | 232 | 100x40 | 102 | 152 | 29 | - | 0.68 | 16 |
| $4 \times 2$ | $41 / 2$ | 6 | 180 | $15 / 8$ | $15 / 8$ | 1.5 | 232 | 100x50 | 114 | 152 | 41 | 41 | 0.68 | 16 |
| $4 \times 3$ | $51 / 4$ | 6 | 180 | $17 / 8$ | $13 / 4$ | 1.6 | 200 | 100x80 | 133 | 152 | 48 | 44 | 0.73 | 13.8 |
| 6x1 | 5 | 6 | 120 | 1 | - | 1.4 | 232 | 150x25 | 127 | 152 | 25 | - | 0.64 | 16 |
| $6 \times 11 / 2$ | 5 | 6 | 120 | $11 / 8$ | - | 1.3 | 232 | 150x40 | 127 | 152 | 29 | - | 0.59 | 16 |
| 6x2 | $51 / 2$ | 6 | 120 | $15 / 8$ | $15 / 8$ | 1.5 | 232 | $150 \times 50$ | 140 | 152 | 41 | 41 | 0.68 | 16 |
| 6x3 | $61 / 4$ | 6 | 120 | $17 / 8$ | $13 / 4$ | 1.6 | 150 | 150x80 | 159 | 152 | 48 | 44 | 0.73 | 10.3 |
| 6x4 | $63 / 8$ | 8 | 140 | 2 | $15 / 8$ | 2.4 | 125 | 150x100 | 162 | 203 | 51 | 41 | 1.09 | 8.6 |
| $8 \times 1^{(2)}$ | $71 / 8$ | 9 | 120 | 1 | - | 3.1 | 232 | $200 \times 25$ | 181 | 229 | 25 | - | 1.41 | 16 |
| $8 \times 11 / 2^{(2)}$ | $71 / 8$ | 9 | 120 | $11 / 8$ | - | 2.8 | 232 | 200x40 | 181 | 229 | 29 | - | 1.27 | 16 |
| $8 \times 2$ | 7 | 9 | 180 | $15 / 8$ | $15 / 8$ | 2.7 | 232 | $200 \times 50$ | 178 | 229 | 41 | 41 | 1.22 | 16 |
| $10 \times 1{ }^{(2)}$ | $81 / 8$ | 9 | 95 | 1 | - | 3.1 | 232 | 250x25 | 206 | 229 | 25 | - | 1.41 | 16 |
| $10 \times 11 / 2^{(2)}$ | $81 / 8$ | 9 | 95 | $1^{1 / 8}$ | - | 2.8 | 232 | 250x40 | 206 | 229 | 29 | - | 1.27 | 16 |
| 10x2 | 8 | 9 | 180 | $15 / 8$ | $15 / 8$ | 2.7 | 232 | 250x50 | 203 | 229 | 41 | 41 | 1.22 | 16 |
| 10x3 | 9 | 14 | 150 | $17 / 8$ | $13 / 4$ | 6.1 | 232 | 250x80 | 229 | 356 | 48 | 44 | 2.77 | 16 |
| $12 \times 1{ }^{(2)}$ | $91 / 8$ | 10 | 90 | 1 | - | 3.6 | 232 | $300 \times 25$ | 232 | 254 | 25 | - | 1.63 | 16 |
| $12 \times 11 / 2^{(2)}$ | $91 / 8$ | 10 | 90 | $11 / 8$ | - | 3.3 | 232 | $300 \times 40$ | 232 | 254 | 29 | - | 1.50 | 16 |
| 12x2 | 9 | 10 | 180 | $15 / 8$ | $15 / 8$ | 3.2 | 232 | $300 \times 50$ | 229 | 254 | 41 | 41 | 1.45 | 16 |
| 12x3 | 10 | 14 | 125 | 17/8 | $13 / 4$ | 6.1 | 232 | $300 \times 80$ | 254 | 356 | 48 | 44 | 2.77 | 16 |
| 12x4 | $93 / 8$ | 17 | 155 | 2 | $15 / 8$ | 8.6 | 232 | $300 \times 100$ | 238 | 432 | 51 | 41 | 3.90 | 16 |
| $14 \times 1{ }^{(2)}$ | 10 | 12 | 95 | 1 | - | 4.7 | 232 | 350x25 | 254 | 305 | 25 | - | 2.13 | 16 |
| $14 \times 1 \frac{1}{2} 2^{(2)}$ | 10 | 12 | 95 | 11/8 | - | 4.4 | 232 | 350x40 | 254 | 305 | 29 | - | 2.00 | 16 |
| $14 \times 2$ | 10 | 12 | 95 | $15 / 8$ | $13 / 8$ | 4.3 | 232 | 350x50 | 254 | 305 | 41 | 35 | 1.95 | 16 |
| $14 \times 3$ | $107 / 8$ | 15 | 120 | $17 / 8$ | $13 / 4$ | 6.9 | 232 | 350x80 | 276 | 381 | 48 | 44 | 3.13 | 16 |
| $14 \times 4$ | $101 / 4$ | 17 | 135 | 2 | $15 / 8$ | 8.4 | 232 | 350x100 | 260 | 432 | 51 | 41 | 3.81 | 16 |
| $16 \times 1^{(2)}$ | 11 | 13 | 90 | 1 | - | 5.4 | 232 | $400 \times 25$ | 279 | 330 | 25 | - | 2.45 | 16 |
| $16 \times 11 / 2^{(2)}$ | 11 | 13 | 90 | $11 / 8$ | - | 5.1 | 232 | 400x40 | 279 | 330 | 29 | - | 2.31 | 16 |
| 16x2 | 11 | 13 | 90 | $15 / 8$ | $13 / 8$ | 5 | 232 | $400 \times 50$ | 279 | 330 | 41 | 35 | 2.27 | 16 |

[^24]
## SADDLES, Continued (Parts are available in Green Thread HP only.)



| Size | A | B | C <br> Angle | $\begin{gathered} \mathbf{X}^{(1)} \\ \text { GT } \\ \text { Pipe } \end{gathered}$ | $\begin{gathered} \mathbf{X}^{(1)} \\ \mathrm{RT} \\ \text { Pipe } \end{gathered}$ | Wt. | Steady Pressure | Size | A | B | $\begin{gathered} \mathbf{X}^{(1)} \\ \text { GT } \\ \text { Pipe } \end{gathered}$ | $\begin{gathered} \mathbf{X}^{(1)} \\ \text { RT } \\ \text { Pipe } \end{gathered}$ | Wt. | Steady Pressure |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in. | in. | in. | Degree | in. | in. | lbs. | psig | mm | mm | mm | mm | mm | kg | bar |
| 16x3 | 11 \%/8 | 15 | 105 | $17 / 8$ | $13 / 4$ | 6.9 | 232 | 400x80 | 302 | 381 | 48 | 44 | 3.13 | 16 |
| 16x4 | $111 / 4$ | 17 | 120 | 2 | $15 / 8$ | 8.6 | 232 | 400x100 | 286 | 432 | 51 | 41 | 3.90 | 16 |

## THREADED SIDE OUTLET NPT INTERNAL THREADS



| Size | A | B | C Angle | Wt. | Steady Pressure | Size | A | B | Wt. | Steady Pressure |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in. | in. | in. | Degree | lbs. | psig | mm | mm | mm | kg | bar |
| 2x1 | $27 / 8$ | 4 | 180 | 0.6 | 435 | 50x25 | 73 | 102 | 0.27 | 30 |
| $2 \times 11 / 4$ | $27 / 8$ | 4 | 180 | 0.6 | 232 | 50x30 | 73 | 102 | 0.27 | 16 |
| $2 \times 11 / 2$ | $27 / 8$ | 4 | 180 | 0.5 | 232 | 50x40 | 73 | 102 | 0.23 | 16 |
| $3 \times 1$ | $31 / 2$ | 6 | 180 | 1.1 | 300 | $80 \times 25$ | 89 | 152 | 0.50 | 20.7 |
| $3 \times 11 / 4$ | $31 / 2$ | 6 | 180 | 1.0 | 232 | 80x30 | 89 | 152 | 0.45 | 16 |
| $3 \times 11 / 2$ | $31 / 2$ | 6 | 180 | 1.0 | 232 | $80 \times 40$ | 89 | 152 | 0.45 | 16 |
| $4 \times 1$ | 4 | 6 | 180 | 1.6 | 232 | 100x25 | 102 | 152 | 0.73 | 16 |
| $4 \times 11 / 4$ | 4 | 6 | 180 | 1.5 | 232 | 100x30 | 102 | 152 | 0.68 | 16 |
| $4 \times 11 / 2$ | 4 | 6 | 180 | 1.4 | 232 | 100x40 | 102 | 152 | 0.64 | 16 |
| 6x1 | 5 | 6 | 120 | 1.5 | 232 | 150x25 | 127 | 152 | 0.68 | 16 |
| $6 \times 11 / 4$ | 5 | 6 | 120 | 1.4 | 232 | 150x30 | 127 | 152 | 0.64 | 16 |
| $6 \times 11 / 2$ | 5 | 6 | 120 | 1.5 | 232 | 150x40 | 127 | 152 | 0.68 | 16 |
| $8 \times 1$ | $71 / 8$ | 9 | 120 | 3.1 | 232 | 200x25 | 181 | 229 | 1.41 | 16 |
| 10x1 | $81 / 8$ | 9 | 95 | 3.1 | 232 | 250x25 | 206 | 229 | 1.41 | 16 |
| 12x1 | $91 / 8$ | 10 | 90 | 3.6 | 232 | 300x25 | 232 | 254 | 1.63 | 16 |
| 14x1 | 10 | 12 | 95 | 4.7 | 232 | 350x25 | 254 | 305 | 2.13 | 16 |
| 16x1 | 11 | 13 | 90 | 5.4 | 232 | 400x25 | 279 | 330 | 2.45 | 16 |

Green Thread HP16 Branch Table

|  |  | Branch Diameter (inch) |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 1 | 1.5 | 2 | 3 | 4 | 6 | 8 | 10 | 12 | 14 | 16 |
|  | 1 | T | - | - | - | - | - | - | - | - | - | - |
|  | 1.5 | RBT | T | - | - | - | - | - | - | - | - | - |
|  | 2 | S | S/RBT | T | - | - | - | - | - | - | - | - |
|  | 3 | S | S/RBT | S/RBT | T | - | - | - | - | - | - | - |
|  | 4 | S | S | S/RBT | S*/RBT | T | - | - | - | - | - | - |
|  | 6 | S | S | S | S*/RBT | S*/RBT | T | - | - | - | - | - |
|  | 8 | S | S | S/T | T | T | T | T | - | - | - | - |
|  | 10 | S | S | S/T | S/T | T | T | T | T | - | - | - |
|  | 12 | S | S | S/T | S/T | S/T | T | T | T | T | - | - |
|  | 14 | S | S | S | S/T | S/T | T | T | T | T | T | - |
|  | 16 | S | S | S | S/T | S/T | T | T | T | T | T | T |

S - Saddle, T - Tee, S/T - Tee or Saddle, S/RBT - Saddle or compression molded Tee with Reducer Bushing.
Notes:

1. In general, saddles are limited to branch sizes that are $1 / 3$ of the header size or smaller.
2. Saddles are limited to outlet size of 6 inch or less.
3. Saddles are rated the same as Tees unless otherwise noted by *.

## END CAPS (Parts are available in GREEN THREAD HP only.)


${ }^{(1)}$ Nominal make-up dimension for drawing layout work only using non-threaded spigots. Do not use for assembly dimensions.

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## Standard $90^{\circ}$ Elbow

(Bell x Bell)

| Pipe Size |  | A |  | $\mathbf{X ~}^{(1)}$ |  | Weight |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | in | mm | in | mm | lbs | kg |
| 18 | 450 | 21.75 | 552 | 8.0 | 203 | 140 | 64 |
| 20 | 500 | 25.25 | 641 | 9.1 | 231 | 200 | 91 |
| 24 | 600 | 29.00 | 737 | 10.0 | 254 | 250 | 114 |
| 30 | 750 | 36.50 | 927 | 13.9 | 353 | 450 | 204 |
| 36 | 900 | 43.50 | 1,105 | 16.8 | 427 | 800 | 364 |

## Standard $45^{\circ}$ Elbow

(Bell x Bell)

| Pipe Size |  | A |  | $\mathbf{X}^{(1)}$ |  | Weight |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| in | $\mathbf{m m}$ | in | $\mathbf{m m}$ | in | $\mathbf{m m}$ | lbs | kg |
| 18 | 450 | 14.75 | 375 | 8.0 | 203 | 100 | 45 |
| 20 | 500 | 17.60 | 447 | 9.1 | 231 | 140 | 64 |
| 24 | 600 | 20.20 | 513 | 10.0 | 254 | 200 | 91 |
| 30 | 750 | 24.80 | 630 | 13.9 | 353 | 375 | 170 |
| 36 | 900 | 29.40 | 747 | 16.8 | 427 | 700 | 318 |
| 42 | 1050 | 35.30 | 897 | 18.7 | 475 | 1,100 | 500 |

## $30^{\circ}$ Elbow

(Bell x Bell)

| Pipe Size |  | A |  | $\mathbf{X}^{(\mathbf{1})}$ |  | Weight |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| in | $\mathbf{m m}$ | in | $\mathbf{m m}$ | in | $\mathbf{m m}$ | lbs | $\mathbf{k g}$ |
| 30 | 750 | 21.90 | 556 | 13.9 | 353 | 300 | 136 |
| 36 | 900 | 25.90 | 658 | 16.8 | 427 | 600 | 272 |
| 42 | 1050 | 30.60 | 777 | 18.7 | 475 | 950 | 431 |

${ }^{(1)}$ This is a nominal make-up dimension for drawing layout work only. Do not use for assembly dimensions.
NOTE: When rated according to ASTM D5685 criteria, the pressure rating for 36 " diameter and smaller fittings is 16 bar and the pressure rating for 42 " is 14 bar.

When rated according to ISO 14692, the pressure rating for 30 " and 36 " is 14.7 bar and the pressure rating for 42 " is 12.7 bar

## Long Radius $90^{\circ}$ Elbow

(Bell x Bell, Long Radius 1.5D)

| Pipe Size |  | A |  | $\mathbf{X}^{(1)}$ |  | Weight |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | in | mm | in | mm | lbs | kg |
| 18 | 450 | 36.75 | 933 | 8.0 | 203 | 167 | 76 |
| 20 | 500 | 42.25 | 1,073 | 9.1 | 231 | 225 | 102 |
| 24 | 600 | 50.00 | 1,270 | 10.0 | 254 | 258 | 117 |

## Long Radius $45^{\circ}$ Elbow

(Bell x Bell, Long Radius 1.5D)

|  |  |  |  |  |  | $\mathbf{X}^{(\mathbf{1})}$ |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
|  |  | Weight |  |  |  |  |  |
| Pipe Size | $\mathbf{m m}$ | in | $\mathbf{m m}$ | in | $\mathbf{m m}$ | lbs | kg |
| 18 | 450 | 20.90 | 531 | 8.0 | 203 | 100 | 45 |
| 20 | 500 | 24.70 | 627 | 9.1 | 231 | 135 | 61 |
| 24 | 600 | 28.90 | 734 | 10.0 | 254 | 155 | 70 |

## $22.5^{\circ}$ Elbow

(Bell x Bell)

|  |  |  |  | A |  | $\mathbf{X}^{(\mathbf{1})}$ |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
|  |  |  |  |  |  |  |  |
| Pipe Size |  | Weight |  |  |  |  |  |
| in | $\mathbf{m m}$ | in | $\mathbf{m m}$ | in | $\mathbf{m m}$ | lbs | kg |
| 30 | 750 | 20.50 | 521 | 13.9 | 353 | 250 | 113 |
| 36 | 900 | 24.30 | 617 | 16.8 | 427 | 525 | 238 |
| 42 | 1050 | 31.90 | 810 | 18.7 | 475 | 800 | 363 |

## $11.25^{\circ}$ Elbow

(Bell x Bell)

|  |  |  |  | A |  | $\mathbf{X}^{(\mathbf{1})}$ |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
|  |  | Weight |  |  |  |  |  |
| in | $\mathbf{m m}$ | in | $\mathbf{m m}$ | in | $\mathbf{m m}$ | lbs | kg |
| 30 | 750 | 19.10 | 485 | 13.9 | 353 | 225 | 102 |
| 36 | 900 | 22.30 | 566 | 16.8 | 427 | 450 | 204 |
| 42 | 1050 | 28.20 | 716 | 18.7 | 475 | 675 | 306 |

View of Fitting Illustrations


## Tees

(Bell x Bell x Bell)

| Pipe Size |  | A |  | $\mathbf{X}^{(1)}$ |  | Weight |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| in | $\mathbf{m m}$ | in | $\mathbf{m m}$ | in | $\mathbf{m m}$ | lbs | kg |
| 18 | 450 | 22.38 | 568 | 8.0 | 203 | 320 | 145 |
| 20 | 500 | 26.25 | 667 | 9.1 | 231 | 360 | 163 |
| 24 | 600 | 28.00 | 711 | 10.0 | 254 | 450 | 204 |
| 30 | 750 | 36.50 | 927 | 13.9 | 353 | 750 | 340 |
| 36 | 900 | 40.50 | 1,029 | 16.8 | 427 | 1,200 | 545 |

## Sleeve Coupling

(Bell x Bell)

| Pipe Size |  | A |  | $\mathbf{X}^{(\mathbf{1})}$ |  | Weight |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| in | $\mathbf{m m}$ | in | $\mathbf{m m}$ | in | $\mathbf{m m}$ | lbs | kg |
| 18 | 450 | 21.00 | 533 | 8.0 | 203 | 51 | 23 |
| 20 | 500 | 26.00 | 660 | 9.1 | 231 | 76 | 35 |
| 24 | 600 | 29.50 | 749 | 10.0 | 254 | 122 | 55 |
| 30 | 750 | 35.00 | 889 | 13.9 | 353 | 200 | 91 |
| 36 | 900 | 41.00 | 1,041 | 16.8 | 427 | 320 | 145 |
| 42 | 1050 | 46.00 | 1,168 | 18.7 | 475 | 500 | 227 |

## Reducing Tees

| Pipe Size |  | AT |  | AS |  | $X_{1}{ }^{(1)}$ |  | $X_{2}{ }^{(1)}$ |  | Weight |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | in | mm | in | mm | in | mm | in | mm | lbs | kg |
| $18 \times 14$ | $450 \times 350$ | 22.38 | 568 | 20.50 | 521 | 8.0 | 203 | 6.4 | 163 | 280 | 127 |
| $18 \times 16$ | $450 \times 400$ | 22.38 | 568 | 21.00 | 533 | 8.0 | 203 | 6.6 | 167 | 300 | 136 |
| $20 \times 16$ | $500 \times 400$ | 26.25 | 667 | 22.50 | 572 | 9.1 | 231 | 6.6 | 167 | 320 | 145 |
| $20 \times 18$ | $500 \times 450$ | 26.25 | 667 | 22.75 | 578 | 9.1 | 231 | 8.0 | 203 | 340 | 154 |
| $24 \times 18$ | $600 \times 450$ | 28.00 | 711 | 25.25 | 641 | 10.0 | 254 | 8.0 | 203 | 400 | 182 |
| $24 \times 20$ | $600 \times 500$ | 28.00 | 711 | 27.75 | 705 | 10.0 | 254 | 9.1 | 231 | 420 | 191 |

## Concentric Reducers

(Bell x Bell)

| Pipe Size |  | A |  | $\mathbf{X}^{(1)}$ |  | $\mathbf{X}^{(2)}$ |  | Weight |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | in | mm | in | mm | in | mm | lbs | kg |
| $18 \times 16$ | $450 \times 400$ | 28.75 | 730 | 8.0 | 203 | 6.8 | 173 | 110 | 50 |
| $20 \times 18$ | $500 \times 450$ | 32.00 | 813 | 9.1 | 231 | 8.0 | 203 | 140 | 64 |
| $24 \times 20$ | $600 \times 500$ | 46.25 | 1,175 | 10.0 | 254 | 9.1 | 231 | 190 | 86 |
| $30 \times 24$ | $750 \times 600$ | 50.50 | 1283 | 13.9 | 353 | 10.0 | 254 | 300 | 136 |
| $36 \times 30$ | $900 \times 750$ | 56.00 | 1422 | 16.8 | 427 | 13.9 | 352 | 450 | 205 |
| $42 \times 36$ | $1050 \times 900$ | 61.50 | 1562 | 18.7 | 475 | 16.8 | 428 | 750 | 340 |

## Nipples

( $\mathrm{X}=$ Available Lengths)

| Pipe Size |  | Overall Length |  |  |
| :---: | :---: | :---: | :---: | :---: |
| in | mm | 24" (610 mm) | 36" (914 mm) | 42" (1067 mm) |
| 18 | 450 | X | X |  |
| 20 | 500 | X | X |  |
| 24 | 600 |  | X |  |
| 30 | 750 |  | X |  |
| 36 | 900 |  |  | X |
| 42 | 1050 |  |  | X |

NOTE: When rated according to ASTM D5685 criteria, the pressure rating for 36 " diameter and smaller fittings is 16 bar and the pressure rating for 42 " is 14 bar.
When rated according to ISO 14692 , the pressure rating for 30 " and 36 " is 14.7 bar and the pressure rating for 42 " is 12.7 bar


## Flanges

(Filament Wound (FW) and Blind Flange ANSI B16.5 Class 150)

| Pipe Size |  | B |  | C |  | CC |  | D |  | E <br> Bold Hole Size <br> Number of Bolts |  | 0 |  | FW <br> Flange <br> $\mathbf{X}^{(1)}$ |  | Bolt Torque |  | FW <br> Flange <br> Weight |  | Blind <br> Flange <br> Weight |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | in | mm | in | mm | in | mm | in | mm | in | mm | in | mm | in | mm | ft-lbs | $\mathrm{N} \cdot \mathrm{m}$ | lbs | kg | Blind | kg |
| 18 | 450 | 9.0 | 229 | 2.75 | 70 | 2.50 | 64 | 22.75 | 578 | 1.25-16 | 32-16 | 25.0 | 635 | 6.8 | 173 | 200 | 271 | 76 | 35 | 125 | 57 |
| 20 | 500 | 11.0 | 279 | 2.75 | 70 | 2.75 | 70 | 25.00 | 635 | 1.25-20 | 32-20 | 27.5 | 699 | 7.8 | 198 | 200 | 271 | 92 | 42 | 140 | 64 |
| 24 | 600 | 13.0 | 330 | 3.00 | 76 | 3.31 | 84 | 29.50 | 749 | 1.38-20 | 35-20 | 32.0 | 813 | 9.5 | 241 | 200 | 271 | 124 | 56 | 155 | 70 |

${ }^{(1)}$ This is a nominal make-up dimension for drawing layout work only. Do not use for assembly dimensions.

## Van Stone Flanges

(ANSI B16.5 Class 150 (18"-24"), ANSI B16.1 Class 125 (30"-42"))

| Pipe <br> Size |  | A |  | B |  | $\mathbf{X}^{(1)}$ |  | D |  | E |  | F |  | G |  | H |  | I |  | Max. Bolt Torque |  | Nom. <br> Weight <br> Hub |  | Nom. <br> Weight <br> Bolt <br> Ring |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | in | mm | in | mm | in | mm | in | mm | in | mm | in | mm | in | mm | in | mm | in | mm | ftolbs | $\mathrm{N} \cdot \mathrm{m}$ | lbs | kg | lbs | kg |
| 18 | 450 | 21.4 | 545 | 19.9 | 506 | 7.5 | 191 | 9.00 | 229 | 8.50 | 216 | 2.25 | 57 | 1.25 | 32 | 22.75 | 578 | 25.00 | 635 | 200 | 271 | 39 | 18 | 98 | 44 |
| 20 | 500 | 23.7 | 602 | 21.9 | 557 | 8.5 | 216 | 9.88 | 251 | 9.38 | 238 | 2.25 | 57 | 1.25 | 32 | 25.00 | 635 | 27.50 | 699 | 200 | 271 | 53 | 24 | 114 | 52 |
| 24 | 600 | 28.1 | 713 | 25.9 | 658 | 10.0 | 254 | 11.75 | 298 | 11.25 | 286 | 2.25 | 57 | 1.38 | 35 | 29.50 | 749 | 32.00 | 813 | 200 | 271 | 79 | 36 | 140 | 64 |
| 30 | 750 | 34.6 | 880 | N/A | N/A | 10.0 | 254 | 10.00 | 254 | 9.50 | 241 | 2.25 | 57 | 1.38 | 35 | 36.00 | 914 | 38.75 | 984 | 400 | 543 | 121 | 55 | 192 | 87 |
| 36 | 900 | 41.1 | 1043 | N/A | N/A | 13.0 | 330 | 13.00 | 330 | 12.50 | 318 | 2.25 | 57 | 1.63 | 41 | 42.75 | 1,086 | 46.00 | 1,168 | 400 | 543 | 208 | 94 | 270 | 122 |
| 42 | 1050 | 47.8 | 1214 | N/A | N/A | 19.5 | 495 | 19.50 | 495 | 19.00 | 483 | 3.00 | 76 | 1.63 | 41 | 49.50 | 1,257 | 53.00 | 1,346 | 400 | 543 | 440 | 200 | 445 | 202 |

## Saddles

| Pipe Size |  | A |  | B |  | C deg | $\begin{aligned} & X_{1}{ }^{(1)} \\ & \text { W/RT Pipe } \end{aligned}$ |  | $\begin{aligned} & X_{1}{ }^{(1)} \\ & \text { W/GT Pipe } \end{aligned}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | in | mm | in | mm |  | in | mm | lbs | kg |
| $18 \times 2$ | $450 \times 50$ | 12.75 | 324 | 13 | 330 | 90 | 1.6 | 41 | 1.6 | 41 |
| $18 \times 3$ | $450 \times 75$ | 13.25 | 381 | 15 | 337 | 90 | 1.8 | 46 | 1.9 | 48 |
| $20 \times 2$ | $500 \times 50$ | 13.75 | 349 | 13 | 330 | 90 | 1.6 | 41 | 1.6 | 41 |
| $20 \times 3$ | $500 \times 75$ | 14.25 | 362 | 15 | 381 | 90 | 1.8 | 46 | 1.9 | 48 |
| $24 \times 2$ | $600 \times 50$ | 16.00 | 406 | 13 | 330 | 70 | 1.6 | 41 | 1.6 | 41 |
| $24 \times 3$ | $600 \times 75$ | 16.25 | 413 | 15 | 381 | 70 | 1.8 | 46 | 1.9 | 48 |

${ }^{(1)}$ This is a nominal make-up dimension for drawing layout work only. Do not use for assembly dimensions.
NOTE: When rated according to ASTM D5685 criteria, the pressure rating for 36 " diameter and smaller fittings is 16 bar and the pressure rating for 42 " is 14 bar.
When rated according to ISO 14692 , the pressure rating for 30 " and $36^{\prime \prime}$ is 14.7 bar and the pressure rating for 42 " is 12.7 bar

View of Fitting Illustrations


Flange - Filament Wound / Blind


Van StoneFlange


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## $90^{\circ}$ Elbow

| Pipe Size |  | A |  | $\mathbf{X}^{(\mathbf{1})}$ |  | Weight |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| in | $\mathbf{m m}$ | in | $\mathbf{m m}$ | in | $\mathbf{m m}$ | lbs | kg |
| 2 | 50 | 6.31 | 160 | 2.44 | 62 | 8 | 4 |
| 3 | 80 | 7.94 | 202 | 2.46 | 63 | 14 | 6 |
| 4 | 100 | 9.75 | 248 | 2.98 | 76 | 22 | 10 |
| 6 | 150 | 12.81 | 325 | 2.70 | 69 | 28 | 13 |
| 8 | 200 | 19.50 | 495 | 5.87 | 149 | 40 | 18 |
| 10 | 250 | 23.25 | 591 | 6.79 | 172 | 60 | 27 |
| 12 | 300 | 27.00 | 686 | 7.43 | 189 | 90 | 41 |
| 14 | 350 | 30.00 | 762 | 6.87 | 175 | 135 | 61 |
| 16 | 400 | 34.00 | 864 | 7.65 | 194 | 180 | 82 |
| 18 | 450 | 40.75 | 1035 | 11.88 | 302 | 480 | 216 |
| 20 | 500 | 47.25 | 1200 | 13.92 | 354 | 550 | 250 |
| 24 | 600 | 57.00 | 1448 | 17.10 | 434 | 650 | 295 |

## $45^{\circ}$ Elbow

| Pipe Size |  | A |  | $\mathbf{X}^{(\mathbf{1})}$ |  | Weight |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| in | $\mathbf{m m}$ | in | $\mathbf{m m}$ | in | $\mathbf{m m}$ | lbs | kg |
| 2 | 50 | 4.55 | 116 | 2.44 | 62 | 6 | 3 |
| 3 | 80 | 5.25 | 133 | 2.46 | 63 | 10 | 5 |
| 4 | 100 | 6.25 | 159 | 2.98 | 76 | 17 | 8 |
| 6 | 150 | 7.50 | 191 | 2.70 | 69 | 21 | 9 |
| 8 | 200 | 12.47 | 317 | 5.87 | 149 | 24 | 11 |
| 10 | 250 | 14.46 | 367 | 6.79 | 172 | 36 | 16 |
| 12 | 300 | 16.46 | 418 | 7.43 | 189 | 50 | 23 |
| 14 | 350 | 17.70 | 450 | 6.87 | 175 | 85 | 38 |
| 16 | 400 | 19.94 | 506 | 7.65 | 194 | 120 | 54 |
| 18 | 450 | 24.93 | 633 | 11.88 | 302 | 290 | 132 |
| 20 | 500 | 29.68 | 754 | 13.92 | 354 | 330 | 150 |
| 24 | 600 | 35.91 | 912 | 17.10 | 434 | 400 | 181 |

Tees

| Pipe Size |  | A |  | $\mathbf{X}^{(1)}$ |  | Weight |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| in | $\mathbf{m m}$ | in | $\mathbf{m m}$ | in | $\mathbf{m m}$ | lbs | kg |
| 2 | 50 | 5.56 | 141 | 2.44 | 62 | 13 | 6 |
| 3 | 80 | 6.25 | 159 | 2.46 | 63 | 21 | 9 |
| 4 | 100 | 7.44 | 189 | 2.98 | 76 | 29 | 13 |
| 6 | 150 | 9.56 | 243 | 2.70 | 69 | 36 | 16 |
| 8 | 200 | 13.50 | 343 | 5.87 | 149 | 60 | 27 |
| 10 | 250 | 15.75 | 400 | 6.79 | 172 | 90 | 41 |
| 12 | 300 | 17.00 | 432 | 7.43 | 189 | 130 | 59 |
| 14 | 350 | 19.50 | 495 | 6.87 | 175 | 190 | 86 |
| 16 | 400 | 21.25 | 540 | 7.65 | 194 | 250 | 113 |
| 18 | 450 | 26.38 | 670 | 11.88 | 302 | 600 | 272 |
| 20 | 500 | 31.25 | 794 | 13.92 | 354 | 700 | 318 |
| 24 | 600 | 35.00 | 889 | 17.10 | 434 | 800 | 363 |

Sleeve Couplings

| Pipe Size |  | A |  | $\mathbf{X}^{(\mathbf{1})}$ |  | Weight |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| in | $\mathbf{m m}$ | in | $\mathbf{m m}$ | in | $\mathbf{m m}$ | lbs | kg |
| 2 | 50 | 6.00 | 152 | 1.61 | 41 | 1 | 0.5 |
| 3 | 80 | 6.00 | 152 | 1.72 | 44 | 3 | 1.5 |
| 4 | 100 | 7.00 | 178 | 2.52 | 64 | 7 | 3 |
| 6 | 150 | 8.38 | 213 | 2.97 | 75 | 14 | 6 |
| 8 | 200 | 12.50 | 318 | 4.77 | 121 | 15 | 7 |
| 10 | 250 | 16.50 | 419 | 5.87 | 149 | 17 | 8 |
| 12 | 300 | 18.00 | 457 | 6.52 | 166 | 25 | 11 |
| 14 | 350 | 16.00 | 406 | 6.30 | 160 | 30 | 14 |
| 16 | 400 | 18.00 | 457 | 5.75 | 146 | 36 | 16 |
| 18 | 450 | 29.00 | 737 | 11.88 | 302 | 125 | 57 |
| 20 | 500 | 36.00 | 914 | 13.92 | 354 | 160 | 73 |
| 24 | 600 | 43.50 | 1105 | 17.10 | 434 | 195 | 88 |

${ }^{(1)}$ Nominal make-up dimension for drawing layout work only using non-threaded spigots. Do not use for assembly dimensions.

View of Fitting Illustrations

$90^{\circ}$ Elbow

$45^{\circ}$ Elbow


Tee


Sleeve Coupling

## Reducing Tees

| Pipe Size |  | AT |  | $X_{1}{ }^{(1)}$ |  | AS |  | $X_{2}{ }^{(1)}$ |  | Weight |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | in | mm | in | mm | in | mm | in | mm | Ibs | kg |
| $3 \times 2$ | $80 \times 50$ | 6.22 | 158 | 2.46 | 62 | 6.99 | 178 | 2.44 | 62 | 19 | 9.0 |
| $4 \times 2$ | $100 \times 50$ | 7.46 | 189 | 2.98 | 76 | 7.46 | 189 | 2.44 | 62 | 28 | 13.0 |
| $4 \times 3$ | $100 \times 80$ | 7.46 | 189 | 2.98 | 76 | 7.46 | 189 | 2.46 | 62 | 31 | 14.0 |
| 6x2 | $150 \times 50$ | 9.53 | 242 | 2.70 | 69 | 8.45 | 215 | 2.44 | 62 | 36 | 16.0 |
| 6x3 | 150x80 | 9.53 | 242 | 2.70 | 69 | 8.55 | 217 | 2.46 | 62 | 38 | 17.0 |
| 6x4 | $150 \times 100$ | 9.53 | 242 | 2.70 | 69 | 8.91 | 226 | 2.98 | 76 | 45 | 20.0 |
| $8 \times 2$ | $200 \times 50$ | 13.50 | 343 | 5.87 | 149 | 9.81 | 249 | 2.44 | 62 | 39 | 18.0 |
| $8 \times 3$ | 200x80 | 13.50 | 343 | 5.87 | 149 | 9.91 | 252 | 2.46 | 62 | 41 | 18.0 |
| $8 \times 4$ | $200 \times 100$ | 13.50 | 343 | 5.87 | 149 | 10.27 | 261 | 2.98 | 76 | 45 | 20.0 |
| $8 \times 6$ | $200 \times 150$ | 13.50 | 343 | 5.87 | 149 | 10.28 | 261 | 2.70 | 69 | 50 | 22.0 |
| 10x3 | 250x40 | 15.75 | 400 | 6.79 | 172 | 11.41 | 290 | 2.46 | 62 | 58 | 26.0 |
| 10x4 | $250 \times 100$ | 15.75 | 400 | 6.79 | 172 | 11.77 | 299 | 2.98 | 76 | 60 | 27.0 |
| 10x6 | 250x150 | 15.75 | 400 | 6.79 | 172 | 11.78 | 299 | 2.70 | 69 | 65 | 29.0 |
| 10x8 | $250 \times 200$ | 15.75 | 400 | 6.79 | 172 | 15.50 | 394 | 5.87 | 149 | 70 | 32.0 |
| $12 \times 4$ | $300 \times 100$ | 17.00 | 432 | 7.43 | 189 | 13.27 | 337 | 2.98 | 76 | 77 | 35.0 |
| 12x6 | $300 \times 150$ | 17.00 | 432 | 7.43 | 189 | 13.28 | 337 | 2.70 | 69 | 81 | 36.0 |
| 12x8 | $300 \times 200$ | 17.00 | 432 | 7.43 | 189 | 17.00 | 432 | 5.87 | 149 | 89 | 40.0 |
| $12 \times 10$ | $300 \times 250$ | 17.00 | 432 | 7.43 | 189 | 17.75 | 451 | 6.79 | 172 | 94 | 43.0 |
| $14 \times 6$ | $350 \times 150$ | 19.50 | 495 | 6.87 | 174 | 13.80 | 351 | 2.70 | 69 | 130 | 59.0 |
| 14x8 | $350 \times 200$ | 19.50 | 495 | 6.87 | 174 | 17.52 | 445 | 5.87 | 149 | 137 | 62.0 |
| 14×10 | $350 \times 250$ | 19.50 | 495 | 6.87 | 174 | 18.27 | 464 | 6.79 | 172 | 144 | 65.0 |
| $14 \times 12$ | $350 \times 300$ | 19.50 | 495 | 6.87 | 174 | 19.02 | 483 | 7.43 | 189 | 152 | 68.0 |
| 16x8 | $400 \times 200$ | 21.25 | 540 | 7.65 | 194 | 18.53 | 471 | 5.87 | 149 | 168 | 76.0 |
| 16x10 | $400 \times 250$ | 21.25 | 540 | 7.65 | 194 | 19.28 | 490 | 6.79 | 172 | 174 | 78.0 |
| $16 \times 12$ | $400 \times 300$ | 21.25 | 540 | 7.65 | 194 | 20.03 | 509 | 7.43 | 189 | 183 | 82.0 |
| $16 \times 14$ | $400 \times 350$ | 21.25 | 540 | 7.65 | 194 | 20.03 | 509 | 6.87 | 174 | 192 | 86.0 |
| $18 \times 10$ | $450 \times 250$ | 26.38 | 670 | 11.88 | 302 | 22.27 | 566 | 6.79 | 172 | 340 | 153.0 |
| $18 \times 12$ | $450 \times 300$ | 26.38 | 670 | 11.88 | 302 | 23.02 | 585 | 7.43 | 189 | 355 | 160.0 |
| $18 \times 14$ | $450 \times 350$ | 26.38 | 670 | 11.88 | 302 | 21.02 | 534 | 6.87 | 174 | 370 | 167.0 |
| $18 \times 16$ | $450 \times 400$ | 26.38 | 670 | 11.88 | 302 | 22.02 | 559 | 7.65 | 194 | 390 | 176.0 |
| 20x12 | $500 \times 300$ | 31.25 | 794 | 13.92 | 354 | 24.52 | 623 | 7.43 | 189 | 380 | 171.0 |
| 20x14 | $500 \times 350$ | 31.25 | 794 | 13.92 | 354 | 22.52 | 572 | 6.87 | 174 | 390 | 176.0 |
| $20 \times 16$ | 500x400 | 31.25 | 794 | 13.92 | 354 | 23.52 | 597 | 7.65 | 194 | 410 | 185.0 |
| $20 \times 18$ | $500 \times 400$ | 31.25 | 794 | 13.92 | 354 | 26.77 | 680 | 11.88 | 302 | 440 | 198.0 |
| 24×14 | $600 \times 350$ | 35.00 | 889 | 17.10 | 434 | 25.02 | 636 | 6.87 | 174 | 490 | 221.0 |
| $24 \times 16$ | $600 \times 400$ | 35.00 | 889 | 17.10 | 434 | 26.02 | 661 | 7.65 | 194 | 500 | 225.0 |
| $24 \times 18$ | 600x450 | 35.00 | 889 | 17.10 | 434 | 29.27 | 743 | 11.88 | 302 | 520 | 234.0 |
| $24 \times 20$ | 600x500 | 35.00 | 889 | 17.10 | 434 | 32.77 | 832 | 13.92 | 354 | 550 | 248.0 |

${ }^{(1)}$ Nominal make-up dimension for drawing layout work only using non-threaded spigots. Do not use for assembly dimensions.

View of Fitting Illustrations


Reducing Tee

## Concentric Reducers

| Pipe Size |  | A |  | $X_{1}{ }^{(1)}$ |  | $\mathrm{X}_{2}{ }^{(1)}$ |  | Weight |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | in | mm | in | mm | in | mm | lbs | kg |
| $3 \times 2$ | $80 \times 50$ | 6.22 | 158 | 2.46 | 62 | 6.99 | 178 | 19 | 9.0 |
| $4 \times 2$ | $100 \times 50$ | 7.46 | 189 | 2.98 | 76 | 7.46 | 189 | 28 | 13.0 |
| $4 \times 3$ | $100 \times 80$ | 7.46 | 189 | 2.98 | 76 | 7.46 | 189 | 31 | 14.0 |
| $6 \times 2$ | $150 \times 50$ | 9.53 | 242 | 2.70 | 69 | 8.45 | 215 | 36 | 16.0 |
| $6 \times 3$ | $150 \times 80$ | 9.53 | 242 | 2.70 | 69 | 8.55 | 217 | 38 | 17.0 |
| $6 \times 4$ | $150 \times 100$ | 9.53 | 242 | 2.70 | 69 | 8.91 | 226 | 45 | 20.0 |
| $8 \times 2$ | $200 \times 50$ | 13.50 | 343 | 5.87 | 149 | 9.81 | 249 | 39 | 18.0 |
| $8 \times 3$ | 200x80 | 13.50 | 343 | 5.87 | 149 | 9.91 | 252 | 41 | 18.0 |
| $8 \times 4$ | $200 \times 100$ | 13.50 | 343 | 5.87 | 149 | 10.27 | 261 | 45 | 20.0 |
| $8 \times 6$ | $200 \times 150$ | 13.50 | 343 | 5.87 | 149 | 10.28 | 261 | 50 | 22.0 |
| 10x3 | $250 \times 40$ | 15.75 | 400 | 6.79 | 172 | 11.41 | 290 | 58 | 26.0 |
| $10 \times 4$ | $250 \times 100$ | 15.75 | 400 | 6.79 | 172 | 11.77 | 299 | 60 | 27.0 |
| 10x6 | $250 \times 150$ | 15.75 | 400 | 6.79 | 172 | 11.78 | 299 | 65 | 29.0 |
| 10x8 | $250 \times 200$ | 15.75 | 400 | 6.79 | 172 | 15.50 | 394 | 70 | 32.0 |
| $12 \times 4$ | $300 \times 100$ | 17.00 | 432 | 7.43 | 189 | 13.27 | 337 | 77 | 35.0 |
| 12x6 | $300 \times 150$ | 17.00 | 432 | 7.43 | 189 | 13.28 | 337 | 81 | 36.0 |
| 12x8 | $300 \times 200$ | 17.00 | 432 | 7.43 | 189 | 17.00 | 432 | 89 | 40.0 |
| $12 \times 10$ | $300 \times 250$ | 17.00 | 432 | 7.43 | 189 | 17.75 | 451 | 94 | 43.0 |
| $14 \times 6$ | $350 \times 150$ | 19.50 | 495 | 6.87 | 174 | 13.80 | 351 | 130 | 59.0 |
| 14x8 | $350 \times 200$ | 19.50 | 495 | 6.87 | 174 | 17.52 | 445 | 137 | 62.0 |
| $14 \times 10$ | $350 \times 250$ | 19.50 | 495 | 6.87 | 174 | 18.27 | 464 | 144 | 65.0 |
| $14 \times 12$ | $350 \times 300$ | 19.50 | 495 | 6.87 | 174 | 19.02 | 483 | 152 | 68.0 |
| 16x8 | $400 \times 200$ | 21.25 | 540 | 7.65 | 194 | 18.53 | 471 | 168 | 76.0 |

${ }^{(1)}$ Nominal make-up dimension for drawing layout work only using non-threaded spigots. Do not use for assembly dimensions.


Concentric Reducer

Flanges

| Pipe Size |  | A |  | B |  | D |  | 0 |  | $\mathbf{X}^{(1)}$ |  | Hole Size |  | \# of <br> Bolts | Max Bolt Torque |  | Weight |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | in | mm | in | mm | in | mm | in | mm | in | mm | in | mm |  | ft•lbs | $\mathrm{N} \cdot \mathrm{m}$ | lbs | kg |
| ANSI 150 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2 | 50 | 2.92 | 74 | 2.75 | 70 | 4.75 | 121 | 6.19 | 157 | 2.39 | 61 | 0.750 | 19 | 4 | 100 | 135 | 3 | 1.3 |
| 3 | 80 | 3.21 | 82 | 3.00 | 76 | 6.00 | 152 | 7.69 | 195 | 3.57 | 91 | 0.750 | 19 | 4 | 100 | 135 | 5 | 2.4 |
| 4 | 100 | 3.74 | 95 | 3.50 | 89 | 7.50 | 191 | 9.19 | 233 | 4.60 | 117 | 0.750 | 19 | 8 | 100 | 135 | 9 | 4.0 |
| 6 | 150 | 4.22 | 107 | 3.95 | 100 | 9.50 | 241 | 11.19 | 284 | 6.70 | 170 | 0.875 | 22 | 8 | 100 | 135 | 14 | 6.1 |
| ANSI 300 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2 | 50 | 3.00 | 76 | 2.75 | 70 | 5.00 | 127 | 6.50 | 165 | 2.67 | 68 | 0.750 | 19 | 8 | 100 | 135 | 3 | 1.4 |
| 3 | 80 | 3.25 | 83 | 3.00 | 76 | 6.63 | 168 | 8.25 | 210 | 2.83 | 72 | 0.875 | 22 | 8 | 100 | 135 | 6 | 2.7 |
| 4 | 100 | 3.75 | 95 | 3.50 | 89 | 7.88 | 200 | 10.00 | 254 | 3.30 | 85 | 0.875 | 22 | 8 | 100 | 135 | 10 | 4.5 |
| 6 | 150 | 4.25 | 108 | 4.00 | 102 | 10.63 | 270 | 12.50 | 317 | 3.78 | 96 | 0.875 | 22 | 12 | 100 | 135 | 15 | 6.8 |

## Van Stone Flanges

| Pipe Size |  | A |  | B |  | C |  | D |  | 0 |  | $\mathbf{X}^{(1)}$ |  | Hole Size |  | \# of <br> Bolts | Max Bolt Torque |  | Weight ${ }^{(2)}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | in | mm | in | mm | in | mm | in | mm | in | mm | in | mm | in | mm |  | ft•lbs | $N \cdot m$ | lbs | kg |
| ANSI 150 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2 | 50 | 2.92 | 74 | 2.75 | 70 | 0.75 | 19 | 4.75 | 121 | 6.00 | 152 | 2.67 | 68 | 0.75 | 19 | 4 | 100 | 135 | 6 | 3 |
| 3 | 80 | 3.21 | 82 | 3.00 | 76 | 0.75 | 19 | 6.00 | 152 | 7.50 | 191 | 2.83 | 72 | 0.75 | 19 | 4 | 100 | 135 | 10 | 4 |
| 4 | 100 | 3.74 | 95 | 3.50 | 89 | 1.00 | 25 | 7.50 | 191 | 9.00 | 229 | 3.30 | 84 | 0.75 | 19 | 8 | 100 | 135 | 15 | 7 |
| 6 | 150 | 4.22 | 107 | 3.95 | 100 | 1.00 | 25 | 9.50 | 241 | 11.00 | 279 | 3.78 | 96 | 0.88 | 22 | 8 | 100 | 135 | 24 | 11 |
| 8 | 200 | 5.00 | 127 | 4.75 | 121 | 1.50 | 38 | 11.75 | 298 | 13.50 | 343 | 4.50 | 114 | 0.88 | 22 | 8 | 200 | 271 | 46 | 21 |
| 10 | 250 | 6.25 | 159 | 6.00 | 152 | 1.88 | 48 | 14.25 | 362 | 16.00 | 406 | 5.75 | 146 | 1.00 | 25 | 12 | 200 | 271 | 74 | 34 |
| 12 | 300 | 7.50 | 191 | 7.25 | 184 | 1.88 | 48 | 17.00 | 432 | 19.00 | 483 | 7.00 | 178 | 1.00 | 25 | 12 | 200 | 271 | 114 | 52 |
| 14 | 350 | 7.00 | 178 | 6.50 | 165 | 1.88 | 48 | 18.75 | 476 | 20.75 | 527 | 6.25 | 159 | 1.13 | 29 | 12 | 200 | 271 | 124 | 56 |
| 16 | 400 | 7.87 | 200 | 7.38 | 187 | 2.25 | 57 | 21.25 | 540 | 23.25 | 591 | 7.12 | 181 | 1.13 | 29 | 16 | 200 | 271 | 180 | 82 |
| 18 | 450 | 9.00 | 229 | 8.50 | 216 | 2.25 | 57 | 22.75 | 578 | 25.00 | 635 | 8.00 | 203 | 1.25 | 32 | 16 | 200 | 271 | 191 | 87 |
| 20 | 500 | 9.88 | 251 | 9.38 | 238 | 2.25 | 57 | 25.00 | 635 | 27.50 | 699 | 8.88 | 226 | 1.25 | 32 | 20 | 200 | 271 | 235 | 107 |
| 24 | 600 | 11.75 | 298 | 11.25 | 286 | 2.25 | 57 | 29.50 | 749 | 32.00 | 813 | 10.45 | 265 | 1.38 | 35 | 20 | 200 | 271 | 303 | 137 |

${ }^{(1)} \mathrm{X}$ dimension is a nominal make-up dimension for drawing layout work only. Do not use for assembly dimensions.
${ }^{(2)}$ Weights are for the fiberglass Stub End and 2-piece Galvanized steel bolt ring combination.

View of Fitting Illustrations


Flange


Van Stone Flange

## Van Stone Flanges

| Pipe Size |  | A |  | B |  | C |  | D |  | 0 |  | $\mathbf{X}^{(1)}$ |  | Hole Size |  | \# of <br> Bolts | Max Bolt Torque |  | Weight ${ }^{(2)}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | in | mm | in | mm | in | mm | in | mm | in | mm | in | mm | in | mm |  | ft•lbs | $\mathrm{N} \cdot \mathrm{m}$ | lbs | kg |
| ANSI 300 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2 | 50 | 2.92 | 74 | 2.75 | 70 | 0.75 | 19 | 5.00 | 127 | 6.50 | 165 | 2.67 | 68 | 0.75 | 19 | 8 | 100 | 135 | 7 | 3 |
| 3 | 80 | 3.21 | 82 | 3.00 | 76 | 0.75 | 19 | 6.63 | 168 | 8.25 | 210 | 2.83 | 72 | 0.88 | 22 | 8 | 100 | 135 | 12 | 5 |
| 4 | 100 | 3.74 | 95 | 3.50 | 89 | 1.00 | 25 | 7.88 | 200 | 10.00 | 254 | 3.30 | 84 | 0.88 | 22 | 8 | 100 | 135 | 19 | 8 |
| 6 | 150 | 4.22 | 107 | 3.95 | 100 | 1.00 | 25 | 10.63 | 270 | 12.50 | 318 | 3.78 | 96 | 0.88 | 22 | 12 | 100 | 135 | 32 | 14 |
| 8 | 200 | 5.00 | 127 | 4.75 | 121 | 1.50 | 38 | 13.00 | 330 | 15.00 | 381 | 4.50 | 114 | 1.00 | 25 | 12 | 200 | 271 | 51 | 23 |
| 10 | 250 | 6.25 | 159 | 6.00 | 152 | 1.88 | 48 | 15.25 | 387 | 17.50 | 445 | 5.75 | 146 | 1.13 | 29 | 16 | 200 | 271 | 78 | 36 |
| 12 | 300 | 7.50 | 191 | 7.25 | 184 | 1.88 | 48 | 17.75 | 451 | 20.50 | 521 | 7.00 | 178 | 1.25 | 32 | 16 | 200 | 271 | 113 | 51 |
| 14 | 350 | 7.00 | 177 | 6.50 | 165 | 1.88 | 48 | 20.25 | 514 | 23.00 | 584 | 6.25 | 159 | 1.25 | 32 | 20 | 200 | 271 | 130 | 59 |
| 16 | 400 | 7.87 | 200 | 7.38 | 187 | 2.25 | 57 | 22.50 | 572 | 25.50 | 648 | 7.12 | 181 | 1.38 | 35 | 20 | 200 | 271 | 174 | 79 |
| 18 | 450 | 9.00 | 229 | 8.50 | 216 | 2.25 | 57 | 24.75 | 629 | 28.00 | 711 | 8.00 | 203 | 1.38 | 35 | 24 | 200 | 271 | 250 | 113 |
| 20 | 500 | 9.88 | 251 | 9.38 | 238 | 2.25 | 57 | 27.00 | 686 | 30.50 | 775 | 8.88 | 226 | 1.38 | 35 | 24 | 200 | 271 | 296 | 134 |
| 24 | 600 | 11.75 | 298 | 11.25 | 286 | 2.25 | 57 | 32.00 | 813 | 36.00 | 914 | 10.45 | 265 | 1.63 | 41 | 24 | 200 | 271 | 447 | 203 |

${ }^{(1)} \mathrm{X}$ dimension is a nominal make-up dimension for drawing layout work only. Do not use for assembly dimensions.
${ }^{(2)}$ Weights are for the fiberglass Stub End and 2-piece Galvanized steel bolt ring combination.

## Nipples

| Pipe Size |  | 4 | 6 | 8 | 10 | 12 | 16 | 24 | 36 | 48 | 54 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | 100 | 150 | 200 | 250 | 300 | 400 | 600 | 900 | 1200 | 1350 |
| 2 | 50 |  | X | X |  |  |  |  |  |  |  |
| 3 | 80 |  | X | X |  |  |  |  |  |  |  |
| 4 | 100 |  | X | X |  |  |  |  |  |  |  |
| 6 | 150 |  | X | X |  | X | X |  |  |  |  |
| 8 | 200 |  |  |  |  |  | X | X |  |  |  |
| 10 | 250 |  |  |  |  |  | X | X | X |  |  |
| 12 | 300 |  |  |  |  |  | X | X | X |  |  |
| 14 | 350 |  |  |  |  |  | X | X | X |  |  |
| 16 | 400 |  |  |  |  |  | X | X | X |  |  |
| 18 | 450 |  |  |  |  |  |  |  | X |  |  |
| 20 | 500 |  |  |  |  |  |  |  | X |  |  |
| 24 | 600 |  |  |  |  |  |  |  | X |  |  |

[^25]

Van Stone Flange


Nipple

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## Fiber Glass Systems

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Fax: 2104777560

## GREEN THREAD"' HP 32/40 Fittings

## 2"-16" Fittings and Accessories

Fittings are filament wound with a reinforced epoxy inner liner and compatible with HP 32/40 bar piping systems. Sizes 2"-12" are rated to 40 bar, and 14" and 16" are rated to 32 bar

## $90^{\circ}$ Elbows <br> Bell x Bell



| Diameter |  | A |  | $\mathbf{X}^{(1)}$ |  | Weight |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | $\mathbf{m m}$ | in | $\mathbf{m m}$ | in | $\mathbf{m m}$ | lbs | kg |
| 2 | 50 | 6.25 | 159 | 2.50 | 64 | 8.0 | 3.6 |
| 3 | 75 | 9.00 | 229 | 3.25 | 83 | 12.0 | 5.4 |
| 4 | 100 | 11.25 | 286 | 4.00 | 102 | 16.0 | 7.3 |
| 6 | 150 | 14.75 | 375 | 4.50 | 114 | 24.0 | 10.9 |
| 8 | 200 | 21.75 | 552 | 7.75 | 197 | 46.3 | 21.0 |
| 10 | 250 | 26.00 | 660 | 8.88 | 225 | 92.6 | 42.0 |
| 12 | 300 | 30.50 | 775 | 10.25 | 260 | 140 | 63.5 |
| 14 | 350 | 33.00 | 838 | 8.75 | 222 | 447 | 203 |
| 16 | 400 | 37.00 | 940 | 10.00 | 254 | 587 | 267 |

## $45^{\circ}$ Elbows <br> Bell x Bell



| Diameter |  | A |  | $\mathbf{X}^{(1)}$ |  | Weight |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | in | $\mathbf{m m}$ | in | $\mathbf{m m}$ | lbs | kg |
| 2 | 50 | 4.50 | 114 | 2.50 | 64 | 13.7 | 6.2 |
| 3 | 75 | 6.25 | 159 | 3.25 | 83 | 17.1 | 7.8 |
| 4 | 100 | 7.75 | 197 | 4.00 | 102 | 27.5 | 12.5 |
| 6 | 150 | 9.50 | 241 | 4.50 | 114 | 32.7 | 14.9 |
| 8 | 200 | 14.75 | 375 | 7.75 | 197 | 92.5 | 42.0 |
| 10 | 250 | 17.00 | 432 | 8.88 | 225 | 145 | 65.8 |
| 12 | 300 | 20.00 | 508 | 10.25 | 260 | 200 | 90.7 |
| 14 | 350 | 20.75 | 527 | 8.75 | 222 | 235 | 107 |
| 16 | 400 | 23.00 | 584 | 10.00 | 254 | 309 | 140 |

[^26]Tees

## Bell $x$ Bell $x$ Bell

## Reducing Tees

Bell x Bell x Bell


| Diameter |  | AT |  | AS |  | $\mathbf{X}_{1}{ }^{(1)}$ |  | $\mathbf{X}_{2}{ }^{(1)}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | in | mm | in | mm | in | mm | in | mm |
| $3 \times 2$ | $75 \times 50$ | 7.19 | 183 | 7.01 | 178 | 3.25 | 83 | 2.50 | 64 |
| $4 \times 3$ | $100 \times 75$ | 8.87 | 225 | 8.45 | 215 | 4.00 | 102 | 3.25 | 83 |
| $4 \times 2$ | $100 \times 50$ | 8.87 | 225 | 7.48 | 190 | 4.00 | 102 | 2.50 | 64 |
| $6 \times 4$ | $150 \times 100$ | 11.50 | 292 | 10.39 | 264 | 4.50 | 114 | 4.00 | 102 |
| $6 \times 3$ | $150 \times 75$ | 11.50 | 292 | 9.51 | 242 | 4.50 | 114 | 3.25 | 83 |
| $8 \times 6$ | $200 \times 150$ | 15.75 | 400 | 12.25 | 311 | 7.75 | 197 | 4.50 | 114 |
| $8 \times 4$ | $200 \times 100$ | 15.75 | 400 | 11.75 | 298 | 7.75 | 197 | 4.00 | 102 |
| $10 \times 8$ | $250 \times 200$ | 18.38 | 467 | 17.75 | 451 | 8.87 | 225 | 7.75 | 197 |
| $10 \times 6$ | $250 \times 150$ | 18.38 | 467 | 13.75 | 349 | 8.87 | 225 | 4.50 | 114 |
| $12 \times 10$ | $300 \times 250$ | 20.50 | 521 | 20.38 | 518 | 10.25 | 260 | 8.87 | 225 |
| $12 \times 8$ | $300 \times 200$ | 20.50 | 521 | 19.25 | 489 | 10.25 | 260 | 7.75 | 197 |
| $14 \times 12$ | $350 \times 300$ | 22.50 | 571 | 22.52 | 572 | 8.75 | 222 | 10.25 | 260 |
| $14 \times 10$ | $350 \times 250$ | 22.50 | 571 | 20.90 | 531 | 8.75 | 222 | 8.75 | 222 |
| $16 \times 14$ | $400 \times 350$ | 24.38 | 619 | 23.03 | 585 | 9.75 | 251 | 8.75 | 222 |
| $16 \times 12$ | $400 \times 300$ | 24.38 | 619 | 23.53 | 598 | 9.75 | 251 | 10.25 | 260 |

${ }^{(1)}$ Nominal make-up dimension for drawing layout work only. Do not use for assembly dimensions.

Concentric Reducer Bell x Bell


| Diameter |  | A |  | $\mathbf{X}_{1}{ }^{(1)}$ |  | $\mathbf{X}_{2}{ }^{(1)}$ |  | Weight |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | in | mm | in | mm | in | $\mathbf{m m}$ | lbs | kg |
| $3 \times 2$ | $75 \times 50$ | 9.25 | 235 | 3.25 | 83 | 2.50 | 64 | 8.1 | 3.7 |
| $4 \times 3$ | $100 \times 75$ | 11.75 | 298 | 4.00 | 102 | 3.25 | 83 | 11.7 | 5.3 |
| $6 \times 4$ | $150 \times 100$ | 15.00 | 381 | 4.50 | 114 | 4.00 | 102 | 15.4 | 7.0 |
| $8 \times 6$ | $200 \times 150$ | 21.00 | 533 | 7.75 | 167 | 4.50 | 114 | 27.0 | 12.2 |
| $10 \times 8$ | $250 \times 200$ | 26.00 | 660 | 8.875 | 229 | 7.75 | 167 | 44.5 | 20.2 |
| $12 \times 10$ | $300 \times 250$ | 29.75 | 756 | 10.25 | 261 | 8.875 | 225 | 69.4 | 31.5 |
| $14 \times 12$ | $350 \times 300$ | 32.75 | 834 | 8.875 | 225 | 10.25 | 261 | 107 | 48.4 |
| $16 \times 14$ | $400 \times 350$ | 35.75 | 906 | 10.00 | 254 | 8.75 | 222 | 154 | 70.1 |

Sleeve Couplings
Bell x Bell


Flanges
ANSI 16.5 Class \#150


[^27]| Diameter |  | A |  | $\mathbf{X}^{(1)}$ |  | Weight |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | $\mathbf{m m}$ | in | $\mathbf{m m}$ | in | $\mathbf{m m}$ | lbs | $\mathbf{k g}$ |
| 2 | 50 | 6.50 | 161 | 2.50 | 64 | 0.9 | 0.4 |
| 3 | 75 | 8.00 | 203 | 3.25 | 83 | 1.9 | 0.8 |
| 4 | 100 | 9.50 | 241 | 4.00 | 102 | 2.0 | 0.9 |
| 6 | 150 | 10.50 | 266 | 4.50 | 114 | 4.4 | 2.0 |
| 8 | 200 | 18.50 | 470 | 7.75 | 197 | 11.5 | 5.2 |
| 10 | 250 | 20.75 | 527 | 8.88 | 225 | 17.6 | 8.0 |
| 12 | 300 | 24.00 | 610 | 10.25 | 260 | 25.4 | 11.5 |
| 14 | 350 | 25.00 | 635 | 8.75 | 222 | 156 | 71.0 |
| 16 | 400 | 27.25 | 692 | 10.00 | 254 | 206 | 93.4 |


| Diameter | A | $\mathbf{B}$ | $\mathbf{D}$ | $\mathbf{O}$ | $\mathbf{X}^{(1)}$ |  <br> Quantity |  | Max Bolt <br> Torque | Wgt. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | in | in | in | in | in | in | Bolts | $\mathbf{f t} \cdot \mathrm{lbs}$ | lbs |
| 2 | 3.00 | 2.75 | 4.75 | 6.00 | 2.75 | 0.75 | 4 | 100 | 4.75 |
| 3 | 3.25 | 3.00 | 6.00 | 7.50 | 3.00 | 0.75 | 4 | 100 | 7.5 |
| 4 | 3.75 | 3.50 | 7.50 | 9.00 | 3.50 | 0.75 | 8 | 150 | 11.9 |
| 6 | 4.25 | 4.00 | 9.50 | 11.00 | 4.00 | 0.88 | 8 | 150 | 17.4 |


| Diameter | $\mathbf{B}$ | $\mathbf{C}$ | $\mathbf{D}$ | $\mathbf{O}$ | $\mathbf{X}^{(1)}$ |  <br> Quantity |  | Max Bolt <br> Torque | $\mathbf{\text { Wgt. }}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{m m}$ | $\mathbf{m m}$ | $\mathbf{m m}$ | $\mathbf{m m}$ | $\mathbf{m m}$ | $\mathbf{m m}$ | $\mathbf{m m}$ | Bolts | $\mathbf{N} \cdot \mathbf{M}$ | $\mathbf{k g}$ |
| 50 | 74 | 70 | 121 | 152 | 70 | 19.0 | 4 | 136 | 2.2 |
| 75 | 82 | 76 | 152 | 190 | 76 | 19.0 | 4 | 136 | 3.4 |
| 100 | 95 | 89 | 191 | 228 | 89 | 19.0 | 8 | 204 | 5.4 |
| 150 | 107 | 100 | 241 | 279 | 101 | 22.2 | 8 | 204 | 7.9 |

Flanges
ANSI 16.5 Class \#300


| Diameter | $\mathbf{A}$ | $\mathbf{B}$ | $\mathbf{D}$ | $\mathbf{O}$ | $\mathbf{X}^{(1)}$ |  <br> Quantity |  | Max Bolt <br> Torque | $\mathbf{W g t .}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{m m}$ | $\mathbf{m m}$ | $\mathbf{m m}$ | $\mathbf{m m}$ | $\mathbf{m m}$ | $\mathbf{m m}$ | $\mathbf{m m}$ | $\mathbf{B o l t s}$ | $\mathbf{N} \cdot \mathbf{M}$ | $\mathbf{k g}$ |
| 50 | 74 | 70 | 127 | 165 | 68 | 19 | 8 | 136 | 2.5 |
| 75 | 82 | 76 | 168 | 210 | 75 | 22 | 8 | 136 | 4.1 |
| 100 | 95 | 89 | 200 | 254 | 89 | 22 | 8 | 204 | 7.1 |
| 150 | 107 | 100 | 270 | 317 | 101 | 22 | 12 | 204 | 11.6 |

Van Stone Flanges
ANSI 16.5
Class \#300

(1) Nominal make-up
dimension for drawing
layout work only. Do
not use for assembly

| Diameter | A | B | C | D | 0 | $X^{(1)}$ | Bolt Size \& Quantity |  | Max Bolt Torque | Wgt. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | in | in | in | in | in | in | in | Bolts | ft - Ibs | Ibs |
| 8 | 5.00 | 4.75 | 1.50 | 13.00 | 15.00 | 5.00 | 1.00 | 12 | 200 | 50.7 |
| 10 | 6.25 | 6.00 | 1.88 | 15.25 | 17.50 | 6.00 | 1.125 | 16 | 200 | 78.4 |
| 12 | 7.50 | 7.25 | 1.88 | 17.75 | 20.50 | 7.50 | 1.25 | 16 | 200 | 113 |
| 14 | 7.00 | 6.50 | 2.25 | 20.25 | 23.00 | 7.00 | 1.25 | 20 | 250 | 130 |
| 16 | 7.88 | 7.38 | 2.25 | 22.50 | 25.50 | 7.75 | 1.375 | 20 | 250 | 174 |
| mm | mm | mm | mm | mm | mm | $\mathrm{mm}^{(1)}$ | mm | Bolts | N • m | kg |
| 200 | 127 | 121 | 38 | 330 | 381 | 124 | 25 | 12 | 272 | 23.0 |
| 250 | 159 | 152 | 48 | 387 | 445 | 156 | 28 | 16 | 272 | 35.6 |
| 300 | 191 | 184 | 48 | 451 | 521 | 187 | 31 | 16 | 272 | 51.3 |
| 350 | 178 | 165 | 57 | 514 | 584 | 175 | 31 | 20 | 340 | 58.9 |
| 400 | 200 | 187 | 57 | 572 | 648 | 197 | 35 | 20 | 340 | 78.9 |

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## SILVER STREAK"' FITTINGS DIMENSIONS

- Silver Streak piping and fittings are designed especially for abrasive and corrosive services such as limestone and gypsum slurries, found in flue gas desulfurization (FGD) scrubber applications.
- Silver Streak piping systems are designed to operate at temperatures up to $225^{\circ} \mathrm{F}$ and pressures up to 225 psig.
- All bell end and assembled flanged* Silver Streak fittings are rated for service up to 225 psig.
- A complete line of standard long-radius fittings are available. Odd degree elbows are available on special order.
- Fittings are constructed with the same abrasion-resistant additives as the pipe.
- All fittings, except compression molded, have a nominal corrosion/abrasion barrier of 100 mils.


| Nominal <br> Pipe Size <br> (In.) | $\mathbf{2 2 5}$ psig <br> $\mathbf{A}$ <br> (In.) | $\mathbf{1 5 0} \mathbf{~ p s i g}$ <br> $\mathbf{B}$ <br> (In.) | $\mathbf{2 2 5} \mathbf{~ p s i g}$ <br> $\mathbf{B}$ <br> (In.) | $\mathbf{X ( 1 )}$ <br> (In.) | $\mathbf{B} \times \mathbf{B}$ <br> Weight <br> (lbs) | F x F <br> Weight <br> (lbs) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2 | 6.31 | -- | 9.50 | 2.64 | 8.80 | 11.80 |
| 3 | 8.00 | -- | 11.62 | 2.86 | 13.20 | 19.20 |
| 4 | 9.75 | -- | 13.50 | 3.13 | 17.60 | 26.20 |
| 6 | 12.75 | -- | 17.00 | 2.76 | 26.50 | 38.00 |
| 8 | 19.50 | 16.12 | $24.5^{\star}$ | 5.28 | 35.00 | 45.00 |
| 10 | 23.25 | 19.88 | $29.0^{\star}$ | 5.12 | 67.00 | 86.00 |
| 12 | 27.00 | 23.12 | $33.0^{\star}$ | 6.40 | 101 | 138 |
| 14 | 30.00 | 24.50 | $34.0^{\star}$ | 4.55 | 198 | 256 |
| 16 | 34.00 | 27.87 | $38.0^{\star}$ | 5.61 | 260 | 322 |
| 18 | 36.75 | -- | 47.0 | 6.63 | 353 | 468 |
| 20 | 42.25 | -- | 53.0 | 7.75 | 470 | 609 |
| 24 | 50.00 | -- | 63.0 | 9.25 | 672 | 866 |

$45^{\circ}$ Elbow


BELL x BELL


| Nominal <br> Pipe Size <br> (In.) | $\mathbf{2 2 5}$ psig <br> $\mathbf{A}$ <br> (In.) | $\mathbf{1 5 0} \mathbf{~ p s i g}$ <br> $\mathbf{B}$ <br> (In.) | $\mathbf{2 2 5}$ psig <br> $\mathbf{B}$ <br> (In.) | $\mathbf{X ( 1 )}^{(\mathbf{I n} .)}$ | $\mathbf{B} \times \mathbf{B}$ <br> Weight <br> (Ibs) | F x F <br> Weight <br> (lbs) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2 | 4.56 | -- | 7.50 | 2.64 | 5.0 | 8.40 |
| 3 | 5.25 | -- | 8.62 | 2.86 | 8.1 | 14.10 |
| 4 | 6.25 | -- | 9.62 | 3.13 | 10.8 | 19.40 |
| 6 | 7.50 | -- | 11.37 | 2.76 | 16.2 | 27.70 |
| 8 | 12.50 | 9.00 | $17.5^{*}$ | 5.28 | 21.6 | 32.00 |
| 10 | 14.50 | 11.12 | $20.3^{*}$ | 5.12 | 43.0 | 62.00 |
| 12 | 16.50 | 12.62 | $23.0^{*}$ | 6.40 | 65.0 | 102 |
| 14 | 17.62 | 12.25 | $22.0^{*}$ | 4.55 | 109 | 167 |
| 16 | 20.00 | 13.75 | $24.0^{*}$ | 5.61 | 144 | 206 |
| 18 | 20.93 | -- | 31.0 | 6.63 | 209 | 324 |
| 20 | 24.68 | -- | 36.0 | 7.75 | 259 | 398 |
| 24 | 28.91 | -- | 42.0 | 9.25 | 389 | 583 |

$B=B E L L \quad F=F L A N G E$
(1) This is a nominal make-up dimension for drawing layout work only. Do not use for assembly dimensions.

* Special Order
 $\times$ FLANGE

| Nominal <br> Pipe Size <br> (In.) | $\mathbf{2 2 5}$ psig <br> A <br> (In.) | $\mathbf{1 5 0} \mathbf{~ p s i g}$ <br> B <br> (In.) | $\mathbf{2 2 5}$ psig <br> B <br> (In.) | $\mathbf{X ( 1 )}$ <br> (In.) | B x B x B <br> Weight <br> (Ibs) | F x F x F <br> Weight <br> (Ibs) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2 | 5.56 | -- | 8.37 | 2.64 | 6.8 | 11.2 |
| 3 | 6.25 | -- | 9.37 | 2.86 | 10.1 | 19.1 |
| 4 | 7.50 | -- | 10.62 | 3.13 | 13.5 | 26.4 |
| 6 | 9.50 | -- | 13.12 | 2.76 | 27.5 | 45.0 |
| 8 | 13.50 | 9.00 | 13.5 | $5.28^{*}$ | 41.0 | 56.0 |
| 10 | 15.75 | 11.00 | 15.8 | $5.12^{*}$ | 56.0 | 85.0 |
| 12 | 17.00 | 12.00 | 17.0 | $6.40^{*}$ | 88.0 | 144 |
| 14 | 19.50 | 14.00 | 19.5 | $4.55^{*}$ | 120 | 207 |
| 16 | 21.25 | 15.00 | 21.3 | $5.61^{*}$ | 150 | 243 |
| 18 | 22.38 | -- | 33.0 | 6.63 | 195 | 300 |
| 20 | 26.25 | -- | 38.0 | 7.75 | 255 | 371 |
| 24 | 28.00 | -- | 41.0 | 9.25 | 356 | 496 |

Sleeve Coupling


BELL x BELL
NOTE 18"-24" Couplings: If coupling length "A" is critical for a piping system design, please specify "A" dimension when ordering

| Nominal <br> Pipe Size <br> (In.) | A <br> (In.) | $\mathbf{B}$ <br> (In.) | $\mathbf{X ( 2 )}$ <br> (In.) | Max. Operating <br> Pressure <br> (psig) | B X B <br> Weight <br> (Ibs) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 2 | 4.87 | 2.50 | 1.84 | 225 | 0.4 |
| 3 | 6.50 | 3.87 | 2.36 | 225 | 0.8 |
| 4 | 6.50 | 4.87 | 1.99 | 225 | 0.9 |
| 6 | 8.00 | 7.00 | 2.87 | 225 | 1.9 |
| 8 | 10.50 | 9.12 | 3.47 | 225 | 3.4 |
| 10 | 11.00 | 11.12 | 4.34 | 225 | 5.2 |
| 12 | 12.50 | 13.12 | 4.82 | 225 | 7.5 |
| 14 | 15.00 | 15.12 | 5.47 | 225 | 11.2 |
| 16 | 17.00 | 17.25 | 6.27 | 225 | 16.0 |
| 18 | 16.00 | 18.75 | 6.88 | 225 | 22.7 |
| 20 | 19.00 | 20.75 | 8.00 | 225 | 27.5 |
| 24 | 23.00 | 25.00 | 10.00 | 225 | 38.0 |

Nipple

| Nominal Pipe Size (In.) | Nipple Length (In.) |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 6 | (lbs) | 8 | (lbs) | 12 | (lbs) | 16 | (lbs) | 24 | (lbs) | 36 | (lbs) |
| 2 | - | 0.6 | - | 0.7 | -- | -- | -- | -- | -- | -- | -- | -- |
| 3 | - | 0.8 | - | 1.1 | -- | -- | -- | -- | -- | -- | -- | -- |
| 4 | -- | -- | - | 1.4 | -- | -- | -- | -- | -- | -- | -- | -- |
| 6 | -- | -- | - | 2.1 | * | 3.1 | * | 4.1 | -- | -- | -- | -- |
| 8 | -- | -- | -- | -- | - | 4.8 | * | 6.4 | -- | -- | -- | -- |
| 10 | -- | -- | -- | -- | * | 6.1 | * | 8.1 | -- | -- | -- | -- |
| 12 | -- | -- | -- | -- | -- | -- | * | 10.0 | -- | -- | -- | -- |
| 14 | -- | -- | -- | -- | -- | -- | , | 13.3 | -- | -- | -- | -- |
| 16 | -- | -- | -- | -- | -- | -- | * | 17.1 | -- | -- | -- | -- |
| 18 | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | * | 30.0 |
| 20 | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | - | 37.0 |
| 24 | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | - | 51.0 |

- Standard stock.
${ }^{(1)}$ This is a nominal make-up dimension for drawing layout work only. Do not use for assembly dimensions.
* Special order.

Flange


| Nominal <br> Pipe Size <br> (In.) | B | C | CC ${ }^{(1)}$ | D | E | 0 | $\mathrm{X}^{(1)}$ | Max. Operation Pressure (psig) |  | Weight (lbs) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  | Flange | Blind Flange | Flange | Blind Flange |
| 2 | 2.25 | . 75 | . 75 | 4.75 | . 75 D-4 holes | 6.00 | 1.75 | 225 | 150 | 1.3 | 1.3 |
| 3 | 2.62 | 1.37 | 1.00 | 6.00 | . 75 D-4 holes | 7.50 | 2.25 | 225 | 150 | 2.6 | 3.0 |
| 4 | 2.62 | 1.37 | 1.00 | 7.50 | . 75 D-8 holes | 9.00 | 2.25 | 225 | 150 | 3.6 | 4.0 |
| 6 | 3.00 | 1.50 | 1.12 | 9.50 | .875 D-8 holes | 11.00 | 2.75 | 225 | 150 | 4.4 | 6.6 |
| 8 | 4.00 | 1.75 | 1.12 | 11.75 | .875 D-8 holes | 13.50 | 3.25 | 225 | 135 | 9.3 | 10.6 |
| 10 | 4.75 | 2.00 | 1.25 | 14.25 | 1 D-12 holes | 16.00 | 3.75 | 225 | 95 | 16.0 | 16.3 |
| 12 | 5.00 | 2.25 | 1.25 | 17.00 | $1 \mathrm{D}-12$ holes | 19.00 | 3.75 | 225 | 65 | 24.0 | 24.0 |
| 14 | 3.12 | 2.50 | 1.62 | 18.75 | 1.125 D-12 holes | 20.75 | 3.00 | 225 | 150 | 30.0 | 45.0 |
| 16 | 3.12 | 2.50 | 1.87 | 21.25 | 1.125 D-16 holes | 23.25 | 3.00 | 225 | 150 | 37.0 | 67.0 |
| 18 | 9.00 | 2.75 | 2.50 | 22.75 | 1.25 D-16 holes | 25.00 | 6.88 | 225 | 150 | 76.0 | 125 |
| 20 | 11.00 | 2.75 | 2.75 | 25.00 | 1.25 D-20 holes | 27.50 | 8.00 | 225 | 150 | 92.0 | 140 |
| 24 | 13.00 | 3.00 | 3.37 | 29.50 | 1.375 D-20 holes | 32.00 | 10.00 | 225 | 150 | 124.0 | 155 |

Note: All flanges are ANSI B16.5-150 lb. Bolt Hole Circle.
(1)Steel back-up plates must be used to achieve pressure ratings equivalent to the pipe.

| Nominal Reducer Size (In.) | A | Max. Pressure (psig) | $\mathrm{X} 1^{(1)}$ | X2 ${ }^{(1)}$ | B | B x B Weight (lbs) | $F \times F$ Weight (lbs) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $3 \times 2$ | 7.50 | 225 | 2.81 | 2.63 | 14.75* | 7.4 | 14.0 |
| $4 \times 3$ | 9.25 | 225 | 3.13 | 2.63 | 15.38* | 10.7 | 20.6 |
| $4 \times 2$ | 9.00 | 225 | 3.13 | 2.63 | 17.00* | 10.1 | 22.2 |
| $6 \times 4$ | 11.50 | 225 | 2.75 | 3.13 | 18.13* | 14.1 | 26.6 |
| $6 \times 3$ | 11.25 | 225 | 2.75 | 2.68 | 19.63* | 13.4 | 28.8 |
| $6 \times 2$ | 11.00 | 225 | 2.75 | 2.63 | 21.25* | 12.7 | 27.8 |
| $6 \times 4$ | 11.50 | 225 | 2.75 | 3.13 | 18.13* | 14.1 | 26.6 |
| $8 \times 6$ | 16.75 | 225 | 5.25 | 2.75 | 25.00* | 17.1 | 34.0 |
| $8 \times 4$ | 16.75 | 225 | 5.25 | 3.13 | 24.13* | 16.4 | 32.0 |
| $8 \times 3$ | 16.25 | 225 | 5.25 | 2.81 | 24.13* | 15.6 | 31.0 |
| $8 \times 2$ | 16.00 | 225 | 5.25 | 2.63 | 24.13* | 14.8 | 29.7 |
| $10 \times 8$ | 21.00 | 225 | 5.06 | 5.25 | 12.00 | 28.2 | 43.0 |
| $10 \times 6$ | 18.00 | 225 | 5.06 | 2.75 | 12.00 | 24.4 | 42.2 |
| $12 \times 10$ | 23.50 | 225 | 6.40 | 5.12 | 14.00 | 44.0 | 72.0 |
| $14 \times 12$ | 26.25 | 225 | 4.50 | 6.38 | 16.00 | 67.0 | 115 |
| $14 \times 10$ | 26.00 | 225 | 4.50 | 5.06 | 16.00 | 60.0 | 106 |
| $16 \times 14$ | 29.50 | 225 | 5.56 | 4.50 | 18.00 | 98.0 | 158 |
| $16 \times 12$ | 29.00 | 225 | 5.56 | 6.38 | 18.00 | 88.8 | 147.4 |
| $18 \times 16$ | 29.75 | 225 | 6.63 | 5.56 | 46.00* | 110 | 204 |
| $18 \times 14$ | 29.38 | 225 | 6.63 | 4.50 | 46.00* | 100 | 199.1 |
| $20 \times 18$ | 32.00 | 225 | 7.75 | 6.63 | 53.00* | 140 | 229 |
| $20 \times 16$ | 32.88 | 225 | 7.75 | 5.56 | 53.00* | 106 | 223.1 |
| $24 \times 20$ | 46.25 | 225 | 9.25 | 7.75 | 70.00* | 190 | 275 |
| $24 \times 18$ | 36.00 | 225 | 9.25 | 6.63 | 70.00* | 133 | 268.4 |

[^28]
## Saddles



| Size | A | B | Angle <br> C | X | Steady Pressure Rating |
| :---: | :---: | :---: | :---: | :---: | :---: |
| In. | In. | In. | Degree | In. | psi |
| 2x1 | 2.88 | 4.00 | 180 | 1.00 | 225 |
| $2 \times 11 / 2$ | 2.88 | 4.00 | 180 | 1.38 | 225 |
| $3 \times 1$ | 3.50 | 6.00 | 180 | 1.00 | 225 |
| $3 \times 11 / 2$ | 3.50 | 6.00 | 180 | 1.38 | 225 |
| $3 \times 2$ | 4.00 | 6.00 | 180 | 2.64 | 225 |
| 4x1 | 4.00 | 6.00 | 180 | 1.00 | 225 |
| $4 \times 11 / 2$ | 4.00 | 6.00 | 180 | 1.38 | 225 |
| $4 \times 2$ | 4.50 | 6.00 | 180 | 2.64 | 225 |
| $4 \times 3$ | 5.25 | 6.00 | 180 | 2.88 | 150 |
| $6 \times 1$ | 5.00 | 6.00 | 120 | 1.00 | 225 |
| $6 \times 11 / 2$ | 5.00 | 6.00 | 120 | 1.38 | 225 |
| 6x2 | 5.50 | 6.00 | 120 | 2.64 | 225 |
| 6x3 | 6.25 | 6.00 | 120 | 2.88 | 150 |
| 6x4 | 6.38 | 8.00 | 140 | 3.13 | 150 |
| $8 \times 2$ | 8.25 | 9.00 | 120 | 2.64 | 225 |
| $8 \times 3$ | 8.25 | 14.00 | 180 | 2.88 | 225 |
| $8 \times 4$ | 8.64 | 14.00 | 180 | 3.13 | 225 |
| 8x6 | 8.64 | 14.00 | 180 | 2.75 | 125 |
| $10 \times 2$ | 9.25 | 9.00 | 95 | 2.64 | 225 |
| 10x3 | 9.25 | 14.00 | 150 | 2.88 | 225 |
| 10x4 | 9.64 | 16.75 | 180 | 3.13 | 225 |
| 10x6 | 9.64 | 16.75 | 180 | 2.75 | 190 |
| 10x8 | 13.88 | 16.75 | 180 | 5.25 | 100 |
| 12x2 | 10.25 | 10.00 | 90 | 2.64 | 225 |
| $12 \times 3$ | 10.25 | 14.00 | 125 | 2.88 | 225 |
| 12x4 | 10.64 | 17.00 | 155 | 3.13 | 225 |
| 12x6 | 10.64 | 21.00 | 180 | 2.75 | 225 |
| 12x8 | 14.88 | 21.00 | 180 | 5.25 | 150 |
| $12 \times 10$ | 15.64 | 21.00 | 180 | 5.13 | 100 |

## Saddles, Cont'd.



| Size | A | B | Angle C | X | Steady Pressure Rating |
| :---: | :---: | :---: | :---: | :---: | :---: |
| In. | In. | In. | Degree | In. | psi |
| $14 \times 2$ | 11.00 | 12 | 95 | 2.64 | 225 |
| $14 \times 3$ | 11.13 | 15 | 120 | 2.88 | 225 |
| $14 \times 4$ | 11.50 | 17 | 135 | 3.50 | 225 |
| $14 \times 6$ | 11.64 | 21 | 165 | 2.75 | 225 |
| $14 \times 8$ | 15.75 | 21 | 165 | 5.25 | 190 |
| $14 \times 10$ | 15.64 | 26 | 180 | 5.13 | 225 |
| $14 \times 12$ | 17.25 | 26 | 180 | 6.38 | 100 |
| 16x2 | 12.00 | 13 | 90 | 2.64 | 225 |
| 16x3 | 12.13 | 15 | 105 | 2.88 | 225 |
| 16x4 | 12.50 | 17 | 120 | 3.13 | 225 |
| 16x6 | 12.64 | 21 | 145 | 2.75 | 225 |
| 16x8 | 16.75 | 26 | 180 | 5.25 | 225 |
| 16x10 | 17.64 | 26 | 180 | 5.13 | 190 |
| 16x12 | 18.25 | 26 | 180 | 6.38 | 150 |
| 18x2 | 12.88 | 13 | 90 | 2.64 | 225 |
| $18 \times 3$ | 13.25 | 15 | 90 | 2.88 | 225 |
| 18x4 | 13.25 | 17 | 110 | 3.13 | 225 |
| 18x6 | 14.50 | 21 | 130 | 2.75 | 225 |
| $18 \times 8$ | 16.00 | 26 | 160 | 5.25 | 225 |
| $18 \times 10$ | 15.88 | 28 | 180 | 5.13 | 225 |
| $18 \times 12$ | 16.25 | 32 | 180 | 6.38 | 190 |
| 20x2 | 13.88 | 13 | 90 | 2.64 | 225 |
| 20x3 | 14.25 | 15 | 90 | 2.88 | 225 |
| 20x4 | 14.25 | 17 | 95 | 3.50 | 225 |
| 20x6 | 15.50 | 21 | 120 | 2.75 | 225 |
| 20x8 | 17.00 | 26 | 150 | 5.25 | 225 |
| 20x10 | 17.00 | 28 | 160 | 5.13 | 225 |
| 20x12 | 17.25 | 32 | 180 | 6.38 | 190 |
| $24 \times 2$ | 16.00 | 13 | 70 | 2.64 | 225 |
| 24x3 | 16.25 | 15 | 70 | 2.88 | 225 |
| 24x4 | 16.25 | 17 | 80 | 3.13 | 225 |
| 24x6 | 17.64 | 21 | 100 | 2.75 | 225 |
| 24x8 | 19.13 | 26 | 120 | 5.25 | 225 |
| 24×10 | 19.. 00 | 28 | 130 | 5.13 | 225 |
| 24×12 | 19.38 | 32 | 150 | 6.38 | 190 |

## REDUCING TEES


(1) This is a nominal make-up dimension for drawing layout work only Do not use for assembly dimensions.

| Nom. <br> Size | A | $\mathrm{X}^{(1)}$ | B | $\mathrm{X}^{(1)}$ | Nom. <br> Wgt. | Steady <br> Pressure |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| In | In | In | In | In | Lbs | psig |
| $8 \times 6$ | 13.50 | 5.30 | 10.25 | 2.80 | 36 | 225 |
| $8 \times 4$ | 13.50 | 5.30 | 10.25 | 3.10 | 33 | 225 |
| $8 \times 3$ | 13.50 | 5.30 | 9.88 | 2.90 | 31 | 225 |
| $8 \times 2$ | 13.50 | 5.30 | 9.81 | 2.60 | 28 | 225 |
| $10 \times 8$ | 15.75 | 5.10 | 13.50 | 5.30 | 48 | 225 |
| $10 \times 6$ | 15.75 | 5.10 | 11.75 | 2.80 | 44 | 225 |
| $10 \times 4$ | 15.75 | 5.10 | 11.75 | 3.10 | 41 | 225 |
| $10 \times 3$ | 15.75 | 5.10 | 11.38 | 2.90 | 37 | 225 |
| $12 \times 10$ | 17.00 | 6.40 | 15.75 | 5.10 | 72 | 225 |
| $12 \times 8$ | 17.00 | 6.40 | 15.00 | 5.30 | 65 | 225 |
| $12 \times 6$ | 17.00 | 6.40 | 13.25 | 2.80 | 60 | 225 |
| $12 \times 4$ | 17.00 | 6.40 | 13.25 | 3.10 | 55 | 225 |
| $14 \times 12$ | 19.56 | 4.60 | 17.00 | 6.40 | 93 | 225 |
| $14 \times 10$ | 19.56 | 4.60 | 16.25 | 5.10 | 85 | 225 |
| $14 \times 8$ | 19.56 | 4.60 | 15.50 | 5.30 | 77 | 225 |
| $14 \times 6$ | 19.56 | 4.60 | 13.75 | 2.80 | 71 | 225 |
| $16 \times 14$ | 21.25 | 5.60 | 20.00 | 4.60 | 111 | 225 |
| $16 \times 12$ | 21.25 | 5.60 | 18.00 | 6.40 | 101 | 225 |
| $16 \times 10$ | 21.25 | 5.60 | 17.25 | 5.10 | 91 | 225 |
| $16 \times 8$ | 21.25 | 5.60 | 16.50 | 5.30 | 83 | 225 |

## Laterals, crosses, and eccentric reducers available upon request.

All dimensions listed in this bulletin are nominal in nature and should only be used for system layout and take off. Actual fittings and fabrication work should be measured before bonding to ensure dimensional accuracy. Fiber Glass Systems does not warrant and is in no way responsible for the workmanship of any distributor, contractor or others involved in the installation of the goods.

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## SILVER_STREAK® LD FITTINGS DIMENSIONS

Silver Streak LD piping and fittings are designed especially for abrasive and corrosive services such as limestone and gypsum slurries found in flue gas desulfurization (FGD) scrubber applications.

Silver Streak LD piping systems are designed to operate at temperatures up to $200^{\circ} \mathrm{F}$ and pressures up to 150 psig.

Sweep elbows are available in $30^{\circ}$ diameters only.
Fittings are constructed with the same abrasion-resistant additives as the pipe.

All fittings have a nominal corrosion/abrasion barrier of 100 mils.

## Stub Flange



| Nominal Pipe Size | A | B | C | D | Bolts | E (psi) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| In | In | In | In | In | Size - No | 50 | 75 | 100 |
| 30 | $383 / 4$ | 36 | $13 / 8$ | 15 | 11/4-28 | $17 / 8$ | $2^{1 / 8}$ | $21 / 4^{*}$ |
| 36 | 46 | $42^{3 / 4}$ | $15 / 8$ | 15 | 11/2-32 | 2 | $2^{3 / 8}$ | $21 / 2^{*}$ |
| 42 | 53 | 49112 | $15 / 8$ | 15 | 11/2-36 | $2^{1 / 8}$ | $2{ }^{5} 8^{*}$ | $2^{7 / 8^{*}}$ |
| 48 | $591 / 2$ | 56 | $15 / 8$ | 18 | 1112-44 | $21 / 4$ | $23 / 4^{*}$ | $31 / 8^{*}$ |

*Flange has special "O" ring type seal. Consult factory for design of each of these flange connections since only one flange face is grooved for placement of the seating " O " ring. Quotations or information on gasket requirements available on request. Flanges meet O.D., bolt circle diameter, number of holes and bolt hole diameter dimensions for ANSI B16.1 125 lb .

## Weights Per Fitting

| Nominal <br> Pipe <br> Size | Plain Ends |  |  | Flanged |  |  | Flange <br> Stub <br> End Drilled |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Elbow | Elbow | Tee | Elbow | Elbow | Tee |  |
| In | $90^{\circ}$ | $45^{\circ}$ | BBB | $90^{\circ}$ | $45^{\circ}$ | FFF |  |
| 30 | 280 | 140 | 280 | 455 | 315 | 545 | 125 |
| 36 | 445 | 220 | 420 | 710 | 490 | 820 | 185 |
| 42 | 665 | 330 | 600 | 1050 | 730 | 1190 | 265 |
| 48 | 945 | 475 | 870 | 1460 | 985 | 1640 | 355 |

## $90^{\circ}$ Elbow



| Nominal <br> Pipe Size | A | B | C | Bolt Holes <br> D | Bolts . |
| :---: | :---: | :---: | :---: | :---: | :---: |
| In | In | In | In | Diameter | Size/No. |
| 30 | 45 | 36 | $383 / 4$ | $1^{3 / 8}$ | $1^{1 / 4}-28$ |
| 36 | 54 | $42^{3 / 4}$ | 46 | $1^{5} / 8$ | $1^{11 / 2}-32$ |
| 42 | 63 | $49^{1 / 2}$ | 53 | $1^{5 / 8}$ | $1^{11 / 2}-36$ |
| 48 | 72 | 56 | $591 / 2$ | $1^{5 / 8}$ | $1^{11 / 2}-44$ |

Elbows will be mitered construction using pipe for the mitered sections. Elbows shall have a minimum of 2 miters. Sweep elbows available in 30 " only.

## $45^{\circ}$ Elbow



FLANGED


PLAIN END

## Tee



PLAIN END

| Nominal <br> Pipe Size | A | B | C | Bolt Holes <br> D | Bolts . |
| :---: | :---: | :---: | :---: | :---: | :---: |
| In | In | In | In | Diameter | Size/No. |
| 30 | 30 | 36 | $383 / 4$ | $1^{3 / 8}$ | $1^{11 / 4}-28$ |
| 36 | 33 | $42^{3 / 4}$ | 46 | $1^{5 / 8}$ | $1^{11 / 2}-32$ |
| 42 | 36 | $491 / 2$ | 53 | $1^{5 / 8}$ | $1^{11 / 2}-36$ |
| 48 | 42 | 56 | $591 / 2$ | $1^{5 / 8}$ | $11 / 2-44$ |

## Cross



PLAJN END

| Nominal Pipe Size | A | B | C | $\begin{gathered} \hline \text { Bolt Holes } \\ \mathrm{D} \end{gathered}$ | Bolts . |
| :---: | :---: | :---: | :---: | :---: | :---: |
| In | In | In | In | Diameter | Size/No. |
| 30 | $18^{5 / 8}$ | 36 | $383 / 4$ | $13 / 8$ | 11/4-28 |
| 36 | $22^{1 / 2}$ | $42^{3 / 4}$ | 46 | $15 / 8$ | 11/2-32 |
| 42 | 26 | $49^{1 / 2}$ | 53 | $15 / 8$ | 11/2-36 |
| 48 | $29^{7 / 8}$ | 56 | 59112 | $15 / 8$ | 11/2-44 |

Elbows will be mitered construction using pipe for the mitered sections. All mitered elbows shall have 1 miter, 2 sections. Sweep elbows available in 30 " only.


2

## Lateral



| Nominal <br> Pipe Size | A | B | C | D | E | F | Bolts . |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| In | In | In | In | In | In | In | Size/No. |
| 30 | 52 | 72 | 20 | 36 | $383 / 4$ | $1^{3 / 8}$ | $11 / 4-28$ |
| 36 | 62 | 84 | 22 | $423 / 4$ | 46 | $1^{5 / 8}$ | $11 / 2-32$ |
| 42 | 72 | 96 | 24 | $491 / 2$ | 53 | $1^{5 / 8}$ | $11 / 2-36$ |

## Reducer



ECCENTRIC


FLANGED
CONCENTRIC

| Nominal Pipe Size A/B | C | D | E | F | G | H |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| In | In | In | In | In | In | In |
| $30 \times 20$ | 25 | 12 | 25 | $271 / 2$ | 36 | $383 / 4$ |
| $30 \times 24$ | 15 | 12 | $291 / 2$ | 32 | 36 | $383 / 4$ |
| $36 \times 24$ | 30 | 12 | $291 / 2$ | 32 | $423 / 4$ | 46 |
| $36 \times 30$ | 15 | 15 | $383 / 4$ | 36 | $423 / 4$ | 46 |
| $42 \times 30$ | 30 | 15 | $383 / 4$ | 36 | $491 / 2$ | 53 |
| $42 \times 36$ | 15 | 15 | $423 / 4$ | 46 | $491 / 2$ | 53 |

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## 1"-14" Fittings and Accessories

## Centricast ${ }^{\text {™ }}$ Piping Systems

NOV Fiber Glass Systems offers a complete line of fittings manufactured from both epoxy and vinyl ester resins. These fittings and adhesives provide the same corrosion resistance and temperature ratings as the compatible grade of pipe. Press molded fittings are manufactured from a resin-rich compound which is corrosion resistant throughout the fitting wall. Hand layup fittings have a 100 mil resin-rich corrosion barrier. Epoxy RB fittings are color-coded brown; Z-CORE fittings are dark green or black; CL vinyl ester fittings are off-white. Because the fittings are designed for the most severe services, they are suitable for the broad range of chemicals shown in the Chemical Resistance Guide. All 1"-14" fittings are available with either a socket fitting or flanged type connection for easy field assembly. Adapters to iron pipe threads are also available.


Order by figure (Fig.) number prefixed with CL for vinyl ester, RB for epoxy and ZC for Z-Core followed by construction type (if applicable), diameter, and outlet sizes.

Example Fig. 34C HLU 3x2

PM - Represents Press Molded Fittings
HLU - Represents Hand Layup Fittings

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## PRESSURE RATINGS

Pressure Rating of CL Vinyl Ester Fittings up to $200^{\circ} \mathrm{F}$ based on Weldfast ${ }^{\text {M }}$
CL-200 and/or CL-200QS Adhesive Uninsulated Piping

|  | Elbows, Tees, Reducers <br> Couplings, Flanges, End <br> Caps, Socket <br> and Threaded Nipples |  | Laterals, <br> Crosses, <br> and <br> Size <br> (In.) |
| :---: | :---: | :---: | :---: |
| Saddles <br> (psi) |  |  |  |
| 1 | 300 | Socket Ftgs. <br> (psi) | Flanged Ftgs. <br> (psi) |
| $1 \frac{1}{2} 2$ | 300 | 300 | -- |
| 2 | 275 | 200 | -- |
| 3 | 200 | 150 | 125 |
| 4 | 150 | 150 | 125 |
| 6 | 150 | 150 | 100 |
| 8 | 150 | 150 | 100 |
| 10 | 150 | 150 | 75 |
| 12 | 150 | 150 | 75 |
| 14 | 125 | 150 | -- |

Reduce pressure by $25 \%$ for $175^{\circ} \mathrm{F}$ to $200^{\circ} \mathrm{F}$ operating temperatures.

Pressure Rating of ZC Epoxy Fittings
up to $225^{\circ} \mathrm{F}$ based on
Weldfast ZC-275 Adhesive Uninsulated Piping

|  | Elbows, Tees, Reducers <br> Couplings, Flanges, End <br> Caps, Socket <br> and Threaded Nipples |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Size <br> (In.) | Socket Ftgs. <br> (psi) | Flanged Ftgs. <br> (psi) | Flanges <br> (psi) | Laterals and <br> Crosses <br> (psi) |
| 1 | 300 | 300 | 300 | -- |
| 1 1/2 | 300 | 150 | 300 | -- |
| 2 | 300 | 150 | 300 | 125 |
| 3 | 275 | 150 | 200 | 125 |
| 4 | 150 | 150 | 150 | 100 |
| 6 | 150 | 150 | 150 | 100 |
| 8 | 150 | 150 | 150 | 100 |
| 10 | 150 | 150 | 150 | 75 |
| 12 | 150 | 150 | 150 | 75 |
| 14 | 125 | 150 | 150 | -- |

For insulated and/or heat traced piping systems, use $100 \%$ of uninsulated piping recommendations up to $225^{\circ} \mathrm{F}$ and reduce these ratings $25 \%$ for $225^{\circ} \mathrm{F}$ to $275^{\circ} \mathrm{F}$ operating temperatures. For uninsulated ZC piping, reduce these ratings $25 \%$ for $250^{\circ} \mathrm{F}$ to $275^{\circ} \mathrm{F}$ operating temperatures.

Note: Quotations for specially fabricated higher pressure fittings are available on request.

## COUPLINGS

Fig. 14 Socket


| Size <br> (In) | A $\pm 1 / 8$ <br> (In.) | PM Ref <br> (In.) | HLU Ref <br> (In.) | C Ref <br> (In.) | Wt. $\dagger$ <br> $($ Lb.) |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | 3 | $21 / 8$ | -- | $5 / 8$ | 0.5 |
| $11 / 2$ | 3 | $23 / 4$ | -- | $3 / 8$ | 0.5 |
| 2 | 4 | $31 / 16$ | -- | $3 / 8$ | 0.7 |
| 3 | 4 | $43 / 16$ | -- | $3 / 8$ | 1.0 |
| 4 | 4 | $51 / 4$ | -- | $3 / 8$ | 1.5 |
| 6 | 4 | 8 | -- | $3 / 8$ | 3.2 |
| 8 | $55 / 8$ | $97 / 8$ | -- | $3 / 8$ | 4.4 |
| 10 | $83 / 8$ | -- | $113 / 8$ | $3 / 8$ | 13.2 |
| 12 | $83 / 8$ | -- | $131 / 2$ | $3 / 8$ | 14.0 |
| $14^{\star}$ | $83 / 8$ | $159 / 16$ | - | $3 / 8$ | 17.2 |

NIPPLES

Fig. 6S Iron Pipe Male Thread

| Size <br> $(\operatorname{In})$ | $\mathrm{A} \pm 1 / 8$ <br> $(\operatorname{In})$. | B <br> $(\operatorname{In})$. | Wt. $\dagger$ <br> $($ Lb. $)$ |
| :---: | :---: | :---: | :---: |
| 1 | 8 | $15 / 16$ | 0.5 |
| $1 \frac{1}{2} 2$ | 8 | $15 / 16$ | 0.8 |
| 2 | 8 | $23 / 8$ | 1.1 |
| 3 | 8 | $31 / 2$ | 1.9 |
| 4 | 8 | $41 / 2$ | 2.6 |
| 6 | 8 | $65 / 8$ | 5.0 |

Fig. 30
RSR Repair Coupling

| Size <br> $(\ln )$ | $A \pm 1 / 8$ <br> $(\operatorname{In})$. | B Ref <br> (In.) | Wt. $\dagger$ <br> $($ Lb. $)$ |
| :---: | :---: | :---: | :---: |
| 1 | $2 \frac{5}{8}$ | $23 / 8$ | 1.0 |
| $11 / 2$ | $31 / 4$ | 3 | 1.0 |
| 2 | 4 | $37 / 16$ | 1.4 |
| 3 | 4 | $49 / 16$ | 2.0 |
| 4 | 4 | $59 / 16$ | 3.0 |
| 6 | $43 / 4$ | $711 / 16$ | 6.5 |
| 8 | $51 / 4$ | 9 | 8.8 |
| 10 | $53 / 4$ | $111 / 8$ | 26 |
| 12 | $61 / 4$ | $131 / 8$ | 28 |
| 14 | $61 / 4$ | $151 / 8$ | 34 |



## THREADED INSERT

## END CAP

Fig. 33S Insert


| Size <br> (In) | A Ref <br> (In.) | $\begin{gathered} \mathrm{B} \pm 1 / 16 \\ \text { (In.) } \end{gathered}$ | C Ref <br> (In.) | $\begin{aligned} & \text { Wt. } \dagger \\ & \text { (Lb.) } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: |
| 1 x blank* | $15 / 16$ | $11 / 4$ | -- | 0.1 |
| 11/2x blank* | 115/16 | $11 / 2$ | -- | 0.2 |
| $2 \times$ blank $^{*}$ | $23 / 8$ | $11 / 2$ | -- | 0.4 |
| $3 \times$ blank $^{*}$ | $31 / 2$ | 2 | -- | 1.2 |
| $2 \times 1 / 4$ | $23 / 8$ | $11 / 2$ | 1/4. I.P. | 0.4 |
| $2 \times 1 / 2$ | $23 / 8$ | $11 / 2$ | $1 / 2 \mathrm{l} . \mathrm{P}$. | 0.4 |
| $2 \times 3 / 4$ | $23 / 8$ | $11 / 2$ | 3/4.P. | 0.3 |
| $2 \times 1$ | $23 / 8$ | $11 / 2$ | 1 I.P. | 0.3 |
| $2 \times 11 / 4$ | $23 / 8$ | $11 / 2$ | $11 / 4$. .P. | 0.3 |
| $2 \times 11 / 2$ | $23 / 8$ | $11 / 2$ | $11 / 2 \mathrm{I} . \mathrm{P}$. | 0.2 |
| $3 \times 1$ | $31 / 2$ | 2 | 1 I.P. | 1.0 |
| $3 \times 11 / 2$ | $31 / 2$ | 2 | $1112 \mathrm{I} . \mathrm{P}$. | 0.8 |

Fig. 101C Socket Pipe Cap


| Size <br> (In) | $\begin{gathered} A \pm 3 / 8 \\ \text { (In.) } \end{gathered}$ | $\begin{gathered} \mathrm{B} \pm 1 / 16 \\ \text { (In.) } \end{gathered}$ | C Ref (In.) | D Ref <br> (In.) | E Ref <br> (In) | $\begin{aligned} & \text { Wt. } \dagger \\ & \text { (Lb.) } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 31116 | $13 / 16$ | $15 / 16$ | $21 / 16$ | $11 / 4$ | 0.7 |
| $11 / 2$ | $33 / 16$ | 1 5/16 | 1 15/16 | $211 / 16$ | $11 / 2$ | 0.9 |
| 2 | 4 | $1{ }^{13 / 16}$ | $23 / 8$ | $31 / 8$ | $11 / 2$ | 1.2 |
| 3 | 4 | $1{ }^{13 / 16}$ | $31 / 2$ | $43 / 16$ | $11 / 2$ | 2.2 |
| 4 | 4 | $1^{13 / 16}$ | $41 / 2$ | $51 / 4$ | $11 / 2$ | 3.7 |
| 6 | 4 | $1{ }^{13 / 16}$ | 6 5/8 | $7 \mathrm{7} / 8$ | $11 / 2$ | 7.4 |
| 8 | 5 5/8 | $25 / 8$ | 8 5/8 | 97/8 | $25 / 8$ | 12.4 |
| 10* | $83 / 8$ | 4 | $103 / 4$ | $121 / 4$ | 2 | 15 |
| 12* | $83 / 8$ | 4 | $123 / 4$ | $143 / 16$ | 2 | -- |

## SADDLE

Fig. 13
Fig. 13
Pipe Saddle
 1/2 PIPE O.D. CL PIPE O.D.

| Size <br> (In) | $\mathrm{A} \pm 1 / 4$ <br> (In.) | B $\pm 1 / 16$ <br> (In.) | C Ref <br> (In.) |  |  |  |  |  |  |  |  | $\begin{aligned} & \text { Wt. } \dagger \\ & \text { (Lb.) } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | 1 | $11 / 2$ | 2 | 3 | 4 | 6 | 8 | 10 |  |
| 2 | $41 / 4$ | $3 / 4$ | 2 | X | X |  |  |  |  |  |  | 0.4 |
| 3 | $53 / 4$ | 2 | $33 / 8$ |  |  | X |  |  |  |  |  | 1.5 |
| 4 | 8 | 2 | $41 / 16$ |  |  | X | X |  |  |  |  | 2.6 |
| 6 | 9 | 2 | $51 / 8$ |  |  | X |  | X |  |  |  | 4.8 |
| 8 | $10^{1 / 2}$ | 2 | $77 / 16$ |  |  | X |  |  | X |  |  | 8.1 |
| 10 | $131 / 2$ | $31 / 8$ | $10^{1 / 8}$ |  |  | X |  |  |  | X |  | 23.1 |
| 12 | $151 / 2$ | $31 / 8$ | $123 / 16$ |  |  | X |  |  |  |  | X | 32.8 |

Note: For Threaded Outlets or Cement Socket Outlets greater than one size reduction, see
Assembled Fittings section.
Figure 13 weights based on blank saddle. Saddles available in CL and RB only.

[^29]
## REDUCERS

Fig. 33 Insert Socket

Reducer inserts which reduce greater than two pipe sizes are available on order only. Reducer inserts 8" and larger which reduce greater than one pipe size may have a reduced pressure rating. Consult factory for specific recommendations.

| Size <br> (In) | $\begin{gathered} \mathrm{A} \pm 1 / 16 \\ \text { (In.) } \end{gathered}$ | $\begin{gathered} \mathrm{B} \pm 1 / 8 \\ \text { (In.) } \end{gathered}$ | C Ref (In.) | D Ref <br> (In.) | $\begin{aligned} & \text { Wt. } \dagger \\ & \text { (Lb.) } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $11 / 2 \times 1$ | $1{ }^{15} / 16$ | $11 / 2$ | $15 / 16$ | 1 | 0.2 |
| $2 \times 1$ | $23 / 8$ | $11 / 2$ | $15 / 16$ | 1 | 0.3 |
| $2 \times 11 / 2$ | $23 / 8$ | $11 / 2$ | $17 / 8$ | $11 / 2$ | 0.2 |
| $3 \times 1$ | $311 / 2$ | 2 | $15 / 16$ | 1 | 0.9 |
| $3 \times 11 / 2$ | $31 / 2$ | 2 | $17 / 8$ | $11 / 2$ | 0.9 |
| $3 \times 2$ | $31 / 2$ | 2 | $23 / 8$ | 2 | 0.6 |
| $4 \times 2$ | $41 / 2$ | 2 | $23 / 8$ | 2 | 1.3 |
| $4 \times 3$ | $41 / 2$ | 2 | $31 / 2$ | 3 | 0.7 |
| $6 \times 2$ | $65 / 8$ | 2 | $23 / 8$ | 2 | 3.5 |
| $6 \times 3$ | $65 / 8$ | 2 | $31 / 2$ | 3 | 2.9 |
| $6 \times 4$ | 65 | 2 | $41 / 2$ | 4 | 2.2 |
| $8 \times 2$ | $85 / 8$ | $21 / 2$ | $23 / 8$ | 2 | 7.4 |
| $8 \times 3$ | 8 5\% | $21 / 2$ | $31 / 2$ | 3 | 7.1 |


| Size <br> $(\operatorname{In})$ | $\mathrm{A} \pm 1 / 16$ <br> $(\operatorname{In})$. | $\mathrm{B} \pm 1 / 8$ <br> $(\operatorname{In})$. | C Ref <br> $(\operatorname{In})$. | D Ref <br> $(\operatorname{In})$. | Wt. $\dagger$ <br> $(\mathrm{Lb})$. |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $8 \times 4$ | $85 / 8$ | $21 / 2$ | $41 / 2$ | 4 | 6.3 |
| $8 \times 6$ | $85 / 8$ | $21 / 2$ | $65 / 8$ | $61 / 8$ | 3.5 |
| $10 \times 2$ | $103 / 4$ | $43 / 16$ | $23 / 8$ | 2 | 20.9 |
| $10 \times 3$ | $103 / 4$ | $43 / 16$ | $31 / 2$ | 3 | 19.9 |
| $10 \times 4$ | $103 / 4$ | $43 / 16$ | $41 / 2$ | 4 | 17.9 |
| $10 \times 6$ | $103 / 4$ | $43 / 16$ | $65 / 8$ | $61 / 8$ | 13.8 |
| $10 \times 8$ | $103 / 4$ | $43 / 16$ | $85 / 8$ | $81 / 8$ | 7.8 |
| $12 \times 2$ | $123 / 4$ | $43 / 16$ | $23 / 8$ | 2 | 34.9 |
| $12 \times 3$ | $123 / 4$ | $43 / 16$ | $31 / 2$ | 3 | 33.1 |
| $12 \times 4$ | $123 / 4$ | $43 / 16$ | $41 / 2$ | 4 | 29.8 |
| $12 \times 6$ | $123 / 4$ | $43 / 16$ | $65 / 8$ | $61 / 8$ | 22.9 |
| $12 \times 8$ | $123 / 4$ | $43 / 16$ | $85 / 8$ | $81 / 8$ | 16.9 |
| $12 \times 10$ | $123 / 4$ | $43 / 16$ | $103 / 4$ | $101 / 4$ | 12.1 |

Fig. 34C
Concentric Tapered
Socket,
Hand Layup
Construction


| Size <br> (In.) | A Ref | $\mathrm{B} \pm 3 / 8$ | C Ref | D Ref | $\begin{aligned} & \text { Wt. } \dagger \\ & \text { (Lb.) } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | (In.) | (In.) | (In.) | (In.) |  |
| $11 / 2 \times 1 *$ | 6 | $33 / 16$ | $31 / 8$ | $2^{11 / 16}$ | 1.6 |
| $2 \times 1$ | 6 | 3 | $31 / 8$ | $2^{11 / 16}$ | 2.0 |
| $2 \times 11 / 2$ | 6 | $27 / 8$ | $31 / 8$ | $2^{11 / 16}$ | 1.2 |
| $3 \times 11 / 2$ | $5^{11 / 16}$ | 2916 | $4^{13 / 16}$ | $31 / 8$ | 2.1 |
| $3 \times 2$ | 6 | $23 / 8$ | $4^{13 / 16}$ | $31 / 8$ | 1.9 |
| $4 \times 2$ | $71 / 4$ | 3 5/8 | $51 / 4$ | $31 / 8$ | 2.6 |
| $4 \times 3$ | $71 / 4$ | $33 / 8$ | $51 / 4$ | $43 / 16$ | 2.9 |
| $6 \times 3$ | 9 \%16 | $5^{15} / 16$ | 7 7/8 | $51 / 4$ | 6.8 |
| $6 \times 4$ | $93 / 8$ | $53 / 8$ | $7^{7 / 8}$ | $51 / 4$ | 6.2 |
| $8 \times 4$ | $15^{7 / 16}$ | 11 | $91 / 2$ | $51 / 4$ | 10.7 |
| $8 \times 6$ | $15^{7 / 16}$ | 11 | $91 / 2$ | $71 / 2$ | 9.5 |
| $10 \times 6$ | $137 / 16$ | $73 / 8$ | $111 / 2$ | $71 / 2$ | 10.0 |
| $10 \times 8$ | 14 | $73 / 8$ | $11^{1 / 2}$ | $91 / 2$ | 11.5 |
| $12 \times 8$ | 16 | $93 / 8$ | $131 / 2$ | $91 / 2$ | 17.2 |
| $12 \times 10$ | 16 3/8 | $93 / 8$ | $131 / 2$ | 111/2 | 20.7 |
| $14 \times 12$ | $173 / 16$ | 93/16 | 15 | 13 3/4 | 22.8 |

* Available on order only - nonreturnable
(1) See Fig. 18 for flange dimensions.
$\dagger$ CL weight, multiply by 1.07 for RB, 1.1 for ZC

Fig. 34F ${ }^{(1)}$
Concentric Tapered
Socket

| Size <br> (In) | A Ref (In.) | $\begin{gathered} \mathrm{B} \pm 1 / 16 \\ \text { (In.) } \\ \hline \end{gathered}$ | C Ref (In.) | $\begin{aligned} & \text { Wt. } \dagger \\ & \text { (Lb.) } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: |
| $11 / 2 \times 1$ * | 6 | $13 / 16$ | 7/8 | 2.3 |
| $2 \times 1$ | 6 | $13 / 16$ | 7/8 | 2.8 |
| $2 \times 11 / 2$ | 6 | $13 / 16$ | $13 / 16$ | 3.4 |
| $3 \times 11 / 2$ | 6 | $13 / 16$ | $13 / 16$ | 5.1 |
| $3 \times 2$ | 6 | $13 / 16$ | $13 / 16$ | 5.2 |
| $4 \times 2$ | 7 | $11 / 2$ | $13 / 16$ | 7.5 |
| $4 \times 3$ | 7 | $11 / 2$ | $13 / 16$ | 8.8 |
| $6 \times 3$ | 9 | $19 / 16$ | $13 / 16$ | 10.1 |
| $6 \times 4$ | 9 | 1916 | $11 / 2$ | 13.9 |
| $8 \times 4$ | 11 | $21 / 16$ | $11 / 2$ | 18.5 |
| $8 \times 6$ | 11 | $21 / 16$ | 1916 | 20.2 |
| $10 \times 6$ | 12 | $31 / 16$ | 1916 | 30.4 |
| $10 \times 8$ | 12 | $31 / 16$ | $21 / 16$ | 35.5 |
| $12 \times 8$ | 14 | $31 / 16$ | $21 / 16$ | 46.9 |
| $12 \times 10$ | 14 | $31 / 16$ | 31116 | 56.3 |
| $14 \times 12^{*}$ | $25^{13 / 16}$ | $43 / 8$ | 31116 | 93.0 |

Fig. 35C
Eccentric Tapered
Socket


| Size <br> (In) | A Ref <br> (In.) | $\begin{gathered} \mathrm{B} \pm 3 / 8 \\ \text { (In.) } \end{gathered}$ | C Ref (In.) | D Ref <br> (In.) | E Ref <br> (In.) | $\begin{gathered} \mathrm{F} \pm 3 / 8 \\ (\ln .) \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{G} \pm 1 / 8 \\ (\ln .) \\ \hline \end{gathered}$ | $\begin{aligned} & \text { Wt. } \dagger \\ & (\mathrm{Lb} .) \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $3 \times 2$ | $65 / 8$ | $215 / 16$ | 4 | $27 / 8$ | 1/2 | $1^{13 / 16}$ | $1^{13 / 16}$ | 1.3 |
| $4 \times 2$ | 6 5\% | $2^{15 / 16}$ | 5 | $27 / 8$ | 1 | $1^{13 / 16}$ | $1{ }^{13 / 16}$ | 1.5 |
| $4 \times 3$ | 6 5/8 | 2 15/16 | 5 | 4 | 1/2 | $1^{13 / 16}$ | $1^{13 / 16}$ | 1.6 |
| $6 \times 3$ | 9 | $53 / 8$ | $71 / 8$ | 4 | $11 / 2$ | $1^{13 / 16}$ | $1^{13 / 16}$ | 6.3 |
| $6 \times 4$ | 9 | $53 / 8$ | $71 / 8$ | 5 | 1 | $1^{13 / 16}$ | $1^{13 / 16}$ | 5.5 |
| $8 \times 4$ | $11^{13 / 16}$ | $73 / 8$ | $91 / 8$ | 5 | 2 | $25 / 8$ | $113 / 16$ | 9.5 |
| $8 \times 6$ | $11^{13 / 16}$ | $73 / 8$ | $91 / 8$ | $71 / 8$ | 1 | 2 5/8 | $113 / 16$ | 7.3 |
| $10 \times 6$ | $133 / 16$ | $73 / 8$ | $11^{1 / 4}$ | $71 / 8$ | 2 | 4 | $1^{13 / 16}$ | 13.7 |
| $10 \times 8$ | 14 | $73 / 8$ | $11^{1 / 4}$ | $91 / 8$ | 1 | 4 | $25 / 8$ | 12.9 |
| $12 \times 8$ | 16 | $93 / 8$ | $131 / 4$ | $91 / 8$ | 2 | 4 | $25 / 8$ | 16.8 |
| $12 \times 10$ | $163 / 8$ | $83 / 8$ | $131 / 4$ | $11^{1 / 4}$ | 1 | 4 | 4 | 20.0 |

Fig. 35F (1)
Eccentric Tapered

## Flanged



| Size <br> (In) | $\begin{gathered} \mathrm{A} \pm 1 / 8 \\ \text { (In.) } \end{gathered}$ | B Ref <br> (In.) | C Ref <br> (In.) | D Ref <br> (In.) | $\begin{aligned} & \text { Wt. } \dagger \\ & \text { (Lb.) } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $2 \times 1$ * | 6 | $13 / 16$ | 7/8 | 1/2 | 3.4 |
| $3 \times 2$ | $103 / 4$ | $13 / 16$ | $13 / 16$ | 1/2 | 6.2 |
| $4 \times 2$ | $103 / 4$ | $11 / 2$ | $13 / 16$ | 1 | 8.2 |
| $4 \times 3$ | $103 / 4$ | $11 / 2$ | $13 / 16$ | 1/2 | 9.2 |
| $6 \times 3$ | 9 | 1916 | $13 / 16$ | $11 / 2$ | 10.0 |
| $6 \times 4$ | 9 | 1916 | $11 / 2$ | 1 | 12.0 |
| $8 \times 4$ | 11 | $21 / 16$ | $11 / 2$ | 2 | 16.1 |
| $8 \times 6$ | 11 | $21 / 16$ | 1916 | 1 | 19.7 |
| $10 \times 6$ | 12 | $31 / 16$ | 19 | 2 | 30.9 |
| $10 \times 8$ | 12 | $31 / 16$ | $21 / 16$ | 1 | 35.2 |
| $12 \times 8$ | 14 | 31116 | $21 / 16$ | 2 | 46.4 |
| $12 \times 10$ | 14 | 31116 | $31 / 16$ | 1 | 54.8 |

## FLANGES

Fig. 18 and Fig. 18L* Flange Socket


| Size <br> (In) | A Ref (In.) | B Ref <br> (In.) | C Ref <br> (In.) | $\begin{gathered} \mathrm{D} \pm 1 / 16 \\ \text { (In.) } \end{gathered}$ | $\mathrm{E} \pm 1 / 16$ <br> (In.) | $\mathrm{F} \pm 1 / 16$ <br> (In.) | Wt. $\dagger$ (Lb.) | Bolts No/Size |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | $41 / 4$ | $31 / 8$ | 5/8 | 7/8 | $17 / 16$ | -- | 0.6 | 4-1/2 |
| $11 / 2$ | 5 | $37 / 8$ | 5/8 | $13 / 16$ | $19 / 16$ | -- | 1.1 | 4-1/2 |
| 2 | 6 | $43 / 4$ | $3 / 4$ | $13 / 16$ | $21 / 16$ | $3^{11 / 16}$ | 1.6 | 4-5/8 |
| 3 | $71 / 2$ | 6 | $3 / 4$ | $13 / 16$ | $21 / 16$ | $3^{11 / 16}$ | 2.5 | 4-5/8 |
| 4 | 9 | $71 / 2$ | $3 / 4$ | $11 / 2$ | $21 / 16$ | $3^{15 / 16}$ | 4.2 | 8-5/8 |
| 6 | 11 | $911 / 2$ | 7/8 | $19 / 16$ | $21 / 16$ | 47/16 | 5.3 | 8-3/4 |
| 8 | $131 / 2$ | $113 / 4$ | 7/8 | $21 / 16$ | 2916 | $47 / 16$ | 9.9 | 8-3/4 |
| 10 | 16 | $141 / 4$ | 1 | $31 / 16$ | $4^{1 / 4}$ | -- | 19.6 | 12-7/8 |
| 12 | 19 | 17 | 1 | $31 / 16$ | $41 / 4$ | -- | 27.8 | 12-7/8 |
| 14 | 21 | $183 / 4$ | $11 / 8$ | $43 / 8$ | $43 / 8$ | -- | 45.5 | 12-1 |

Fig. 18R * Reducer Socket

| Size <br> (In) | A Ref <br> (In.) | B Ref (In.) | C Ref (In.) | $\begin{gathered} \mathrm{D} \pm 1 / 16 \\ \text { (In.) } \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{E} \pm 1 / 16 \\ \text { (In.) } \\ \hline \end{gathered}$ | $\begin{aligned} & \text { Wt. } \dagger \\ & \text { (Lb.) } \end{aligned}$ | $\begin{aligned} & \text { Bolts } \\ & \text { No/Size } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $11 / 2 \times 1$ | 5 | $37 / 8$ | 5/8 | $13 / 16$ | $19 / 16$ | 1.3 | 4-1/2 |
| $2 \times 1$ | 6 | $43 / 4$ | $3 / 4$ | $13 / 16$ | $21 / 16$ | 1.4 | 4-5/8 |
| $2 \times 11 / 2$ | 6 | $43 / 4$ | $3 / 4$ | $13 / 16$ | $21 / 16$ | 1.7 | 4-5/8 |
| $3 \times 2$ | $71 / 2$ | 6 | $3 / 4$ | $13 / 16$ | $21 / 16$ | 3.3 | 4-5/8 |
| $4 \times 2$ | 9 | $71 / 2$ | $3 / 4$ | $11 / 2$ | $21 / 16$ | 5.4 | 8-5/8 |
| $4 \times 3$ | 9 | $71 / 2$ | $3 / 4$ | $11 / 2$ | $21 / 16$ | 4.9 | 8-5/8 |
| $6 \times 2$ | 11 | $91 / 2$ | 7/8 | $19 / 16$ | $21 / 16$ | 7.6 | 8-3/4 |
| $6 \times 3$ | 11 | $91 / 2$ | 7/8 | 1916 | $21 / 16$ | 8.0 | 8-3/4 |
| $6 \times 4$ | 11 | $911 / 2$ | 7/8 | $19 / 16$ | $21 / 16$ | 8.8 | 8-3/4 |
| $8 \times 2$ | $131 / 2$ | $113 / 4$ | 7/8 | $21 / 16$ | 2916 | 17.6 | 8-3/4 |
| $8 \times 3$ | $131 / 2$ | $113 / 4$ | 7/8 | $21 / 16$ | 2916 | 17.0 | 8-3/4 |
| $8 \times 4$ | $131 / 2$ | $113 / 4$ | 7/8 | $21 / 16$ | 2916 | 16.0 | 8-3/4 |
| $8 \times 6$ | $131 / 2$ | $113 / 4$ | 7/8 | $21 / 16$ | 2916 | 13.4 | 8-3/4 |
| $10 \times 6$ | 16 | $141 / 4$ | 1 | $31 / 16$ | $41 / 4$ | 33.4 | 12-7/8 |
| $10 \times 8$ | 16 | $141 / 4$ | 1 | $31 / 16$ | $41 / 4$ | 27.3 | 12-7/8 |
| $12 \times 8$ | 16 | 17 | 1 | $31 / 16$ | $41 / 4$ | 49.9 | 12-7/8 |
| $12 \times 10$ | 16 | 17 | 1 | 31116 | $41 / 4$ | 43.3 | 12-7/8 |

Flanges meet O.D. bolt circle diameter, number of holes, and bolt hole diameter dimensions for ANSI B16.1 125 lb . cast iron sizes 1 "-72" and ANSI B16.5 lb. steel for 1"-24" diameters.

* Available on order only - nonreturnable
(1) See Fig. 18 for flange dimensions.
$\dagger$ CL weight, multiply by 1.07 for RB, 1.1 for ZC

Fig. 18M*
Flange Metric Socket


| Size |  | A Ref | B Ref <br> $(\mathrm{mm})$ | C Ref <br> $(\mathrm{mm})$ | $\mathrm{D} \pm^{1.588}$ <br> $(\mathrm{~mm})$ | $\mathrm{E} \pm^{1.588}$ <br> $(\mathrm{~mm})$ | Bolts <br> $(\mathrm{mm})$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| No/Size |  |  |  |  |  |  |  |$|$

Fig. 22 Blind Flange


Fig 22S ${ }^{(2)}$ Iron Pipe Tapped

| Size <br> (In) | $\mathrm{A} \pm 1 / 8$ <br> (In.) | $\begin{gathered} \mathrm{B} \pm 1 / 16 \\ (\ln .) \end{gathered}$ | C Ref (In.) | $\begin{aligned} & \mathrm{D} \pm 1 / 16 \\ & \text { (In.) } \end{aligned}$ | Wt. † (Lb.) | Bolts No/Size |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | $41 / 4$ | $31 / 8$ | 5/8 | 7/8 | 0.6 | 4-1/2 |
| $11 / 2$ | 5 | $37 / 8$ | 5/8 | $13 / 16$ | 1.2 | 4-1/2 |
| 2 | 6 | $43 / 4$ | $3 / 4$ | $13 / 16$ | 1.8 | 4-5/8 |
| 3 | $71 / 2$ | 6 | $3 / 4$ | $13 / 16$ | 3.0 | 4-5/8 |
| 4 | 9 | $71 / 2$ | $3 / 4$ | $11 / 2$ | 5.2 | 8-5/8 |
| 6 | 11 | $91 / 2$ | 7/8 | $19 / 16$ | 8.2 | 8-3/4 |
| 8 | $131 / 2$ | $11^{3 / 4}$ | 7/8 | $21 / 16$ | 16.6 | 8-3/4 |
| 10 | 16 | $141 / 4$ | 1 | $31 / 16$ | 34.3 | 12-7/8 |
| 12 | 19 | 17 | 1 | 31116 | 49.1 | 12-7/8 |

Fig. 21/24/25*
Van Stone Flange

|  |  |  |  |  |  | Fig. 24 | Fig. 25 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | F |  |
| Size <br> (In) | A Ref <br> (In.) | B Ref <br> (In.) | C Ref <br> (In.) | $\begin{aligned} & \mathrm{D} \pm 1 / 16 \\ & \text { (ln.) } \end{aligned}$ | $\begin{gathered} \mathrm{E} \pm 1 / 16 \\ \text { (In.) } \end{gathered}$ | Fiberglass Ring $\pm 1 / 16$ | Steel Ring $\pm 1 / 8$ |
| 2 | 6 | $43 / 4$ | $3 / 4$ | 1 | 2 | 7/8 | 5/8 |
| 3 | $71 / 2$ | 6 | $3 / 4$ | 1 | 2 | 7/8 | 5/8 |
| 4 | 9 | $71 / 2$ | $3 / 4$ | 1 | 2 | 7/8 | 5/8 |
| 6 | 11 | $91 / 2$ | 7/8 | 1 | 2 | 7/8 | $3 / 4$ |



## ELBOWS

Fig. 255C
$90^{\circ}$ Short Radius
Elbow, Socket

| Size <br> (In.) | $\begin{gathered} \mathrm{A} \pm 1 / 16 \\ \text { (In.) } \end{gathered}$ | $\begin{gathered} \mathrm{B} \pm 1 / 16 \\ \text { (In.) } \\ \hline \end{gathered}$ | $\begin{aligned} & \text { Wt. † } \\ & (\mathrm{Lb} .) \end{aligned}$ |
| :---: | :---: | :---: | :---: |
| 1 | $21 / 2$ | $13 / 16$ | 0.4 |
| $11 / 2$ | $23 / 4$ | $15 / 16$ | 0.6 |
| 2 | $313 / 16$ | 113/16 | 1.5 |
| 3 | 47/16 | 113/16 | 2.4 |
| 4 | $51 / 16$ | 13/16 | 3.5 |
| 6 | 6 | 113/16 | 7.6 |
| 8 | $711 / 2$ | $25 / 8$ | 12.0 |

Sizes 1"-6"PM Construction
8" HLU Construction

* Available on order only - nonreturnable
(2) Maximum Iron Pipe Thread size = 1"
$\dagger$ CL weight, multiply by 1.07 for RB, 1.1 for ZC

Fig. 257C
$90^{\circ}$ Long Radius Elbow, Socket

| $\begin{aligned} & \text { Size } \\ & \text { (In.) } \end{aligned}$ | $\begin{gathered} \mathrm{A} \pm 3 / 16 \\ \text { (In.) } \end{gathered}$ | $\begin{gathered} \mathrm{B} \pm 1 / 8 \\ (\ln .) \end{gathered}$ | $\begin{aligned} & \text { Wt. † } \\ & \text { (Lb.) } \end{aligned}$ |
| :---: | :---: | :---: | :---: |
| 1 | 5 | $13 / 16$ | 1.0 |
| 11/2 | 6 | 1 5/16 | 1.5 |
| 2 | $61 / 2$ | $1^{13 / 16}$ | 1.9 |
| 3 | $73 / 4$ | $1^{13 / 16}$ | 2.2 |
| 4 | 9 | $1^{13 / 16}$ | 3.6 |
| 6 | $10^{13 / 16}$ | $1^{13 / 16}$ | 7.6 |
| 8 | 14 5/8 | $25 / 8$ | 13.8 |
| 10 | $17^{11 / 16}$ | 4 | 22.8 |
| 12 | $203 / 16$ | 4 | 31.4 |
| 14 | 22 | 4 | 41.0 |

HLU Construction

Fig. 255S*
$90^{\circ}$ Short Radius Elbow, Flange x Socket


| Size <br> (In.) | $\begin{gathered} \mathrm{A} \pm 1 / 16 \\ \text { (In.) } \\ \hline \end{gathered}$ | B Ref <br> (In.) | C Ref <br> (In.) | D Ref <br> (In.) | E Ref <br> (In.) | F Ref <br> (In.) | $\begin{aligned} & \text { Wt. } \dagger \\ & \text { (Lb.) } \end{aligned}$ | Bolts <br> No/Size |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | $315 / 16$ | $31 / 8$ | $41 / 4$ | 7/8 | 5/8 | $21 / 2$ | 1.1 | 4-1/2 |
| 11/2 | 4516 | $37 / 8$ | 5 | $13 / 16$ | 5/8 | $23 / 4$ | 1.9 | 4-1/2 |
| 2 | $57 / 8$ | $43 / 4$ | 6 | $13 / 16$ | $3 / 4$ | $313 / 16$ | 3.3 | 4-5/8 |
| 3 | $61 / 2$ | 6 | $71 / 2$ | $13 / 16$ | $3 / 4$ | 47/16 | 5.1 | 4-5/8 |
| 4 | $71 / 8$ | $71 / 2$ | 9 | $11 / 2$ | $3 / 4$ | $51 / 16$ | 8.3 | 8-5/8 |
| 6 | $81 / 16$ | $911 / 2$ | 11 | 1916 | 7/8 | 6 | 14.2 | 8-3/4 |
| 8 | 101116 | $113 / 4$ | $131 / 2$ | 21116 | 7/8 | $711 / 2$ | 25 | 8-3/4 |


| Size <br> (In.) | $\begin{gathered} \mathrm{A} \pm 1 / 16 \\ \text { (In.) } \end{gathered}$ | B Ref <br> (In.) | C Ref <br> (In.) | D Ref <br> (In.) | E Ref <br> (In.) | Wt. $\dagger$ (Lb.) | Bolts No/Size |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | $3{ }^{15} / 16$ | $31 / 8$ | $41 / 4$ | 7/8 | 5/8 | 1.8 | 4-1/2 |
| 11/2 | $4^{13 / 16}$ | $37 / 8$ | 5 | $13 / 16$ | 5/8 | 3.3 | 4-1/2 |
| 2 | $41 / 2$ | $43 / 4$ | 6 | $11 / 16$ | $3 / 4$ | 4.4 | 4-5/8 |
| 3 | $51 / 2$ | 6 | $711 / 2$ | $11 / 4$ | $3 / 4$ | 8.3 | 4-5/8 |
| 4 | $61 / 2$ | $71 / 2$ | 9 | $13 / 8$ | $3 / 4$ | 13.0 | 8-5/8 |
| 6 | 8 | $91 / 2$ | 11 | $1 \% 16$ | 7/8 | 20.8 | 8-3/4 |
| 8 | 9 | $113 / 4$ | $131 / 2$ | $21 / 16$ | 7/8 | 36.4 | 8-3/4 |
| 10 | 11 | $141 / 4$ | 16 | $31 / 16$ | 1 | 52.6 | 12-7/8 |
| 12 | 12 | 17 | 19 | 31116 | 1 | 73.4 | 12-7/8 |


| Size <br> (In.) | $\begin{gathered} \mathrm{A} \pm 1 / 16 \\ \text { (In.) } \end{gathered}$ | B Ref <br> (In.) | C Ref <br> (In.) | D Ref <br> (In.) | E Ref <br> (In.) | Wt. $\dagger$ <br> (Lb.) | Bolts No/Size |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | $67 / 16$ | $31 / 8$ | $41 / 4$ | 7/8 | 5/8 | 2.4 | 4-1/2 |
| 11/2 | 79 | $37 / 8$ | 5 | $13 / 16$ | 5/8 | 4.2 | 4-1/2 |
| 2 | $8 \%$ | $43 / 4$ | 6 | $13 / 16$ | $3 / 4$ | 5.2 | 4-5/8 |
| 3 | $9^{13 / 16}$ | 6 | $711 / 2$ | $13 / 16$ | $3 / 4$ | 9.1 | 4-5/8 |
| 4 | $11^{1 / 16}$ | $71 / 2$ | 9 | $11 / 2$ | $3 / 4$ | 14.6 | 8-5/8 |
| 6 | 11 1/2 | $911 / 2$ | 11 | $19 / 16$ | 7/8 | 17.1 | 8-3/4 |
| 8 | 14 | $113 / 4$ | $131 / 2$ | $21 / 16$ | 7/8 | 29.3 | 8-3/4 |
| 10 | 16 1/2 | $14^{1 / 4}$ | 16 | $31 / 16$ | 1 | 52.6 | 12-7/8 |
| 12 | 19 | 17 | 19 | $31 / 16$ | 1 | 72.2 | 12-7/8 |
| 14 | 26 3/8** | $183 / 4$ | 21 | $43 / 8$ | $11 / 8$ | 134.6 | 12-1 |

Fig. 257F
$90^{\circ}$ Long Radius Elbow, Flanged


Fig. 257S*
$90^{\circ}$ Long Radius Elbow, Flange x Socket


| Size <br> (In.) | $\begin{gathered} \mathrm{A} \pm 1 / 8 \\ (\mathrm{ln} .) \end{gathered}$ | B Ref <br> (In.) | C Ref <br> (In.) | D Ref <br> (In.) | E Ref <br> (In.) | $\mathrm{F} \pm 1 / 8$ <br> (In.) | Wt. $\dagger$ <br> (Lb.) | Bolts No/Size |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | $67 / 16$ | $31 / 8$ | $41 / 4$ | 7/8 | 5/8 | 5 | 1.7 | 4-1/2 |
| 11/2 | 7916 | $37 / 8$ | 5 | $13 / 16$ | 5/8 | 6 | 2.8 | 4-1/2 |
| 2 | $8 \%$ | $43 / 4$ | 6 | $13 / 16$ | $3 / 4$ | $611 / 2$ | 3.3 | 4-5/8 |
| 3 | $9^{13 / 16}$ | 6 | $71 / 2$ | $13 / 16$ | $3 / 4$ | $73 / 4$ | 5.8 | 4-5/8 |
| 4 | $11^{1 / 16}$ | $71 / 2$ | 9 | $11 / 2$ | $3 / 4$ | 9 | 8.5 | 8-5/8 |
| 6 | $12 \mathrm{~T} / 8$ | $911 / 2$ | 11 | 1916 | 7/8 | $103 / 16$ | 14.4 | 8-3/4 |
| 8 | $173 / 16$ | $113 / 4$ | $131 / 2$ | $21 / 16$ | 7/8 | 14 5/8 | 25.7 | 8-3/4 |
| 10 | $21^{15 / 16}$ | $14^{1 / 4}$ | 16 | $31 / 16$ | 1 | $17^{11 / 16}$ | 49.7 | 12-7/8 |
| 12 | $24^{7 / 16}$ | 17 | 19 | $31 / 16$ | 1 | $203 / 16$ | 65.2 | 12-7/8 |
| 14* | $263 / 8$ | $183 / 4$ | 21 | $43 / 8$ | 11/8 | 22 | 105.1 | 12-1 |

* Available on order only - nonreturnable
** Tolerance exception - Fig. 257F x 14 - A $\pm 1 / 8$
$\dagger$ CL weight, multiply by 1.07 for RB, 1.1 for ZC

Fig. 265C $45{ }^{\circ}$ Short Radius Elbow, Socket


Fig. 265F
$45{ }^{\circ}$ Short Radius
Elbow, Flanged


| Size <br> (In.) | A |  | B Ref* <br> (In.) | $\begin{aligned} & \text { Wt. † } \\ & \text { (Lb.) } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: |
|  | $\begin{gathered} \mathrm{PM} \pm^{1 / 1 / 6} \\ \text { (In.) } \end{gathered}$ | HLU $\pm 1 / 8$ <br> (In.) |  |  |
| 1 | $21 / 2$ | $13 / 4^{*}$ | $13 / 16$ | 0.7 |
| 11/2 | $25 / 16$ | $21 / 4 *$ | $15 / 16$ | 0.6 |
| 2 | $31 / 4$ | $21 / 2^{*}$ | 1 13/16 | 1.3 |
| 3 | $33 / 4$ | 3* | $1{ }^{13 / 16}$ | 2.1 |
| 4 | $4^{1 / 16}$ | 4* | $1^{13 / 16}$ | 3.4 |
| 6 | $43 / 4$ | 5* | 1 13/16 | 7.0 |
| 8 | -- | $515 / 16$ | $25 / 8$ | 7.7 |
| 10 | -- | $711 / 16$ | 4 | 15.8 |
| 12 | -- | $8{ }^{11 / 16}$ | 4 | 20.2 |
| 14 | -- | $93 / 8$ | 4 | 24.5 |


$\left.$| Size <br> (In.) | A |  |  | B Ref <br> (In.) | C Ref <br> (In.) | D Ref <br> (In.) | E Ref <br> (In.) | Wt. $\dagger$ <br> (Lb.) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | | HLU $\pm 1 / 8$ |
| :---: |
| Bo/Size |
| No/Size | \right\rvert\,

Fig. 265S* $45^{\circ}$ Elbow, Flange x Socket


| Size(In.) | A |  | B Ref <br> (In.) | C Ref <br> (In.) | D Ref <br> (In.) | E Ref <br> (In.) | $\begin{gathered} \text { F } \\ \text { (In.) } \end{gathered}$ | G |  | $\begin{aligned} & \text { Wt. } \dagger \\ & \text { (Lb.) } \end{aligned}$ | $\begin{aligned} & \text { Bolts } \\ & \text { No/Size } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\mathrm{PM} \pm 1 / 16$ <br> (In.) | HLU $\pm 1 / 8$ <br> (In.) |  |  |  |  |  | PM $\pm 1 / 16$ <br> (In.) | $\text { HLU } \pm 1 / 8$ <br> (In.) |  |  |
| 1 | $315 / 16$ | $33 / 16^{*}$ | $31 / 8$ | $41 / 4$ | 7/8 | 5/8 | $13 / 16$ | $21 / 2$ | $13 / 4$ | 1.3 | 4-1/2 |
| 11122 | $37 / 8$ | $3^{13 / 16^{*}}$ | $37 / 8$ | 5 | $13 / 16$ | 5/8 | $15 / 16$ | $25 / 16$ | $2^{1 / 4}$ | 2.0 | 4-1/2 |
| 2 | 5 5/16 | $4 \% 16{ }^{*}$ | $43 / 4$ | 6 | $13 / 16$ | $3 / 4$ | 13/16 | $31 / 4$ | $21 / 2$ | 3.2 | 4-5/8 |
| 3 | $5^{13 / 16}$ | $51 / 16^{*}$ | 6 | $71 / 2$ | $13 / 16$ | $3 / 4$ | 133/16 | $33 / 4$ | 3 | 4.9 | 4-5/8 |
| 4 | $61 / 8$ | $61 / 16^{*}$ | $71 / 2$ | 9 | $11 / 2$ | $3 / 4$ | 133/16 | 4116 | 4 | 8.0 | 8-5/8 |
| 6 | $613 / 16$ | $71116^{*}$ | $911 / 2$ | 11 | $19 / 16$ | 7/8 | 13/16 | $43 / 4$ | 5 | 13.7 | 8-3/4 |
| 8 | -- | $81 / 2$ | $113 / 4$ | $131 / 2$ | $21 / 16$ | 7/8 | $25 / 8$ | -- | $515 / 16$ | 15.9 | 8-3/4 |
| 10 | -- | $11^{15 / 16}$ | $141 / 4$ | 16 | 31116 | 1 | 4 | -- | $711 / 16$ | 39.3 | 12-7/8 |
| 12 | -- | 12 15/16 | 17 | 19 | 3116 | 1 | 4 | -- | $811 / 16$ | 57.5 | 12-7/8 |
| 14 | -- | 13 3/4 | $183 / 4$ | 21 | $43 / 8$ | 11/8 | 4 | -- | $93 / 8$ | 70 | 12-1 |

[^30]
## TEES

| $\begin{aligned} & \text { Size } \\ & \text { (In.) } \end{aligned}$ | A |  | B |  | $\begin{aligned} & C \pm 1 / 8 \\ & (\ln .) \end{aligned}$ | $\begin{aligned} & \text { Wt. † } \\ & \text { (Lb.) } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{gathered} \mathrm{PM} \pm 1 / 16 \\ (\ln .) \end{gathered}$ | $\begin{gathered} \mathrm{HLU} \pm 1 / 8 \\ \text { (In.) } \end{gathered}$ | $\begin{gathered} \mathrm{PM} \pm 1 / 16 \\ \text { (In.) } \end{gathered}$ | $\begin{aligned} & \mathrm{HLU} \pm 1 / 8 \\ & \text { (In.) } \end{aligned}$ |  |  |
| 1 | $21 / 2$ | $31 / 2^{*}$ | 5 | 7 | $13 / 16$ | 0.8 |
| 11/2 | $23 / 4$ | 4* | $51 / 2$ | 8 | $15 / 16$ | 0.9 |
| 2 | $313 / 16$ | $41 / 2^{*}$ | 7 5/8 | 9 | 113/16 | 2.1 |
| 3 | $47 / 16$ | $51 / 2^{*}$ | 8 7/8 | 11 | 11316 | 3.4 |
| 4 | $51 / 16$ | $61 / 2^{*}$ | 10 1/8 | 13 | 113/16 | 5.3 |
| 6 | -- | 8 | -- | 16 | 113/16 | 11.2 |
| 8 | -- | $7^{11 / 16}$ | -- | $153 / 8$ | 2 5/8 | 15.5 |
| 10 | -- | $123 / 16$ | -- | $243 / 8$ | 4 | 29.3 |
| 12 | -- | $133 / 16$ | -- | 26 3/8 | 4 | 38.8 |
| 14 | -- | 13 5/8 | -- | 271/4 | 4 | 40.8 |

Fig. 275C
Tee, Socket


Tolerance Exception $\underline{\underline{275 \mathrm{C} \times 12} \times 10} \frac{\frac{A \pm 1 / 8}{\frac{A \pm 1 / 8}{A \pm 1 / 8}}}{\underline{275}}$

Fig. 275F
Tee, Flanged


| $\begin{aligned} & \text { Size } \\ & \text { (In.) } \end{aligned}$ | A |  | B |  | C Ref (In.) | D Ref <br> (In.) | E Ref <br> (In.) | F Ref <br> (In.) | $\begin{aligned} & \text { Wt. } \dagger \\ & \text { (Lb.) } \end{aligned}$ | BoltsNo/Size |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{gathered} \mathrm{PM} \pm 1 / 16 \\ \text { (In.) } \\ \hline \end{gathered}$ | $\begin{aligned} & \mathrm{HLU} \pm 1 / 8 \\ & \text { (In.) } \end{aligned}$ | $\begin{gathered} \mathrm{PM} \pm 1 / 16 \\ \text { (In.) } \\ \hline \end{gathered}$ | HLU $\pm 1 / 8$ <br> (In.) |  |  |  |  |  |  |
| 1 | 3 15/16 | 415/16 | 7 \%/8 | $97 / 8$ | $41 / 4$ | 7/8 | 5/8 | $31 / 8$ | 2.9 | 4-1/2 |
| 11/2 | $413 / 16$ | $5 \%$ | $95 / 8$ | 11 1/8 | 5 | $13 / 16$ | 5/8 | $37 / 8$ | 5.0 | 4-1/2 |
| 2 | $41 / 2$ | $6 \% 16$ | 9 | $131 / 8$ | 6 | $11 / 16$ | $3 / 4$ | $43 / 4$ | 7.6 | 4-5/8 |
| 3 | $51 / 2$ | $7 \%$ | 11 | $151 / 8$ | $71 / 2$ | $11 / 4$ | $3 / 4$ | 6 | 12.6 | 4-5/8 |
| 4 | $61 / 2$ | $8 \%$ | 13 | 17 1/8 | 9 | $13 / 8$ | $3 / 4$ | $71 / 2$ | 19.0 | 8-5/8 |
| 6 | -- | 8 | -- | 16 | 11 | $1 \% 16$ | 7/8 | $911 / 2$ | 32.7 | 8-3/4 |
| 8 | -- | 9 | -- | 18 | 13 1/2 | $21 / 16$ | 7/8 | $113 / 4$ | 51.7 | 8-3/4 |
| 10 | -- | 11 | -- | 22 | 16 | $31 / 16$ | 1 | $141 / 4$ | 90 | $12-7 / 8$ |
| 12 | -- | 12 | -- | 24 | 19 | $31 / 16$ | 1 | 17 | 125 | 12-7/8 |
| 14 | -- | 18 | -- | 36 | 21 | $43 / 8$ | $11 / 8$ | $183 / 4$ | 180 | 12-1 |


| Size <br> (In.) | A |  | B Ref <br> (In.) | C Ref <br> (In.) | D Ref <br> (In.) | E Ref <br> (In.) | F Ref <br> (In.) | G |  | Wt. $\dagger$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{gathered} \text { PM } \pm^{1 / 166} \\ \text { (In.) } \end{gathered}$ | $\mathrm{HLU} \pm 1 / 8$ <br> (In.) |  |  |  |  |  | $\begin{gathered} \text { PM } \pm 1 / 16 \\ \text { (In.) } \end{gathered}$ | $\mathrm{HLU} \pm 1 / 8$ <br> (In.) | One Flg (Lb.) | Two Flgs (Lb.) |
| 1 | 3 15/16 | $4{ }^{15 / 16^{*}}$ | $41 / 4$ | 7/8 | 7/8 | $31 / 8$ | $13 / 16$ | $21 / 2$ | $31 / 2$ | 1.5 | 2.2 |
| 11/2 | 4 5/16 | $5 \%$ * | 5 | 13/16 | 5/8 | $37 / 8$ | $15 / 16$ | $23 / 4$ | 4 | 2.2 | 3.5 |
| 2 | $57 / 8$ | $6 \%$ * | 6 | 13/16 | $3 / 4$ | $43 / 4$ | 113/16 | $313 / 16$ | $41 / 2$ | 3.9 | 5.8 |
| 3 | $61 / 2$ | 7 \% 16 * | $711 / 2$ | 13/16 | $3 / 4$ | 6 | 113/16 | $47 / 16$ | $51 / 2$ | 7.0 | 10.6 |
| 4 | $71 / 8$ | 8 \% 16 * | 9 | $11 / 2$ | $3 / 4$ | $71 / 2$ | 113/16 | -- | $611 / 2$ | 11.4 | 17.4 |
| 6 | -- | $10^{1 / 16}$ | 11 | 1916 | 7/8 | $91 / 2$ | 13/16 | 6 | 8 | 19.3 | 27.5 |
| 8 | -- | $101 / 4$ | $131 / 2$ | $21 / 16$ | 7/8 | $113 / 4$ | $25 / 8$ | -- | $711 / 16$ | 22.2 | 28.9 |
| 10 | -- | $16^{7 / 16}$ | 16 | $31 / 16$ | 1 | $14^{1 / 4}$ | 4 | -- | $123 / 16$ | 60 | 90 |
| 12 | -- | $17^{7 / 16}$ | 19 | $31 / 16$ | 1 | 17 | 4 | -- | $133 / 16$ | 95 | 140 |

Fig. 275S* Tee, Flanged x Socket

*" PM available in CL only

* Available on order only - nonreturnable
$\dagger$ CL weight, multiply by 1.07 for RB, 1.1 for ZC


## LATERALS

Fig. 266C Lateral, Socket


Fig. 266F*
Lateral, Flanged


| Size <br> (In) | $\mathrm{A} \pm 1 / 4$ <br> (In.) | $\begin{gathered} \hline \mathrm{B} \pm 1 / 4 \\ \text { (In.) } \end{gathered}$ | $\begin{gathered} C \pm 1 / 8 \\ (\mathrm{In} .) \end{gathered}$ | $\begin{aligned} & \text { Wt. † } \\ & \text { (Lb.) } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: |
| 2 | 10 1/8 | $71 / 2$ | $1^{13 / 16}$ | 2.0 |
| 3 | $117 / 8$ | $8{ }^{15} 16$ | $1^{13 / 16}$ | 3.7 |
| 4 | $13^{11 / 16}$ | 11 | $1^{13 / 16}$ | 8 |
| 6 | $24^{1 / 2}$ | $173 / 8$ | $1^{13 / 16}$ | 13.9 |
| 8 | $29^{1 / 4}$ | $215 / 16$ | $25 / 8$ | 35.5 |
| 10 | $367 / 8$ | $26^{7 / 16}$ | 4 | 51.7 |
| 12 | $431 / 4$ | 31 15/16 | 4 | 69.1 |


| $\begin{aligned} & \text { Size } \\ & \text { (In.) } \end{aligned}$ | $\begin{gathered} \mathrm{A} \pm 1 / 8 \\ \text { (In.) } \end{gathered}$ | $\begin{aligned} & \mathrm{B} \pm 1 / 8 \\ & \text { (In.) } \\ & \hline \end{aligned}$ | C Ref <br> (In.) | D Ref <br> (In.) | E Ref <br> (In.) | F Ref <br> (In.) | $\begin{aligned} & \text { Wt. } \dagger \\ & \text { (Lb.) } \end{aligned}$ | Bolts No/Size |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2 | 12 1/2 | $8^{11 / 16}$ | 6 | $43 / 4$ | $3 / 4$ | $11 / 16$ | 7.6 | 4-5/8 |
| 3 | $141 / 2$ | $10^{1 / 8}$ | $71 / 2$ | 6 | $3 / 4$ | $11 / 4$ | 12.6 | 4-5/8 |
| 4 | $16^{11 / 16}$ | $121 / 2$ | 9 | $71 / 2$ | $3 / 4$ | $13 / 8$ | 19.0 | 8-5/8 |
| 6 | 28 5/8 | $197 / 16$ | 11 | $911 / 2$ | 7/8 | 1916 | 32.7 | 8-3/4 |
| 8 | $313 / 4$ | 22916 | $131 / 2$ | $113 / 4$ | 7/8 | $21 / 16$ | 51.7 | 8-3/4 |
| 10 | $453 / 8$ | $30^{11 / 16}$ | 16 | $141 / 4$ | 1 | $31 / 16$ | 112 | 12-7/8 |
| 12 | 51 3/4 | $363 / 16$ | 19 | 17 | 1 | $31 / 16$ | 152 | 12-7/8 |

Note: Reducing Laterals and crosses are available on request.

## CROSSES

Fig. 285C


| Size <br> (In) | $\mathrm{A} \pm 1 / 4$ <br> $(\ln )$. | $\mathrm{B} \pm 1 / 8$ <br> $(\ln )$. | $\mathrm{C} \pm 1 / 8$ <br> (In.) | $\mathrm{Wt} . \dagger$ <br> $(\mathrm{Lb})$. |
| :---: | :---: | :---: | :---: | :---: |
| 2 | $63 / 8$ | $33 / 16$ | $113 / 16$ | 1.4 |
| 3 | 8 | 4 | $13 / 16$ | 2.3 |
| 4 | $105 / 8$ | $55 / 16$ | $13 / 16$ | 5.5 |
| 6 | 16 | 8 | $13 / 16$ | 15.7 |
| 8 | $153 / 8$ | $711 / 16$ | $25 / 8$ | 15.5 |
| 10 | $243 / 8$ | $123 / 16$ | 4 | 45.6 |
| 12 | $263 / 8$ | $133 / 16$ | 4 | 57.2 |


| $\begin{aligned} & \text { Size } \\ & \text { (In.) } \end{aligned}$ | $\begin{gathered} \mathrm{A} \pm 1 / 8 \\ \text { (ln.) } \end{gathered}$ | $\begin{aligned} & \mathrm{B} \pm 1 / 8 \\ & \text { (ln.) } \end{aligned}$ | C Ref (In.) | $\begin{gathered} \hline \text { D Ref } \\ \text { (In.) } \end{gathered}$ | E Ref <br> (In.) | F Ref (In.) | Wt. $\dagger$ (Lb.) | Bolts No/Size |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2 | $83 / 4$ | $43 / 8$ | 6 | $43 / 4$ | $13 / 16$ | $3 / 4$ | 9.3 | 4-5/8 |
| 3 | 10 3/8 | $53 / 16$ | $71 / 2$ | 6 | $13 / 16$ | $3 / 4$ | 13.9 | 4-5/8 |
| 4 | 13 5/8 | $6^{13 / 16}$ | 9 | $71 / 2$ | $11 / 2$ | $3 / 4$ | 23.5 | 8-5/8 |
| 6 | 16 | 8 | 11 | $91 / 2$ | $19 / 16$ | 7/8 | 57.5 | 8-3/4 |
| 8 | 18 | 9 | $131 / 2$ | $113 / 4$ | $21 / 16$ | 7/8 | 71.7 | 8-3/4 |
| 10 | 22 | 11 | 16 | $141 / 4$ | 3116 | 1 | 126 | 12-7/8 |
| 12 | 24 | 12 | 19 | 17 | 31116 | 1 | 170 | 12-7/8 |

[^31]$\dagger$ CL weight, multiply by 1.07 for RB, 1.1 for ZC

## PIPE SUPPORT/WEAR PAD

Fig. 391
Pipe Support


| Size <br> (In) | R | $\mathrm{L} \pm 1 / 8$ <br> (In.) | TRef <br> (In.) |
| :---: | :---: | :---: | :---: |
| 1 | $1-1 / 16$ | 3 | $13 / 32$ |
| $11 / 2$ | $1-3 / 8$ | 3 | $7 / 16$ |
| 2 | $1-17 / 32$ | 4 | $11 / 32$ |
| 3 | $2-3 / 32$ | 4 | $11 / 32$ |
| 4 | $2-5 / 8$ | 4 | $3 / 8$ |
| 6 | $3-15 / 16$ | 4 | $5 / 8$ |
| 8 | $4-15 / 16$ | $5-5 / 8$ | $5 / 8$ |
| 10 | $6-1 / 8$ | $8-3 / 8$ | $3 / 4$ |
| 12 | $7-3 / 32$ | $8-3 / 8$ | $23 / 32$ |
| $14^{\star}$ | $7-25 / 32$ | $8-3 / 8$ | $25 / 32$ |

*Available on order only - nonreturnable.

## FLOOR DRAIN

Fig. 203
Sealable Floor Drain

| Size <br> (In.) | $\begin{gathered} \mathrm{A} \pm 1 / 8 \\ \text { (In.) } \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{B} \\ \text { (In.) } \end{gathered}$ | $\begin{gathered} \mathrm{C} \\ \text { (ln.) } \end{gathered}$ | $\begin{gathered} \mathrm{D} \\ \text { (In.) } \end{gathered}$ | $\begin{gathered} \mathrm{E} \\ (\mathrm{In} .) \end{gathered}$ | $\begin{gathered} \hline \mathrm{F} \pm 1 / 8 \\ \text { (In.) } \end{gathered}$ | $\begin{gathered} \mathrm{G} \\ \text { (ln.) } \end{gathered}$ | $\begin{gathered} \mathrm{H} \\ (\mathrm{In} .) \end{gathered}$ | $\begin{gathered} 1 \\ (\ln .) \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $6 \times 2$ | $61 / 4$ | $23 / 8$ | 2 | $63 / 8$ | 6 | $87 / 8$ | $53 / 4$ | 7 | $73 / 4$ |
| $6 \times 3$ | $61 / 4$ | $311 / 2$ | 2 | $63 / 8$ | 6 | $87 / 8$ | $53 / 4$ | 7 | $73 / 4$ |
| $6 \times 4$ | 6 | $41 / 2$ | 2 | $63 / 8$ | 6 | $87 / 8$ | $53 / 4$ | 7 | $73 / 4$ |
| $12 \times 4$ | $811 / 16$ | $41 / 2$ | 1916 | 13 3/8 | 8 | $151 / 2$ | $12^{3 / 4}$ | 14 | $14^{1 / 2}$ |
| $12 \times 6$ | $8^{11 / 16}$ | 6 5/8 | $1 \%$ | 13 3/8 | 8 | $151 / 2$ | $12^{3 / 4}$ | 14 | $14^{1 / 2}$ |
| $12 \times 8$ | 8 | 8 5/8 | $19 / 16$ | 13 3/8 | 8 | 15 1/2 | $12^{3 / 4}$ | 14 | $14^{1 / 2}$ |

Sealable Drain Dimensional Data


Sealable Drain Standard Configurations

| Description | Figure | Viton <br> Plug | $1 / 4$ <br> Solid Cover Plate <br> with O-Ring Seal | $1 / 4^{\prime \prime}$ Drilled <br> Drain Grate | 16 Gauge <br> Strainer Basket |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Clean Out | 203 CO | $\boxtimes$ | $\boxtimes$ |  |  |
| Floor Drain | 203 FD | $\boxtimes$ |  | $\boxtimes$ | $\boxtimes$ |
| Equipment Drain | $203 E D$ | $\boxtimes$ | $\boxtimes$ |  | $\boxtimes$ |

## CENTRICLAMP

## Physical Data



| Size <br> (In.) | Pressure Rating |  | Max Rec. Torque (In-Lbs.) | $\begin{array}{\|c} \text { Precision } \\ \text { O-Ring } \\ \text { Size } \\ \hline \end{array}$ | Wrench Size <br> (In.) |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{gathered} \text { EP } \\ @ 225^{\circ} \end{gathered}$ | VE <br> @175 ${ }^{\circ}$ |  |  |  |
| 2 | 150 | 150 | 50 | 333 | 7/16 |
| 3 | 150 | 150 | 75 | 342 | 7/16 |
| 4 | 150 | 150 | 150 | 428 | $1 / 2$ |
| 6 | 150 | 150 | 150 | 441 | $1 / 2$ |
| 8 | 150 | 125 | 175 | 448 | $1 / 2$ |

Fig. 36*
End Adapter


| $\begin{aligned} & \text { Size } \\ & \text { (In.) } \end{aligned}$ | A Ref <br> (In.) | B Ref <br> (In.) | C Ref (In.) | $\begin{aligned} & \text { Wt. † } \\ & \text { (Lb.) } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: |
| 2 | $33 / 4$ | $21 / 16$ | $1^{13 / 16}$ | 0.5 |
| 3 | 5 | $21 / 16$ | $1^{13 / 16}$ | 0.7 |
| 4 | $63 / 8$ | $21 / 16$ | $1^{13 / 16}$ | 1.2 |
| 6 | $87 / 8$ | $21 / 16$ | $113 / 16$ | 2.2 |
| 8 | 11 1/2 | $21 / 16$ | $1{ }^{13 / 16}$ | 3.8 |

Fig. 38* SS Clamp


|  |  |  |  | Nut(s) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Size <br> (In.) | A Ref <br> (In.) | B Ref <br> (In.) | C Ref <br> (In.) | No. | Size <br> (In.) | Wt. $\dagger$ <br> $($ Lb. $)$ |
| 2 | $15 / 16$ | 4 | 3 | 1 | $7 / 16$ | 0.5 |
| 3 | $13 / 8$ | $51 / 4$ | $35 / 8$ | 1 | $7 / 16$ | 0.7 |
| 4 | $13 / 4$ | 7 | 5 | 1 | $1 / 2$ | 1.2 |
| 6 | $21 / 16$ | $91 / 4$ | $55 / 8$ | 1 | $1 / 2$ | 2.4 |
| 8 | 2916 | 12 | $71 / 2$ | 1 | $1 / 2$ | 5.5 |

[^32]Fig. 39* Blind Flange


| Size <br> (In.) | A Ref <br> (In.) | B Ref <br> (In.) | C Ref <br> (In.) |
| :---: | :---: | :---: | :---: |
| 2 | $33 / 4$ | $11 / 16$ | $31 / 8$ |
| 3 | 5 | $11 / 8$ | $45 / 16$ |
| 4 | $63 / 8$ | $11 / 4$ | $55 / 16$ |
| 6 | $87 / 8$ | $11 / 2$ | $715 / 16$ |
| 8 | $111 / 2$ | 2 | $105 / 16$ |

## ASSEMBLED FITTINGS REFERENCE DIMENSIONS

Fig. 8C*
Reducer Socket
$\rightarrow 1 \mathrm{kc}$
41 co

Fig. 6*
Adapter
Iron Pipe Male x Socket Female


| Size <br> (In.) | A <br> (In.) | B Ref <br> (In.) | C <br> (In.) | D <br> (In.) | Wt. $\dagger$ <br> (Lb.) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | $913 / 16$ | $85 / 8$ | $21 / 16$ | $15 / 16$ | 0.8 |
| $11 / 2$ | $9^{11 / 16}$ | $83 / 8$ | $2^{11 / 16}$ | $151 / 16$ | 1.1 |
| 2 | $103 / 16$ | $83 / 8$ | $31 / 8$ | $23 / 8$ | 1.6 |
| 3 | $103 / 16$ | $83 / 8$ | $43 / 16$ | $31 / 2$ | 2.6 |
| 4 | $103 / 16$ | $83 / 8$ | $51 / 4$ | $41 / 2$ | 3.6 |
| 6 | $103 / 16$ | $83 / 8$ | $77 / 8$ | $65 / 8$ | 6.6 |

Assemble using Fig. 6S Adapter and Fig. 14 Socket Coupling

Fig. 19
Stub Flange

| Size <br> (In.) | $\mathrm{A} \pm 1 / 8$ <br> (In.) | $\mathrm{B} \pm 1 / 8$ <br> (In.) | Wt. $\dagger$ <br> (Lb.) |
| :---: | :---: | :---: | :---: |
| 1 | $2^{5 / 8}$ | $1^{3 / 16}$ | 0.7 |
| $11 / 2$ | $3^{7 / 8}$ | $1^{5 / 16}$ | 1.3 |
| 2 | $3^{7 / 8}$ | $1^{13 / 16}$ | 2.0 |
| 3 | $3^{7 / 8}$ | $1^{13 / 16}$ | 3.0 |
| 4 | $3^{7 / 8}$ | $1^{13 / 16}$ | 4.9 |
| 6 | $3^{7 / 8}$ | $1^{13 / 16}$ | 6.5 |
| 8 | $5^{3 / 16}$ | $25 / 8$ | 11.7 |
| 10 | $81 / 4$ | 4 | 23.9 |
| 12 | $81 / 4$ | 4 | 33.9 |
| 14 | $83 / 8$ | 4 | 36.9 |

Assemble using Fig. 18 Socket Flange and
Fig. 17 Pipe Stub

Assemble using Fig. 18 Socket Flange and Fig. 6S Iron Pipe Adapter

| Size <br> (In.) | A Ref <br> (In.) | B Ref <br> (In.) | C Ref <br> $($ In. $)$ | Wt. $\dagger$ <br> $($ Lb. $)$ |
| :---: | :---: | :---: | :---: | :---: |
| 1 | $81 / 4$ | $15 / 16$ | $7 / 8$ | 1.0 |
| $11 / 2$ | $81 / 4$ | $15 / 16$ | $13 / 16$ | 1.8 |
| 2 | $81 / 4$ | $23 / 8$ | $13 / 16$ | 2.5 |
| 3 | $81 / 4$ | $31 / 2$ | $13 / 16$ | 4.1 |
| 4 | $81 / 4$ | $41 / 2$ | $11 / 2$ | 6.5 |
| 6 | $81 / 4$ | $65 / 8$ | $19 / 16$ | 9.3 |

Fig. 13*
Pipe Saddle


| Size <br> (In.) | $\begin{gathered} \mathrm{A} \pm 1 / 4 \\ \text { (In.) } \end{gathered}$ | $\begin{gathered} \mathrm{B} \pm 1 / 8 \\ \text { (ln.) } \\ \hline \end{gathered}$ | C Ref (In.) | Threaded Outlet NPT |  |  |  |  |  | Cement Outlet |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | 1/4 | 1/2 | $3 / 4$ | 1 | 11/4 | 11/2 | 1 | 13/4 | 2 | 3 | 4 | 6 | 8 | 10 |
| 2 | $41 / 4$ | $3 / 4$ | $2^{3} / 8$ |  |  |  |  |  |  | S |  |  |  |  |  |  |  |
| 3 | $53 / 4$ | 2 | $3^{3 / 8}$ | X | X | X | X | X | X | V | V | S |  |  |  |  |  |
| 4 | 8 | 2 | $4^{1 / 16}$ | XV | XV | XV | X | XV | X | V | V | S | S |  |  |  |  |
| 6 | 9 | 2 | $5^{1 / 8}$ | XV | XV | XV | XV | XV | XV | W | W | S | V | S |  |  |  |
| 8 | $10^{1 / 2}$ | 2 | $7^{7 / 16}$ | XV | XV | XV | XV | XV | XV | W | W | S | V | V | S |  |  |
| 10 | $131 / 2$ | $31 / 8$ | $10^{1 / 8}$ | XV | XV | XV | XV | XV | XV | W | W | S | V | V | V | S |  |
| 12 | $8^{3 / 8}$ | $3^{1 / 8}$ | $12^{3 / 16}$ | XV | XV | XV | XV | XV | XV | W | W | S | V | V | V | V | S |

* Available on order only - nonreturnable.

X=Fabricated using Fig 13 Cement Socket Outlet Pipe Saddle and Fig 33S Threaded Bushing Insert.

V=Fabricated using Fig 13 Cement Socket Outlet Pipe Saddle and Fig 33 Socket Reducer Bushing Insert.

S=Standard Pipe Saddle, no fabrication needed.

XV=Fabricated using Fig 13 Cement Socket Outlet Pipe Saddle, Fig 33 Socket Reducer Bushing and Fig 33S Threaded Bushing Insert.

W=Fabricated using Fig 13 Cement Socket Outlet Pipe Saddle and 2 or more Fig 33 Socket Reducer Bushing Inserts.
$\dagger$ CL weight, multiply by 1.07 for RB, 1.1 for ZC

Fig. 255CR* $90^{\circ}$ Short Radius Reducer, Socket


| Size <br> (In.) | A Ref <br> (In.) | B Ref <br> (In.) | C Ref <br> (In.) |
| :---: | :---: | :---: | :---: |
| $11 / 2$ | $2^{3 / 4}$ | $2^{15 / 16}$ | $15 / 16$ |
| 2 | $3^{131} 16$ | $3^{1 / 2}$ | $15 / 16$ |
| 3 | $4^{7 / 16}$ | $4^{5} / 8$ | $113 / 16$ |
| 4 | $51 / 16$ | $51 / 4$ | $113 / 16$ |
| 6 | 6 | $63 / 16$ | $113 / 16$ |
| 8 | $71 / 2$ | $71 / 2$ | $25 / 16$ |

Assemble using Fig. 255C Elbow and Fig. 33 Reducer Bushing

Fig. 255FR* $90^{\circ}$ Short Radius Reducer, Flanged


| Size <br> (In.) | A Ref <br> (In.) | B Ref <br> (In.) | C Ref <br> (In.) | D Ref <br> (In.) | E Ref <br> (In.) | F Ref <br> (In.) | Bolts <br> No/Size |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $11 / 2 \times 1$ | $45 / 16$ | $31 / 8$ | $41 / 4$ | $7 / 8$ | $63 / 16$ | $5 / 8$ | $4-1 / 2$ |
| $2 \times 11 / 2$ | $57 / 8$ | $37 / 8$ | 5 | $13 / 16$ | 7 | $5 / 8$ | $4-5 / 8$ |
| $3 \times 2$ | $61 / 2$ | $43 / 4$ | 6 | $13 / 16$ | $75 / 8$ | $3 / 4$ | $4-5 / 8$ |
| $4 \times 3$ | $71 / 8$ | 6 | $71 / 2$ | $13 / 16$ | $81 / 4$ | $3 / 4$ | $4-5 / 8$ |
| $6 \times 4$ | $81 / 16$ | $71 / 2$ | 9 | $11 / 2$ | $91 / 2$ | $3 / 4$ | $8-5 / 8$ |
| $8 \times 6$ | 101116 | $91 / 2$ | 11 | $19 / 16$ | $101 / 2$ | $7 / 8$ | $8-3 / 4$ |

Assemble using Fig. 255 C Elbow and Fig. 33 Reducer Bushing, Fig. 17 Pipe Stub and Fig. 18 Socket Flange

Fig. 265CR ${ }^{(3)}$ $45^{\circ}$ Reducer, Socket


Fig. 265FR ${ }^{(3)}{ }^{\text {* }}$ $45^{\circ}$ Reducer, Flanged

| Size <br> (In.) | A Ref <br> (In.) | B Ref <br> (In.) | C Ref <br> (In.) | D Ref <br> (In.) | E Ref <br> (In.) | F Ref <br> (In.) | Bolts <br> No/Size |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $6 \times 4$ | $127 / 8$ | $71 / 2$ | 9 | $11 / 2$ | $145 / 16$ | $3 / 4$ | $8-5 / 8$ |
| $8 \times 6$ | $173 / 16$ | $91 / 2$ | 11 | $19 / 16$ | $173 / 8$ | $7 / 8$ | $8-3 / 4$ |
| $10 \times 8$ | $2115 / 16$ | $113 / 4$ | $131 / 2$ | $21 / 16$ | $211 / 4$ | $7 / 8$ | $8-3 / 4$ |
| $12 \times 10$ | $247 / 16$ | $141 / 4$ | 16 | $31 / 16$ | $263 / 8$ | 1 | $12-7 / 8$ |

Assemble using Fig. 257C Elbow, Fig. 33 Reducer Bushing, Fig. 17 Pipe Stub and Fig. 18 Socket Flange


| Size <br> (In.) | A |  | B Ref <br> (In.) | C Ref (In.) | $\begin{aligned} & \text { D Ref } \\ & \text { (In.) } \\ & \hline \end{aligned}$ | E Ref <br> (In.) | F Ref <br> (In.) | $\begin{aligned} & \text { Bolts } \\ & \text { No/Size } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{gathered} \mathrm{PM} \pm 1 / 16 \\ (\mathrm{In} .) \end{gathered}$ | $\mathrm{HLU} \pm 1 / 8$ <br> (In.) |  |  |  |  |  |  |
| $11 / 2 \times 1$ | $37 / 8$ | 31316 | $31 / 8$ | $41 / 4$ | 7/8 | 5/8 | $53 / 4$ | 4-1/2 |
| $2 \times 11 / 2$ | 5 5/16 | $4 \% 16$ | $37 / 8$ | 5 | $13 / 16$ | 5/8 | 7 5/16 | 4-5/8 |
| $3 \times 2$ | $513 / 16$ | $51 / 16$ | $43 / 4$ | 6 | $13 / 16$ | $3 / 4$ | $7^{13 / 16}$ | 4-5/8 |
| $4 \times 3$ | $61 / 8$ | $61 / 16$ | 6 | $711 / 2$ | $13 / 16$ | $3 / 4$ | $81 / 8$ | 8-5/8 |
| $6 \times 4$ - | $6{ }^{13 / 16}$ | $71 / 16$ | $71 / 2$ | 9 | $11 / 2$ | 7/8 | $81 / 4$ | 8-3/4 |
| $8 \times 6$ | -- | $81 / 2$ | $911 / 2$ | 11 | $19 / 16$ | 7/8 | $8^{11 / 16}$ | 8-3/4 |
| $10 \times 8$ | -- | 1115/16 | $11^{3 / 4}$ | $131 / 2$ | $21 / 16$ | 1 | $11^{1 / 4}$ | 12-7/8 |
| $12 \times 10$ | -- | $12^{15 / 16}$ | $14^{1 / 4}$ | 16 | $31 / 16$ | 1 | 14 7/8 | 12-7/8 |

Assemble using Fig. 265F Elbow and Fig. 33 Reducer Bushing,
Assemble using Fig. 265C Elbow and Fig. 33
Reducer Bushing
Pipe Stubs and Fig 18 Socket Flanges

- 6" PM available in CL only
* Available on order only - nonreturnable.
(3) Reductions beyond one pipe size for reduced pressure applications are available. (See Fig. 33)

Fig. 275CR*
Reducer, Socket

Assemble using Fig 275C and Fig 33 Reducer Bushing


| Size <br> (In.) | PM $\pm 1 / 16$ |  | HLU $\pm 1 / 8$ | PM Ref | HLU Ref |
| :---: | :---: | :---: | :---: | :---: | :---: |

Fig. 37*
Adapter Nipple

Fig. 17
Assembly Pipe Stubs


| Size <br> (In.) | A Ref <br> (In.) | B Ref <br> (In.) | C Ref <br> (In.) | Wt. $\uparrow$ <br> (Lb.) |
| :---: | :---: | :---: | :---: | :---: |
| 2 | $33 / 4$ | $21 / 16$ | $413 / 16$ | 1.0 |
| 3 | 5 | $21 / 16$ | $413 / 16$ | 1.7 |
| 4 | $63 / 8$ | $21 / 16$ | $4^{13} 16$ | 2.2 |
| 6 | $87 / 8$ | $21 / 16$ | $413 / 16$ | 4.0 |
| 8 | $111 / 2$ | $21 / 16$ | $413 / 16$ | 6.3 |

Fig. 275FR ${ }^{(3)}$ *
Reducer,
Flanged
Single Size Reduction Shown


| Size <br> (In.) | A |  | B Ref <br> (In.) | C Ref <br> (In.) | $\begin{array}{\|l} \hline \text { D Ref } \\ \text { (In.) } \end{array}$ | $\begin{aligned} & \text { FRef } \\ & \text { (In.) } \end{aligned}$ | J Ref(ln.) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | PM Ref | HLU Ref |  |  |  |  |  |
| $11 / 2 \times 1$ | $45 / 16$ | $5 \%$ | 41/4 | 31/8 | 7/8 | 5/8 | $63 / 16$ |
| $2 \times 11 / 2$ | $57 / 8$ | $6 \%$ | 5 | 37/8 | 13/16 | 5/8 | 7 |
| $3 \times 2$ | $611 / 2$ | 7916 | 6 | $43 / 4$ | 13/16 | $3 / 4$ | 7 5/8 |
| $4 \times 3$ | $71 / 8$ | $8 \%$ | 71/2 | 6 | 13/16 | $3 / 4$ | $81 / 4$ |
| $6 \times 4$ | 81116 | $10^{1 / 16}$ | 9 | 71/2 | 11/2 | $3 / 4$ | $911 / 2$ |
| $8 \times 6$ |  | $101 / 4$ | 11 | 91/2 | 19/16 | 7/8 | 10 \% 16 |
| $10 \times 8$ |  | $16^{7 / 16}$ | $131 / 2$ | 113/4 | 21116 | 7/8 | $15^{11 / 16}$ |
| $12 \times 10$ |  | $17^{7 / 16}$ | 16 | 14114 | 311116 | 1 | $193 / 8$ |

## DIMENSIONS

Take off Dimensions for Adhesive Socket Fittings


Pipe Stop to Fittings' Center Line Dimensions

| $\begin{aligned} & \text { Size } \\ & \text { (In.) } \end{aligned}$ | $45^{\circ}$ Elbow |  | Short Radius 90́ Elbow | Long Radius $90^{\circ}$ Elbow | Tee |  | Lateral |  | Cross |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{gathered} \hline \mathrm{PM} \\ \mathrm{~A} \\ \text { (In.) } \\ \hline \end{gathered}$ | HLU A <br> (In.) | $\begin{gathered} \text { A } \\ \text { (In.) } \end{gathered}$ | $\begin{gathered} \text { A } \\ \text { (In.) } \end{gathered}$ | $\begin{gathered} \mathrm{PM} \\ \mathrm{~A} \\ (\mathrm{In} .) \end{gathered}$ | $\begin{gathered} \mathrm{HLU} \\ \mathrm{~A} \\ \text { (In.) } \\ \hline \end{gathered}$ | $\begin{gathered} \text { A } \\ \text { (In.) } \end{gathered}$ | $\begin{gathered} \text { B } \\ (\ln .) \end{gathered}$ | $\begin{gathered} \text { A } \\ \text { (In.) } \end{gathered}$ |
| 1 | 1 5/16 | 9/16 | $15 / 16$ | $313 / 16$ | $15 / 16$ | $25 / 16$ | -- | -- | -- |
| $11 / 2$ | 1 | 15/16 | $17 / 16$ | $4^{11 / 16}$ | $17 / 16$ | $2^{11 / 16}$ | -- | -- | -- |
| 2 | 17/16 | $11 / 16$ | 2 | $4^{11 / 16}$ | 2 | $2^{11 / 16}$ | $5^{11 / 16}$ | 13/16 | $13 / 8$ |
| 3 | 1 15/16 | $13 / 16$ | $25 / 8$ | $5{ }^{15 / 16}$ | $25 / 8$ | $3^{11 / 16}$ | $71 / 8$ | 11/8 | $2^{3 / 16}$ |
| 4 | $21 / 4$ | $23 / 16$ | $31 / 4$ | $73 / 16$ | $31 / 4$ | $4^{11 / 16}$ | 93/16 | 7/8 | $31 / 2$ |
| 6 | 2 15/16 | $33 / 16$ | $43 / 16$ | 9 | -- | $63 / 16$ | $15 \% 16$ | 5 5/16 | 63/16 |
| 8 | -- | 35/16 | $47 / 8$ | 12 | -- | 51116 | $18^{11 / 16}$ | 5 5/16 | 51/16 |
| 10 | -- | $3^{11 / 16}$ | -- | $13^{11 / 16}$ | -- | $83 / 16$ | $227 / 16$ | $67 / 16$ | $83 / 16$ |
| 12 | -- | $4^{11 / 16}$ | -- | $163 / 16$ | -- | 93/16 | $27^{15 / 16}$ | $75 / 16$ | 93/16 |
| 14 | -- | $53 / 8$ | -- | 18 | -- | 9 5/8 | -- | -- | -- |

How to Read Flanged or Reducing Fittings
tee

Run x Run x Branch

( $\mathrm{A} \times \mathrm{B} \times \mathrm{C}$ )

Run x Run x Branch
( $\mathrm{A} \times \mathrm{B} \times \mathrm{C}$ )


CROSS


D
Run $\times$ Run $\times$ Branch $\times$ Branch
( $\mathrm{A} \times \mathrm{B} \times \mathrm{C} \times \mathrm{D}$ )

The sequences illustrated should be used when describing fitting outlets. Drawings or sketches showing outlet types, locations, sizes and dimensional requirements are required for more complicated fitting configurations.

## Special Configuration Fittings <br> Contact NOV Fiber Glass Systems for Details

- 11/16 through 12" Orifice flanges, 150\# \& 300\#
- Odd degree elbows, $15,22^{1 / 2}, 30 \& 60$ degree
- 5D Socket \& Flanged Elbows
- Sump Fittings
- 4" thru 10" Reducing Lateral, Socket, Fig. 266CR
- 2" thru 12 " Fig 267F Long Turn Tee, Socket, Fig. 267C
- 2" thru 12" Long Turn Tee, Flanged, Fig 267F
- 2" thru $12^{\prime \prime} 45^{\circ}$ Double Y Branch, Socket, Fig. 268C
- 2" thru 12 " $45^{\circ}$ Double Y Branch, Flanged, Fig. 268F
-2" thru $12^{\prime \prime} 90^{\circ}$ Double Y Branch, Socket, Fig. 269C
- 2 " thru $12^{\prime \prime} 90^{\circ}$ Double Y Branch, Flanged, Fig. 269F


## ADHESIVES

## Weldfast ZC-275 Epoxy Adhesive for Adhesive Socket Joints

Order for Z-Core epoxy piping systems. Weldfast ZC-275 adhesive can also be used to bond RB and CL pipe and fittings. Usage should be limited to applications recommended for both Z-Core product and the pipe and fittings grade being used.

## Contents:

Adhesive (Part A)
Hardener (Part B)
Wooden Stir Stick
Plastic Putty Knife
Fabrication Instructions

| No. 1 Kit Size- $1 / 2$ Pint |  |
| :---: | :---: |
| Number of Bonds Per Kit |  |
| Joints | Pipe Size |
| 12 | 1 " connections |
| 10 | $11 / 2^{\prime \prime}$ connections |
| 8 | 2 " connections |
| 5 | $3^{\prime \prime}$ connections |
| 3 | 4 " connections |
| 2 | 6 " connections |
| 1 | 8 " connections |
| $1 / 2$ | 10 " connections |
| $1 / 2$ | $12^{\prime \prime}$ connections |



For complete instructions, refer to fab Bulletin D4090 included in each kit of WELDFAST ZC-275 Adhesive.

## Weldfast CL-200-QS Part "C"



Accelerator used with WELDFAST CL-200 to provide a quick set vinyl ester adhesive. Joints fabricated with this quick set adhesive can be made and quickly cured in as little as one hour (at room temperature) compared to 24 hours (at room temperature) for conventional adhesives.

## Weldfast CL-200

## Contents:

Adhesive (Part A)
Catalyst
Wooden Stir Stick
Plastic Putty Knife
Fabrication Instructions

Order for CL-2030 and CL-1520 vinyl ester piping systems.

| No. 1 Kit Size- $1 / 2$ Pint |  |
| :---: | :---: |
| Number of Bonds Per Kit |  |
| Joints | Pipe Size |
| 12 | 1 " connections |
| 10 | $11 / 2^{\prime \prime}$ connections |
| 8 | 2 " connections |
| 5 | 3 " connections |
| 3 | 4 " connections |
| 2 | 6 " connections |
| 1 | 8 " connections |
| $1 / 2$ | $10^{\prime \prime}$ connections |
| $1 / 2$ | 12 " connections |
| $1 / 3$ | 14 " connections |



For complete instructions refer to fab Bulletin D4210 included in each kit of WELDFAST CL-200.

## ACCESSORIES

Strap Clamp Kit ${ }^{*}$


Silicone Rubber Heat Blanket*


For Heat Curing 1"-20" connections

| Pipe Size | Model Number for <br> Pipe Size |
| :---: | :---: |
| $1-3$ inches | B |
| $4-8$ inches | C |
| $10-14$ inches | D |
| $16-20$ inches | E |

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## Bondstrand $^{\text {Tm }}$ 2000, 4000, 5000 and 7000 Fittings Dimensions

Introduction
The Quick-Lock bell end has a $1 / 2^{\circ}$ taper and is the standard end configuration. All other end configurations, including size reductions, are made to order. Flanges are drilled in accordance with ANSI B16.5, Class 150. Other drilling specifications are available upon request. For pressure and temperature ratings; refer to product data sheet for specific series.
Tolerance for centerline-to-face dimensions on fittings with flanged ends is $\pm 1 / 8$ inch; for centerline-to-face dimensions with bell-end fittings $\pm^{1 / 16}$ inch: and for angular measures is $\pm 1^{\circ}$.
Shipping weights are approximate.

## Manufacturing Methods

|  | Material | Applicable Fittings |
| :---: | :---: | :---: |
| Filament winding | Epoxy resin <br> Vinyl ester resin <br> Glass fibers | Elbows, tees, couplings <br> Flanges, laterals, nipples <br> Saddles, crosses, reducers <br> Maintenance couplings <br> Special angle fittings |
| Compression molding | Epoxy resin Vinyl ester resin Discontinuous glass fibers | Flanges, bushings, plugs Caps, blind flanges Elbows, $45^{\circ}, 90^{\circ}$; tees Eccentric reducers |
| Machining | - 316 stainless steel | - Orifice flanges <br> - Saddles for reductions |

## Assembly Instructions

Consult the following publications for installation details regarding Bondstrand Series 2000, 4000, 5000 and 7000 piping systems.
Quick-Lock Adhesive-bonded Bell and Spigot Joints, Contains instructions for preparing the Quick-Lock adhesive joint, using end preparation tools, applying and curing adhesives and mounting Bondstrand flanges on fiberglass pipe. Usage instructions for the various Bondstrand adhesives are included in the adhesive kits.
Assembly Instructions for Bondstrand fiberglass flanges, Contains information pertinent to selection of gaskets, nuts, washers, and bolts when joining Bondstrand fiberglass flanges to fiberglass flanges and to flanges of other materials. Includes recommended bolt torques and bolt tightening sequence diagrams.
Maintenance Coupling Assembly for butt-end joints, Assembly instructions for the Bondstrand maintenance coupling.
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Fittings are filament wound unless otherwise indicated. Fittings marked with an asterisk (*) are molded.

| Nom Pipe Size | Laying Length (L) | Overall Length (B) |  | Socket Depth ( $\mathrm{D}_{\mathrm{s}}$ ) | Approx Wt |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in. $\cdot \mathrm{mm}$ | in. $\cdot \mathrm{mm}$ | in. $\cdot \mathrm{mm}$ |  | in. $\cdot \mathrm{mm}$ | lb. ${ }^{\text {kg }}$ |  |
| 125 | 2.5665 | 3.62 | 92 | 1.0627 | 1 | 0.5 |
| $11 / 240$ | 3.1981 | 4.44 | 113 | 1.2532 | 1 | 0.5 |
| 250 | 3.0076 | 4.82 | 122 | 1.8246 | 1 | 0.5 |
|  | 2.01* 51 | 3.83 | 97 | 1.8246 | 1 | 0.5 |
| 380 | 4.50114 | 6.32 | 161 | 1.8246 | 3 | 1.4 |
|  | 2.61* 66 | 4.43 | 113 | 1.8246 | 2 | 0.9 |
| 4100 | 6.00152 | 7.82 | 199 | 1.8246 | 4 | 1.8 |
|  | 3.69* 94 | 5.51 | 140 | 1.8246 | 3 | 1.4 |
| 6150 | 9.00229 | 11.25 | 286 | $2.25 \quad 57$ | 8 | 3.6 |
|  | 5.25* 133 | 7.50 | 191 | $2.25 \quad 57$ | 7 | 3.2 |
| 8200 | 12.00305 | 14.50 | 368 | 2.5064 | 15 | 6.8 |
| 10250 | 15.00381 | 17.75 | 451 | 2.7570 | 25 | 11.3 |
| 12300 | 18.00457 | 21.00 | 533 | 3.0076 | 41 | 18.6 |
| 14350 | 14.12359 | 17.62 | 448 | 3.5089 | 37 | 16.8 |
| 16400 | 15.62397 | 19.62 | 498 | 4.00102 | 68 | 30.8 |

## $90^{\circ}$ Flanged Elbows



Flanged $90^{\circ}$ elbows feature filament-wound bodies and filament-wound ( $f / w$ ) or molded ( m ) flanges. They are available in ANSI short-radius ( $\mathrm{s} / \mathrm{r}$ ) or long-radius (I/r) laying lengths. Flanged short-radius elbows meeting ANSI laying lengths are not available in $1,1^{1 / 2}$, 14 or 16 inch sizes. Fittings marked with two asterisks (**) are available only with filament-wound flanges.

$90^{\circ}$ Combination Elbows


| Nom Pipe Size | Radius <br> Type | Laying Length $\left(\mathrm{L}_{1}\right)$ |  | Flange ThicknessFaceAt Hub  <br> (t) (D) |  |  |  | Overall Length (B) |  | Laying Length ( $\mathrm{L}_{2}$ ) |  | Socket Depth ( $\mathrm{D}_{\mathrm{S}}$ ) |  | Approx Wt Flange Type (m) $\qquad$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in. $\cdot \mathrm{mm}$ |  | in. $\cdot \mathrm{mm}$ |  | in. mm |  | in. mm |  | in. $\cdot \mathrm{mm}$ |  | in. $\cdot \mathrm{mm}$ |  | in. $\cdot \mathrm{mm}$ |  | $\mathrm{lb} \cdot \mathrm{kg}$ |  | $\mathrm{lb} \cdot \mathrm{kg}$ |  |
| 125 | $1 / r$ | 5.00 | 127 | 1.13** |  | 1.13 | 29 | 3.62 | 92 | 2.56 | 65 | 1.06 | 27 | - | - | 2 | 0.9 |
| $11 / 240$ | $1 / \mathrm{r}$ | 6.00 | 152 | 1.38** |  | 1.38 | 35 | 4.44 | 113 | 3.19 | 81 | 1.25 | 32 | - | - | 3 | 1.4 |
| 250 | $s / r$ | 4.50 | 114 | 1.00 | 25 | 2.00 | 51 | 6.56 | 167 | 4.75 | 121 | 1.81 | 46 | 4 | 1.8 | 3 | 1.4 |
|  | 1/r | 6.50 | 165 | 1.00 | 25 | 2.00 | 51 | 8.56 | 217 | 6.75 | 171 | 1.81 | 46 | 4 | 1.8 | 4 | 1.8 |
| 380 | $s / r$ | 5.50 | 140 | 1.13 | 29 | 2.00 | 51 | 7.56 | 192 | 5.75 | 146 | 1.81 | 46 | 6 | 2.7 | 5 | 2.3 |
|  | 1/r | 7.75 | 197 | 1.13 | 29 | 2.00 | 51 | 9.81 | 249 | 8.00 | 203 | 1.81 | 46 | 6 | 2.7 | 6 | 2.7 |
| 4100 | $s / r$ | 6.50 | 165 | 1.25 | 32 | 2.00 | 51 | 8.56 | 217 | 6.75 | 171 | 1.81 | 46 | 8 | 3.6 | 8 | 3.6 |
|  | 1/r | 9.00 | 229 | 1.25 | 32 | 2.00 | 51 | 11.06 | 281 | 9.25 | 235 | 1.81 | 46 | 10 | 4.5 | 10 | 4.5 |
| 6150 | $s / r$ | 8.00 | 203 | 1.75 | 44 | 2.38 | 60 | 10.50 | 267 | 8.25 | 210 | 2.25 | 57 | 16 | 7.3 | 14 | 6.4 |
|  | $1 / \mathrm{r}$ | 11.50 | 292 | 1.75 | 44 | 2.38 | 60 | 14.00 | 356 | 11.75 | 298 | 2.25 | 57 | 20 | 9.1 | 18 | 8.2 |
| 8200 | $s / r$ | 9.00 | 229 | 2.00 | 51 | 2.63 | 67 | 11.75 | 298 | 9.25 | 235 | 2.50 | 64 | 26 | 11.8 | 23 | 10.4 |
|  | 1/r | 14.00 | 356 | 2.00 | 51 | 2.63 | 67 | 16.75 | 425 | 14.25 | 362 | 2.50 | 64 | 32 | 14.5 | 31 | 14.1 |
| 10250 | $s / r$ | 11.00 | 279 | 2.00 | 51 | 2.88 | 73 | 14.00 | 356 | 11.25 | 286 | 2.75 | 70 | 38 | 17.2 | 34 | 15.4 |
|  | 1/r | 16.50 | 419 | 2.00 | 51 | 2.88 | 73 | 19.50 | 495 | 16.75 | 425 | 2.75 | 70 | 45 | 20.4 | 45 | 20.4 |
| 12300 | $\mathrm{s} / \mathrm{r}$ | 12.00 | 305 | 2.13 | 54 | 3.13 | 80 | 15.25 | 387 | 12.25 | 311 | 3.00 | 76 | 61 | 27.7 | 61 | 27.7 |
|  | 1/r | 19.00 | 483 | 2.13 | 54 | 3.13 | 80 | 22.25 | 565 | 19.25 | 489 | 3.00 | 76 | 70 | 31.8 | 70 | 31.8 |
| 14350 | 1/r | 21.50 | 546 | 2.88** |  | 3.75 | 95 | 17.62 | 448 | 14.12 | 359 | 3.50 | 89 | - | - | 85 | 38.6 |
| 16400 | $1 / \mathrm{r}$ | 24.00 | 610 | $3.25 * *$ |  | 4.25 | 108 | 19.62 | 498 | 15.62 | 397 | 4.00 | 102 | - | - | 104 | 47.2 |

## $45^{\circ}$ Elbows



Fittings are filament wound unless otherwise designated. Fittings marked with an asterisk (*) are molded.

| Nom Pipe Size |  | Laying Length (L) |  | Overall Length (B) |  | Socket Depth ( $\mathrm{D}_{\mathrm{s}}$ ) |  | Approx Wt |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in. $\cdot \mathrm{mm}$ |  | in. $\cdot \mathrm{mm}$ |  | in. $\cdot \mathrm{mm}$ |  | in. $\cdot \mathrm{mm}$ |  | lb. kg |  |
| 1 | 25 | 0.88 | 22 | 1.94 | 49 | 1.06 | 27 | 1 | 0.5 |
| $11 / 2$ | 40 | 1.12 | 28 | 2.37 | 60 | 1.25 | 32 | 1 | 0.5 |
| 2 | 50 | 1.38 | 35 | 3.20 | 81 | 1.82 | 46 | 1 | 0.5 |
|  |  | 1.38* | 35 | 3.20 | 81 | 1.82 | 46 | 1 | 0.5 |
| 3 | 80 | 2.00 | 51 | 3.82 | 97 | 1.82 | 46 | 2 | 0.9 |
|  |  | 1.62* | 41 | 3.43 | 87 | 1.82 | 46 | 2 | 0.9 |
| 4 | 100 | 2.50 | 64 | 4.32 | 110 | 1.82 | 46 | 3 | 1.4 |
|  |  | 2.42* | 61 | 4.23 | 107 | 1.82 | 46 | 3 | 1.4 |
| 6 | 150 | 3.75 | 95 | 6.00 | 152 | 2.25 | 57 | 5 | 2.3 |
|  |  | 3.31* | 84 | 5.56 | 141 | 2.25 | 57 | 8 | 3.6 |
| 8 | 200 | 5.00 | 127 | 7.50 | 191 | 2.50 | 64 | 9 | 4.1 |
| 10 | 250 | 6.25 | 159 | 9.00 | 229 | 2.75 | 70 | 16 | 7.3 |
| 12 | 300 | 7.50 | 191 | 10.50 | 267 | 3.00 | 76 | 26 | 11.8 |
| 14 | 350 | 4.69 | 119 | 8.19 | 208 | 3.50 | 89 | 38 | 17.2 |
| 16 | 400 | 5.38 | 137 | 9.38 | 238 | 4.00 | 102 | 45 | 20.4 |

$45^{\circ}$ Flanged Elbows


Flanges are filament wound unless otherwise designated. Fittings marked with an asterisk (*) have molded flanges. Laying lengths meet ANSI criteria.
Fittings with double asterisk (**) do not meet ANSI laying length.

| Nom Pipe Size |  | Laying Length (L) |  | Flange Thickness |  |  |  | Approx |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | At Face <br> (t) | At Hub <br> (D) |  | (m) |  | (f/w) |  |
|  | -mm |  |  | in. ${ }^{\text {c }}$ | mm |  |  | in. $\cdot \mathrm{m}$ |  |  | kg |  |  |
| 2 | 50 | 2.50 | 64 | 1.00 | 25 | 2.00 | 51 | 5 | 2.3 | 4 | 1.8 |
| 3 | 80 | 3.00 | 76 | 1.13 | 29 | 2.00 | 51 | 7 | 3.2 | 6 | 2.7 |
| 4 | 100 | 4.00 | 102 | 1.25 | 32 | 2.00 | 51 | 10 | 4.5 | 10 | 4.5 |
| 6 | 150 | 5.00 | 127 | 1.75 | 44 | 2.38 | 60 | 21 | 9.5 | 17 | 7.7 |
| 8 | 200 | 5.50 | 140 | 2.00 | 51 | 2.63 | 67 | 32 | 14.5 | 29 | 13.2 |
| 10 | 250 | 6.50 | 165 | 2.00 | 51 | 2.88 | 73 | 50 | 22.7 | 47 | 21.3 |
| 12 | 300 | 7.50 | 191 | 2.13 | 54 | 3.13 | 80 | 76 | 34.5 | 70 | 31.8 |
| 14 | 350 | 12.25** | 311 | 2.81 | 71 | 3.81 | 97 | - | - | 59 | 26.8 |
| 16 | 400 | 13.94** | 354 | 3.25 | 83 | 4.25 | 108 | - | - | 77 | 34.9 |

$45^{\circ}$ Combination Elbows


Flanges are available in molded ( $m$ ) or filament-wound ( $f / w$ ) construction. Dimensions marked with an asterisk (*) indicate molded flanges.
Fittings with double asterisk (**) do not meet ANSI laying length.

| Nom Pipe Size |  | Laying Length ( $\mathrm{L}_{1}$ ) |  | At Face <br> (t) |  | At Hub <br> (D) |  | Overall Length (B) |  | Laying Length $\left(\mathrm{L}_{2}\right)$ |  | Socket Depth ( $\mathrm{D}_{\mathrm{s}}$ ) |  |  | App Flang <br> (m) | Wt ype | v) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | mm | in.• m |  | in. |  | in.• | mm | in. mm |  | in. mm |  | in. $\cdot \mathrm{mm}$ |  | $\mathrm{lb} \cdot \bullet \mathrm{kg}$ |  | lb. kg |  |
| *2 | 50 | 2.50 | 64 | 1.00 | 25 | 2.00 | 51 | 4.56 | 116 | 2.75 | 70 | 1.82 | 46 | 3 | 1.4 | *3 | 1.4 |
| *3 | 80 | 3.00 | 76 | 1.13 | 29 | 2.00 | 51 | 5.06 | 129 | 3.25 | 83 | 1.82 | 46 | 5 | 2.3 | *4 | 1.8 |
| *4 | 100 | 4.00 | 102 | 1.25 | 32 | 2.00 | 51 | 6.06 | 154 | 4.25 | 108 | 1.82 | 46 | 7 | 3.2 | 7 | 3.2 |
| *6 | 150 | 5.00 | 127 | 1.75 | 44 | 2.38 | 60 | 7.50 | 191 | 5.25 | 133 | 2.25 | 57 | 15 | 6.8 | 13 | 5.9 |
| *8 | 200 | 5.50 | 140 | 2.00 | 51 | 2.63 | 67 | 8.25 | 210 | 5.75 | 146 | 2.50 | 64 | 23 | 10.4 | 23 | 10.4 |
| 10 | 250 | 6.50 | 165 | 2.00 | 51 | 2.88 | 73 | 9.50 | 241 | 6.75 | 171 | 2.75 | 70 | 38 | 17.2 | 38 | 17.2 |
| 12 | 300 | 7.50 | 191 | 2.13 | 54 | 3.13 | 80 | 10.75 | 273 | 7.75 | 197 | 3.00 | 76 | 55 | 24.9 | 54 | 24.5 |
| 14 | 350 | 12.25** | 311 | 2.81 | 71 | 3.81 | 97 | 8.18 | 208 | 4.69 | 119 | 3.50 | 89 | 63 | 28.6 | 60 | 27.2 |
| 16 | 400 | 13.94** | 354 | 3.25 | 83 | 4.25 | 108 | 9.38 | 238 | 5.38 | 137 | 4.00 | 102 | 69 | 31.3 | 66 | 29.9 |

$22^{1 / 2}{ }^{\circ}$ Elbows


Fittings feature filament-wound Quick-Lock bell ends. Elbows with angles such as $11^{11} 4^{\circ}, 30^{\circ}, 60^{\circ}$ and $75^{\circ}$ and other special angles are available. Consult your representative.

| Nom <br> Pipe <br> Size |  | Laying Length (L) |  | Overall Length (B) |  | Socket Depth ( $\mathrm{D}_{\mathrm{S}}$ ) |  | Approx Wt |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in. $\cdot \mathrm{mm}$ |  | in. $\cdot \mathrm{mm}$ |  | in. mm |  | in. mm |  | $\mathrm{lb} \cdot \mathrm{kg}$ |  |
| 1 | 25 | 0.38 | 10 | 1.44 | 37 | 1.06 | 27 | 0.3 | 0.1 |
| 11/2 | 40 | 0.38 | 10 | 1.63 | 41 | 1.25 | 32 | 0.5 | 0.2 |
| 2 | 50 | 0.50 | 13 | 2.31 | 59 | 1.82 | 46 | 0.7 | 0.3 |
| 3 | 80 | 0.81 | 21 | 2.62 | 67 | 1.82 | 46 | 1.3 | 0.6 |
| 4 | 100 | 1.12 | 28 | 2.94 | 75 | 1.82 | 46 | 2.0 | 0.9 |
| 6 | 150 | 1.69 | 43 | 3.94 | 100 | 2.25 | 57 | 4.0 | 1.8 |
| 8 | 200 | 2.25 | 57 | 4.75 | 121 | 2.50 | 64 | 7.0 | 3.2 |
| 10 | 250 | 2.62 | 67 | 5.38 | 137 | 2.75 | 70 | 13.0 | 5.9 |
| 12 | 300 | 3.00 | 76 | 6.00 | 152 | 3.00 | 76 | 16.0 | 7.3 |
| 14 | 350 | 3.25 | 83 | 6.75 | 171 | 3.50 | 89 | 26.0 | 11.8 |
| 16 | 400 | 3.50 | 89 | 7.50 | 191 | 4.00 | 102 | 30.0 | 13.6 |

Fittings are filament wound unless otherwise noted. Molded fittings are indicated with an asterisk (*).



6

Flanged Tees


Flanges are filament wound unless otherwise noted. Molded flanges available in 2-through 12-inch sizes. Fittings noted with an asterisk (*) do not meet ANSI laying lengths. Flange thickness with double asterisk (**) represents molded flange dimension.

| Nom Pipe Size |  | Laying Length (L) |  | At Fa | Flan | kness | $\begin{aligned} & \text { Hub } \\ & \text { () } \end{aligned}$ | Approx Wt |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in. $\cdot \mathrm{mm}$ |  | in.•mm |  | in. $\cdot \mathrm{mm}$ |  | in. mm |  | lb.•kg |  |
| 1 | 25 | 3.50 | 89 | 1.13 | 29 | 1.13 | 29 | 2 | 0.9 |
| 11/2 | 40 | 4.00 | 102 | 1.38 | 35 | 1.38 | 35 | 3 | 1.4 |
| 2 | 50 | 4.50 | 114 | 1.00 | 25 | 2.00 | 51 | 7 | 3.2 |
| 3 | 80 | 5.50 | 140. | 1.13 | 29 | 2.00 | 51 | 11 | 5.0 |
| 4 | 100 | 6.50 | 165 | 1.25 | 32 | 2.00 | 51 | 17 | 7.7 |
|  |  | 6.50 | 165 | 1.56** | 40 | - | - | 17 | 7.7 |
| 6 | 150 | 8.00 | 203 | 1.75 | 44 | 2.38 | 60 | 32 | 14.5 |
| 8 | 200 | 9.00 | 229 | 2.00 | 51 | 2.63 | 67 | 47 | 21.3 |
| 10 | 250 | 11.00 | 279 | 2.00 | 51 | 2.88 | 73 | 70 | 31.8 |
| 12 | 300 | 12.00 | 305 | 2.13 | 54 | 3.13 | 80 | 114 | 51.7 |
| 14 | 350 | 18.00* | 457 | 2.81 | 71 | 3.81 | 97 | 220 | 99.8 |
| 16 | 400 | 20.00* | 508 | 3.25 | 83 | 4.25 | 108 | 280 | 127.0 |

## Combination Tees



Flanges are filament wound unless otherwise noted. Molded flanges are available in 2-through 12 -inch sizes. Any combination of flanged or Quick-Lock ends is available. Fittings noted with an asterisk (*) do not match ANSI laying length dimensions. Quick-Lock bell ends in 14- and 16-inch sizes are integrally wound.


| Nom Pipe |  | Laying Length |  | Laying Length |  | Flange Thickness |  |  |  | Approx Wt |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | At F |  |  |  |  |  |  |  |  |  |
|  |  |  |  | $\left(L_{1}\right)$ |  | $\left(L_{2}\right)$ |  | (t) |  | (D) |  | 2 flgs |  | 1 flg |  |
| in. mm |  | in. $\cdot \mathrm{mm}$ |  | in. $\cdot \mathrm{mm}$ |  | in. mm |  | in. $\cdot \mathrm{mm}$ |  | lb. kg |  | lb. kg |  |
| 1 | 25 | 3.50 | 89 | 1.06 | 27 | 1.13 | 29 | 1.13 | 29 | 3 | 1.4 | 3 | 1.4 |
| 11/2 | 40 | 4.07 | 103 | 1.19 | 30 | 1.38 | 35 | 1.38 | 35 | 4 | 1.8 | 4 | 1.8 |
| 2 | 50 | 4.50 | 114 | 4.75 | 121 | 1.00 | 25 | 2.00 | 51 | 6 | 2.7 | 5 | 2.3 |
| 3 | 80 | 5.50 | 140 | 5.75 | 146 | 1.13 | 29 | 2.00 | 51 | 10 | 4.5 | 8 | 3.6 |
| 4 | 100 | 6.50 | 165 | 6.75 | 171 | 1.25 | 32 | 2.00 | 51 | 14 | 6.4 | 12 | 5.4 |
| 6 | 150 | 8.00 | 203 | 8.25 | 210 | 1.75 | 44 | 2.38 | 60 | 28 | 12.7 | 24 | 10.9 |
| 8 | 200 | 9.00 | 229 | 9.25 | 235 | 2.00 | 51 | 2.63 | 67 | 41 | 18.6 | 35 | 15.9 |
| 10 | 250 | 11.00 | 279 | 11.25 | 286 | 2.00 | 51 | 2.88 | 73 | 61 | 27.7 | 52 | 23.6 |
| 12 | 300 | 12.00 | 305 | 12.25 | 311 | 2.13 | 54 | 3.13 | 80 | 98 | 44.5 | 82 | 37.2 |
| 14 | 350 | 18.00* | 457 | 10.50 | 267 | 2.81 | 71 | 3.81 | 97 | 130 | 59.0 | 120 | 54.4 |
| 16 | 400 | 20.00* | 508 | 11.50 | 292 | 3.25 | 83 | 4.25 | 108 | 145 | 65.8 | 130 | 59.0 |

Flanged Reducing Tees
 in 2- through 12-inch sizes. Fittings with asterisk (*) do not meet ANSI laying lengths. Flange thicknesses with double asterisk (**) represent molded flange dimensions.


| Nom <br> Pipe <br> Size |  | Laying Length $\left(\mathrm{L}_{1}\right)$ |  | Laying Length ( $\mathrm{L}_{2}$ ) |  | Socket Depth ( $\mathrm{D}_{\mathrm{s}}$ ) |  | Approx Wt |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in. mm |  | in. $\cdot \mathrm{mm}$ |  | in. mm |  | in. mm |  | lb.*kg |  |
| 2 | 50 | 2.50 | 64 | 8.00 | 203 | 1.82 | 46 | 4 | 1.8 |
| 3 | 80 | 3.00 | 76 | 10.00 | 254 | 1.82 | 46 | 7 | 3.2 |
| 4 | 100 | 3.00 | 76 | 12.00 | 305 | 1.82 | 46 | 9 | 4.1 |
| 6 | 150 | 3.50 | 89 | 14.50 | 368 | 2.25 | 57 | 15 | 6.8 |
| 8 | 200 | 4.50 | 114 | 17.50 | 445 | 2.50 | 64 | 27 | 12.2 |
| 10 | 250 | 5.00 | 127 | 20.50 | 521 | 2.75 | 70 | 47 | 21.3 |
| 12 | 300 | 5.50 | 140 | 24.50 | 622 | 3.00 | 76 | 67 | 30.4 |
| 14 | 350 | 5.50 | 140 | 24.50 | 622 | 3.50 | 89 | 87 | 39.5 |
| 16 | 400 | 5.50 | 140 | 24.50 | 622 | 4.00 | 102 | 110 | 49.9 |

$45^{\circ}$ Flanged Laterals
Flanges are filament wound and meet ANSI B 16.5 Cl 150 requirements.

| Nom Pipe Size |  | Laying Length ( $\mathrm{L}_{1}$ ) |  | Laying Length ( $\mathrm{L}_{2}$ ) |  | Flange ThicknessAt FaceAt Hub  <br> (t) (D) |  |  |  | Approx Wt |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in. mm |  | in. $\cdot \mathrm{mm}$ |  | in. $\cdot \mathrm{mm}$ |  | in. mm |  | in. mm |  | lb. kg |  |
| 2 | 50 | 6.44 | 164 | 11.94 | 303 | 1.00 | 25 | 2.00 | 51 | 9 | 4.1 |
| 3 | 80 | 6.94 | 176 | 13.94 | 354 | 1.13 | 29 | 2.00 | 51 | 14 | 6.4 |
| 4 | 100 | 6.94 | 176 | 15.94 | 405 | 1.25 | 32 | 2.00 | 51 | 20 | 9.1 |
| 6 | 150 | 8.25 | 210 | 19.25 | 489 | 1.75 | 44 | 2.38 | 60 | 34 | 15.4 |
| 8 | 200 | 9.76 | 248 | 22.75 | 578 | 2.00 | 51 | 2.63 | 67 | 57 | 25.9 |
| 10 | 250 | 10.75 | 273 | 26.25 | 667 | 2.00 | 51 | 2.88 | 73 | 89 | 40.4 |
| 12 | 300 | 11.75 | 298 | 30.75 | 781 | 2.13 | 54 | 3.13 | 80 | 136 | 61.7 |
| 14 | 350 | 13.06 | 332 | 32.00 | 813 | 2.81 | 71 | 3.81 | 97 | 201 | 91.2 |
| 16 | 400 | 14.00 | 356 | 33.00 | 838 | 3.25 | 83 | 4.25 | 108 | 269 | 122.0 |

Tapered Body Reducers


| Nom Pipe Size |  | Overall Length (B) |  | Laying Length (L) |  | Socket Depth ( $\mathrm{D}_{\mathrm{s} 1}$ ) |  | Socket Depth $\left(\mathrm{D}_{\mathrm{s} 2}\right)$ |  | Approx Wt |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | mm |  | mm |  | mm |  |  |  | mm |  |  |
| $1^{1 / 2 \times 1}$ | $40 \times 25$ | 3.56 | 90 | 1.31 | 33 | 1.06 | 27 | 1.25 | 32 | 0.4 | 0.2 |
| 2x1 | $50 \times 25$ | 5.38 | 137 | 2.50 | 64 | 1.06 | 27 | 1.82 | 46 | 0.6 | 0.3 |
| $2 \times 11 / 2$ | $20 \times 40$ | 4.32 | 110 | 1.25 | 32 | 1.25 | 32 | 1.82 | 46 | 1.0 | 0.5 |
| $3 \times 2$ | $80 \times 50$ | 5.75 | 146 | 2.12 | 54 | 1.82 | 46 | 1.82 | 46 | 1.4 | 0.6 |
| $4 \times 2$ | $100 \times 50$ | 6.62 | 168 | 3.00 | 76 | 1.82 | 46 | 1.82 | 46 | 2.0 | 0.9 |
| $4 \times 3$ | $100 \times 80$ | 6.50 | 165 | 2.88 | 73 | 1.82 | 46 | 1.82 | 46 | 2.0 | 0.9 |
| $6 \times 3$ | 150x80 | 7.88 | 200 | 3.81 | 97 | 1.82 | 46 | 2.25 | 57 | 4.0 | 1.8 |
| $6 \times 4$ | $150 \times 100$ | 7.75 | 197 | 3.69 | 94 | 1.82 | 46 | 2.25 | 57 | 4.0 | 1.8 |
| $8 \times 4$ | 200x100 | 9.75 | 248 | 5.44 | 138 | 1.82 | 46 | 2.50 | 64 | 7.0 | 3.2 |
| $8 \times 6$ | 200x150 | 8.63 | 219 | 3.88 | 99 | 2.25 | 57 | 2.50 | 64 | 7.0 | 3.2 |
| 10x6 | 250x150 | 9.62 | 244 | 4.62 | 117 | 2.25 | 57 | 2.75 | 70 | 9.0 | 4.1 |
| 10x8 | $250 \times 200$ | 9.37 | 238 | 4.12 | 105 | 2.50 | 64 | 2.75 | 70 | 8.0 | 3.6 |
| 12x8 | $300 \times 200$ | 11.38 | 289 | 5.88 | 149 | 2.50 | 64 | 3.00 | 76 | 14.0 | 6.4 |
| $12 \times 10$ | $300 \times 250$ | 11.12 | 282 | 5.38 | 137 | 2.75 | 70 | 3.00 | 76 | 13.0 | 5.9 |
| $14 \times 10$ | $350 \times 250$ | 13.50 | 343 | 7.25 | 184 | 2.75 | 70 | 3.50 | 89 | 36.0 | 16.3 |
| $14 \times 12$ | $350 \times 300$ | 13.50 | 343 | 7.00 | 178 | 3.00 | 76 | 3.50 | 89 | 37.0 | 16.8 |
| $16 \times 12$ | $400 \times 300$ | 13.50 | 343 | 6.50 | 165 | 3.00 | 76 | 4.00 | 102 | 54.0 | 24.5 |
| $16 \times 14$ | $400 \times 350$ | 13.50 | 343 | 6.00 | 152 | 3.50 | 89 | 4.00 | 102 | 57.0 | 25.9 |

Flanged Tapered Body Reducers


Combination Reducers (Flanged Small End)

Flanges are filament wound. Flanges in 2-, 3- and 4-inch sizes are available only in heavy-duty (hubless) configuration. Molded flanges available in 2 - through 12 -inch sizes. Fittings with asterisk (*) meet ANSI laying lengths.


* Laying length is measured from contact surface to pipe stop in Quick Lock bell.

Combination Reducers (Flanged Large End)


Standard flanges are filament wound. Molded flanges available in 2 through 12 inch sizes.

| Nom Pipe Size |  | Laying Length* <br> (L) |  | Overall Length (B) |  | Flange Thickness |  |  |  | Approx Wt |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  | Hub <br> (D) |  |  |
| in.•mm |  |  |  | in.•mm |  | in. mm |  | in.•mm |  | in. mm |  | lb.•kg |  |
| $3 \times 2$ | $80 \times 50$ | 6.25 | 159 | 8.06 | 205 | 1.00 | 25 | 2.00 | 51 | 7 | 3.2 |
| $4 \times 2$ | $100 \times 50$ | 7.25 | 184 | 9.06 | 230 | 1.00 | 25 | 2.00 | 51 | 8 | 3.6 |
| $4 \times 3$ | 100x80 | 7.25 | 184 | 9.06 | 230 | 1.13 | 29 | 2.00 | 51 | 9 | 4.1 |
| $6 \times 3$ | 150x80 | 9.25 | 235 | 11.25 | 286 | 1.13 | 29 | 2.00 | 51 | 11 | 5.0 |
| 6x4 | 150x100 | 9.25 | 235 | 11.25 | 286 | 1.25 | 32 | 2.00 | 51 | 13 | 5.9 |
| $8 \times 4$ | 200x100 | 11.25 | 286 | 13.75 | 349 | 1.25 | 32 | 2.00 | 51 | 15 | 6.8 |
| $8 \times 6$ | 200x150 | 11.25 | 286 | 13.75 | 349 | 1.75 | 44 | 2.38 | 60 | 17 | 7.7 |
| 10x6 | 250x150 | 12.25 | 311 | 15.00 | 381 | 1.75 | 44 | 2.38 | 60 | 19 | 8.6 |
| 10x8 | $250 \times 200$ | 12.25 | 311 | 15.00 | 381 | 2.00 | 51 | 2.63 | 67 | 26 | 11.8 |
| 12x8 | $300 \times 200$ | 14.25 | 362 | 17.25 | 438 | 2.00 | 51 | 2.63 | 67 | 29 | 13.2 |
| $12 \times 10$ | $300 \times 250$ | 14.25 | 362 | 17.25 | 438 | 2.00 | 51 | 2.88 | 73 | 34 | 15.4 |
| 14×10 | $350 \times 250$ | 16.13 | 410 | 19.88 | 505 | 2.00 | 51 | 2.88 | 73 | 39 | 17.7 |
| $14 \times 12$ | $350 \times 300$ | 16.13 | 410 | 19.88 | 505 | 2.13 | 54 | 3.81 | 97 | 47 | 21.3 |
| $16 \times 12$ | $400 \times 300$ | 18.13 | 461 | 22.38 | 568 | 2.13 | 54 | 4.25 | 108 | 54 | 24.5 |
| 16x14 | $400 \times 350$ | 18.38 | 467 | 22.38 | 568 | 2.81 | 71 | 4.25 | 108 | 66 | 29.9 |

* Laying length is measured from contact surface to pipe stop in Quick Lock bell.


## Pipe Nipples



| Nom Pipe Size |  | Overall Length (B) |  | Approx Wt |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| in. mm |  | in. mm |  | $\mathrm{lb} \cdot \mathrm{kg}$ |  |
| 1 | 25 | 2.25 | 57 | 0.1 | 0.0 |
| 11/2 | 40 | 2.62 | 67 | 0.2 | 0.1 |
| 2 | 50 | 3.75 | 95 | 0.2 | 0.1 |
| 3 | 80 | 3.75 | 95 | 0.3 | 0.1 |
| 4 | 100 | 3.75 | 95 | 0.5 | 0.2 |
| 6 | 150 | 4.62 | 117 | 0.9 | 0.4 |
| 8 | 200 | 5.12 | 130 | 1.4 | 0.6 |
| 10 | 250 | 5.62 | 143 | 1.9 | 0.9 |
| 12 | 300 | 6.12 | 155 | 2.4 | 1.1 |
| 14 | 350 | 7.25 | 184 | 6.7 | 3.0 |
| 16 | 400 | 8.25 | 210 | 9.7 | 4.4 |

Couplings and End Caps Couplings are filament wound. End caps consist of filament-wound couplings with molded plugs bonded in.


Crosses


Crosses are filament wound. Mitered crosses are available in 14-and 16-inch sizes. Contact FGS for dimensions and pressure ratings.

| Nom Pipe Size |  | Laying Length (L) |  | Socket Depth ( $\mathrm{D}_{\mathrm{s}}$ ) |  | Approx Wt |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  | $\mathrm{lb} \cdot \stackrel{\mathrm{kg}}{ }$ |
| 2 | 50 | 2.50 | 64 | 1.81 | 46 | 3 | 1.4 |
| 3 | 80 | 3.38 | 86 | 1.81 | 46 | 6 | 2.7 |
| 4 | 100 | 4.12 | 105 | 1.81 | 46 | 7 | 3.2 |
| 6 | 150 | 5.62 | 143 | 2.25 | 57 | 13 | 5.9 |
| 8 | 200 | 7.00 | 178 | 2.50 | 64 | 23 | 10.4 |
| 10 | 250 | 8.50 | 216 | 2.75 | 70 | 37 | 16.8 |
| 12 | 300 | 10.00 | 254 | 3.00 | 76 | 61 | 27.7 |



Reducing Flanges

|  | $\rightarrow \mathrm{D}$ |  | bolting and gasket recommendations. Use $1 / 2$-inch drive to avoid wrench socket to flange hub interference while torquing bolts. |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |  |
| Nom <br> Pipe <br> Size | Flange Dia (A) | Bolt Circle (BC) | Laying Length (L) | Flange At Hub (D) | Thickness At Face (t) | Hole Dia <br> (F) | Hole Count | Socket Depth ( $\mathrm{D}_{\mathrm{s}}$ ) | Bolt Dia | Approx Wt |
| in. $\cdot \mathrm{mm}$ | in. mm | in. $\cdot \mathrm{mm}$ | in. $\cdot \mathrm{mm}$ | in. mm | in. $\cdot \mathrm{mm}$ | in. $\cdot \mathrm{mm}$ |  | in. $\cdot \mathrm{mm}$ | in. $\cdot \mathrm{mm}$ | lb. kg |
| $2 \times 11 / 2 \quad 50 \times 40$ | 6.00152 | 4.75121 | 0.7519 | 2.0051 | 1.0025 | 0.7519 | 4 | 1.2532 | 0.6316 |  |
| $3 \times 2 \quad 80 \times 50$ | 7.50191 | 6.00152 | 0.123 | 1.9349 | 1.1228 | 0.7519 | 4 | 1.8146 | 0.6316 | 31.4 |
| $4 \times 2$ 100x50 | 9.00229 | 7.50191 | 0.123 | 1.9349 | 1.2532 | 0.7519 | 8 | 1.8146 | 0.6316 | 62.7 |
| $4 \times 3$ 100x80 | 9.00229 | 7.50191 | 0.123 | 1.9349 | 1.2532 | 0.7519 | 8 | 1.8146 | 0.6316 | 52.3 |
| $6 \times 3$ 150x80 | 11.00279 | 9.50241 | 0.6918 | 2.5064 | 1.7544 | 0.8822 | 8 | 1.8146 | 0.7519 | 125.4 |
| $6 \times 4150 \times 100$ | 11.00279 | 9.50241 | 0.6918 | 2.5064 | 1.7544 | 0.8822 | 8 | 1.8146 | 0.7519 | 115.0 |
| $8 \times 4200 \times 100$ | 13.50343 | 11.75298 | 0.9424 | 2.7570 | 2.0051 | 0.8822 | 8 | 1.8146 | 0.7519 | 219.5 |
| $8 \times 6200 \times 150$ | 13.50343 | 11.75298 | 0.5013 | 2.7570 | 2.0051 | 0.8822 | 8 | 2.2557 | 0.7519 | 177.7 |
| $10 \times 6250 \times 150$ | 16.00406 | 14.25362 | 0.7519 | 3.0076 | 2.0051 | 1.0025 | 12 | 2.2557 | 0.8822 | 2913.2 |
| $10 \times 8250 \times 200$ | 16.00406 | 14.25362 | 0.5013 | 3.0076 | 2.0051 | 1.0025 | 12 | 2.5064 | 0.8822 | 2410.9 |
| $12 \times 8300 \times 200$ | 19.00483 | 17.00432 | 0.7519 | 3.2583 | 2.1254 | 1.0025 | 12 | 2.5064 | 0.8822 | 4319.5 |
| $12 \times 10300 \times 250$ | 19.00483 | 17.00432 | 0.5013 | 3.2583 | 2.1254 | 1.0025 | 12 | 2.7570 | 0.8822 | 3616.3 |



Heavy-Duty Flanges
Heavy-duty (hubless) flanges are filament-wound.



| Nom Pipe Size | Flange Dia (A) | Bolt Circle (BC) | Flange Thickness <br> Maximum Minimum <br> (D) <br> (t) |  | Socket Depth ( $\mathrm{D}_{\mathrm{s}}$ ) |  | Hole Count | Hole Dia | Bolt Dia |  | Approx Wt |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in. mm | in. $\cdot \mathrm{mm}$ | in. $\cdot \mathrm{mm}$ | in. $\cdot \mathrm{mm}$ | in. $\cdot \mathrm{mm}$ |  | mm |  | in. $\cdot \mathrm{mm}$ | in. $\cdot \mathrm{m}$ |  | lb. kg |
| 250 | 6.00152 | 4.75121 | 3.3886 | 2.3860 | 1.82 | 46 | 4 | 0.7519 | 0.63 | 16 | $3 \quad 1.4$ |
| 380 | 7.50191 | 6.00152 | 3.3886 | 2.5064 | 1.82 | 46 | 4 | 0.7519 | 0.63 | 16 | $5 \quad 2.3$ |
| 4100 | 9.00229 | 7.50191 | 3.3886 | 2.6367 | 1.82 | 46 | 8 | 0.7519 | 0.63 | 16 | 73.2 |
| 6150 | 11.00279 | 9.50241 | 3.7595 | 2.9475 | 2.25 | 57 | 8 | 0.8822 | 0.75 | 19 | 115.0 |
| 8200 | 13.50343 | 11.75298 | 4.00102 | 3.1981 | 2.50 | 64 | 8 | 0.8822 | 0.75 | 19 | $17 \quad 7.7$ |
| 10250 | 16.00406 | 14.25362 | 4.25108 | 3.2583 | 2.75 | 70 | 12 | 1.0025 | 0.88 | 22 | 2410.9 |
| 12300 | 19.00483 | 17.00432 | 4.50114 | 3.5089 | 3.00 | 76 | 12 | 1.0025 | 0.88 | 22 | 3616.3 |
| 14350 | 21.00533 | 18.75476 | 5.00127 | 4.00102 | 3.50 | 89 | 12 | 1.1228 | 1.00 | 25 | 4922.2 |
| 16400 | 23.50597 | $21.25 \quad 540$ | 5.50140 | 4.50114 | 4.00 | 102 | 16 | 1.1228 | 1.00 | 25 | 5725.9 |

Maintenance Couplings
Bondstrand maintenance coupling kits include inner and outer sections, hose clamp(s), and instructions for assembly (Bondstrand Installation Maintenance Coupling). Adhesive must be ordered separately.


| Nom Pipe <br> Size |  | Overall <br> Length |  | Pressure <br> Rating | Adhesive Kits <br> Required |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{in} \cdot \mathrm{mm}$ |  | $\mathrm{in} \cdot \bullet \mathrm{mm}$ |  | psi. $\cdot \mathrm{N} / \mathrm{m}^{2}$ | 6 oz. |  |
| 1 | 25 | 2.50 | 64 | 150 | $1.03 \times 10^{6}$ | $1 / 2$ |
| $11 / 2$ | 40 | 3.00 | 76 | 150 | $1.03 \times 10^{6}$ | 1 |
| 2 | 50 | 4.00 | 102 | 150 | $1.03 \times 10^{6}$ | 1 |
| 3 | 80 | 4.00 | 102 | 150 | $1.03 \times 10^{6}$ | 1 |
| 4 | 100 | 4.00 | 102 | 150 | $1.03 \times 10^{6}$ | 2 |
| 6 | 150 | 4.88 | 124 | 150 | $1.03 \times 10^{6}$ | 2 |
| 8 | 200 | 5.38 | 137 | 150 | $1.03 \times 10^{6}$ | 3 |
| 10 | 250 | 5.88 | 149 | 150 | $1.03 \times 10^{6}$ | 4 |
| 12 | 300 | 6.38 | 162 | 150 | $1.03 \times 10^{6}$ | 4 |
| 14 | 350 | 7.38 | 187 | 150 | $1.03 \times 10^{6}$ | 6 |
| 16 | 400 | 8.38 | 213 | 150 | $1.03 \times 10^{6}$ | 8 |

## Adapters (Threaded and

 Victaulic)

Adapters are available in Quick-Lock bell $\times$ NPT threaded male (M), and Quick-Lock bell x Victaulic male end (V) configurations. Sizes 1" ( 25 mm ) and $11 / 2^{\prime \prime}$ are filament wound; 2" through 6 " are compression molded. Consult manufacturer for dimensions of QL bell x victaulic adapters.

| Nom Pipe Size |  | Overall Length (B) |  | Socket Depth ( $\mathrm{D}_{\mathrm{s}}$ ) |  | Inside Dia (ID) |  | Approx Wt |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in.•mm |  | in. mm |  | in. mm |  | in.•mm |  | lb. kg |  |
| 1 | 25 | 2.38 | 60 | 1.06 | 27 | 0.76 | 19 | 0.3 | 0.1 |
| 11/2 | 40 | 2.81 | 71 | 1.25 | 32 | 1.43 | 36 | 0.4 | 0.2 |
| 2 | 50 | 3.57 | 91 | 1.81 | 46 | 1.89 | 48 | 0.6 | 0.3 |
| 3 | 80 | 4.36 | 111 | 1.81 | 46 | 2.80 | 71 | 1.2 | 0.5 |
| 4 | 100 | 4.63 | 118 | 1.81 | 46 | 3.89 | 99 | 1.6 | 0.7 |
| 6 | 150 | 4.67 | 119 | 2.25 | 57 | 5.90 | 150 | 2.6 | 1.2 |

Molded Plugs


50 psi maximum

| Nom <br> Pipe <br> Size | Total <br> Thickness <br> $(\mathrm{T})$ | Approx <br> Wt |  |  |  |
| :---: | ---: | ---: | ---: | ---: | ---: |
| in. $\cdot \mathrm{mm}$ | in. $\cdot \mathrm{mm}$ |  | $\mathrm{lb} \cdot \bullet \mathrm{kg}$ |  |  |
| 2 | 50 | 1.94 | 49 | 0.6 | 0.3 |
| 3 | 80 | 1.94 | 49 | 1.3 | 0.6 |
| 4 | 100 | 1.94 | 49 | 2.0 | 0.9 |
| 6 | 150 | 2.38 | 60 | 6.0 | 2.7 |
| 8 | 200 | 2.63 | 67 | 10.0 | 4.5 |
| 10 | 250 | 2.88 | 73 | 17.0 | 7.7 |
| 12 | 300 | 3.13 | 80 | 27.0 | 12.2 |

Molded Reducer Bushings


50 psi maximum

| Nom Pipe Size |  | Overall Length (B) |  | Pipe Stop (L) |  | Eccentricity <br> (E) |  | Approx Wt |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | - mm | in.• |  | in.- | mm | in. $\cdot 1$ |  |  |  |
| $3 \times 2$ | 80X50 | 1.94 | 49 | 0.13 | 3 | 0.25 | 6 | 0.7 | 0.3 |
| $4 \times 2$ | $100 \times 50$ | 1.94 | 49 | 0.13 | 3 | 0.75 | 19 | 1.5 | 0.7 |
| $4 \times 3$ | 100x80 | 1.94 | 49 | 0.13 | 3 | 0.13 | 3 | 0.8 | 0.4 |
| $6 \times 3$ | 150x80 | 2.38 | 60 | 0.56 | 14 | 1.25 | 32 | 4.1 | 1.9 |
| 6x4 | $150 \times 100$ | 2.38 | 60 | 0.56 | 14 | 0.63 | 16 | 3.1 | 1.4 |
| $8 \times 4$ | 200x100 | 2.63 | 67 | 0.81 | 21 | 1.63 | 41 | 8.0 | 3.6 |
| $8 \times 6$ | 200x150 | 2.63 | 67 | 0.38 | 10 | 0.63 | 16 | 5.0 | 2.3 |
| 10x6 | $250 \times 150$ | 2.88 | 73 | 0.63 | 16 | 1.63 | 41 | 12.0 | 5.4 |
| 10x8 | $250 \times 200$ | 2.88 | 73 | 0.38 | 10 | 0.63 | 16 | 7.0 | 3.2 |
| 12x8 | $300 \times 200$ | 3.13 | 80 | 0.63 | 16 | 1.63 | 41 | 15.0 | 6.8 |
| 12×10 | $300 \times 250$ | 3.13 | 80 | 0.38 | 10 | 0.63 | 16 | 8.0 | 3.6 |

Blank Saddles


Blank saddles are filament wound and are used for pipe support and restraint. Thickness for all saddles is 0.56 inches. Available in same lengths as reducing saddles.

| Nom Pipe <br> Size |  | Approx <br> Wt |  | Adhesive Kits <br> Required |  |
| :---: | ---: | :---: | :---: | :---: | :---: |
| in. $\cdot \mathrm{mm}$ |  | $\mathrm{lb} . / \mathrm{in} \cdot \bullet \mathrm{kg} / \mathrm{mm}$ | $(3 \mathrm{oz})$ | $(6 \mathrm{oz})$ |  |
| 1 | 25 | 0.1 | 0.05 | 1 |  |
| $11 / 2$ | 40 | 0.2 | 0.09 | 1 |  |
| 2 | 50 | 0.2 | 0.09 | 1 |  |
| 3 | 80 | 0.3 | 0.14 | 1 |  |
| 4 | 100 | 0.4 | 0.18 | 1 |  |
| 6 | 150 | 0.5 | 0.23 | 1 |  |
| 8 | 200 | 0.6 | 0.27 | 1 |  |
| 10 | 250 | 0.8 | 0.36 |  | $1 \frac{1}{2} / 2$ |
| 12 | 300 | 1.0 | 0.45 |  | $1 \frac{1}{2} / 2$ |
| 14 | 350 | 1.1 | 0.50 |  | 2 |
| 16 | 400 | 1.2 | 0.54 |  | 2 |

Standard reducing saddles come with $1^{1 / 2}$-in NPT plastic bushing. All smaller bushings are 316 stainless steel. Other materials available on special order. Saddles are filament wound.

|  | m ize red | Outlet Nom Size |  | Length (B) |  | Saddle Girth (a) | Approx Wt |  | Adhesive Kits |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in.mm |  | in.•mm |  | in.•mm |  | degrees | lb.*kg |  | 3oz. 6 oz |  |
| 2 | 50 | $1 / 4,3 / 8,1 / 2,3 / 4$ | 6,9,13,19 | 4.00 | 102 | 180 | 1.0 | 0.5 | 1 |  |
|  |  | 1 | 25 | 6.00 | 152 | 180 | 2.0 | 0.9 | 1 |  |
| 3 | 80 | $1 / 4$ | 6 | 4.00 | 102 | 90 | 1.6 | 0.7 | 1 |  |
|  |  | $1 / 4,3 / 8,1 / 2,3 / 4$ | 6,9,13,19 | 4.00 | 102 | 180 | 1.6 | 0.7 | 1 |  |
|  |  | $1,1 \frac{1}{4}, 1 \frac{1}{2} 2$ | 25,30,40 | 6.00 | 152 | 180 | 3.9 | 1.8 | 1 |  |
| 4 |  | $1 / 4,3 / 8$ | 6,9 | 4.00 | 102 | 90 | 2.0 | 0.9 | 1 |  |
|  |  | $1 / 4,3 / 8,1 / 2,3 / 4$ | 6,9,13,19 | 4.00 | 102 | 180 | 2.0 | 0.9 | 1 |  |
|  |  | $1,11 / 4,1^{1 / 2}$ | 25,30,40 | 6.00 | 152 | 180 | 4.0 | 1.8 | 1 |  |
| 6 | 150 | $1 / 4,3 / 8,1 / 2$ | 6, 9, 13 | 4.00 | 102 | 180 | 2.4 | 1.1 | 1 |  |
|  |  | $1 / 4,3 / 8,1 / 2,3 / 4$ | 6,9,13,19 | 4.00 | 102 | 180 | 2.4 | 1.1 | 1 |  |
|  |  | $1,1 \frac{1}{4}, 1^{1 / 2} 2$ | 25,30,40 | 6.00 | 152 | 180 | 4.6 | 2.1 |  | 1 |
| 8 | 200 | $1 / 4,3 / 8,1 / 2,3 / 4$ | 6,9,13,19 | 4.00 | 102 | 90 | 2.8 | 1.3 | 1 |  |
|  |  | $1,1^{1 / 4}, 1^{1 / 2} 2$ | 25,30,40 | 6.00 | 152 | 180 | 5.2 | 2.4 |  | 1 |
| 10 | 250 | $1 / 4,3 / 8,1 / 2$ | 6, 9, 13 | 4.00 | 102 | 45 | 3.8 | 1.7 |  | 1 |
|  |  | $3 / 4$ | 19 | 4.00 | 102 | 90 | 3.8 | 1.7 |  | 1 |
|  |  | $1,1^{1 / 4}, 1^{1 / 2} 2$ | 25,30,40 | 6.00 | 152 | 90 | 6.3 | 2.9 |  | 1 |
| 12 | 300 | $1 / 4,3 / 8,1 / 2,3 / 4$ | 6,9,13,19 | 4.00 | 102 | 45 | 4.2 | 1.9 |  | 1 |
|  |  | $1,1^{1 / 4}, 1^{1 / 2} 2$ | 25,30,40 | 6.00 | 152 | 90 | 7.4 | 3.4 |  | 1 |
| 14 | 350 | $1 / 4,3 / 8,1 / 2,3 / 4$ | 6,9,13,19 | 4.00 | 102 | 45 | 4.2 | 1.9 |  | 2 |
|  |  | $1,1^{1 / 4}, 1^{1 / 2} 2$ | 25,30,40 | 6.00 | 152 | 90 | 7.4 | 3.4 |  | 2 |
| 16 | 400 | $1 / 4,3 / 8,1 / 2,3 / 4$ | 6,9,13,19 | 4.00 | 102 | 45 | 4.2 | 1.9 |  | 2 |
|  |  | $1,1^{1 / 4}, 1^{1 / 2}$ | 25,30,40 | 6.00 | 152 | 45 | 7.4 | 3.4 |  | 2 |

Reducing Saddles with Flanged and Quick-Lock Outlets

Both filament-wound and molded flanges are available. Saddles are filament wound. See Quick-Lock coupling table for socket depth, $\mathrm{D}_{\mathrm{s}}$. See Quick-Lock flange table for flange thickness.


- $45^{\circ}$ elbows, bell end
- $90^{\circ}$ elbows, bell end
- $45^{\circ}$ elbows, flanged
- $90^{\circ}$ elbows, flanged
- Tees, bell end
- Tees, flanged

| Nom <br> Pipe <br> Size |  | Filament-wound |  |  |  | Molded |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Quick-Lock |  | Flanged |  | Quick-Lock |  | Flanged |  |
| in. | mm | psi | bar | psi | bar | psi | bar | psi | bar |
| 1 | 25 | 300 | 21 | 300 | 21 | - | - | - | - |
| $11 / 2$ | 40 | 300 | 21 | 300 | 21 | - | - | - | - |
| 2 | 50 | 375 | 26 | 375 | 26 | 300 | 21 | 300 | 21 |
|  |  | 300* | 21* | 300* | 21* | 200* | $14^{*}$ | 200* | 14* |
| 3 | 80 | 325 | 22 | 325 | 22 | 225 | 16 | 225 | 16 |
|  |  | 275* | 19* | 275* | 19* | 150* | 10* | 150* | 10* |
| 4 | 100 | 300 | 21 | 300 | 21 | 175 | 12 | 175 | 12 |
|  |  | 200* | $14^{*}$ | 200* | 14* | 125* | 9* | 125* | 9* |
| 6 | 150 | 225 | 16 | 225 | 16 | 150 | 10 | 150 | 10 |
|  |  | 175* | $12^{*}$ | 175* | 12* | 100* | 7* | 100* | 7* |
| 8 | 200 | 225 | 16 | 225 | 16 | - | - | - | - |
|  |  | 150* | 10* | 150* | 10* | - | - | - | - |
| 10 | 250 | 200 | 14 | 200 | 14 | - | - | - | - |
|  |  | 150* | 10* | 150* | 10* | - | - | - | - |
| 12 | 300 | 175 | 12 | 150 | 10 | - | - | - | - |
|  |  | 150 * | 10* | 150* | 10* | - | - | - | - |
| 14 | 350 | 150 | 10 | 150 | 10 | - | - | - | - |
| 16 | 400 | 150 | 10 | 150 | 10 | - | - | - | - |

*Note: Pressure ratings for Series 5000 are lower than for other pipe series.

- Tapered body reducers
- Tapered body reducers, flanged
- Flanges
- Flanges, blind
- Saddles, bell end
- Crosses, bell end
- Crosses, flanged
- End caps
- Reducer bushings

| $\begin{aligned} & \text { Nom } \\ & \text { Pipe } \\ & \text { Size } \end{aligned}$ | Tapered body reducers Tapered body reducers, flanged Flanges |  |  | Saddles, bell end Saddles, flanged Blind Flanges |  | Crosses, bell end Crosses, flanged |  | End caps Reducer bushings |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in. | mm | psi | bar | psi | bar | psi | bar | psi | bar |
| 1 | 25 | 600 | 41 | 150 | 10 | - | - | 50 | 3 |
| $11 / 2$ | 40 | 550 | 38 | 150 | 10 | - | - | 50 | 3 |
| 2 | 50 | 450 | 31 | 150 | 10 | 150 | 10 | 50 | 3 |
| 3 | 80 | 350 | 24 | 150 | 10 | 150 | 10 | 50 | 3 |
| 4 | 100 | 350 | 24 | 150 | 10 | 150 | 10 | 50 | 3 |
| 6 | 150 | 250 | 17 | 150 | 10 | 100 | 7 | 50 | 3 |
| 8 | 200 | 225 | 16 | 150 | 10 | 100 | 7 | 50 | 3 |
| 10 | 250 | 175 | 12 | 150 | 10 | 100 | 7 | 50 | 3 |
| 12 | 300 | 150 | 10 | 150 | 10 | 100 | 7 | 50 | 3 |
| 14 | 350 | 150 | 10 | 150 | 10 | - | - | 50 | 3 |
| 16 | 400 | 150 | 10 | 150 | 10 | - | - | 50 | 3 |

- Laterals, bell end
- Laterals, flanged
- Sleeve couplings
- Adapters, threaded
- Adapters, grooved

| Nom pipe Size |  | Laterals, bell end Laterals, flanged |  | Sleeve couplings |  | Adapters, threaded Adapters, grooved |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in. | mm | psi | bar | psi | bar | psi | bar |
| 1 | 25 | - | - | 450 | 31 | - | - |
| $11 / 2$ | 40 | - | - | 450 | 31 | - | - |
| 2 | 50 | 150 | 10 | 450 | 31 | 200 | 14 |
|  |  | 150* | 10* | 450 | 31 | 150* | 10* |
| 3 | 80 | 150 | 10 | 425 | 29 | 200 | 14 |
|  |  | 150* | 10* | 350* | 24* | 150* | 10* |
| 4 | 100 | 150 | 10 | 400 | 28 | 150 | 10 |
|  |  | 150* | 10* | 350 | 24* | 100* | 7* |
| 6 | 150 | 100 | 7 | 300 | 21 | 150 | 10 |
|  |  | 100* | 7* | 250 | 17* | 100* | 7* |
| 8 | 200 | 100 | 7 | 250 | 17 | - | - |
|  |  | 100* | 7* | 225* | 16* | - | - |
| 10 | 250 | 100 | 7 | 200 | 14 | - | - |
|  |  | 100* | 7* | 175* | 12* | - | - |
| 12 | 300 | 100 | 7 | 170 | 12 | - | - |
|  |  | 100* | 7* | 150* | 10* | - | - |
| 14 | 350 | - | - | 165 | 11 | - | - |
|  |  | - | - | 150* | 10* | - | - |
| 16 | 400 | - | - | 165 | 11 | - | - |
|  |  | - | - | 150* | 10* | - | - |

*Note: Pressure ratings for Series 5000 are lower than for other pipe series.

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## Fittings \& Flanges for 32-50 Bar Pipe Series 2400

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## 32 Bar Fittings

## $90^{\circ}$ Elbows



| Nominal <br> Pipe Size |  | A | X | Wgt. |
| :---: | :---: | :---: | :---: | :---: |
| mm | in | mm | mm | kg |
| 50 | 2 | 137 | 50 | 0.6 |
| 80 | 3 | 190 | 80 | 2.1 |
| 100 | 4 | 235 | 80 | 3.8 |
| 150 | 6 | 350 | 110 | 8.7 |
| 200 | 8 | 455 | 140 | 24.0 |
| 250 | 10 | 561 | 170 | 39.0 |
| 300 | 12 | 663 | 200 | 61.0 |
| 350 | 14 | 594 | 230 | 66.0 |
| 400 | 16 | 632 | 230 | 84.0 |
| 450 | 18 | 732 | 260 | 168.0 |
| 500 | 20 | 813 | 290 | 230.0 |
| 600 | 24 | 975 | 350 | 367.0 |

## $45^{\circ}$ Elbows



| Nominal <br> Pipe Size |  | A | X | Wgt. |
| :---: | :---: | :---: | :---: | :---: |
| mm | in | mm | mm | kg |
| 50 | 2 | 95 | 50 | 0.5 |
| 80 | 3 | 141 | 80 | 1.7 |
| 100 | 4 | 153 | 80 | 2.4 |
| 150 | 6 | 216 | 110 | 7.0 |
| 200 | 8 | 277 | 140 | 15.5 |
| 250 | 10 | 339 | 170 | 32.0 |
| 300 | 12 | 396 | 200 | 45.0 |
| 350 | 14 | 355 | 230 | 58.0 |
| 400 | 16 | 372 | 230 | 80.0 |
| 450 | 18 | 464 | 260 | 115.0 |
| 500 | 20 | 515 | 290 | 157.0 |
| 600 | 24 | 618 | 350 | 281.0 |

## 32 Bar Fittings

## $2211^{\circ}$ Elbows



| Nominal <br> Pipe Size |  | A | X | Wgt. |
| :---: | :---: | :---: | :---: | :---: |
| mm | in | mm | mm | kg |
| 50 | 2 | 79 | 50 | 0.4 |
| 80 | 3 | 117 | 80 | 1.5 |
| 100 | 4 | 123 | 80 | 2.0 |
| 150 | 6 | 170 | 110 | 5.9 |
| 200 | 8 | 216 | 140 | 10.5 |
| 250 | 10 | 238 | 170 | 19.1 |
| 300 | 12 | 277 | 200 | 32.0 |
| 350 | 14 | 301 | 230 | 43.0 |
| 400 | 16 | 315 | 230 | 57.0 |
| 450 | 18 | 366 | 260 | 78.0 |
| 500 | 20 | 406 | 290 | 107.0 |
| 600 | 24 | 486 | 350 | 185.0 |

## Tees



## 32 Bar Fittings

Reducing Tees


## 32 Bar Fittings

## Reducing Tees cont



| Nominal <br> Pipe Size |  | A | $\mathrm{X}_{1}$ | B | $\mathrm{X}_{2}$ | Wgt |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| mm | in | mm | mm | mm | mm | kg |
| $600 \times 600 \times 350$ | $24 \times 24 \times 14$ | 784 | 350 | 636 | 230 | 589.0 |
| $600 \times 600 \times 400$ | $24 \times 24 \times 16$ | 784 | 350 | 636 | 230 | 598.0 |
| $600 \times 600 \times 450$ | $24 \times 24 \times 18$ | 784 | 350 | 688 | 260 | 619.0 |
| $600 \times 600 \times 500$ | $24 \times 24 \times 20$ | 784 | 350 | 716 | 290 | 638.0 |

## Concentric Reducers



| Nominal <br> Pipe Size |  | A | $\mathrm{X}_{1}$ | $\mathrm{X}_{2}$ | Wgt. |
| :---: | :---: | :---: | :---: | :---: | :---: |
| mm | in | mm | mm | mm | kg |
| $80 \times 50$ | $3 \times 2$ | 204 | 80 | 50 | 0.9 |
| $100 \times 50$ | $4 \times 2$ | 226 | 80 | 50 | 2.7 |
| $100 \times 80$ | $4 \times 3$ | 254 | 80 | 80 | 2.8 |
| $150 \times 80$ | $6 \times 3$ | 307 | 110 | 80 | 3.9 |
| $150 \times 100$ | $6 \times 4$ | 314 | 110 | 80 | 4.2 |
| $200 \times 100$ | $8 \times 4$ | 383 | 140 | 80 | 9.5 |
| $200 \times 150$ | $8 \times 6$ | 379 | 140 | 110 | 9.5 |
| $250 \times 150$ | $10 \times 6$ | 428 | 170 | 110 | 14.5 |
| $250 \times 200$ | $10 \times 8$ | 445 | 170 | 140 | 16.0 |
| $300 \times 200$ | $12 \times 8$ | 520 | 200 | 140 | 33.0 |
| $300 \times 250$ | $12 \times 10$ | 537 | 200 | 170 | 35.0 |
| $350 \times 250$ | $14 \times 10$ | 614 | 230 | 170 | 45.0 |
| $350 \times 300$ | $14 \times 12$ | 638 | 230 | 200 | 50.0 |
| $400 \times 300$ | $16 \times 12$ | 625 | 230 | 200 | 42.0 |
| $400 \times 350$ | $16 \times 14$ | 643 | 230 | 230 | 48.0 |
| $450 \times 400$ | $18 \times 16$ | 618 | 260 | 230 | 71.0 |
| $500 \times 400$ | $20 \times 16$ | 769 | 290 | 230 | 113.0 |
| $500 \times 450$ | $20 \times 18$ | 701 | 290 | 260 | 117.0 |
| $600 \times 400$ | $24 \times 16$ | 1066 | 350 | 230 | 156.0 |
| $600 \times 450$ | $24 \times 18$ | 998 | 350 | 260 | 155.0 |
| $600 \times 500$ | $24 \times 20$ | 907 | 350 | 290 | 164.0 |

[^33]
## 32 Bar Fittings

## Couplings

|  | Nominal Pipe Size |  | A | x | B | Wgt. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | mm | in | mm | mm | mm | kg |
| $A \longrightarrow$ | 50 | 2 | 170 | 50 | 70 | 0.4 |
|  | 80 | 3 | 230 | 80 | 100 | 0.9 |
| $\rightarrow \times \sim$ | 100 | 4 | 230 | 80 | 124 | 1.2 |
| M-m | 150 | 6 | 290 | 110 | 180 | 2.2 |
| - | 200 | 8 | 350 | 140 | 238 | 5.0 |
| - | 250 | 10 | 410 | 170 | 296 | 7.9 |
|  | 300 | 12 | 470 | 200 | 350 | 11.6 |
| - | 350 | 14 | 530 | 230 | 381 | 13.2 |
|  | 400 | 16 | 530 | 230 | 435 | 17.4 |
|  | 450 | 18 | 590 | 260 | 472 | 17.8 |
|  | 500 | 20 | 650 | 290 | 524 | 23.0 |
|  | 600 | 24 | 770 | 350 | 630 | 41.0 |

## Nipples



| Nominal <br> Pipe Size |  | A | X | Wgt. |
| :---: | :---: | :---: | :---: | :---: |
| mm | in | mm | mm | kg |
| 50 | 2 | 125 | 50 | 0.1 |
| 80 | 3 | 185 | 80 | 0.2 |
| 100 | 4 | 185 | 80 | 0.3 |
| 150 | 6 | 245 | 110 | 0.8 |
| 200 | 8 | 310 | 140 | 1.6 |
| 250 | 10 | 370 | 170 | 3.1 |
| 300 | 12 | 440 | 200 | 5.0 |
| 350 | 14 | 500 | 230 | 7.4 |
| 400 | 16 | 500 | 230 | 9.1 |
| 450 | 18 | 580 | 260 | 12.9 |
| 500 | 20 | 640 | 290 | 17.8 |
| 600 | 24 | 760 | 350 | 30.0 |

## 32 Bar Fittings

## Heavy-Duty Flanges



| Nominal <br> Pipe Size |  | A | X | Wgt.(1) |
| :---: | :---: | :---: | :---: | :---: |
| mm | in | mm | mm | kg |
| 50 | 2 | 55 | 50 | 1.7 |
| 80 | 3 | 85 | 80 | 4.0 |
| 100 | 4 | 85 | 80 | 5.9 |
| 150 | 6 | 115 | 110 | 11.2 |
| 200 | 8 | 146 | 140 | 19.2 |
| 250 | 10 | 176 | 170 | 28.0 |

Notes:
(1)The weights shown are for ANSI B16.5 Class 300 drilled flanges. Weights for other drilling classes may be different. For more detailed information reference is made to the appropriate product data.
*Heavy Duty Flanges are standard available in drillings according to ANSI and ISO (DIN).
**Full-face elastomeric gaskets may be used, suitable for the service pressure, service temperature and fluid. Shore A durometer hardness of $60 \pm 5$ is recommended and a thickness of 3 mm .
Compressed fiber gaskets, 3 mm thick, compatible with the pressure, temperature and medium, may also be used. The mechanical properties should be in accordance with DIN 3754 (IT 400) or equal.
***For maximum bolt torque refer to the appropriate Bondstrand literature. Please be aware that excessive torque may result in flange failure and, therefore a torque-wrench is required.

## 32 Bar Fittings

Stub-end Flanges (Van Stone)


| Nominal Pipe Size |  | A | X | H | Wgt. <br> Stub <br> End | Wgt. <br> Steel <br> Ring ${ }^{(1)}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| mm | in | mm | mm | mm | kg | kg |
| 50 | 2 | 65 | 50 | 10 | 0.2 | 2.5 |
| 80 | 3 | 95 | 80 | 16 | 0.7 | 4.8 |
| 100 | 4 | 95 | 80 | 16 | 1.1 | 7.0 |
| 150 | 6 | 125 | 110 | 23 | 2.3 | 12.2 |
| 200 | 8 | 155 | 140 | 29 | 4.0 | 18.3 |
| 250 | 10 | 185 | 170 | 33 | 5.5 | 26.0 |
| 300 | 12 | 215 | 200 | 38 | 7.6 | 39.0 |
| 350 | 14 | 245 | 230 | 40 | 7.9 | 56.0 |
| 400 | 16 | 250 | 230 | 47 | 11.6 | 70.0 |
| 450 | 18 | 280 | 260 | 51 | 22.0 | 85.0 |
| 500 | 20 | 310 | 290 | 58 | 26.0 | 107.0 |
| 600 | 24 | 370 | 350 | 71 | 29.0 | 182.0 |

Notes:
(1)The weight shown is for ANSI B16.5 Class 300 drilled flanges. Weights for other drilling classes may be different. For more detailed information reference is made to the appropriate product data.
*Stub-End Flange Rings are standard available in drillings according to ANSI and ISO (DIN).
**Stub-End Flanges are available with and without O-ring groove in the face.
Suitable O-ring seals should be used, available on request.
***Make sure that the O-ring grooved stub-end is compatible with its counter flange, e.g. use a stub-end without groove or another flat surface flange as counter flange.
****Maximum bolt-torque for use with O-rings seals may be calculated based on pressure, size and number of bolts.

## 40 Bar Fittings

## $90^{\circ}$ Elbows



| Nominal <br> Pipe Size |  | A | X | Wgt. |
| :---: | :---: | :---: | :---: | :---: |
| mm | in | mm | mm | kg |
| 50 | 2 | 167 | 80 | 0.9 |
| 80 | 3 | 190 | 80 | 2.1 |
| 100 | 4 | 280 | 110 | 5.2 |
| 150 | 6 | 380 | 140 | 13.0 |
| 200 | 8 | 485 | 170 | 34.0 |
| 300 | 10 | 616 | 200 | 54.0 |
| 350 | 12 | 748 | 260 | 94.0 |
| 400 | 16 | 649 | 260 | 100.0 |
| 50 | 18 | 717 | 297 | 320 |

## $45^{\circ}$ Elbows



| Nominal <br> Pipe Size |  | A | X | Wgt. |
| :---: | :---: | :---: | :---: | :---: |
| mm | in | mm | mm | kg |
| 50 | 2 | 125 | 80 | 0.8 |
| 80 | 3 | 141 | 80 | 1.7 |
| 100 | 4 | 198 | 110 | 4.0 |
| 150 | 6 | 246 | 140 | 10.8 |
| 200 | 8 | 307 | 170 | 23.0 |
| 250 | 10 | 394 | 200 | 45.0 |
| 300 | 12 | 481 | 260 | 73.0 |
| 350 | 14 | 410 | 260 | 86.0 |
| 400 | 16 | 457 | 290 | 121.0 |
| 450 | 18 | 559 | 320 | 182.0 |
| 500 | 20 | 630 | 380 | 258.0 |

## 40 Bar Fittings

## 22 $12^{\circ}$ Elbows



| Nominal <br> Pipe Size |  | A | X | Wgt. |
| :---: | :---: | :---: | :---: | :---: |
| mm | in | mm | mm | kg |
| 50 | 2 | 109 | 80 | 0.7 |
| 80 | 3 | 117 | 80 | 1.5 |
| 100 | 4 | 168 | 110 | 3.5 |
| 150 | 6 | 200 | 140 | 9.2 |
| 200 | 8 | 246 | 170 | 16.1 |
| 250 | 10 | 293 | 200 | 30.0 |
| 300 | 12 | 362 | 260 | 54.0 |
| 350 | 14 | 356 | 260 | 64.0 |
| 400 | 16 | 400 | 290 | 87.0 |
| 500 | 18 | 461 | 320 | 126.0 |

Tees


## 40 Bar Fittings

Reducing Tees


| Nominal Pipe Size |  | A | $\mathrm{X}_{1}$ | B | $\mathrm{X}_{2}$ | Wgt. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| mm | in | mm | mm | mm | mm | kg |
| 80X80X50 | $3 \times 3 \times 2$ | 176 | 80 | 166 | 80 | 3.5 |
| 100×100×50 | 4X4X2 | 240 | 110 | 179 | 80 | 8.5 |
| 100X100X80 | 4X4X3 | 240 | 110 | 188 | 80 | 8.7 |
| 150X150X50 | 6X6X2 | 293 | 140 | 204 | 80 | 18.3 |
| 150X150X80 | 6X6X3 | 293 | 140 | 214 | 80 | 19.1 |
| 150X150X100 | 6X6X4 | 293 | 140 | 265 | 110 | 21.0 |
| 200X200×80 | 8X8X3 | 358 | 170 | 239 | 80 | 39.0 |
| 200X200X100 | $8 \times 8 \times 4$ | 358 | 170 | 297 | 110 | 41.0 |
| 200X200X150 | 8X8X6 | 358 | 170 | 318 | 140 | 44.0 |
| 250X250×100 | 10X10×4 | 451 | 200 | 319 | 110 | 62.0 |
| 250X250X150 | 10X10X6 | 451 | 200 | 344 | 140 | 66.0 |
| 250X250X200 | 10X10X8 | 451 | 200 | 383 | 170 | 70.0 |
| $300 \times 300 \times 100$ | 12X12X4 | 549 | 260 | 341 | 110 | 107.0 |
| $300 \times 300 \times 150$ | 12X12X6 | 549 | 260 | 369 | 140 | 111.0 |
| $300 \times 300 \times 200$ | 12X12X8 | 549 | 260 | 409 | 170 | 116.0 |
| $300 \times 300 \times 250$ | 12X12X10 | 549 | 260 | 476 | 200 | 125.0 |
| $350 \times 350 \times 150$ | 14X14X6 | 557 | 260 | 394 | 140 | 134.0 |
| 350X350X200 | 14X14X8 | 557 | 260 | 434 | 170 | 140.0 |
| 350X350X250 | 14X14X10 | 557 | 260 | 502 | 200 | 150.0 |
| 350X350×300 | 14X14X12 | 557 | 260 | 574 | 260 | 163.0 |
| 400X400X150 | 16X16X6 | 610 | 290 | 414 | 140 | 176.0 |
| 400X400×200 | 16X16X8 | 610 | 290 | 453 | 170 | 182.0 |
| 400×400×250 | 16X16X10 | 610 | 290 | 518 | 200 | 193.0 |
| $400 \times 400 \times 300$ | 16X16X12 | 610 | 290 | 590 | 260 | 206.0 |
| 400X400×350 | 16X16X14 | 610 | 290 | 600 | 260 | 137.0 |
| 450X450X200 | 18X18X8 | 694 | 320 | 486 | 170 | 317.0 |
| 450X450X250 | 18X18X10 | 694 | 320 | 554 | 200 | 3330.0 |
| 450X450X300 | 18X18X12 | 694 | 320 | 614 | 260 | 350.0 |
| 450X450X350 | 18X18X14 | 694 | 320 | 615 | 260 | 356.0 |
| 450X450X400 | 18X18X16 | 694 | 320 | 645 | 290 | 370.0 |
| 500×500×250 | 20X20X10 | 775 | 380 | 580 | 200 | 521.0 |
| $500 \times 500 \times 300$ | 20×20×12 | 775 | 380 | 640 | 260 | 543.0 |
| $500 \times 500 \times 350$ | 20X20X14 | 775 | 380 | 641 | 260 | 551.0 |
| $500 \times 500 \times 400$ | 20X20X16 | 775 | 380 | 671 | 290 | 570.0 |
| 500X500X450 | 20×20X18 | 775 | 380 | 720 | 320 | 593.0 |

## 40 Bar Fittings

## Concentric Reducers



| Nominal Pipe Size |  | A | $\mathrm{X}_{1}$ | $\mathrm{X}_{2}$ | Wgt. |
| :---: | :---: | :---: | :---: | :---: | :---: |
| mm | in | mm | mm | mm | kg |
| 80X50 | 3X2 | 234 | 80 | 80 | 1.4 |
| 100X50 | 4X2 | 301 | 110 | 80 | 4.2 |
| 100X80 | 4X3 | 299 | 110 | 80 | 4.3 |
| 150X80 | 6X3 | 337 | 140 | 80 | 4.4 |
| 150X100 | 6X4 | 389 | 140 | 110 | 5.0 |
| 200X100 | 8X4 | 458 | 170 | 110 | 14.2 |
| 200X150 | 8X6 | 439 | 170 | 140 | 16.5 |
| 250X150 | 10X6 | 513 | 200 | 140 | 23.0 |
| 250X200 | 10x8 | 530 | 200 | 170 | 26.0 |
| $300 \times 200$ | $12 \times 8$ | 635 | 260 | 170 | 50.0 |
| $300 \times 250$ | $12 \times 10$ | 677 | 260 | 200 | 57.0 |
| $350 \times 250$ | 14X10 | 724 | 260 | 200 | 67.0 |
| $350 \times 300$ | 14X12 | 778 | 260 | 260 | 79.0 |
| $400 \times 300$ | 16X12 | 795 | 290 | 260 | 95.0 |
| $400 \times 350$ | 16X14 | 783 | 290 | 260 | 64.0 |
| $450 \times 400$ | 18X16 | 798 | 320 | 290 | 116.0 |
| $500 \times 400$ | $20 \times 16$ | 969 | 380 | 290 | 187.0 |
| $500 \times 450$ | $20 \times 18$ | 911 | 380 | 320 | 194.0 |
| 500X400 | 20X16 | 879 | 290 | 290 | 164.0 |
| $500 \times 450$ | 20X18 | 821 | 290 | 320 | 171.0 |

Note: Eccentric Reducers are available on request

## 40 Bar Fittings

## Couplings

|  | Nominal Pipe Size |  | A | X | B | Wgt. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $-\mathrm{A} \longrightarrow$ | mm | in | mm | mm | mm | kg |
|  | 50 | 2 | 230 | 80 | 70 | 0.5 |
| $\rightarrow \times$ | 80 | 3 | 230 | 80 | 100 | 0.9 |
| -1070] | 100 | 4 | 290 | 110 | 124 | 1.3 |
|  | 150 | 6 | 350 | 140 | 188 | 3.7 |
|  | 200 | 8 | 410 | 170 | 238 | 5.3 |
|  | 250 | 10 | 470 | 200 | 296 | 7.9 |
| - 1 | 300 | 12 | 590 | 260 | 350 | 12.0 |
| H | 350 | 14 | 590 | 260 | 390 | 18.5 |
|  | 400 | 16 | 650 | 290 | 445 | 26.0 |
|  | 450 | 18 | 710 | 320 | 480 | 24.0 |
|  | 500 | 20 | 830 | 380 | 544 | 40.0 |

## Nipples

|  | Nominal Pipe Size |  | A | X | Wgt. |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | mm | in | mm | mm | kg |
|  | 50 | 2 | 185 | 80 | 0.1 |
|  | 80 | 3 | 185 | 80 | 0.2 |
|  | 100 | 4 | 245 | 110 | 0.5 |
|  | 150 | 6 | 305 | 140 | 1.3 |
|  | 200 | 8 | 370 | 170 | 2.5 |
|  | 250 | 10 | 430 | 200 | 4.8 |
|  | 300 | 12 | 560 | 260 | 8.8 |
|  | 350 | 14 | 560 | 260 | 10.3 |
|  | 400 | 16 | 620 | 290 | 14.6 |
| -rs | 450 | 18 | 700 | 320 | 21.0 |
|  | 500 | 20 | 820 | 380 | 26.0 |

## 40 Bar Fittings

## Heavy-Duty Flanges



| Nominal <br> Pipe Size |  | A | $X^{(1)}$ | Wgt. $^{(2)}$ |
| :---: | :---: | :---: | :---: | :---: |
| mm | in | mm | mm | kg |
| 50 | 2 | 55 | 50 | 1.7 |
| 80 | 3 | 85 | 80 | 4.0 |
| 100 | 4 | 115 | 110 | 7.9 |
| 150 | 6 | 145 | 140 | 14.1 |

Notes:
(1) Underlined insertion depth for subsequent flanges deviates from other fittings.
(2)The weights shown are for ANSI B16.5 Class 400 drilled flanges. Weights for other drilling classes may be different. For more detailed information reference is made to the appropriate product data.
*Heavy Duty Flanges are standard available in drillings according to ANSI and ISO (DIN).
**Compressed fibre gaskets, 3 mm thick, compatible with the pressure, temperature and medium, may be used. The mechanical properties should be in accordance with DIN 3754 (IT 400) or equal.

## 40 Bar Fittings

## Stub-end Flanges

 (Van Stones)

| Nominal <br> Pipe Size |  | A | X | H | Wgt. <br> Stub <br> Ring |
| :---: | :---: | :---: | :---: | :---: | :---: |
| mm | in | mm | mm | mm | kg |
| 50 | 2 | 95 | 80 | 14 | 0.3 |
| 80 | 3 | 95 | 80 | 16 | 0.7 |
| Steel |  |  |  |  |  |
| Ring |  |  |  |  |  |

Notes:
(1)The weight shown is for ANSI B16.5 Class 400 drilled flanges. Weights for other drilling classes may be different. For more detailed information reference is made to the appropriate product data.
*Stub-End Flange Rings are standard available in drillings according to ANSI and ISO (DIN).
**Stub-End Flanges are available with and without O-ring groove in the face.
Suitable O-ring seals should be used, available on request.
***Make sure that the O-ring grooved stub-end is compatible with its counter flange, e.g. use a stub-end without groove or another flat surface flange as counter flange.
****Maximum bolt-torque for use with O-rings seals may be calculated based on pressure, size and number of bolts.

## 50 Bar Fittings

## $90^{\circ}$ Elbow



| Nominal <br> Pipe Size |  | A | X | Wgt. |
| :---: | :---: | :---: | :---: | :---: |
| mm | in | mm | mm | kg |
| 50 | 2 | 167 | 80 | 1.1 |
| 80 | 3 | 235 | 110 | 3.4 |
| 100 | 4 | 330 | 140 | 7.0 |
| 150 | 6 | 420 | 170 | 22.0 |
| 200 | 8 | 540 | 200 | 48.0 |
| 250 | 10 | 676 | 260 | 77.0 |
| 300 | 12 | 753 | 290 | 122.0 |

## $45^{\circ}$ Elbows



| Nominal <br> Pipe Size |  | A | X | Wgt. |
| :---: | :---: | :---: | :---: | :---: |
| mm | in | mm | mm | kg |
| 50 | 2 | 125 | 80 | 1.0 |
| 80 | 3 | 186 | 110 | 2.9 |
| 100 | 4 | 248 | 140 | 6.3 |
| 150 | 6 | 286 | 170 | 16.7 |
| 200 | 8 | 362 | 200 | 35.0 |
| 250 | 10 | 454 | 260 | 70.0 |
| 300 | 12 | 486 | 290 | 97.0 |

## 50 Bar Fittings

## 22 $1 / 2^{\circ}$ Elbows



| Nominal <br> Pipe Size |  | A | X | Wgt. |
| :---: | :---: | :---: | :---: | :---: |
| mm | in | mm | mm | mm |
| 50 | 2 | 109 | 80 | 0.8 |
| 80 | 3 | 162 | 110 | 2.5 |
| 100 | 4 | 218 | 140 | 5.5 |
| 150 | 6 | 240 | 170 | 14.1 |
| 200 | 8 | 301 | 200 | 24.0 |
| 250 | 10 | 353 | 260 | 48.0 |
| 300 | 12 | 367 | 290 | 74.0 |

Tees


| Nominal <br> Pipe Size |  | A | B | X | Wgt. |
| :---: | :---: | :---: | :---: | :---: | :---: |
| mm | in | mm | mm | mm | kg |
| 50 | 2 | 308 | 154 | 80 | 2.3 |
| 80 | 3 | 442 | 221 | 110 | 7.3 |
| 100 | 4 | 580 | 290 | 140 | 16.4 |
| 150 | 6 | 666 | 333 | 170 | 28.0 |
| 200 | 8 | 826 | 413 | 200 | 58.0 |
| 250 | 10 | 1022 | 511 | 260 | 114.0 |
| 300 | 12 | 1108 | 554 | 290 | 174.0 |

## 50 Bar Fittings

Reducing Tees


## 50 Bar Fittings

## Concentric Reducers



| Nominal <br> Pipe Size |  | A | $\mathrm{X}_{1}$ | $\mathrm{X}_{2}$ | Wgt |
| :---: | :---: | :---: | :---: | :---: | :---: |
| mm | in | mm | mm | mm | mm |
| $80 \times 50$ | $3 \times 2$ | 279 | 110 | 80 | 2.0 |
| $100 \times 50$ | $4 \times 2$ | 351 | 140 | 80 | 6.2 |
| $100 \times 80$ | $4 \times 3$ | 394 | 140 | 110 | 6.9 |
| $150 \times 80$ | $6 \times 3$ | 422 | 170 | 110 | 6.8 |
| $150 \times 100$ | $6 \times 4$ | 479 | 170 | 140 | 8.0 |
| $200 \times 100$ | $8 \times 4$ | 563 | 200 | 140 | 21.0 |
| $200 \times 150$ | $8 \times 6$ | 534 | 200 | 170 | 25.0 |
| $250 \times 150$ | $10 \times 6$ | 613 | 260 | 170 | 35.0 |
| $250 \times 200$ | $10 \times 8$ | 645 | 260 | 200 | 41.0 |
| $300 \times 200$ | $12 \times 8$ | 695 | 290 | 200 | 70.0 |
| $300 \times 250$ | $12 \times 10$ | 742 | 290 | 260 | 82.0 |

Note: Eccentric Reducers are available on request.

## 50 Bar Fittings

## Couplings



| Nominal <br> Pipe Size |  | A | X | B | Wgt. |
| :---: | :---: | :---: | :---: | :---: | :---: |
| mm | in | mm | mm | mm | kg |
| 50 | 2 | 230 | 80 | 70 | 0.5 |
| 80 | 3 | 290 | 110 | 100 | 1.0 |
| 100 | 4 | 350 | 140 | 128 | 1.8 |
| 150 | 6 | 410 | 170 | 188 | 3.9 |
| 200 | 8 | 470 | 200 | 242 | 6.4 |
| 250 | 10 | 590 | 260 | 302 | 11.1 |
| 300 | 12 | 650 | 290 | 380 | 31.0 |

Nipples


| Nominal <br> Pipe Size |  | A | X | Wgt. |
| :---: | :---: | :---: | :---: | :---: |
| mm | in | mm | mm | kg |
| 50 | 2 | 25 | 80 | 0.1 |
| 80 | 3 | 25 | 110 | 0.4 |
| 100 | 4 | 25 | 140 | 0.8 |
| 150 | 6 | 25 | 170 | 2.0 |
| 200 | 8 | 30 | 200 | 3.8 |
| 250 | 10 | 30 | 260 | 7.7 |
| 300 | 12 | 40 | 290 | 11.8 |

## 50 Bar Fittings

Heavy-Duty Flanges


## Notes:

(1)The weights shown are for ANSI B16.5 Class 400 drilled flanges. Weights for other drilling classes may be different. For more detailed information reference is made to the appropriate product data.
*Heavy Duty Flanges are standard available in drillings according to ANSI and ISO (DIN).
**Compressed fibre gaskets, 3 mm thick, compatible with the pressure, temperature and medium, may be used. The mechanical properties should be in accordance with DIN 3754 (IT 400) or equal.
***For maximum bolt torque refer to the appropriate Bondstrand literature. Please be aware that excessive torque may result in flange failure and, therefore a torque-wrench is required.

## 50 Bar Fittings

## Stub-end Flanges

 (Van Stone)

| Nominal <br> Pipe Size |  | A | X | H | Wgt. <br> Stub <br> End | Wgt. <br> Steel <br> Ring |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| mm | in | mm | mm | mm | kg | kg |
| 50 | 2 | 95 | 80 | 14 | 0.3 | 2.8 |
| 80 | 3 | 125 | 110 | 19 | 0.8 | 5.3 |
| 100 | 4 | 155 | 140 | 22 | 1.6 | 8.4 |
| 200 | 6 | 185 | 170 | 34 | 3.0 | 13.3 |
| 250 | 8 | 215 | 200 | 43 | 4.8 | 21.0 |
| 300 | 10 | 275 | 260 | 48 | 6.7 | 29.0 |

## Notes:

(1)The weight shown is for ANSI B16.5 Class 400 drilled flanges. Weights for other drilling classes may be different. For more detailed information reference is made to the appropriate product data.
*Stub-End Flange Rings are standard available in drillings according to ANSI and ISO (DIN).
**Stub-End Flanges are available with and without O-ring groove in the face.
Suitable O-ring seals should be used, available on request.
***Make sure that the O-ring grooved stub-end is compatible with its counter flange, e.g. use a stub-end without groove or another flat surface flange as counter flange.
****Maximum bolt-torque for use with O-rings seals may be calculated based on pressure, size and number of bolts.

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## Fittings Dimensions in 2" through 16"

(For Bondstrand"' pipe systems 3000, 3200, 3300, 3000A, 3200A and 3300A)
Units: All dimensions are in U.S. Customary units (inches). Diametric dimensions are maximums. Insertion depths $(\mathrm{X}$ ) are typical. All weights (lbs.) are approximate and assume bell-end configurations.

Tolerances: Tolerance for center line to face dimensions on fittings with flange-end configurations is $\pm 1 / 2$ inch. Tolerance for center line to face dimensions on fittings with bell-end configurations is $\pm 1 / 2$ inch. Tolerance for angular dimensions is $\pm 1^{\circ}$.

Standard end configurations: Bell end is standard configurations. All other end configurations, including size reductions, are made to order.

Taper angle: Taper angle on all bell x spigot end configurations is $1^{3 /} /^{\circ}$ for 2 through 6 inch nominal and $2^{\circ}$ for sizes 8 through 16 inch pipe sizes.

Manufacturing methods: The fiberglass-reinforced epoxy resin fittings shown in this publication are manufactured by the methods as indicated - Filament winding, Compression molding, Centrifugal casting and Contact molding.

Pressure ratings: See the appropriate Bondstrand Product Data sheet for pressure ratings.
Individual system components may not have the same ratings as the pipe. Refer to the detailed product information for the specific components to determine the pressure rating for the system as a whole.

Flange rings: Bolt hole patterns are drilled in accordance with ANSI B16.5, Cl. 150.
$90^{\circ}$ Elbows


| Nominal <br> Pipe Size | Bell | Flange | Bell | BxB <br> Wgt. |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | mm | in | F | X | in |
| 2 | 50 | 3.82 | 7.00 | 2.1 | 1.0 |
| 3 | 80 | 4.42 | 9.20 | 2.3 | 1.5 |
| 4 | 100 | 5.50 | 10.40 | 3.2 | 3.0 |
| 6 | 150 | 7.50 | 13.60 | 4.0 | 8.5 |
| 8 | 200 | 13.00 | 22.30 | 4.0 | 18.0 |
| 10 | 250 | 15.50 | 25.50 | 4.3 | 24.0 |
| 12 | 300 | 17.80 | 27.30 | 4.3 | 40.0 |
| 14 | 350 | 20.80 | 30.50 | 5.8 | 85.0 |
| 16 | 400 | 23.00 | 35.00 | 6.2 | 161.0 |

## $60^{\circ}$ Elbows



| Nominal <br> Pipe Size |  | Bell | Flange | Bell | BxB <br> Wgt. |
| :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | in | in | X |  |
| 8 | 200 | 9.80 | 18.80 | 4.0 | 25.0 |
| 10 | 250 | 11.00 | 21.00 | 4.3 | 33.0 |
| 12 | 300 | 12.50 | 22.00 | 4.3 | 50.0 |
| 14 | 350 | 14.80 | 24.50 | 5.8 | 100.0 |
| 16 | 400 | 16.30 | 28.30 | 6.2 | 161.0 |

## $45^{\circ}$ Elbows



| Nominal <br> Pipe Size |  | Bell | Flange | Bell | BxB |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | A | F | X | Wgt. |  |
| in | mm | in | in | in | Ibs. |
| 2 | 50 | 3.18 | 6.40 | 2.1 | 0.9 |
| 3 | 80 | 3.43 | 8.10 | 2.3 | 1.5 |
| 4 | 100 | 4.23 | 9.10 | 3.2 | 2.5 |
| 6 | 150 | 5.56 | 11.50 | 4.0 | 7.0 |
| 8 | 200 | 8.30 | 17.50 | 4.0 | 15.0 |
| 10 | 250 | 9.30 | 19.30 | 4.3 | 28.0 |
| 12 | 300 | 10.50 | 20.00 | 4.3 | 36.0 |
| 14 | 350 | 12.50 | 22.30 | 5.8 | 50.0 |
| 16 | 400 | 13.80 | 25.80 | 6.2 | 106.0 |

## $45^{\circ}$ Laterals

|  | Nominal Pipe Size |  | Bell | Bell | Flange | Flange | Bell | BxB <br> Wgt. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | in | mm | in | in | in | in | in | Ibs. |
|  | 2 | 50 | 12.31 | 9.81 | 7.62 | 10.12 | 1.8 | 1.7 |
|  | 3 | 80 | 14.16 | 10.66 | 8.26 | 11.76 | 2.1 | 3.5 |
|  | 4 | 100 | 16.44 | 11.94 | 9.48 | 13.98 | 2.4 | 5.4 |
| $A \rightarrow \vec{C} \rightarrow\|x\|-$ | 6 | 150 | 22.95 | 15.95 | 12.27 | 19.27 | 2.7 | 15.8 |
|  | 8 | 200 | 26.00 | 16.00 | 13.00 | 20.50 | 4.0 | 80.0 |
|  | 10 | 250 | 30.00 | 16.00 | 14.00 | 24.50 | 4.3 | 110.0 |
| P1/ | 12 | 300 | 32.50 | 18.50 | 16.00 | 26.00 | 4.3 | 134.0 |
|  | 14 | 350 | 37.50 | 19.50 | 16.50 | 30.00 | 5.8 | 204.0 |
|  | 16 | 400 | 40.50 | 22.50 | 16.50 | 32.50 | 6.2 | 254.0 |

Tees*


The length of the reducing branch is equal to the length of the branch of the run diameter with the appropriate end configuration. Specify end configuration in the sequence: run(1), run(2), branch(3).

## Crosses



| Nominal <br> Pipe Size |  | Bell | Flange | Bell | BxB <br> Wgt. |
| :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | in | F | X |  |
| 2 | 50 | 10.81 | 8.62 | 1.8 | 2.1 |
| 3 | 80 | 11.91 | 9.51 | 2.1 | 4.4 |
| 4 | 100 | 13.44 | 10.98 | 2.4 | 6.8 |
| 6 | 150 | 17.95 | 14.27 | 2.7 | 19.8 |
| 8 | 200 | 13.00 | 22.30 | 4.0 | 89.0 |
| 10 | 250 | 15.50 | 25.50 | 4.3 | 122.0 |
| 12 | 300 | 17.80 | 27.30 | 4.3 | 149.0 |
| 14 | 350 | 20.80 | 30.50 | 5.8 | 226.0 |
| 16 | 400 | 23.00 | 35.00 | 6.2 | 282.0 |

The length of the reducing branch is equal to the length of the branch of the run diameter with the appropriate end configuration. Specify end configuration in the sequence: run(1), run(2), branch(3), branch(4).

FW Reducing Tee


| Run Nominal <br> Pipe Size | "B" Branch Lenght for Bell |  |  |  |  | Bell | Bell |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 8 | 10 | 12 | 14 | A | X |  |
| in | mm | in | in | in | in | in | in |
| 10 | 250 | 12.81 | -- | -- | -- | 13.06 | 4.3 |
| 12 | 300 | 13.79 | 14.05 | -- | -- | 15.50 | 4.3 |
| 14 | 350 | -- | 14.90 | 16.35 | -- | 19.00 | 5.8 |
| 16 | 400 | -- | -- | 17.36 | 20.01 | 20.25 | 6.2 |

Reducing Tees*


| Run Nominal Pipe Size |  | "B" Branch length for bell or Flange |  |  |  |  |  |  |  | Bell | Flange | Bell |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 2 | 3 | 4 | 6 | 8 | 10 | 12 | 14 | A | F | X |
| in | mm | in | in | in | in | in | in | in | in | in | in | in |
| 8 | 200 | 13.0 | 13.5 | 14.8 | 18.8 | -- | -- | -- | -- | 13.0 | 22.3 | 4.0 |
| 10 | 250 | 14.3 | 14.8 | 16.0 | 20.0 | 21.5 | -- | -- | -- | 15.5 | 25.5 | 4.3 |
| 12 | 300 | 15.3 | 15.8 | 17.0 | 21.0 | 22.5 | 25.5 | -- | -- | 17.8 | 27.3 | 4.3 |
| 14 | 350 | 16.0 | 16.5 | 17.8 | 21.8 | 23.3 | 26.3 | 28.3 | -- | 20.8 | 30.5 | 5.8 |
| 16 | 400 | 17.0 | 17.5 | 18.8 | 22.8 | 24.3 | 27.3 | 29.3 | 31.3 | 23.0 | 35.0 | 6.2 |

*Specify end configurations (bell or flanges) in sequence: run(1), run(2), branch(3).

FW Concentric Reducers*


2
*Specify end configurations (bell or flange) in the sequence: major diameter(1), minor diameter(2).

FW Concentric Reducers


| Nominal <br> Pipe Size |  | Bell | Flange | Bell |
| :---: | :---: | :---: | :---: | :---: |
| in | mm | in | in | X |
| 2 | 50 | 4.30 | 12.50 | 1.80 |
| 3 | 80 | 5.00 | 12.50 | 2.13 |
| 4 | 100 | 5.80 | 14.50 | 2.44 |
| 6 | 150 | 8.00 | 14.50 | 2.69 |
| 8 | 200 | 9.00 | 14.50 | 4.0 |
| 10 | 250 | 9.00 | 15.50 | 4.3 |
| 12 | 300 | 9.60 | 15.50 | 4.3 |
| 14 | 350 | 10.50 | 17.00 | 5.8 |
| 16 | 400 | 11.30 | 19.50 | 6.2 |

NOTE: The overall length is determined by adding the two end configurations and the cone length " D ".

| Cone length "D" |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Major Nominal Pipe Size |  | Minor Nominal Pipe Size |  |  |  |  |  |  |  |  |
|  |  | 2 | 3 | 4 | 6 | 8 | 10 | 12 | 14 | Wgt. |
| in | mm | in | in | in | in | in | in | in | in | Ibs. |
| 8 | 200 | 17.60 | 14.00 | 11.20 | 5.30 | -- | -- | -- | -- | 30 |
| 10 | 250 | 23.20 | 20.50 | 17.20 | 11.30 | 6.00 | -- | -- | -- | 44 |
| 12 | 300 | 28.50 | 25.40 | 23.60 | 16.60 | 11.30 | 5.20 | -- | -- | 65 |
| 14 | 350 | 33.40 | 30.20 | 27.40 | 21.50 | 16.20 | 11.00 | 4.80 | -- | 86 |
| 16 | 400 | 39.10 | 36.00 | 33.10 | 27.20 | 21.80 | 15.90 | 10.60 | 5.70 | 110 |

## SLEEVE Couplings

| 2"-6" | Nominal Pipe Size |  | Bell | Bell | Wgt. |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | A | X |  |
|  | in | mm | in | in | lbs. |
|  | 2 | 50 | 4.87 | 2.1 | 0.7 |
|  | 3 | 80 | 5.12 | 2.2 | 1.3 |
|  | 4 | 100 | 5.50 | 2.4 | 1.9 |
|  | 6 | 150 | 7.00 | 3.1 | 4.1 |
| - | 8 | 200 | 12.00 | 4.0 | 12.0 |
|  | 10 | 250 | 12.00 | 4.3 | 18.0 |
| 8"-16" | 12 | 300 | 13.25 | 4.3 | 23.0 |
| $\longleftarrow A \longrightarrow 1$ | 14 | 350 | 15.00 | 5.8 | 28.0 |
| ¢ | 16 | 400 | 16.50 | 6.2 | 37.0 |

True Wyes


| Nominal <br> Pipe Size |  | Bell | Bell | Flange | Flange | Bell | Wgt. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | A | B | C | D | X |  |  |
| in | mm | in | in | in | in | in | lbs. |
| 2 | 50 | 10.81 | 9.81 | 7.62 | 8.62 | 2.1 | 1.7 |
| 3 | 80 | 11.91 | 10.66 | 8.26 | 9.51 | 2.2 | 3.5 |
| 4 | 100 | 13.44 | 11.94 | 9.48 | 10.98 | 2.4 | 5.4 |
| 6 | 150 | 17.95 | 15.95 | 12.27 | 14.27 | 3.1 | 15.8 |
| 8 | 200 | 22.00 | 22.00 | 16.00 | 16.00 | 4.0 | 98.0 |
| 10 | 250 | 26.50 | 26.00 | 20.00 | 20.00 | 4.3 | 122.0 |
| 12 | 300 | 30.50 | 30.50 | 24.00 | 24.00 | 4.3 | 157.0 |
| 14 | 350 | 35.50 | 35.50 | 28.00 | 28.00 | 5.8 | 238.0 |
| 16 | 400 | 40.00 | 40.00 | 32.00 | 32.00 | 6.2 | 297.0 |

Specify end configuration in the sequence: run(1), branch(2), branch(3).

| Nominal <br> Pipe Size |  | Pressure <br> Rating | A | B | D | X | Wgt. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | psi | in | in | in | in | lbs. |
| 2 | 50 | 250 | 2.75 | 0.27 | 3.91 | 2.1 | 0.5 |
| 3 | 80 | 200 | 2.88 | 0.28 | 5.16 | 2.4 | 0.7 |
| 4 | 100 | 150 | 2.88 | 0.28 | 6.66 | 2.4 | 1.0 |
| 6 | 150 | 150 | 3.88 | 0.39 | 8.53 | 3.3 | 2.4 |
| 8 | 200 | 300 | 4.00 | 0.80 | 10.90 | 3.8 | 6.5 |
| 10 | 250 | 300 | 5.00 | 1.30 | 13.00 | 4.8 | 9.0 |
| 12 | 300 | 300 | 5.00 | 1.50 | 15.60 | 4.8 | 13.0 |
| 14 | 350 | 200 | 6.00 | 1.60 | 17.40 | 5.8 | 19.0 |
| 16 | 400 | 200 | 6.00 | 1.60 | 19.80 | 5.8 | 26.0 |

Flange Rings


| Nominal <br> Pipe Size |  | A | B | E | Bolt Hole <br> Size | Wgt. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | in | in | in | in | Ibs. |
| 2 | 50 | 2.78 | 0.82 | 6.00 | $3 / 4-4$ holes | 1.1 |
| 3 | 80 | 3.90 | 1.10 | 7.50 | $3 / 4-4$ holes | 2.1 |
| 4 | 100 | 4.90 | 1.10 | 9.00 | $3 / 4-8$ holes | 2.9 |
| 6 | 150 | 7.26 | 1.25 | 11.00 | $7 / 8-8$ holes | 3.8 |
| 8 | 200 | 10.00 | 1.30 | 13.50 | $7 / 8-8$ holes | 5.0 |
| 10 | 250 | 12.20 | 1.30 | 16.00 | $1-12$ holes | 7.0 |
| 12 | 300 | 14.30 | 1.50 | 19.00 | $1-12$ holes | 12.0 |
| 14 | 350 | 16.30 | 1.60 | 21.00 | $11 / 812$ holes | 14.5 |
| 16 | 400 | 18.60 | 1.90 | 23.50 | $11 / 8-16$ holes | 19.0 |

## 3000A/3200A Blind Flanges

ANSI B16.5, 150 Bolt Hole configuration


| Nominal <br> Pipe Size |  | B | E | H | Bolt- <br> Holes | Wgt. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | in | in | in | $\#$ | lbs. |
| 2 | 50 | 0.75 | 6.00 | 0.75 | 4 | 0.9 |
| 3 | 80 | 1.00 | 7.50 | 0.75 | 4 | 1.9 |
| 4 | 100 | 1.00 | 9.00 | 0.75 | 8 | 2.7 |
| 6 | 150 | 1.13 | 11.00 | 0.88 | 8 | 4.7 |
| 8 | 200 | 1.80 | 13.50 | 0.90 | 8 | 11.5 |
| 10 | 250 | 2.00 | 16.00 | 1.00 | 12 | 15.9 |
| 12 | 300 | 2.40 | 19.00 | 1.00 | 12 | 25.1 |
| 14 | 350 | 2.60 | 21.00 | 1.10 | 12 | 36.2 |
| 16 | 400 | 2.80 | 23.50 | 1.10 | 16 | 49.8 |

## 3300A Blind Flanges

ANSI B16.5, 150 Blot Hole configuration


| Nominal <br> Pipe Size |  | B | E | H | Bolt- <br> Holes | Wgt. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | in | in | in | $\#$ | Ibs. |
| 2 | 50 | 0.75 | 6.00 | 0.75 | 4 | 0.9 |
| 3 | 80 | 1.00 | 7.50 | 0.75 | 4 | 1.9 |
| 4 | 100 | 1.00 | 9.00 | 0.75 | 8 | 2.7 |
| 6 | 150 | 1.13 | 11.00 | 0.88 | 8 | 4.7 |
| 8 | 200 | 2.00 | 13.50 | 0.90 | 8 | 17.7 |
| 10 | 250 | 2.40 | 16.00 | 1.00 | 12 | 29.5 |
| 12 | 300 | 2.70 | 19.00 | 1.00 | 12 | 47.2 |
| 14 | 350 | 3.00 | 21.00 | 1.10 | 12 | 64.4 |
| 16 | 400 | 3.10 | 23.50 | 1.10 | 16 | 85.5 |



| Minor Nominal <br> Pipe Size | Bell | Major NPS Dimension C |  |  |  |  |  | Bell |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | A | 8 | 10 | 12 | 14 | 16 | X |  |
| in | mm | in | in | in | in | in | in | in |
| 2 | 50 | 10.00 | 7.80 | 8.90 | 9.90 | 10.80 | 11.80 | 1.80 |
| 3 | 80 | 11.00 | 8.40 | 9.50 | 10.50 | 11.40 | 12.40 | 2.13 |
| 4 | 100 | 12.00 | 8.40 | 9.50 | 10.50 | 11.40 | 12.40 | 2.44 |
| 6 | 150 | 14.00 | 8.80 | 9.90 | 10.90 | 11.80 | 12.80 | 2.69 |
| 8 | 200 | 16.00 | -- | 10.90 | 11.90 | 12.80 | 13.80 | 5.0 |
| 10 | 250 | 20.00 | -- | -- | 11.90 | 12.80 | 13.80 | 5.0 |
| 12 | 300 | 24.00 | -- | -- | -- | -- | 14.20 | 5.5 |

Saddles are available in the sizes shown above. The standard branch end configuration is bell. The taper angle on $2^{\prime \prime}-6$ " NPS bells is $1.75^{\circ}$ and $2^{\circ}$ for $8 "-12^{\prime \prime}$

Bonded Branch Saddles


| Nominal <br> Pipe Size |  | A | B | X | Wgt. |
| :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | in | in | in | lbs. |
| $3 \times 2$ | $80 \times 50$ | 6.00 | 4.00 | 1.80 | 1.2 |
| $4 \times 2$ | $100 \times 50$ | 6.00 | 4.50 | 1.80 | 1.4 |
| $4 \times 3$ | $100 \times 80$ | 6.00 | 5.25 | 2.13 | 1.4 |
| $6 \times 2$ | $150 \times 50$ | 7.75 | 5.56 | 1.80 | 3.0 |
| $6 \times 3$ | $150 \times 80$ | 7.75 | 6.31 | 2.13 | 3.0 |
| $6 \times 4$ | $150 \times 100$ | 7.75 | 7.63 | 2.44 | 3.0 |

Threaded Branch Saddles


| Nominal <br> Pipe Size |  | A | B | C | X | Wgt. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | in | in | in | in | lbs. |
| $2 x^{11 / 2}$ | $50 \times 12$ | 4.00 | 2.00 | $1 / 2 \times 14$ | 0.50 | 1.0 |
| $3 x^{1 / 2} 2$ | $80 \times 12$ | 4.00 | 2.62 | $1 / 2 \times 14$ | 0.50 | 1.6 |
| $4 x^{1 / 2}$ | $100 \times 12$ | 4.00 | 3.12 | $1 / 2 \times 14$ | 0.50 | 2.0 |
| $6 x^{1 / 2}$ | $150 \times 12$ | 4.00 | 4.18 | $1 / 2 \times 14$ | 0.50 | 2.4 |

## Bonded Reducer Bushings



| Nominal <br> Pipe Size |  | A | B | X | Wgt. |
| :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | in | in | in | lbs. |
| $3 \times 2$ | $80 \times 50$ | 1.88 | 3.51 | 1.75 | 0.7 |
| $4 \times 3$ | $100 \times 80$ | 1.96 | 4.51 | 1.75 | 0.9 |
| $6 \times 4$ | $150 \times 100$ | 2.86 | 6.65 | 2.20 | 4.1 |

## Threaded Reducer Bushings



| Nominal <br> Pipe Size |  | A | B | C | X | Wgt. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | in | in | in | in | lbs. |
| $2 \times{ }^{1 / 2} 2$ | $50 \times 12$ | 1.80 | 2.40 | $1 / 2 \times 14$ | 0.50 | 0.9 |
| $2 x^{3} / 4$ | $50 \times 19$ | 1.80 | 2.40 | $3 / 4 \times 14$ | 0.50 | 0.8 |
| $2 \times 1$ | $50 \times 25$ | 1.80 | 2.40 | $1 \times 11^{11 / 2}$ | 0.70 | 0.8 |
| $2 \times 1^{1 / 1 / 4}$ | $50 \times 32$ | 1.80 | 2.40 | $1^{1 / 4 \times 11^{1 / 2} 2}$ | 0.70 | 0.6 |
| $2 \times 1^{1 / 2}$ | $50 \times 40$ | 1.80 | 2.40 | $1^{1 / 2} \times 11^{11 / 2}$ | 0.70 | 0.3 |

## Wear Saddles



| Nominal <br> Pipe Size |  | A | Wgt. |
| :---: | :---: | :---: | :---: |
| in | mm | in | Ibs. |
| 2 | 50 | 6.00 | 0.12 |
| 3 | 80 | 6.00 | 0.17 |
| 4 | 100 | 6.00 | 0.25 |
| 6 | 150 | 6.00 | 0.48 |
| 8 | 200 | 6.00 | 0.78 |
| 10 | 250 | 6.00 | 1.13 |
| 12 | 300 | 6.00 | 1.53 |
| 14 | 350 | 6.00 | 1.88 |
| 16 | 400 | 6.00 | 2.35 |

## Adapters: Bell x NPT Male



| Nominal <br> Pipe Size |  | A | C | E | X | Wgt. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | in | in | in | in | Ibs. |
| 2 | 50 | 4.16 | $2 \times 11^{1 / 2} 2$ | 1.90 | 2.00 | 0.4 |
| 3 | 80 | 5.00 | $3 \times 8$ | 2.80 | 2.05 | 0.7 |
| 4 | 100 | 5.19 | $4 \times 8$ | 3.90 | 2.05 | 0.9 |
| 6 | 150 | 6.00 | $6 \times 8$ | 5.90 | 3.20 | 2.1 |

Adapters: Bell x NPT Female


| Nominal <br> Pipe Size |  | A | C | E | $\mathrm{X}_{1}$ | $\mathrm{X}_{2}$ | Wgt. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | in | in | in | in | in | lbs. |
| 2 | 50 | 4.75 | $2 \times 11^{1 / 2}$ | 2.00 | 0.70 | 1.85 | 0.4 |
| 3 | 80 | 5.38 | $3 \times 8$ | 3.00 | 1.00 | 2.00 | 0.7 |
| 4 | 100 | 5.38 | $4 \times 8$ | 4.00 | 1.10 | 2.25 | 0.9 |
| 6 | 150 | 6.75 | $6 \times 8$ | 6.00 | 1.20 | 3.20 | 2.1 |

Adapters: Spigot x NPT Male


| Nominal <br> Pipe Size |  | A | C | E | Wgt. |
| :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | in | in | in | lbs. |
| 2 | 50 | 5.65 | $2 \times 11^{1 / 2} 2$ | 2.00 | 0.5 |
| 3 | 80 | 6.90 | $3 \times 8$ | 3.00 | 1.3 |
| 4 | 100 | 7.55 | $4 \times 8$ | 4.00 | 1.7 |
| 6 | 150 | 10.15 | $6 \times 8$ | 6.00 | 4.2 |

Adapters: Spigot x NPT Female


| Nominal <br> Pipe Size |  | A | C | E | X | Wgt. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | in | in | in | in | Ibs. |
| 2 | 50 | 5.65 | $2 \times 11^{1 / 2} 2$ | 2.00 | 0.70 | 0.5 |
| 3 | 80 | 6.90 | $3 \times 8$ | 3.00 | 1.00 | 1.3 |
| 4 | 100 | 7.55 | $4 \times 8$ | 4.00 | 1.20 | 1.7 |
| 6 | 150 | 10.15 | $6 \times 8$ | 6.00 | 1.00 | 4.2 |

Adapters: Bell x Grooved End*


| Nominal <br> Pipe Size |  | A | C | E | X | Wgt. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | in | in | in | in | Ibs. |
| 2 | 50 | 4.16 | 2.38 | 1.90 | 2.00 | 0.5 |
| 3 | 80 | 5.00 | 3.50 | 2.80 | 2.05 | 1.1 |
| 4 | 100 | 5.20 | 4.50 | 3.90 | 2.05 | 1.3 |
| 6 | 150 | 6.00 | 6.63 | 5.90 | 3.20 | 3.2 |
| 8 | 200 | 6.63 | 8.63 | 7.64 | 5.00 | 7.5 |
| 10 | 250 | 8.00 | 10.75 | 10.0 | 5.00 | 9.6 |
| 12 | 300 | 8.75 | 12.75 | 12.0 | 5.50 | 12.5 |

*Compatible with Victaulic coupling style 77 Standard or HP-70ES.

Adapters: Spigot x Grooved End*

*Compatible with Victaulic coupling style 77 Standard or HP-70ES.

## End Caps



| Nominal <br> Pipe Size |  | A | X | Wgt. |
| :---: | :---: | :---: | :---: | :---: |
| in | mm | in | in | Ibs. |
| 2 | 50 | 3.25 | 2.00 | 0.6 |
| 3 | 80 | 3.38 | 2.25 | 1.0 |
| 4 | 100 | 3.38 | 2.25 | 1.4 |
| 6 | 150 | 4.63 | 3.30 | 4.5 |

## Nipples



| Nominal <br> Pipe Size |  | A | B | C | D | Wgt. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | in | in | in | in | lbs/ft |
| 2 | 50 | 6.00 | 8.00 | 10.00 | 12.00 | 0.5 |
| 3 | 80 | -- | 8.00 | 10.00 | 12.00 | 0.7 |
| 4 | 100 | -- | -- | 10.00 | 12.00 | 1.0 |
| 6 | 150 | - | -- | -- | 12.00 | 2.1 |

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## Secondary Containment Pipe and Two-Piece Fittings

(Red Thread ${ }^{\text {TM }}$, Green Thread ${ }^{\text {TM }}$, Z-Core ${ }^{\text {TM }}$, Centricast Plus ${ }^{\text {TM }}$ RB-2530 or CL-2030 and Centricast ${ }^{\text {TM }}$ RB-1520 or CL-1520)

## Product

NOV Fiber Glass Systems offers secondary containment piping systems with two-piece fittings that meet EPA requirements and help protect the environment by containing possible fluid leaks in case of damage to the system. Both vinyl ester and epoxy resin systems are available to match your application.

Secondary containment piping systems are available in 3"-16" sizes. The primary and secondary containment piping is manufactured by either filament winding or the centrifugal casting process. Refer to Brochure Cl1000 for more details.

The secondary containment system is designed for use with Red Thread, Green Thread, Z-CORE ${ }^{\text {TM }}$, Centricast Plus RB-2530 or CL-2030, and Centricast RB-1520 or CL-1520 primary (product) pipe. Primary piping can be centered in the containment piping by using centralizers and anchors as needed.

The secondary containment piping system consists of the next larger pipe size (as a minimum) and special two-piece fittings. The size of the containment pipe may be dictated by the leak detection method used. Standard fittings are manufactured with epoxy vinyl ester resin. Fittings are manufactured by either the compression molding process, or the contact molding process.

The specific primary, or product, piping should be selected to meet your particular temperature, chemical, and pressure requirements. Depending on size and type of product, the pipe can withstand pressures to 450 psig and temperatures to $275^{\circ}$ F. Refer to Brochure CI1000 and associated Product Data bulletins for your primary pipe selection. The containment systems can be pressure tested and continuously monitored.

Refer to Matched Taper Joint, Socket Joint, and Clam Shell Installation Manuals..

Years of experience have proven that fiberglass pipe from NOV Fiber Glass Systems will outlast pipe made of traditional materials. The service life of fiberglass pipe is far greater than that of pipe made from protected steel, copper, black iron, and even stainless steel.
The advantages of lightweight fiberglass piping are even greater when installing secondary containment systems. Very little equipment is required, and the ease of installation results in material handling and installation cost savings.

## Fittings

A complete range of primary fittings is manufactured with the same temperature and pressure capabilities as the pipe. For containment systems, easy to use two-piece fittings constructed of epoxy vinyl ester resin and fiberglass are available.


Standard Secondary Containment Piping Systems

| Primary Pipe Size | Minimum Containment Pipe Size for Red <br> Thread \& Green Thread Primary Pipe | Minimum Containment Pipe Size for <br> Centricast RB \& CL and Z-Core Primary Pipe |
| :--- | :--- | :--- |
| in | $\mathbf{m m}$ | in |
| 1 | -- | 3 |
| $1 / 2$ | -- | 3 |
| 2 | $3^{(1)}$ | $3^{(1)}$ |
| 3 | $4^{(1)}$ | $4^{(1)}$ |
| 4 | $6^{(1)}$ | $6^{(1)}$ |
| 6 | 8 | 8 |
| 8 | 10 | $10^{(2)}$ |
| 10 | 12 | 12 |
| 12 | 14 | 14 |
| 14 | 16 | 16 |

${ }^{(1)}$ When using $2^{\prime \prime}, 3$ ", or 4 " sweep fittings, use containment pipe and fittings that are two diameter sizes larger than the primary. Contact the factory for recommendations.
${ }^{(2)}$ When using $8^{\prime \prime} 90^{\circ}$ elbows, $12^{\prime \prime}$ containment $90^{\circ}$ elbows may be needed. Contact factory for recommendations.
NOTE: When using 3 " $90^{\circ}$ elbows, $6^{\prime \prime}$ containment $90^{\circ}$ elbow may be needed. Contact the factory for recommendations.
NOTE: Primary couplings must be installed inside of secondary containment coupling fittings.

## Installation

Refer to installation manuals for instructions.
NOTE: It is highly recommended that assembly training be conducted by a factory representative prior to installation start up.
When connecting containment pipe and fittings, plain ends of the containment pipe are machined or thoroughly sanded to accept the two-piece containment fitting. Containment pipe must be positioned over the primary piping before assembly and bonding of the primary pipe system. The size of the containment fittings may dictate the minimum center line dimensions for the primary piping.

Upon completion of a successful primary pipe test procedure, the two-piece secondary containment fittings may be installed. They are installed using threaded inserts embedded in the fittings and the hex-head bolts supplied by NOV Fiber Glass Systems. A systemmatching adhesive must be applied to all bonding surfaces just prior to being joined by the bolts. The secondary containment system must be given time for the adhesive to properly cure before testing the annular space.

The testing of secondary containment piping systems is recommended to ensure the integrity of the pipe, fittings and joints of all types. The introduction of the test fluid during testing should be controlled to prevent sudden pressure surges (Water Hammer). Water Hammer can produce pressures that greatly exceed recommended system test pressure.

[^34]
## Air Testing

Hydrostatic test should be used instead of air or compressed gas if possible. When air or compressed gas is used for testing, tremendous amounts of energy can be stored in the system. If a failure occurs, the energy may be released catastrophically, which can result in property damage and personal injury. In cases where system contamination or fluid weight prevents the use of hydrostatic test, air test may be used with extreme caution. To reduce the risk of air testing, use the use the table below to determine maximum pressure. When pressurizing the system with air or compressed gas, the area surrounding the piping must be cleared of personnel to prevent injury. Hold air pressure for one hour, then reduce the pressure to one half the original. Personnel can then enter the area to perform soap test of all joints. Again, extreme caution must be exercised during air testing to prevent property damage or personnel injury. If air or compressed gas testing is used, NOV Fiber Glass Systems will not be responsible for any resulting injury to personnel or damage to property, including the piping system. Air or compressed gas testing is done entirely at the discretion and risk of management at the job site.

## Maximum Allowable Air Test Pressure

| Containment Pipe Size | $3 "-8 "$ | $10 "$ | $12^{\prime \prime}-16^{\prime \prime}$ |
| :--- | :--- | :--- | :--- |
| Pressure, psig | 15 | 10 | 5 |

## Anchors

Anchors are available to control pipe movement due to thermal expansion/contractions or fluid flow transients. Secondary containment anchors bond directly to the primary pipe and to the inside of the secondary containment fittings to eliminate relative movement between the two piping systems. The secondary piping can be anchored externally by the methods in Manual No. ENG1000 as required.

## Custom Design

NOV Fiber Glass Systems can help you in solving secondary containment piping design problems. NOV Fiber Glass Systems also has experience in designing and installing double-wall secondary containment systems $16^{\prime \prime}$ diameter and larger. Contact NOV Fiber Glass Systems for additional information.

## Dimensional Data for Containment Fittings

| Containment ${ }^{(2)}$ Size |  | A |  | B |  | C |  | $\mathrm{D}^{(1)}$ |  | E |  | F |  | H |  | I |  | W |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | in | mm | in | mm | in | mm | in | mm | in | mm | in | mm | in | mm | in | mm | in | mm |
| 3 | 80 | 6 | 152 | 7 | 178 | 14 | 356 | -- | -- | 11 | 298 | 7 | 178 | 2 | 51 | 7 | 178 | $11 / 2$ | 38 |
| 4 | 100 | $71 / 2$ | 191 | 8 | 203 | 14 | 356 | 6 | 152 | 13 | 333 | 7 | 181 | 2 | 51 | 8 | 203 | $11 / 2$ | 38 |
| 6 | 150 | 8 | 203 | 9 | 229 | 16 | 406 | 8 | 279 | 15 | 387 | 8 | 203 | 2 | 51 | 9 | 229 | $11 / 2$ | 38 |
| 8 | 200 | 11 | 279 | 13 | 330 | 20 | 508 | 12 | 305 | $231 / 4$ | 591 | 13 | 330 | 21/2 | 64 | 14 | 356 | $11 / 2$ | 44 |
| 10 | 250 | 18 | 457 | 211/2 | 546 | 24 | 610 | 15 | 381 | $321 / 2$ | 826 | 19 | 483 | 43/16 | 106 | 211/2 | 546 | $13 / 4$ | 44 |
| 12 | 300 | 211/2 | 546 | 26 | 660 | 261/4 | 667 | 17 | 432 | $371 / 2$ | 953 | 221/2 | 572 | 43/16 | 106 | 26 | 660 | 13/4 | 44 |
| 14 | 350 | 221/2 | 572 | 27 | 686 | 28 | 711 | 29 | 737 | $431 / 2$ | 1,105 | $281 / 2$ | 724 | 5 | 127 | 27 | 686 | $13 / 4$ | 44 |
| 16 | 400 | 221/2 | 572 | 29 | 737 | 32 | 813 | $311 / 2$ | 800 | $471 / 2$ | 1,207 | 32 | 813 | 5 | 127 | 29 | 737 | $13 / 4$ | 44 |

${ }^{(1)}$ The overall length is based on the largest size.
${ }^{(2)}$ Sizes 3 " -6 " are compression molded and 8"-16" are contact molded.

View of Fitting Illustrations


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## Engineering \& Piping Design Guide

Fiberglass Reinforced Piping Systems


NOV Fiber Glass Systems' fiberglass reinforced epoxy and vinyl ester resin piping systems possess excellent corrosion resistance and a combination of mechanical and physical properties that offer many advantages over traditional piping systems. We are recognized worldwide as a leading supplier of piping systems for a wide range of chemical and industrial applications.
This manual is provided as a reference resource for some of the specific properties of our piping systems. It is not intended to be a substitute for sound engineering practices as normally employed by professional design engineers.

NOV Fiber Glass Systems has an international network of distributors and trained field personnel to advise on proper installation techniques. It is recommended they be consulted for assistance when installing the piping system. This not only enhances the integrity of the piping system, but also increases the efficiency and economy of the installation.
Additional information regarding installation techniques is provided in the following installation manuals:

| Manual No. F6000 | Pipe Installation Handbook <br> for Tapered Bell \& Spigot Joints |
| :---: | :--- |
| Manual No. F6080 | Pipe Installation Handbook <br> for Straight Socket Joints and <br> Butt \& Wrap Joints |
| Manual No. F6300 | Pipe Installation Handbook <br> for Marine-Offshore Piping |

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## SAFETY

This safety alert symbol indicates an important safety message. When you see this symbol, be alert to the possibility of personal injury.

## PIPING SYSTEMS

Epoxy Resin Systems:

- Z-Core ${ }^{\oplus}$ (High Performance Resin)
- Centricast Plus ${ }^{\circledR}$ RB-2530

Centricast ${ }^{\circledR}$ RB-1520

- Green Thread ${ }^{\circledR}$
- Marine-Offshore
- Green Thread 175
- Green Thread 175 Conductive
- Green Thread 250
- Green Thread 250 Conductive
- Green Thread 250 Fire Resistant
- Red Thread ${ }^{\text {II }}$

Red Thread II JP

- Silver Streak ${ }^{\circledR}$ (FGD Piping)
- Ceram Core ${ }^{\oplus}$ (Ceramic-lined Piping)

F-Chem ${ }^{\circledR}$ (Custom Piping)

- HIGH PRESSURE Line Pipe and Downhole Tubing*


## Vinyl Ester Systems:

Centricast Plus CL-2030

- Centricast CL-1520
- F-Chem (Custom Piping)
* Available from NOV Fiber Glass Systems, San Antonio, Texas Phone: (210) 434-5043 • FAX: (210) 434-7543 Web site: http://www.fgspipe.com

NOV Fiber Glass Systems has developed a computer program specifically for our fiberglass products. This software program called Success By Design is available on our web site at http://www.fgspipe.com.
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## PIPING SYSTEM SELECTION AND APPLICATIONS

## PIPING SYSTEM SELECTION

When selecting a piping system for a particular application, it is important to consider the corrosive characteristics of the media to which the pipe and fittings will be exposed, the normal and potential upset temperatures and pressures of the system, as well as other environmental factors associated with the project. Fiberglass reinforced plastic (FRP) piping systems provide excellent corrosion resistance, combined with high temperature and pressure capabilities, all at a relatively low installed cost. NOV Fiber Glass Systems engineers, using epoxy, vinyl ester, and polyester resins, have developed a comprehensive array of piping systems designed to meet the most demanding application requirements. Piping systems are available with liners of varying type and thickness, with molded, fabricated, or filament wound fittings, ranging in size from 1" to 72"(25 to 1800 mm ) in diameter.

## TYPICAL APPLICATIONS

Fiberglass piping is used in most industries requiring corrosion resistant pipe. FRP piping is used in vent and liquid applications that operate from $-70^{\circ} \mathrm{F}$ to $300^{\circ} \mathrm{F}\left(-57^{\circ} \mathrm{C}\right.$ to $149^{\circ} \mathrm{C}$ ). NOV Fiber Glass Systems piping systems use high grade resins that are resistant to acids, caustics or solvents. Abrasion resistant materials can be used in the piping inner surface liner to enhance wear resistance to slurries. Table 1.0 is a brief list of the many applications and industries where fiberglass piping has been used successfully. See Bulletin No. E5615 for a complete chemical resistance guide.
Our piping systems can be installed in accordance with the ASME B 31.3 piping code. Second party listings from regulatory authorities such as Factory Mutual, NSF, UL/ULC, and marine registrars are in place on several of these piping systems.

## TABLE 1.0 Typical Fiberglass Pipe Applications by Industry

| Applications | INDUSTRY |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Chemical Process | Petro Chemical | Marine Offshore | Pharmaceutical | Food Processing | Power <br> Plants | Pulp and Paper | Waste Water Treatment | Mining and Metal Refining |
| Aeration |  |  |  |  |  |  |  | x |  |
| Brine Slurry | x |  |  |  |  |  |  |  |  |
| Bottom Ash |  |  |  |  |  | x |  |  |  |
| Chemical Feed | x | x |  |  | x | x | x | x | x |
| Column Piping |  |  | X |  |  |  |  |  |  |
| Condensate Return | x | X | X | x | X | x | x |  |  |
| Conduit |  | x |  |  | x | x | x |  |  |
| Cooling Water | X | X |  | X | X | X |  |  |  |
| Disposal Wells | X | X | X |  |  |  |  | X | X |
| DownholeTubing \& Casing |  | X | X |  |  |  |  | X |  |
| Effluent Drains | x | x | x | x | x | x | x | X | x |
| Fire Mains |  | X | X |  |  | X | X |  | X |
| Flue Gas Desulfurization |  |  |  |  |  | X |  |  |  |
| Guttering \& Downspouts | X |  |  |  | X | X | X |  |  |
| Oily Water |  | X | X |  |  |  |  |  | X |
| Scrubber Headers | X | X |  |  |  | x |  |  |  |
| Seawater |  | X | X |  |  | x |  |  |  |
| Slurry | x |  |  |  |  | x |  |  |  |
| Vents | x | x | x | x | x |  | x | x | x |
| Water | X | X | X | X | X | X | X |  | X |
| Waste Treatment | X |  | X | X | X | X | X | X | X |
| Buried Gasoline |  | x |  |  |  |  |  |  |  |

## SECTION 1. Flow Properties

The smooth interior surface of fiberglass pipe, combined with inside diameters larger than steel or thermoplastic pipe of the same nominal diameter, yield significant flow advantages. This section provides design techniques for exploiting the flow capacity of fiberglass pipe.

## PRELIMINARY PIPE SIZING

The determination of the pipe size required to transport a given amount of fluid is the first step in designing a piping system.

## Minimum recommended pipe diameters.

## Clear fluids

Eq. 1 $d:=\frac{0.73 \cdot \sqrt{\frac{Q}{S g}}}{\rho^{0.33}}$
Corrosive or erosive fluids
Eq. $2 \mathrm{~d}:=\frac{1.03 \cdot \sqrt{\frac{\mathrm{Q}}{\mathrm{Sg}}}}{\rho^{0.33}}$

Where:
$d=$ Pipe inner diameter, inch
$\mathrm{Q}=$ Flow rate, gal/min (gpm)
$\mathrm{Sg}=$ Fluid specific gravity, dimensionless
$p=$ Fluid density, $\mathrm{Ib} / \mathrm{ft}^{3}$

## Recommended maximum fluid velocities

Clear fluids

$$
\text { Eq. } 3 \mathrm{~V}:=\frac{48}{\rho^{0.33}}
$$

## Corrosive or erosive fluids

Eq. $4 \quad \mathrm{~V}:=\frac{24}{\rho^{0.33}}$

Where:
$\mathrm{V}=$ velocity, ft/sec
$p=$ fluid density, $\mathrm{lb} / \mathrm{ft}^{3}$

Typical fiberglass piping systems are operated at flow velocities between 3 \& $12 \mathrm{ft} / \mathrm{sec}$.

DETAILED PIPE SIZING

## A. Liquid Flow

Fluid flow characteristics are very sensitive to the absolute roughness of the pipe inner surface. The absolute roughness of NOV Fiber Glass Systems piping is ( 0.00021 inches) 1.7 x $10^{-5}$ feet ${ }^{(1)}$. This is less than $1 / 8$ the average value for (non-corroded) new steel of ( 0.0018 inch) $15 \times 10^{-5}$ feet ${ }^{(2)}$. For ambient temperature water, the equivalent Manning value $(\mathrm{n})$ is 0.009 and the Hazen-Williams coefficient is 150.

The most commonly used pipe head loss formula is the Darcy-Weisbach equation.
Eq. $5 \quad \mathrm{Hf}:=\mathrm{f} \cdot \frac{\mathrm{L}}{\mathrm{D}} \cdot \frac{\mathrm{V}^{2}}{2 \mathrm{~g}}$
Where:
$\mathrm{Hf}=$ Pipe friction loss, $\mathrm{ft}(\mathrm{m})$
$\mathrm{f}=$ Friction factor
$\mathrm{L}=$ Length of pipe run, $\mathrm{ft}(\mathrm{m})$
$\mathrm{D}=$ Inner diameter, $\mathrm{ft}(\mathrm{m})$
$\mathrm{V}=$ Fluid velocity, ft/sec ( $\mathrm{m} / \mathrm{sec}$ )
$\mathrm{g}=$ Acceleration of gravity, $32.2 \mathrm{ft} / \mathrm{s}^{2}\left(9.81 \mathrm{~m} / \mathrm{s}^{2}\right)$

The friction factor is dependent on the flow conditions, pipe diameter and pipe smoothness. The flow conditions are determined by the value of the Reynolds Number. There are four flow zones defined by the Reynolds Number; they are laminar, critical, transitional and turbulent.
For laminar flow (Reynolds Number below 2,000), the friction factor is calculated by Eq. 6

Eq. $6 \quad \mathrm{f}:=\frac{64}{\mathrm{Nr}}$
Where Nr is the dimensionless Reynolds Number
Eq. $7 \quad \mathrm{Nr}:=\frac{\mathrm{D} \cdot \mathrm{V}}{v}$
Where:
$\mathrm{D}=$ Pipe inner diameter, $\mathrm{ft}(\mathrm{m})$
$\mathrm{V}=$ Fluid velocity, ft/sec ( $\mathrm{m} / \mathrm{sec}$ )
$v=$ Fluid kinematic viscosity, $\mathrm{ft}^{2} / \mathrm{sec}\left(\mathrm{m}^{2} / \mathrm{sec}\right)$
$\mathrm{Nr}=$ Reynolds Number
$f=$ Friction Factor

[^35]For turbulent flow (Reynolds Number greater than 4,000), the friction factor is calculated by the Colebrook Equation.

Eq. $8 \quad \frac{1}{\sqrt{\mathrm{f}}}=-2 \cdot \log \left(\frac{\mathrm{e}}{3.7 \cdot \mathrm{D}}+\frac{2.51}{\mathrm{Nr} \cdot \sqrt{\mathrm{f}}}\right)$

## Where:

$D=$ Pipe inner diameter, inch (mm)
$\mathrm{e}=$ Absolute roughness, inch (mm)
$\mathrm{Nr}=$ Reynolds Number, unit less
$f=$ Friction Factor, unit less
The flow with Reynolds numbers between 2,000 and

4,000 is considered the critical zone. Flow is neither fully laminar or turbulent, although it is often assumed to be laminar for calculation purposes. Flow with Reynolds numbers between 4,000 and 10,000 is called the transitional zone where use of the Colebrook equation is considered more appropriate.

These equations are quickly solved using a computer program, Success By Design, developed by NOV Fiber Glass Systems specifically for our fiberglass products.

A demonstration of the Darcy-Weisbach and Colebrook equations for fiberglass pipe is shown in Figure 1.0.

Figure 1.0
Fiberglass Pipe Pressure Loss Curves for Water
Basis: Specific Gravity of 1.0 and Viscosity of 1.0 cps


## B. Loss in Pipe Fittings

The head loss through a fitting is proportional to the fluid velocity squared $\left(\mathrm{V}^{2}\right)$. Equation 9 relates the head loss in fittings to the fluid velocity by incorporating a fitting loss factor obtained from experimental test data.

Eq. $9 \quad \mathrm{hf}:=\frac{\mathrm{k} \cdot \mathrm{V}^{2}}{2 \cdot \mathrm{~g}}$
Where:
$\mathrm{hf}=$ Fitting head loss, $\mathrm{ft}(\mathrm{m})$
$\mathrm{k}=$ Flow resistance coefficient
$\mathrm{V}=$ fluid velocity, ft/sec
$\mathrm{g}=$ acceleration of gravity, $32.2 \mathrm{ft} / \mathrm{s}^{2}$

Typical values of $k$ are given in Table 1.1.
The most common method for determining the contribution to the overall piping system of the fittings head loss is to convert the fitting head loss into an equivalent pipe length. As an example, use $60^{\circ} \mathrm{F}$ water as the working fluid in a 3 -inch diameter piping system with an internal flow of $10 \mathrm{ft} / \mathrm{sec}$. The equivalent pipe length for a short radius $90^{\circ}$ elbow would be 6.9 feet for Red Thread II and 5.9 feet for Centricast Plus CL-2030 . The two piping systems have different inner diameters that contribute to the differences in equivalent footage. Therefore, for best accuracy it is recommended that our computer software Success By Design be used to determine fittings equivalent piping footage.
Typical liquid properties are presented in Table 1.2.

TABLE 1.1 Flow Resistance coefficients for Fittings

| Fitting/Size (In.) | 1 | $11 / 2$ | 2 | 3 | 4 | 6 | $8-10$ | $12-16$ |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Short Radius $90^{\circ}$ Elbow | 0.75 | 0.66 | 0.57 | 0.54 | 0.51 | 0.45 | 0.42 | 0.39 |
| Sweep Radius $90^{\circ}$ Elbow | 0.37 | 0.34 | 0.30 | 0.29 | 0.27 | 0.24 | 0.22 | 0.21 |
| Short Radius $45^{\circ}$ Elbow | 0.37 | 0.34 | 0.30 | 0.29 | 0.27 | 0.24 | 0.22 | 0.19 |
| Sweep Radius $45^{\circ}$ Elbow | 0.20 | 0.18 | 0.16 | 0.15 | 0.14 | 0.13 | 0.12 | 0.11 |
| Tee Side Run | 1.38 | 1.26 | 1.14 | 1.08 | 1.02 | 0.90 | 0.84 | 0.78 |
| Tee Thru Branch | 0.46 | 0.42 | 0.38 | 0.36 | 0.34 | 0.30 | 0.28 | 0.19 |

## TABLE 1.2 Typical Liquid Properties

| Type of Liquid | Specific Gravity at $60^{\circ} \mathrm{F}$ | Viscosity at $60^{\circ} \mathrm{F}$ Centipoise |
| :--- | :---: | :---: |
| $10 \%$ Salt Water | 1.07 | 1.40 |
| Brine, 25\% NaCl | 1.19 | 2.20 |
| Brine, 25\% CaCl | 2.45 |  |
| $30^{\circ}$ API Crude Oil | 1.23 | 13.00 |
| Average Fuel Oils | 0.87 | 8.90 |
| Kerosene | 0.93 | 1.82 |
| Auto Gasoline | 0.83 | 1.20 |
| Aviation Gasoline | 0.72 | 0.46 |
| 50\% Sodium Hydroxide (NaOH) | 0.70 | 95.00 |
| Mil 5624 Jet Fuels: | 1.53 |  |
| JP3 |  | 0.79 |
| JP5 | 0.75 | 2.14 |
| JP8 | 0.84 | 1.40 |
| Acids: | 0.80 | $A t 68^{\circ} \mathrm{F}$ |
| 60\% Sulfuric $\left(\mathrm{H}_{2} \mathrm{SO}_{4}\right)$ | At $68^{\circ} \mathrm{F}$ | 6.40 |
| 98\% Sulfuric $\left(\mathrm{H}_{2} \mathrm{SO}_{4}\right)$ | 1.50 | 24.50 |
| 85\% Phosphoric $\left(\mathrm{H}_{2} \mathrm{PO}_{4}\right)$ | 1.83 | 12.00 |
| 37.5\% Hydrochloric (HCl) | 1.69 | 1.94 |

## C. Open Channel Flow

One of the most widely used, formulas for open-channel flow is that of Robert Manning. This formula in Equation 10 is useful in predicting the flow in open "gravity feed" fiberglass sewer lines. Our Success By Design software is recommended to perform these calculations.

Eq. 10

$$
\mathrm{Q}:=\frac{\mathrm{k}}{\mathrm{n}} \cdot \mathrm{~A} \cdot \mathrm{Rh}^{0.666} \cdot \mathrm{~S}^{0.5}
$$

Where:
$\mathrm{Q}=$ Flow rate in $\mathrm{ft}^{3} / \mathrm{sec}\left(\mathrm{m}^{3} / \mathrm{sec}\right)$
$A=$ Flow cross sectional area, $\mathrm{ft}^{2}\left(\mathrm{~m}^{2}\right)$
Rh = Hydraulic radius, ft (m)
S = Hydraulic slope, dimensionless
S = H/L
$\mathrm{H}=$ elevation change over the pipe length
"L", ft (m)
$\mathrm{L}=$ Length measured along the pipe, $\mathrm{ft}(\mathrm{m})$
$\mathrm{k}=1.49$ (US Customary units, ft. \& sec.)
$k=1.0$ for flow in $\mathrm{m}^{3} / \mathrm{sec}$. Use meter for A , Rh, \& D.
$\mathrm{n}=0.009$ Manning's constant for fiberglass
Eq. $11 \quad \mathrm{Rh}_{\mathrm{h}}:=\frac{\mathrm{D}}{4} \cdot\left(1-\frac{\sin (2 \cdot \theta)}{2 \cdot \theta}\right)$
Where:
$D=$ Pipe inner diameter, $\mathrm{ft}(\mathrm{m})$
$\Theta=$ Wet contact angle, radians


## D. Gas Flow

NOV Fiber Glass Systems piping systems can be used in pressurized gas service when the pipe is buried at least three feet deep.


In above ground applications, they can be used provided the pressure does not exceed the values shown below and further that the pipe is properly safeguarded when conveying a hazardous gas.

| Pipe Diameter | 1" | $1^{1} / 2{ }^{\prime \prime}$ | 2" | 3" | 4" | 6" | 8" | 10" | 12" | 14" | 16" |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| psig | 25 | 25 | 25 | 25 | 25 | 25 | 14 | 9 | 6 | 5 | 4 |

Consult your local representative for safeguard procedures.
Since the inside diameter of the pipe is smoother and larger than steel pipe of corresponding nominal diameters, less frictional resistance is developed under turbulent flow conditions, resulting in greater flow capacities. There are two basic equations used to calculate pressure loss for flow of gases. To determine which equation is required, the transition flow rate must be determined from Equations 12, 13 and 14. If the desired flow rate is greater than the value calculated from equation 14, then the equations for fully turbulent or rough pipe flow must be used. If the desired flow rate is less than the value calculated from equation 14, then the equation for partially turbulent or smooth pipe flow must be used.

Equations for transition flow rate:

Eq. $12 \quad \mathrm{KT}:=\left(\frac{0.4692 \cdot \mathrm{~T}}{\mathrm{P}_{\mathrm{b}} \cdot \sqrt{\mathrm{G} \cdot \mathrm{T} \cdot Z}}\right)^{2}$

Eq. $13 \quad \mathrm{KS}:=\left(\frac{0.6643 \cdot \mathrm{~T}_{\mathrm{b}}}{\mathrm{P}_{\mathrm{b}} \cdot \mathrm{T}^{0.5556} \cdot \mathrm{Z}^{0.5556} \cdot \mathrm{G}^{0.4444} \cdot \mu^{0.1111}}\right)^{1.8}$

Eq. 14

$$
\mathrm{QT}:=\left(\frac{\mathrm{KT}}{\mathrm{KS}}\right)^{5} \cdot \mathrm{D} \cdot\left(\log \left(\frac{3.7 \cdot \mathrm{D}}{\mathrm{~K}}\right)\right)^{10}
$$

Where $Q T=$ Transition Flow Rate

For fully turbulent or rough pipe flow:(1)
Eq. $15 \quad \mathrm{Q}:=\frac{0.4692 \cdot \mathrm{~T}_{\mathrm{b}}}{\mathrm{P}_{\mathrm{b}}} \cdot\left[\frac{\left(\mathrm{P}_{\mathrm{i}}^{2}-\mathrm{P}_{\mathrm{o}}^{2}\right) \cdot \mathrm{D}^{5}}{\mathrm{G} \cdot \mathrm{T} \cdot \mathrm{Z} \cdot \mathrm{L}}\right]^{0.5} \cdot \log \left(\frac{3.7 \cdot \mathrm{D}}{\mathrm{K}}\right)$
(1) IGT Distribution Equations from American Gas Association Plastic Pipe Handbook for Gas Service.
or

Eq. $16 \quad \mathrm{P}_{\mathrm{o}}:=\left[\mathrm{P}_{\mathrm{i}}^{2}-\left[\frac{\mathrm{G} \cdot \mathrm{T} \cdot \mathrm{Z} \cdot \mathrm{L}}{\mathrm{D}^{5}} \cdot\left(\frac{\mathrm{Q} \cdot \mathrm{P}_{\mathrm{b}}}{0.4692 \cdot \mathrm{~T}_{\mathrm{b}} \cdot \log \left(\frac{3.7 \cdot \mathrm{D}}{\mathrm{K}}\right)}\right)^{2}\right]^{0.5}\right.$
For partially turbulent or smooth pipe flow ${ }^{(1)}$
Eq. $17 \quad \mathrm{Q}:=\frac{0.6643 \cdot T_{b}}{P_{b}} \cdot\left(\frac{P_{i}{ }^{2}-P_{o}{ }^{2}}{T \cdot Z \cdot L}\right)^{0.5556} \cdot \frac{D^{2.6667}}{G^{0.4444} \cdot \mu^{0.1111}}$

Where:
Eq. $18 \quad \mathrm{P}_{\mathrm{o}}:=\left[\mathrm{P}_{\mathrm{i}}{ }^{2}-\mathrm{L} \cdot \mathrm{T} \cdot \mathrm{Z} \cdot\left(\frac{\mathrm{Q} \cdot \mathrm{P}_{\mathrm{b}} \cdot \mathrm{G}^{0.4444} \cdot \mu^{0.1111}}{0.6643 \cdot \mathrm{~T}_{\mathrm{b}} \cdot \mathrm{D}^{2.6667}}\right)^{1.8}\right]^{0.5}$

D = Inside Diameter (in.)
$\mathrm{G}=$ Specific Gravity (S.G. of air $=1.0$ )
L = Length of Pipe Section (ft.)
$\mathrm{P}_{\mathrm{b}}=$ Base Pressure (psia)
$P_{i}=$ Inlet Pressure (psia)
$\mathrm{P}_{\mathrm{o}}=$ Outlet Pressure (psia)
$\mathrm{Q}=$ Flow Rate (MSCFH - thousand standard cubic ft. per hr.)
$\mathrm{T}_{\mathrm{b}}=$ Base Temperature ( ${ }^{\circ} \mathrm{R}$ )
$\mathrm{T}=$ Temperature of Gas ( ${ }^{\circ} \mathrm{R}$ )
Z = Compressibility Factor
m = Viscosity (lb./ft. sec.)
$\mathrm{K}=$ Absolute Roughness of Pipe $=$ 0.00021 (in.) for Fiber Glass Systems pipe
$\mathrm{R}=$ Rankine ( ${ }^{\circ} \mathrm{F}+460^{\circ}$ )
$\mathrm{m}=$ ( $\mathrm{lb} . / \mathrm{ft} . \mathrm{sec}.)=m$ (centipoise) $\div 1488$
psia $($ Absolute $)=$ psig $($ Gauge $)+14.7$
You can perform computer calculations using the Success By Design program to solve gas flow problems for: pipe size, Q , $P_{i}$, or $P_{0}$ if the other variables are known.
TABLE 1.3 Typical Gas Properties

| Type of Gas | Specific Gravity <br> at $\mathbf{6 0}^{\circ} \mathbf{F}^{(\mathbf{1 )}}$ | Viscosity at $60^{\circ} \mathrm{F}$ <br> Ib./ft. sec. |
| :--- | :---: | :---: |
| Air | 1.02 | 0.0000120 |
| Carbon Dioxide | 1.56 | 0.0000098 |
| Carbon Monoxide | 0.99 | 0.0000116 |
| Chlorine | 2.51 | 0.0000087 |
| Ethane | 1.06 | 0.0000060 |
| Methane | 0.57 | 0.0000071 |
| Natural Gas | 0.64 | 0.0000071 |
| Nitrogen | 0.99 | 0.0000116 |
| Nitrous Oxide | 1.56 | 0.0000096 |
| Oxygen | 1.13 | 0.0000132 |
| Sulfur Dioxide | 2.27 | 0.0000083 |

(1) All Specific Gravity based on air $=1.0$ at $70^{\circ} \mathrm{F}$.

## SECTION 2. Above Ground System Design - Supports, Anchors and Guides

## PIPING SUPPORT DESIGN

Above ground piping systems may be designed as restrained or unrestrained. Selection of the design method is dependent on variables such as operating temperature, flow rates, pressures and piping layout. System designs combining the two methods often lead to the most structurally efficient and economical piping layout.

## Unrestrained System Design

The unrestrained system is often referred to as a "simple supported" design. It makes use of the inherent flexibility of fiberglass pipe to safely absorb deflections and bending stresses. Simple pipe hangers or steel beams are used to provide vertical support to the pipe. These simple supports allow the piping system to expand and contract freely resulting in small axial stresses in the piping system. Long straight runs often employ changes-in-direction to safely absorb movement due to thermal expansion and contractions, flow rate changes, and internal pressure.

Experience has shown the use of too many simple pipe hangers in succession can result in an unstable line when control valves operate and during pump start-up and shutdown. To avoid this condition the designer should incorporate guides periodically in the line to add lateral stability. In most cases, the placement of lateral guides at intervals of every second or third support location will provide adequate stability. Axial stability in long pipe runs may be improved by the proper placement of a "Pipe Hanger with Axial Guide" as shown in Figure 2.6. The project piping engineer must determine the guide requirements for system stability.

## Restrained System Design

The restrained system is often referred to as an "anchored and guided design". The low modulus of elasticity for fiberglass piping translates to significantly smaller thermal forces when compared to steel. Anchors are employed to restrain axial movement and provide vertical support in horizontal pipelines. Anchors used to restrain thermal expansion create compressive forces in the pipeline. These forces must be controlled by the use of pipe guides to prevent the pipe from buckling. In cases where axial loads created by anchoring a pipe run are excessively high, the use of expansion loops or expansion joints must be employed. When using anchors, the effect of system contraction should be considered. See the thermal analysis section for more thorough information on handling thermal loads.

## FIBERGLASS PIPING SYSTEM "SUPPORT" TERMINOLOGY

Fiberglass piping engineers use three basic structural components to design a piping system. They are the support, anchor and guide.

## Support

Pipe supports hold the pipe in position and when properly spaced prevent excessive deflections due to the weight of the pipe, fluid, external insulation and other loads.

## Anchor

Pipe anchors restrain axial movement and applied forces. These forces may result from thermal loads, water hammer, vibrating equipment, or externally applied mechanical loads.

## Guide

Pipe guides prevent lateral (side-to-side) movement of the pipe. Guides are required to prevent the pipe from buckling under compressive loading. For example: When anchors are used to control thermal expansion, guides are always required.

## A. Support Design

The hanger support in Figure 2.0 must have sufficient contact areas to distribute the load. The preferred circumferential load bearing contact is $180^{\circ}$. Refer to Table 2.0 for minimum width requirements. When less than $180^{\circ}$ of circumference contact and/or larger diameters are encountered, support saddles as shown in Figure 2.1 are recommended.


TABLE 2.0 Minimum Support Width*

| Pipe Size <br> (In.) | Class I <br> (In.) | Class II <br> (In.) |
| :---: | :---: | :---: |
| 1 | $7 / 8$ | $7 / 8$ |
| $1^{1 / 2}$ | $7^{7 / 8}$ | $7 / 8$ |
| 2 | $7 / 8$ | 1 |
| 3 | $1^{1 / 4}$ | $1^{1 / 2}$ |
| 4 | $1^{1 / 1}$ | $1^{1 / 2}$ |
| 6 | $1^{1 / 2}$ | 2 |
| 8 | $1^{3 / 4}$ | 3 |
| 10 | $1^{3 / 4}$ | 4 |
| 12 | 2 | 4 |
| 14 | 2 | 6 |

*Note: Valid for $\mathrm{Sg}<1.25$

Class I Products: Centricast Plus CL-2030, Centricast Plus RB-2530, Z-Core. Minimum recommended support saddle contact angle is $110^{\circ}$

Class II Products: Red Thread II, Green Thread, Silver Streak, F-Chem, Centricast CL-1520, Centricast RB-1520. Recommended support saddle contact angle is $180^{\circ}$

Support saddles are recommended for 16-24 inch diameter pipe. The pipe surface bearing stress should not exceed $50 \mathrm{lb} / \mathrm{in}^{2}$ for support designs.

Figure 2.1


Support Saddle

TABLE 2.1 Saddle Length

| Pipe Size <br> (In.) | Class I <br> (In.) | Class II <br> (In.) |
| :---: | :---: | :---: |
| 1 | 3 | 2 |
| $1^{1 / 2}$ | 3 | 2 |
| 2 | 4 | 4 |
| 3 | 4 | 4 |
| 4 | 4 | 4 |
| 6 | 4 | 6 |
| 8 | 6 | 8 |
| 10 | 9 | 10 |
| 12 | 9 | 12 |
| 14 | 9 | 14 |
| $16-24$ | - | $(1)(2)$ |

(1) Use the pipe diameter as minimum saddle length.
(2) Refer to F-Chem product bulletin for sizes greater than 24-inch diameter.

Typical supports requiring support saddles are shown in Figures 2.2 \& 2.3. The support saddles should be bonded to the pipe or held in place by flexible clamps. If clamped to filament wound pipe a $1 / 16^{\prime \prime}$ rubber pad should be placed between the pipe and the saddle. Saddle lengths should ac-

commodate pipe movements to prevent them from sliding off the supports.

## B. Guide Design

## Typical Guide Usage

1. Between anchors to prevent buckling of pipeline at elevated temperatures.
2. Near entry points of expansion joints and loops to ensure proper functionality.
3. To provide system stability.

Properly designed and installed guides prevent the pipe from sliding off support beams and allow the pipe to freely move in the axial direction. Guides should be used with $180^{\circ}$ support saddles to reduce wear and abrasion of the pipe walls.

${ }^{(1)}$ Not required if support saddle is bonded to pipe.
Figure 2.4 shows a common method of guiding fiberglass pipe. A clearance of $1 / 16$ to $1 / 8$-inch is recommended between the guide and the support saddle. A $180^{\circ}$ support "wear" saddle is recommended to prevent point contact between the U-bolt and pipe. The U-bolt should not be tightened down onto the pipe. It should be tightened to the structural support member using two nuts and appropriate washers. A $1 / 8$-inch clearance is recommended between the U-bolt and the top of the pipe.

Eight-inch diameter and larger pipe are generally allowed more clearance than smaller sizes. The determination of acceptable clearance for these sizes is dependent on the piping system and should be determined by the project piping engineer.

Another design practice is to use U-straps made from flat rolled steel instead of U-bolts. Flat U-straps are less apt than U-bolts to "point" load the pipe wall. U-strap use is most common when guiding pipe sizes greater than 6 -inches diameter.

Pipe Hanger with Lateral Guide

Figure 2.5


When U-bolts are used in vertical piping, then two $180^{\circ}$ wear saddles should be used to protect the pipe around its entire circumference. It is appropriate to gently snug the U-bolt if a $1 / 8$-inch thick rubber pad is positioned between the U-bolt and the saddle. If significant thermal cycles are expected, then the U-bolts should be installed with sufficient clearance to allow the pipe to expand and contract freely. See the "Vertical Riser Clamps" section for additional options in supporting vertical piping.

Figure 2.5 shows a more sophisticated pipe hanger and guide arrangement. It may be used without wear saddles as long as the tie rod allows free axial movement. The hanger must meet the width requirements in Table 2.0. If a clamp width does not meet the requirements in Table 2.0 or the pipe sizes are greater than 14 -inch diameter, then support saddles should be used. See Table 2.1 for support saddle sizing recommendations.

Lateral loading on guides is generally negligible under normal operating conditions in unrestrained piping systems. In restrained piping systems, guides provide the stability required to prevent buckling of pipelines under compressive loads. If the guides are located properly in the pipeline, the loads required to prevent straight pipe runs from buckling will be very small.


Upset conditions can result in significant lateral loads on the guides and should be considered during the design phase by a qualified piping engineer. Water hammer and thermal expansion or contraction may cause lateral loading on guides near changes in direction. Therefore, it is always prudent to protect the pipe from point contact with guides near changes in directions and side runs.

Figure 2.6 shows a pipe hanger with an axial guide using a double bolt pipe clamp arrangement. This support provides limited axial stability to unrestrained piping systems.

Pipe lines supported by long swinging hangers may experience instability during rapid changes in fluid flow.
Stability of such lines benefit from the use of pipe guides as shown in Figures 2.5 and 2.6.
The support widths for guided pipe hangers should meet the recommendations in Tables 2.0 \& 2.1.

## Vertical Riser Clamps

Riser clamps as shown in Figure 2.7 may act as simple supports, as well as guides, depending upon how they are attached to the substructure. The clamp should be snug but not so tight as to damage the pipe wall. The use of an anchor sleeve


Figure 2.7 bonded onto the pipe is required to transfer the load from the pipe to the riser clamp. See the "Anchor Designs" section for detailed information concerning the anchor sleeve or FRP buildup.

It is important to note that this type of clamp only provides upward vertical support. Certain design layouts and operating conditions could lift the pipe off the riser clamp. This would result in a completely different load distribution on the piping system. A pipe designer needs to consider whether the column will be under tension, or in a state of compression. Additional guides may be required to prevent unwanted movement or deflection.

A qualified piping engineer should be consulted to ensure an adequate design.

Riser clamps designed to provide lateral support should incorporate support saddles to distribute the lateral loads.

## C. Anchor Design

## Anchor Usage

1. To protect piping at "changes-in-directions" from excessive bending stresses.
2. To protect major branch connections from primary pipeline induced shears and bending moments. Particular consideration should be given to saddle and lateral fitting side runs.
3. Installed where fiberglass piping is connected to steel piping and interface conditions are unavailable.
4. To protect a piping system from undesirable movement caused by water hammer or seismic events.
5. To protect sensitive in-line equipment.
6. To absorb axial thrust at in-line reducer fittings when fluid velocities exceed $7.5 \mathrm{ft} / \mathrm{sec}$.
7. To provide stability in long straight runs of piping.


To be effective, an anchor must be attached to a substructure capable of supporting the applied forces. In practice, pumps, tanks, and other rigidly fixed equipment function as anchors for fiberglass piping systems.

Anchors as previously described are used to provide axial restraint to piping systems. In most cases an anchor provides bidirectional lateral support to the pipe thus acting like both a support and guide. Furthermore, anchors can be designed to provide partial or complete rotational re-

## Restrains pipe movement in all directions



Restrains pipe movement in all directions


Restrains pipe movement in all directions and directly supports heavy fittings

straint. But, this is not normally the case in practice. Figures 2.8 through 2.11 show typical methods of anchoring fiberglass piping systems.

The anchor in Figure 2.9 will provide considerably less lateral stiffness than the anchor in Figure 2.8. The effect of lateral stiffness on the overall system stability should always be considered when selecting an anchor design.

The anchor widths should meet the recommendations for support designs in Table 2.0.

The reactions generated at anchors when restraining large thermal loads can be significant and should be calculated by a qualified piping engineer. The anchor brackets and substructure design should be designed with sufficient stiffness and strength to withstand these loads combined with any other system loads. Other system loads may include water hammer,seismic, static weight of pipe, fluid and any external loads such as insulation, wind, ice, and snow.

## Anchor Sleeves

An anchor sleeve as shown in Figure 2.12 is necessary to transfer axial load from a pipe body to an anchor bracket.
Pairs of anchor sleeves are bonded to the outer surface of a pipe to provide a shear load path around the complete circumference of the pipe body. To restrain pipe motion


Figure 2.12 in two directions, two pairs of anchor sleeves are required. They must be bonded on both sides of an anchor bracket to completely restrain a pipe axially. There are design conditions where only one set of anchor sleeves is required. The piping engineer should make this determination and size the sleeves appropriately for the design loads. Lengths equal to the pipe diameter are generally satisfactory for most load conditions

During installation the anchor sleeve end faces must be aligned to mate precisely against the anchor brackets when engaged. If only one of the two halves of an anchor sleeve contacts the anchor bracket, the loading will be off center or eccentric. Eccentric loading will increase the shear stress on the contacted anchor sleeve. It may also cause the pipe to rotate at the anchor resulting in unwanted deflections in the pipe. Refer to Figures 2.8 \& 2.9 for typical configurations.

It is important to understand how the load is transferred from the pipe to the anchor brackets. First the axial load is sheared from the pipe wall into the anchor sleeves through the adhesive bond. The load is then transferred from the anchor sleeve by direct contact bearing stress
between the end of the anchor sleeve and the anchor bracket which ultimately transfers it to the substructure.

Under no circumstances is the anchor to be tightened down on the pipe surface and used as a friction clamp to transfer load. The pipe should be free to slide until the anchor sleeves contact the anchor bracket to transfer the load. Piping engineers often take advantage of this anchoring procedure by allowing the pipe to slide a small amount before contacting the anchor. This effectively reduces restrained thermal loads.

Split repair couplings, split fiberglass pipe sections or hand lay ups of fiberglass and resin are commonly used as anchor sleeves. Contact your fiberglass distributor to determine the most appropriate choice for Fiber Glass Systems' wide variety of piping products.

## D. Piping Support Span Design

A support span is the distance between two pipe supports. Proper support span lengths ensure the pipe deflections and bending stresses are within safe working limits. For static weight loads, it is standard practice to limit the maximum span deflection in horizontal pipe lines to $1 / 2^{\prime \prime}$ and the bending stresses to $1 / 8^{\prime \prime}$ of the ultimate allowable bending stress. NOV Fiber Glass Systems applies these design limits to the engineering analysis used to determine the allowable support spans.

## Span Analysis Methodology

The maximum allowable piping support spans are determined using the "Three Moment Equations" for uniformly loaded continuous beams. The equations may be modified to represent various end conditions, load types and even support settlements. Refer to Appendix A for the fundamental equations. NOV Fiber Glass Systems uses these equations to calculate the bending moments in piping spans. The pipe bending stresses and deflections are then evaluated for compliance with the aforementioned design criteria.

To avoid lengthy engineering calculations, our individual product bulletins contain recommended piping support span lengths. These span lengths are easily modified to match fluid specific gravity, operating temperatures and end conditions. Figures 2.13 and 2.14 provide span adjustment factors for various end conditions found in most horizontal piping system layouts. Tables for fluid specific gravity and temperature adjustment factors are product unique. Please refer to the product data bulletins for detailed design information.

Success By Design software quickly calculates support spans for uniformly loaded piping systems and takes into consideration product type, temperature, specific gravity, uniform external loads, and end conditions as shown in Figures 2.13 and 2.14.

Complex piping system designs and load conditions may require detailed flexibility and stress analysis using finite element modeling. The project design engineer must determine the degree of engineering analysis required for the system at hand.

Figure 2.13 Piping Span Adjustment Factors With Unsupported Fitting at Change in Direction

*For example: If continuous support span is 10 ft ., $\mathrm{c}+\mathrm{d}$ must not exceed 7.5 ft . ( $\mathrm{c}=3 \mathrm{ft}$. and $\mathrm{d}=4.5 \mathrm{ft}$. would satisfy this condition).

Figure 2.14 Piping Span Adjustment Factors With Supported Fitting at Change in Direction


## Support Design Summary

1. Do not exceed the recommended support span.
2. Support valves and heavy in-line equipment independently. This applies to both vertical and horizontal piping.
3. Protect pipe from external abrasion at supports.
4. Avoid point contact loads.
5. Avoid excessive bending. This applies to handling, transporting, initial layout, and final installed position.
6. Avoid excessive vertical loading to minimize bending stresses on pipe and fittings.
7. Provide adequate axial and lateral restraint to ensure line stability during rapid changes in flow.

## SECTION 3. Temperature Effects on Fiberglass Pipe

## SYSTEM DESIGN

The properly designed piping system provides safe and efficient long-term performance under varying thermal environments. The system design dictates how a piping system will react to changes in operating temperatures.

The unrestrained piping system undergoes expansion and contraction in proportion to changes in the pipe wall mean temperature. Fiberglass piping systems that operate at or near the installation temperature are normally unrestrained designs, where the most important design consideration is the basic support span spacing. Since few piping systems operate under these conditions, some provisions must be made for thermal expansion and contraction.

The simplest unrestrained piping systems use directional changes to provide flexibility to compensate for thermal movements. When directional changes are unavailable or provide insufficient flexibility, the use of expansion loops or expansion joints should be designed into the system to prevent overstressing the piping system. These systems are considered unrestrained even though partial anchoring and guiding of the pipe is required for proper expansion joint, expansion loop performance and system stability.

The fully restrained "anchored" piping system eliminates axial thermal movement. Pipe and fittings generally benefit from reduced bending stresses at directional changes. Restrained systems develop internal loads required to maintain equilibrium at the anchors due to temperature changes. When the pipe is in compression, these internal loads require guided supports to keep the pipe straight preventing Euler buckling. Thus, the commonly referred to name of restrained systems is "anchored and guided". Anchored and guided systems have anchors at the ends of straight runs that protect fittings from thermal movement and stresses.

Anchors at directional changes (elbows and tees) transmit loads to the support substructure. Special attention should be given to these loads by the piping engineer to ensure an adequate substructure design. When multiple anchors are used to break up long straight runs, the loads between them and the substructure are generally small. The axial restraining loads are simply balanced between the two opposing sides of the pipeline at the anchor.

## THERMAL PROPERTIES \& CHARACTERISTICS

The reaction of fiberglass piping to changes in temperature depends on two basic material properties, the thermal "coefficient of expansion"(a) and the axial moduli of elasticity. The composite nature of fiberglass piping results in two distinctive axial moduli of elasticity. They are the axial compression and axial tensile moduli. Systems installed at ambient temperature and operated at higher temperatures will generate internal compression piping stress when anchored. Although this is the most common engineering design condition, the piping engineer should not overlook the opposite thermal condition that generates tensile stresses.

The thermal properties of fiberglass pipe distinguish it from steel in important ways. The coefficient of expansion is roughly twice that of steel. This translates to twice the thermal movement of steel in unrestrained systems. The axial compression modulus of elasticity of fiberglass pipe varies from $3 \%$ to $10 \%$ that of steel. When restraining thermal movements in fiberglass piping the anchor loads would be $1 / 5$ or less than the loads created by a same size and wall thickness in steel piping system.

Thermoplastic pipe coefficients of expansion are typically more than four times that of fiberglass. The elastic modulus of thermoplastic piping is considerably smaller than the moduli of fiberglass and steel. The modulus of elasticity of thermoplastic pipe decreases rapidly as the temperatures increases above $100^{\circ} \mathrm{F}$. This results in very short support spans at elevated temperatures. A restrained thermoplastic piping systems operating at elevated temperatures is very susceptible to buckling thus requiring extensive guiding.

It is important to properly determine the temperature gradient. The gradient should be based on the pipeline temperature at the time that the system is tied down or anchored. If the operating temperature is above this temperature, then the gradient is positive and conversely if it is less than this temperature, then the gradient is negative. Many piping systems will see both positive and negative temperature gradients that must be considered during the system design.

Success By Design software performs thermal analysis on fiberglass piping systems based on the methods discussed in this section. The benefits of using Success By Design are not only ease of use, but increased analysis accuracy. The software evaluates the fiberglass material properties at the actual operating temperatures, eliminating the conservatism built into charts and tables designed to cover worst case scenarios for all designs.

## FUNDAMENTAL THERMAL ANALYSIS FORMULAS

## A. Thermal Expansion and Contraction

The calculation of thermal expansion or contraction in straight pipelines is easily accomplished using the following equation.

Eq. $19 \quad \delta:=\alpha \cdot L \cdot\left(T_{0}-T_{i}\right)$
Where:
$d=$ Length change, in (m)
$\mathrm{a}=$ Thermal coefficient of expansion, in/in/ $/{ }^{\circ} \mathrm{F}\left(\mathrm{m} / \mathrm{m} /{ }^{\circ} \mathrm{C}\right)$
$\mathrm{L}=$ Pipe length, in (m)
$\mathrm{To}=$ Operating temperature, ${ }^{\circ} \mathrm{F}\left({ }^{\circ} \mathrm{C}\right)$
$\mathrm{Ti}=$ Installation temperature, ${ }^{\circ} \mathrm{F}\left({ }^{\circ} \mathrm{C}\right)$
Final tie-in or completion temperature.
( $\mathrm{To}-\mathrm{Ti}$ ) is the temperature gradient
B. Anchor Restraint Load

The calculation of the restrained load in a pipeline between two anchors is easily accomplished using the following equation.

$$
\text { Eq. } 20 \quad F_{r}:=\alpha \cdot A \cdot E \cdot\left(T_{0}-T_{i}\right)
$$

Where:
$\mathrm{Fr}=$ Restraining load, $\mathrm{lb}(\mathrm{N})$
$\mathrm{a}=$ Thermal coefficient of expansion, in/in/ $/{ }^{\circ} \mathrm{F}\left(\mathrm{m} / \mathrm{m} /{ }^{\circ} \mathrm{C}\right)$
$A=$ Reinforced pipe wall cross sectional area, $\mathrm{in}^{2}\left(\mathrm{~m}^{2}\right)$
To = Operating temperature, ${ }^{\circ} \mathrm{F}\left({ }^{\circ} \mathrm{C}\right)$
$\mathrm{Ti}=$ Installation temperature, ${ }^{\circ} \mathrm{F}\left({ }^{\circ} \mathrm{C}\right)$
Final tie-in or completion temperature.
(To - Ti) Temperature gradient
$\mathrm{E}=$ Axial modulus of elasticity, $\mathrm{lb} / \mathrm{in}^{2}\left(\mathrm{~N} / \mathrm{m}^{2}\right)$
The compression modulus should be used with a positive temperature change ( $\mathrm{To}>\mathrm{Ti}$ ) and the tensile modulus with a negative temperature change ( $\mathrm{To}<\mathrm{Ti}$ ).

The reactions on the external support structure at internally spaced anchors in long straight runs are negligible because the in-line forces balance. However, the anchors at the end of straight runs will transmit the full load to the support structure.

## C. Guide Spacing

The Guide spacing calculations are derived from Euler's critical elastic buckling equation for a slender column with pivot ends.

Eq. $21 \quad \mathrm{Lg}:=\sqrt{\frac{\pi^{2} \cdot \mathrm{E} \cdot \mathrm{I}}{\mathrm{Fr}}}$

## Where:

$\mathrm{Lg}=$ Guide spacing, in (m)
$\mathrm{Fr}=$ Restraining force, $\mathrm{lb}(\mathrm{N})$
$\mathrm{E}=$ Bending modulus of elasticity, $\mathrm{lb} / \mathrm{in}^{2}\left(\mathrm{~N} / \mathrm{m}^{2}\right)$
$\mathrm{I}=$ Pipe area moment of inertia, in $\left.\mathrm{in}^{4}\right)$

## FLEXIBILITY ANALYSIS AND DESIGN

There are four basic methods of controlling thermal expansion and contraction in above ground piping systems. They are:

1. Anchoring and Guiding
2. Directional Changes
3. Expansion Loops
4. Mechanical Expansion Joints

The use of anchors and guides as discussed earlier simply restrain thermal growth. Directional changes, expansion loops and mechanical expansion joints use component flexibility to safely absorb thermal movements.

## A. Directional Change Design

The flexibility analysis of a directional change is based on a guided cantilever beam model. The cantilever must be of sufficient length to ensure the pipe will not be overstressed while absorbing the thermal movement. This is accomplished by satisfying the following equations.

Eq. 22 Based on pipe allowable bending stress

$$
\mathrm{L}:=\sqrt{\frac{\mathrm{K} \cdot \delta \cdot \mathrm{E} \cdot \mathrm{OD}}{\sigma}}
$$

Where:
$K=3$, Guided cantilever beam coefficient
$\mathrm{L}=$ Length of cantilever leg, in (m)
$E=$ Pipe beam bending modulus of elasticity,
$\mathrm{lb} / \mathrm{in}^{2}\left(\mathrm{~N} / \mathrm{m}^{2}\right)$
$\mathrm{OD}=$ Pipe outer diameter, in (m)
$\delta=$ Total deflection to be absorbed, in (m)
$\sigma=$ Pipe allowable bending stress, $\mathrm{Ib} / \mathrm{in}^{2}\left(\mathrm{~N} / \mathrm{m}^{2}\right)$
Eq. 23 Based on fitting allowable bending moment

$$
\mathrm{L}:=\sqrt{\frac{\mathrm{K} \cdot \mathrm{E} \cdot \mathrm{I} \cdot \delta}{\mathrm{M}}}
$$

Where:
$K=6$, Guided cantilever beam coefficient
$\mathrm{L}=$ Length of cantilever leg, in(m)
$E=$ Pipe beam bending modulus of elasticity,
$\mathrm{lb} / \mathrm{in}^{2}\left(\mathrm{~N} / \mathrm{m}^{2}\right)$
$\mathrm{I}=$ Pipe reinforced area moment of inertia, $\mathrm{in}^{4}\left(\mathrm{~m}^{4}\right)$
$d=$ Total deflection to be absorbed, in(m)
$\mathrm{M}=$ Fitting allowable bending moment, in-lb (N-m)
Minor out of plane rotation of the elbow should be allowed to minimize bending moments on the elbow.

The use of the guided cantilever beam equation results in conservative leg lengths.


Figure 3.0

See Figure 3.0 for a typical horizontal directional change layout.

## B. Expansion Loop Design

The flexibility of an expansion loop is modeled using two equal length guided cantilever beams. Each cantilever absorbs half of the thermal expansion or contraction. The cantilevers must be of sufficient length to ensure the pipe and fittings will not be overstressed. Determination of the minimum required lengths is accomplished by satisfying equation 22 with $\mathrm{K}=1.5$ and equation 23 with $\mathrm{K}=3$.
These equations should be used with the total deflection ( $d=d_{1}+d_{2}$ ) to be absorbed by both expansion loop legs.

See Figure 3.1 for a typical expansion loop layout.
The pipe should be guided into the expansion loop as shown in Figure 3.1. The positioning of two guides on each side of the expansion loop is required to maintain proper alignment. The recommended guide spacing is four and fourteen nominal pipe diameters from the elbow for the first and second guides respectively.
To achieve the required flexibility $90^{\circ}$ elbows should be used in directional changes and expansion loops. The substitution of $45^{\circ}$ elbows will result in an unsatisfactory design.

## C. Expansion Joint Design

Mechanical expansion joint use requires the engineer to determine the complete range of thermal movement expected in the system. This is accomplished by calculating the maximum thermal expansion and thermal
contraction for the operating conditions. The mechanical expansion joint must be capable of absorbing the full range of thermal movement with an appropriate margin of safety. During installation the set position must be determined to ensure the expansion joint will accommodate the entire range of movement. This is accomplished using the following equation.

Eq. $24 \quad$ SetPoint : $=$ R.Travel
Where:
Set Point = Installed position of mechanical expansion joint "Distance from the joint being fully compressed", in(m)
Travel $=$ Mechanical expansion joint maximum movement, in(m)

Eq. 25

$$
\mathrm{R}:=\frac{\mathrm{T}_{\mathrm{i}}-\mathrm{T}_{\text {min }}}{\mathrm{T}_{\text {max }}-\mathrm{T}_{\text {min }}}
$$

$\mathrm{R}=$ Thermal ratio
$\mathrm{Ti}=$ Installation tie-in temperature, $\mathrm{F}^{\circ}\left(\mathrm{C}^{\circ}\right)$
Tmin $=$ Minimum operating temperature, $\mathrm{F}^{\circ}\left(\mathrm{C}^{\circ}\right)$
$\operatorname{Tmax}=$ Maximum operating temperature, $\mathrm{F}^{\circ}\left(\mathrm{C}^{\circ}\right)$
$\operatorname{Tmin} \leq \mathrm{Ti}$

## Example Problem:

Determine the "Travel" and "Set Point" for the following conditions.
$\mathrm{Ti}=75^{\circ} \mathrm{F}, \mathrm{Tmin}=45^{\circ} \mathrm{F}, \operatorname{Tmax}=145^{\circ} \mathrm{F}, \mathrm{R}=0.3$
Pipe total thermal movement is 6 inches Design factor 1.5

## Expansion Joint

Typical guides and supports require pads a shown when there is point contact. Supports can be snug or loose fitting around the pipe. Guides must be loose.

First guide, 4 diameters distance from expansion joint. Second guide, 14 di-


Figure 3.2


Expansion joint "Travel" required is 9 inches ( $6 \times 1.5$ ).
The "Set Point" should be $0.3 \times 9=2.7$ inches (compression). This set point allows for 1.5 times the thermal growth or contraction for the given operating conditions. See Figure 3.2 for a typical expansion joint layout.

The proper selection of an expansion joint design depends on the available activation loads generated by the piping system. Equation 20 should be used to determine the fully restrained activation load capability of the piping system. If a mechanical expansion joint requires an activation force higher than the fully restrained activation load then the expansion joint will not function. The expansion joint activation force in practice should not exceed $1 / 4$ of the load in a fully restrained piping system. Mechanical expansion joints requiring higher activation forces may not provide sufficient flexibility to warrant its use.

## D. Heat Tracing

Heat tracing is the practice of heating a piping system to prevent freezing or cooling of a process line. Steam tracing and electrical heat tapes are typical methods of heat tracing fiberglass piping. The maximum heat tracing temperature is governed by one of three criteria:
(1) The mean wall temperature must not exceed the maximum temperature rating of the pipe,

$$
\text { Eq. } 26 \quad \frac{\mathrm{~T}_{\mathrm{in}}+\mathrm{T}_{\mathrm{ra}}}{2} \leq \mathrm{T}_{\mathrm{pt}}
$$

(2) The maximum tracing element temperature must not exceed $100^{\circ} \mathrm{F}\left(55.6 \mathrm{C}^{\circ}\right)$ above the temperature rating of the pipe

$$
\text { Eq. } 27 \quad \mathrm{~T}_{\mathrm{ra}} \leq \mathrm{T}_{\mathrm{pr}}+100
$$

(3) The maximum recommended temperature for the service chemical must not be exceeded at the surface of the pipe inner wall.

Eq. $28 \quad \mathrm{~T}_{\mathrm{in}} \leq \mathrm{T}_{\mathrm{ct}}$
For stagnant flow, the temperature of the fluid and inner surface of the pipe can be assumed to equal the trace temperature. This assumption is valid if the heat trace element provides sufficient energy to overcome heat losses to the environment. For the stagnant or no flow condition, equation 29 is used to determine the maximum allowable heat trace temperature.

Eq. $29 \mathrm{~T}_{\mathrm{ra}} \leq \mathrm{T}_{\mathrm{Ct}}$

For Eq. 26-29:
$\mathrm{T}_{\mathrm{in}}=$ Pipe inner surface temperature, ${ }^{\circ} \mathrm{F}\left({ }^{\circ} \mathrm{C}\right)$
$\mathrm{T}_{\mathrm{ra}}=$ Heat trace element temperature, ${ }^{\circ} \mathrm{F}\left({ }^{\circ} \mathrm{C}\right)$
$\mathrm{T}_{\mathrm{pr}}=$ Pipe temperature rating, ${ }^{\circ} \mathrm{F}\left({ }^{\circ} \mathrm{C}\right)$
$\mathrm{T}_{\mathrm{Cr}}=$ Chemical resistance temperature rating of pipe, ${ }^{\circ} \mathrm{F}\left({ }^{\circ} \mathrm{C}\right)$

Determination of the pipe inner wall temperature under active flow conditions depends on flow rate, specific heat of the fluid, temperature of fluid entering pipe, conduction through the pipe wall, external environmental heat losses and the heating element capacity. The complexity of this analysis is beyond the scope of this manual. Therefore, prudent engineering practices should be employed to determine the safe heat tracing temperatures under these conditions.

These criteria are most easily explained by the following examples:

Example: What is the maximum heat tracing temperature allowed to maintain a $5 \%$ caustic solution at $95^{\circ} \mathrm{F}$ inside Red Thread II pipe rated to $210^{\circ}$ F?

The three governing criteria must be considered in order to determine the maximum tracing element temperature.

Step I: Solving for criterion (1) equation 26 is applied.

$$
\begin{aligned}
& \mathrm{T}_{\mathrm{ra}} \leq 2 \cdot \mathrm{~T}_{\mathrm{pr}}-\mathrm{T}_{\mathrm{in}} \\
& \mathrm{~T}_{\mathrm{ra}} \leq 2 \cdot 210-95 \\
& \mathrm{~T}_{\mathrm{ra}} \leq 325
\end{aligned}
$$

Rearranging and solving for the maximum trace temperature, Tra we get $325^{\circ} \mathrm{F}$.

Step II: Solving for criterion (2) equation 27 is applied.

$$
\begin{aligned}
& \mathrm{T}_{\mathrm{ra}} \leq \mathrm{T}_{\mathrm{pr}}+100 \\
& \mathrm{~T}_{\mathrm{ra}} \leq 210+100 \\
& \mathrm{~T}_{\mathrm{ra}} \leq 310
\end{aligned}
$$

Rearranging and solving for the maximum trace temperature, Tra we get $310^{\circ} \mathrm{F}$.

Step III: Solving for criterion (3) equation 29 the stagnant flow condition is applied.

$$
\mathrm{T}_{\mathrm{ra}}:=\mathrm{T}_{\mathrm{ct}}
$$

Therefore the maximum allowable heat trace temperature equals the maximum chemical resistance temperature for the piping. Referencing Chemical Resistance Guide, Bulletin No. E5615, Red Thread II pipe is rated to $100^{\circ} \mathrm{F}$ in $5 \%$ caustic. Therefore the maximum heat trace temperature is $100^{\circ} \mathrm{F}$.

However, if the fluid were flowing into the pipeline at temperatures below $100^{\circ} \mathrm{F}$, then the heat trace temperature would be higher than $100^{\circ} \mathrm{F}$. A thorough heat transfer analysis would be required to determine the appropriate heat trace temperature for this condition.

The maximum heat trace temperature for stagnant flow is $100^{\circ} \mathrm{F}$, the lowest temperature calculated using the three criteria.

## E. Thermal Conductivity

The thermal conductivity of fiberglass piping is approximately $1 / 100$ that of steel, making it a poor conductor of heat compared to steel. However, the use of insulation to prevent heat loss or gain is recommended when there are economic consequences due to heat loss or gain. Typical fiberglass thermal conductivity values vary from $0.07-0.29 \mathrm{BTU} /(\mathrm{Ft}).(\mathrm{Hr}).\left({ }^{\circ} \mathrm{F}\right)$.

## F. Thermal Expansion in Buried Pipe

Soil restraint inherently restrains movement of buried fiberglass pipelines because these pipes develop relatively small forces during a temperature change. Special precautions (thrust blocks, guides, expansion joints, etc.) for handling thermal expansion are not necessary if the pipe is buried at least two to three feet and the bedding material is of a soil type capable of restraining the line. Sand, loam, clay, silt, crushed rock and gravel are suitable bedding for restraining a pipeline; however, special precautions must be taken to properly anchor the pipe in swamps, bogs, etc. where bedding might easily shift and yield to even the low forces developed in fiberglass pipe.

## G. Pipe Torque Due to Thermal Expansion

Torsion shear stresses in piping systems containing multiple elevation and directional changes normally do not have to be considered in pipe analysis. The allowable bending moments are lower than the allowable torsional moments in a pipe. Therefore, bending moments in a pipe leg reacted by torsion in a connecting pipe will be limited by the bending moment capability of the pipe not the torsional load. Computer modeling is recommended for this sophisticated level of piping system analysis.

## SECTION 4. Pipe Burial

## INTRODUCTION

The guidelines in this section pertain to the design and burial of fiberglass pipe. The structural design process assumes the pipe will receive adequate support in typically encountered soil conditions. Recommendations for trenching, selecting, placing and compacting backfill will be discussed.

The successful installation depends on all components working together to form a sound support system. Therefore, once a pipe is selected, it is of utmost importance to carefully review the native soil conditions, select the backfill material and closely monitor the trenching and installation process. Properly positioned and compacted bedding and backfill reduces pipe deformations maximizing long-term performance of a buried pipeline.

Detailed design and installation data for buried fiberglass piping systems may be found in AWWA M45, Manual of Water Supply Practices, Fiberglass Pipe Design, First Edition. Contact NOV Fiber Glass Systems applications engineer for detailed burial calculations.

## PIPE FLEXIBILITY

The response of fiberglass pipe to burial loads is highly dependent on the flexibility of the pipe walls. The best measure of pipe flexibility can be found using the "pipe stiffness" value as defined and determined by ASTM D2412 tests.

Pipe with pipe stiffness values greater than 72 psi typically resist native backfill loads with minimal pipe deformation. The pipe stiffness of small diameter fiberglass pipe, 1 to 8 inch diameters, typically meets or exceeds 72 psi. Two to three feet of native backfill cover with a soil modulus greater than or equal to $1,000 \mathrm{psi}$ is generally sufficient to protect this category of pipe from HS-20 vehicular and dead weight soil loads.

Pipe that is buried under concrete or asphalt roadways that support vehicular loads requires less cover. Design data and burial depth recommendation for specific piping can be found in our product bulletins and installation handbooks. Manual No. B2160 contains special installation instructions for UL Listed Red Thread IIA piping commonly used under pavements.

Pipe with pipe stiffness values less than 72 psi, are considered flexible and are more susceptible to the effects of poor compaction or soil conditions. Because of this, larger diameter piping requires detailed attention during the design and installation of buried pipelines.

## BURIAL ANALYSIS

Pipe burial depth calculations are based on Spangler's deflection equation and Von Mise's buckling equation as outlined in AWWA M45. Application of these methods is based on the assumption that the design values used for bedding, backfill and compaction levels will be achieved with good field practice and appropriate equipment. If these assumptions are not met, the deflections can be higher or lower than predicted by calculation.

## A. Soil Types

A soil's ability to support pipe depends on the type of soil, degree of compaction and condition of the soil, i.e. density and moisture content. A stable soil is capable of providing sufficient long-term bearing resistance to support a buried pipe. Unstable soils such as peat, organic soil, and highly expansive clays exhibit a significant change in volume with a change in moisture content. Special trenching and backfill requirements are necessary when the native soil is unstable. Some guidelines to aid the engineer in determining the stability at a particular site follow:

1. For cohesive soils or granular-cohesive soils, if the unconfined compressive strength per ASTM D2166 exceeds $1,500 \mathrm{lb} / \mathrm{ft}^{2}$, the soil will generally be stable.
2. For cohesive soils, if the shear strength of the soil per ASTM D2573 is in excess of $750 \mathrm{lb} / \mathrm{ft}^{2}$, the soil will generally be stable.
3. For sand, if the standard penetration "Blow" value, N , is above 10 , the soil will generally be stable.

Soils types are grouped into "stiffness categories" (SC). They are designated SC1 through SC5. SC1 indicates a soil that provides the highest soil stiffness at any given Proctor density. An SC1 classified soil requires the least amount of compaction to achieve the desired soil stiffness. The higher numbered soil classifications (SC2SC4) become, the more compaction is required to obtain specific soil stiffness at a given Proctor density. The SC5 soils are unstable and should not be used as backfill or bedding. Decaying organic waste and frozen materials fall in the SC5 category. Lists of recommended backfill materials are shown in Table 4.0.

TABLE 4.0 Recommended Bedding and Backfill Materials

| Stiffness <br> Category ${ }^{1}$ | Pipe Zone Backfill Material ${ }^{2,5}$ | Degree of Compaction ${ }^{3}$ <br> \% |
| :---: | :---: | :---: |
| SC1 | Crushed rock ${ }^{4}$ with $\leq 15 \%$ sand, maximum $25 \%$ passing the $3 / 8$ " sieve and maximum $5 \%$ fines | As Dumped (No compaction required) |
| SC2 | Coarse-grained soils with $\leq 12 \%$ fines | 75-85 |
| SC3 | Coarse-grained soils with $>12 \%$ fines | 85-95 |
| SC3 | Fine-grained soils with $>12 \%$ fines | 85-95 |
| SC4 | Fine-grain soils with medium to no plasticity with $<30 \%$ coarse-grained particles | >95 |

1 AWWA M45 soil stiffness categories
2 Maximum particle size of $3 / 4$ inch for all types.
3 Compaction to achieve a soil modulus of $1,000 \mathrm{psi}$.
4 Pea gravel is a suitable alternative.
5 A permeable fabric trench liner may be required where significant ground water flow is anticipated.
B. Soil Modulus

The soil modulus is a common variable that is very important to fiberglass piping burial analysis regardless of the soil type. Extensive research and engineering analysis has shown that a soil modulus of 1,000 psi provides very good support to fiberglass pipe. Table 4.0 shows the degree of compaction based on the Proctor density to obtain a soil modulus of $1,000 \mathrm{psi}$. It is worth noting that for all stiffness categories this soil modulus may be obtained, although with varying compaction requirements.

Although a modulus of $1,000 \mathrm{psi}$ is preferred, values as low as 750 psi will provide sufficient support to fiberglass pipe if it is properly engineered and installed.

## TRENCH EXCAVATION AND PREPARATION

## A. Trench Size

The purpose of the trench is to provide working space to easily install the pipeline. The trench depth must account for the bedding thickness, pipe height and backfill cover. Trench widths must accommodate workers and their tools, as well as allow for side bedding and backfill. The trench widths listed in Table 4.1 are satisfactory for most installations.

## B. Trench Construction

## 1. Solid rock conditions

If solid rock is encountered during trench construction, the depth and width of the trench must be sufficient to allow a minimum of 6 -inches of bedding between the rock and pipe surface.

## 2. Granular or loose soils

These types of soils are characterized by relatively high displacement under load, and soft to medium soft consistencies. The walls of trenches in this type of soil usually have to be sheeted or shored, or the trench made wide enough to place a substantial amount of bedding material in order to prevent excessive deformation in the pipe sides (see figures 4.0 \& 4.1). In some cases, additional depth or supplementary trench foundation material may be required.

## TABLE 4.1 Trench Widths

| Pipe Size <br> (In.) | Minimum Width <br> (In.) | Maximum Width* <br> (In.) |
| :---: | :---: | :---: |
| 2 | 18 | 26 |
| 3 | 18 | 27 |
| 4 | 18 | 28 |
| 6 | 20 | 30 |
| 8 | 23 | 32 |
| 10 | 25 | 34 |
| 12 | 28 | 36 |
| 14 | 31 | 38 |
| 16 | 33 | 40 |
| 18 | 36 | 42 |
| 20 | 39 | 44 |
| 24 | 44 | 58 |
| 30 | 52 | 64 |
| 36 | 60 | 70 |
| 42 | 66 | 80 |
| 48 | 72 | 86 |
| 54 | 78 | 96 |
| 60 | 84 | 108 |
| 72 | 96 | 120 |
| 84 | 108 |  |
| Trench widths may be wider depending on soil conditions. |  |  |

Trench for Soft and Medium Consistency Soils



Figure 4.1

## 3. Unstable soils

Unstable soils require special precautions to develop a stable environment for fiberglass pipe. See Figure 4.2 for a recommended trenching procedure. SC1 bedding and backfill material should be used with a permeable, fabric liner to prevent migration of fill into the native soil. Due to the unpredictable nature of unstable soils a soils engineer should be consulted for project specific design recommendations.

Wide Trench for Very Soft or Unstable Soils


## C. Maximum Burial Depth

Surface loads do not usually affect the maximum burial depths. The maximum burial depth ultimately depends on the soil backfill modulus. When burying pipe in stable soil with a backfill modulus of $1,000 \mathrm{psi}$, the maximum allowable depth of cover is normally 15-20 feet. When burying pipe in soil with a backfill modulus of 700 psi , the maximum allowable cover is seven feet. Although the above maximum burial depths are typical, NOV Fiber Glass Systems will design custom products suitable for your application. Reference NOV Fiber Glass System's product bulletins for specific product recommendations.

## D. Roadway Crossing

Pipe passing under unpaved roadways should be protected from vehicular loads and roadbed settlement. Burial depths under stable roadbeds should be determined per AWWA M45 for vehicular traffic. If the roadbed is unstable or burial-depths are shallow then steel or concrete sleeves are required see Figure 4.3.

## Typical Roadway Crossing



## BEDDING AND BACKFILL

## A. Trench bottom

The trench bottom is the foundation of the pipe support system. Select bedding material is required for flexible fiberglass pipelines. The bedding should be shaped to conform to the bottom of pipe. Proper placement and compaction of the bedding is required to ensure continuous pipe support. See Figures 4.4, 4.5 \& 4.6 for examples of standard bedding practices.


Figure 4.4

Improper Bedding


Figure 4.5

## Bedding and Backfill for Firm or Hard Native Soil



Figure 4.6

## B. Backfill materials

Backfill material at the sides of the pipe is to be added in lifts, not to exceed 6 -inches at a time, mechanically compacted to the required density and continued to 6 -inches above the top of the pipe. The degree of compaction is dependent upon the type of fill material used. Water flooding for compaction is not recommended, nor is compacting the fill material while it is highly saturated with water.

Proper compaction of the backfill material is required for pipeline stability and longevity. Sand, pea gravel or crushed rocks are the recommended SC1 backfill materials requiring minimal compaction if per Table 4.0.

If excavated native material meets the requirements listed in Table 4.0, it may be used for bedding and backfill. Soils containing large amounts of organic material or frozen materials should not be used. If there is any question as to the suitability of the native soil, a soil engineer should be consulted.

## C. Backfill cover

The cover layers above the backfill should be applied in lifts of 6 inches. Native soil may be used, provided it is not unstable type SC5 soil. This includes soils loaded with organic material or frozen earth and ice. Each lift should be compacted to a Proctor Density to achieve a 1,000-psi modulus per Table 4.0. Lifts applied 18 inches or more above the top of the pipe may be applied in 12inch layers provided there are not chunks of soil larger than 12 inches. Again, each layer is to be compacted to the required density. Lift heights should never exceed the capacity of the compaction equipment.

Heavy machinery should not be allowed to cross over trenches unless completely covered and compacted.

## D. High water table

Areas with permanent high water tables are usually coincident with very poor soil conditions. In most of these areas, it will be necessary to use crushed rock or pea gravel as the bedding and backfill material. In addition, permeable fabric trench liner should be used to prevent migration of the fill material into the native soil. In extreme cases such as soft clay and other plastic soils, it will be necessary to use "Class A" bedding. (See Figure 4.7). Also, if the depth of the pipe and the depth of cover is less than one diameter, tie downs or concrete encasement is recommended in sufficient quantity to prevent flotation.

Areas prone to flooding or poor draining soil should be treated similar to high water table areas.

Class "A" Bedding


## SECTION 5. Other Considerations

## A. ABRASIVE FLUIDS

NOV Fiber Glass Systems piping systems are used to convey abrasive fluids that may also be corrosive. Since fiberglass pipe does not depend upon a protective oxide film for corrosion resistance, it is not subject to the combination of corrosion and abrasion that occurs with metals.

The effects of abrasive fluids on any piping system are difficult to predict without test spools or case history information. Particle size, density, hardness, shape, fluid velocity, percent solids, and system configuration are some of the variables that affect abrasion rates. Standard fiberglass piping with a resin-rich liner can generally handle particle sizes less than 100 mesh (150 micron) at flow rates up to 8 ft ./sec. The abrasion resistance can be improved by adding fillers such as fine silica, silicon carbide, or ceramic to the abrasion barrier (such as with Silver Streak, F-Chem, and Ceram Core products). Wear resistance of fiberglass fittings can be improved by using long-radius fittings.

Since each abrasive service application is different and peculiar to its industry, please consult your local representative for a recommendation.

## B. LOW TEMPERATURE APPLICATIONS

Fiberglass pipe is manufactured with thermosetting resin systems that do not become brittle at low temperatures, as do thermoplastic materials. NOV Fiber Glass Systems pipe and fittings can be used for low temperature applications such as liquid gases (refer to Chemical Resistance Guide for compatibility with liquid gases). Tensile tests performed at $-75^{\circ} \mathrm{F}\left(-59.4^{\circ} \mathrm{C}\right)$ actually show an increase in strength and modulus. Typical low temperature applications are the conveyance of fuel, oil, and other petroleum production applications in Alaska.
C. PIPE PASSING THROUGH WALLS OR CONCRETE STRUCTURES

The design of wall penetrations must consider the possible effects of wall settlement and the resulting reactions on the pipe body. Wall penetrations below grade must also be sealed to prevent water seepage. Typically fiberglass pipe is sealed into the wall opening with
epoxy grout material such as if manufactured by ITW Devcon Corporation, Danvers, MA. Fiberglass piping systems should be designed with sufficient flexibility near wall penetrations to minimize reactions to slight wall movements. To prevent leakage around the grout, it is common to embed a steel sleeve with a water-stop during the wall construction (Figure 5.0).

The use of flexible seals between the pipe and wall penetration is a standard practice used to protect fiberglass pipe from abrasion and minimize effects of wall movements. A segmented rubber seal such as Link-Seal® manufactured by Thunderline/Link-Seal, 19500 Victor Parkway, Suite 275, Livonia, MI 48152 is commonly used with fiberglass pipe.

If the pipe is not sealed into the wall, it must be protected from surface abrasion. A heavy gage sheet metal sleeve will provide sufficient protection.

## D. PIPE BENDING

Pipe is often bent during transportation, handling and during installation to match trenching contours, etc. As long as the minimum bending radius is not exceeded, these practices will not harm the pipe. Minimum bending radius values are unique to product type and diameter. Therefore, NOV Fiber Glass System piping bulletins must be referred to for accurate data.

Bending of pipe with in-line saddles, tees, or laterals should be avoided. Bending moments in the pipe will create undesirable stresses on the bonded joints and fittings.
$®$ Link-Seal is registered trademark of Thunderline/Link-Seal

## E. STATIC ELECTRICITY

The generation of static electricity is not a problem in most industrial applications. The effects of static electricity usually become a design problem only if a dry, electrically non-conductive gas or liquid is piped at high velocity through an ungrounded system.

The generation of static electricity under fluid flow conditions is primarily related to the flow rate, ionic content of the fluid, material turbulence, and surface area at the interface of the fluid and the pipe. The rate of electrostatic generation in a pipe increases with increasing length of pipe to a maximum limiting value. This maximum limiting value is related to fluid velocity and is greater for high velocities. Highly refined hydrocarbons, such as jet fuels, accumulate charges more rapidly than more conductive hydrocarbons, such as gasoline. However, the rate of charge buildup in buried piping systems handling jet fuels at a maximum flow velocity of $5 \mathrm{ft} / \mathrm{sec}$ is such that special grounding is not necessary.

Static charges are generated at approximately the same rate in fiberglass piping and metallic pipe. The difference in the two systems is that the charge can be more easily drained from a metal line than from a fiberglass line. Under the operating conditions encountered in most industrial applications, any static charge generated is readily drained away from the pipe at hangers or by other contact with the ground, and any small charge in the fluid is drained away at metallic valves and/or instrumentation lines.

NOV Fiber Glass Systems manufactures an electrically conductive piping system that should be employed when static electricity is a critical design parameter.


Occasionally in piping a dry gas at high velocity, a charge may build up on an ungrounded valve. If this charge is not drained off by humid air, it can shock personnel who come in contact with the valve. This situation can be easily remedied by grounding the valve.


Bulk fuel-loading facilities, because of high fluid velocities, present a problem to both metallic and fiberglass pipe. Filters and other high surface area devices are prolific generators of static electricity at these facilities. Special grounding procedures may be necessary under these conditions.

## F. STEAM CLEANING

Short duration steam cleaning of epoxy fiberglass pipe is acceptable provided the following recommendations are adhered to:

- The piping system must be open-ended to prevent pressure buildup.
- The maximum steam pressure does not exceed 15 psig
corresponding to a steam saturation temperature of approximately $250^{\circ} \mathrm{F}$. Contact a factory representative for specific product design information.
- The piping system design must consider the effects of the steam cleaning temperatures. In most cases the support spans will be reduced $15-35 \%$.
- Contact the factory before steam cleaning vinyl ester or polyester pipe.


## G. THRUST BLOCKS

Thrust blocks are not required for NOV Fiber Glass System's adhesive bonded piping systems. Large diameter F-Chem O-ring pipe is not restrained and may require the use of thrust blocks. Consult the factory for specific recommendations.

## H. VACUUM SERVICE

Vacuum service may be a system design condition, or it may occur as the result of an inadvertent condition. Sudden pump shut off, valve closures, slug flow and system drain down are examples of flow conditions that result in vacuum. They should always be considered during the design phase. Regardless of the source, vacuum conditions result when the external atmospheric pressure exceeds the internal pressure. The pipe wall must be capable of resisting this external pressure without buckling. Consult our product bulletins for specific external pressure (vacuum) ratings. Large diameter pipe through 72-inches manufactured specifically for vacuum conditions are available upon request.

## I. VALVES

When using valves with fiberglass piping products, consideration must be given to the corrosion resistance of the valve with respect to the fluid being conveyed and the external environment. Heavy valves should be independently supported to reduce bending stresses on adjacent pipe. Flanged valves mated to molded fiberglass flanges must have a full flat face to prevent overstressing the flanges. To ensure a good seal, use a $1 / 8$-inch thick fullface, $60-70$ durometer gasket between the valve sealing surface and the fiberglass flange for up to 14 -inch diameter pipe. Use $1 / 4$-inch thick gaskets on larger sizes. If the valves do not have full flat faces consult installation manuals for additional recommendations.

## J. VIBRATION

Low amplitude vibrations such as those produced by well-anchored centrifugal pumps will have little effect on fiberglass piping. Such vibrations will be dampened and absorbed by the relatively low modulus pipe. However, care must be taken to protect the exterior of the pipe from surfaces that might abrade and wear through the
pipe wall over a long period of time. This can be accomplished by using support "wear" saddles at the supports or padding the supports with $1 / 8$-inch rubber gasket material. See Section 2 for recommended support designs.

High amplitude vibration from pumps or other equipment must be isolated from the piping system by flexible connectors.

## K. FLUID HAMMER

A moving column of fluid has momentum proportional to its mass and velocity. When flow is abruptly stopped, the fluid momentum is converted into an impulse or highpressure surge. The higher the liquid velocity and longer the pipe line, the larger the impulse.

These impulse loads can be of sufficient magnitude to damage pipe, fittings and valves.

$\triangle$Accurate determination of impulse loads is very complex and typically requires computer modeling of the piping system. However, the Talbot equation, given in Appendix A, may be used to calculate theoretical impulses assuming an instantaneous change in velocity. Although, it is physically impossible to close a valve instantaneously, Talbot's equation is often employed to calculate worst case conditions.

In the real world quick reacting valves, reverse flow into check valves and sudden variations in pump flow rates will cause water hammer surges. Engineers typically incorporate slow operating valves, surge tanks and softstarting pumps into piping systems to minimize fluid hammer. Piping systems that experience surge conditions should be restrained to prevent excessive movement.

If the system operating pressure plus the peak surge pressure exceeds the system pressure rating, then a higher pressure class piping system should be employed.

## L. ULTRAVIOLET (U.V.) RADIATION AND WEATHERING

Fiberglass pipe undergoes changes in appearance when exposed to sunlight. This is a surface phenomenon caused by U.V. degradation of the resin. The degradation depends upon the accumulated exposure and the intensity of the sunlight. Long-term surface degradation may expose the outer layer of glass fibers; this condition is called "fiber-blooming". These exposed glass fibers will block and reflect a significant portion of ultraviolet radiation resulting in a slower rate of degradation. This minimizes future damage to the remaining pipe wall. Because NOV Fiber Glass Systems pipe bodies are designed with significant safety factors, minor fiber blooming does not prevent the pipe from safely performing at its published pressure rating. If service conditions are such that exposed fibers will be abraded with time, it is highly recommended that surface be protected. Painting the
pipe with a good quality acrylic or solvent-based paint is useful in blocking UV radiation.

## M. FUNGAL, BACTERIAL, AND RODENT RESISTANCE

Some plastics (thermoplastics) are subject to fungal, bacterial, and/or rodent attack, but fiberglass pipe offers no nourishment or attraction to these annoyances. Under stagnant conditions, some marine growths will attach to fiberglass surfaces, but they do not attack or bore into the pipe and are usually easily removed. Note regarding zebra mussels: It was recently reported that a utility compared zebra mussel growth in similar metal and fiberglass intake lines at the same location. Only two liters of zebra mussels were removed from the fiberglass line, while two dumpster loads of mussels were removed from a metal line.

## N. FLANGE CONNECTIONS

Our flanges are designed to meet ANSI B16.5 Class 150 bolt hole standards. Alternate bolt hole standards are available. Flanges are designed for $1 / 8$ inch thick gaskets made from materials with a 60-70 durometer Shore A hardness. The use of flat washers under nuts and bolt heads is required. Refer to the appropriate product specific fittings bulletin for recommended bolt torque values.

## Raised Face Flange Connections

Special mating requirements exist when connecting flatface compression molded fiberglass flanges to raisedface metallic flanges or valves having partial liner facings. The addition of a metallic spacer ring placed between the raised face and the outer edge of the flange to form a full flat-face on the mating flange is recommended. The purpose of the spacer ring is to fill the gap outside the raised-face to prevent bolt loads from bending and breaking the fiberglass flange. An alternative to the spacer ring is the use of metallic back-up rings behind molded fiberglass flanges. Filament wound flanges may be connected directly to raised-face flanges without the use of spacer rings. Refer to installation manual for backing ring sizes.

## Lug and Wafer Valves

Lined lug and wafer valves that use integral seals, require a $1 / 4$-inch steel spacer plate with an inner diameter equal to Schedule 40 steel or as required by the valve manufacturer. The spacer plate outer diameter should match the fiberglass flange outer diameter.

Unlined lug and wafer valves without integral seals may be directly connected to fiberglass filament flanges without back up rings or to molded flanges with metal back-up rings. Refer to installation manual for backing ring sizes.

## SECTION 6. Specifications and Approvals

## A. COMPLIANCE WITH NATIONAL SPECIFICATIONS

## American Petroleum Institute

API Specification 15LR
Red Thread II Pipe \& Fittings, 2"-24 Cyclic Design

## American Society for Testing \& Materials (ASTM)

ASTM D2310 (See Table 6.0 \& 6.2)
"Standard Classification for Machine Made 'Fiberglass' (Glass-Fiber-Reinforced Thermosetting-Resin) Pipe" Classifications of Pipe at $73.4^{\circ} \mathrm{F}$ are:

TABLE 6.0 ASTM D2310 Classification

| Pipe | Size | ASTM D2310 Classification |
| :---: | :---: | :---: |
| Red Thread II | $\begin{gathered} 2 "-3 " \\ 4 "-24 " \end{gathered}$ | RTRP-11AF RTRP-11AH |
| Green Thread | 1"-16" | RTRP-11FY |
| Z-Core | 1"-8" | RTRP-21CO |
| Silver Streak | 2"-48" | RTRP-11FY |
| Ceram Core | 6"-16" | RTRP-11CF |
| F-Chem | 1"-72" | RTRT-12EU |
| Centricast |  |  |
| RB-1520 | $1^{1 / 2 "-14 " ~}$ | RTRP-21CW |
| RB-2530 | 1"-14" | RTRP-21CW |
| CL-1520 | 11/2"-14" | RTRP-22BT |
| CL-2030 | 1"-14" | RTRP-22BS |

## ASTM D2996

"Standard Specification for Filament-Wound 'Fiberglass' (Glass-Fiber-Reinforced ThermosettingResin) Pipe"
Designation Codes are available in product bulletins.

## ASTM D2997

"Standard Specification for Centrifugally Cast 'Fiberglass' (Glass-Fiber-Reinforced ThermosettingResin) Pipe"
Designation Codes are available in product bulletins.

## ASTM D4024 (See Table 6.1)

"Standard Specification for Machine Made 'Fiberglass'
(Glass-Fiber-Reinforced Thermosetting-Resin)
Flanges"
Designation Codes at $73.4^{\circ} \mathrm{F}$, by flange size, are available in product bulletins.

## ASTM D5685

"Standard Specification for "Fiberglass" (Glass-FiberReinforced Thermosetting-Resin) Pressure Pipe Fittings Designation Codes are available in technical application bulletins.

## B. APPROVALS, LISTINGS, AND COMPLIANCE WITH REGULATIONS

## American Water Works Association

Red Thread II pipe, Green Thread pipe, and F-Chem pipe can be made in compliance with AWWA M45 for use as pressure pipes for water distribution (including services) and transmission systems for both above and below ground installations. When ordering, specify AWWA M45.

## ASMEIANSI B31.3

"Process Piping"
Red Thread II and Green Thread pipe that are manufactured in compliance with ASTM D2996, and Centricast pipe manufactured in compliance with D2997, can be installed in compliance with ASME/ANSI B31.3.

## Factory Mutual

Pipe and fittings, sizes 4"-16", are available with Factory Mutual approval for underground fire protection piping systems; pressure ratings to 200 psig. When ordering, specify Factory Mutual Products.

## Food and Drug Administration

The resins and curing agents used in the manufacture of Red Thread II Pipe and Fittings and Green Thread Pipe and Fittings are defined as acceptable with the U.S. Food, Drug, and Cosmetic Act as listed under 21 CFR Part 177 Subpart C Section 177.2280 and 21 CFR Part 175 Subpart C Section 175.300.

Military Specifications
MIL-P-29206 or MIL-P-29206A—Red Thread II JP and Green Thread JP pipe and fittings, sizes 2"-12", are certified to be in compliance with MIL-P-29206 or MIL-P29206A, Military Specification: "Pipe and Pipe Fittings, Glass Fiber Reinforced Plastic for Liquid Petroleum Lines."

## NSF International

## (National Sanitation Foundation)

ANSI/NSF Standard No. 61 (Drinking Water System Components-Health Effects) Listing: Note: Standard No. 61 was developed by a consortium and with support from the U.S. Environmental Protection Agency under cooperative agreement No. CR-812144:

2"-24" Red Thread II Pipe and Fittings<br>1"-36" Green Thread Pipe and Fittings 3033 and 8000 Series (Epoxy Adhesive)<br>F-Chem Pipe ${ }^{(1)}$<br>F-Chem Fittings ${ }^{(1)}$

(1) Piping greater than 14" diameter using NSF Listed resin system.

Underwriters Laboratories Inc. (UL) and Underwriters' Laboratories of Canada (ULC)
Red Thread II pipe and compatible primary fittings, along with secondary containment pipe and fittings, and adhesives are listed for use in conveying petroleum products, alcohols, and alcohol-gasoline mixtures including ethanol, methanol and MTBE underground (UL). The primary pipe sizes are 2", 3 " and 4"; the secondary containment pipe and fittings sizes are $3^{\prime \prime}, 4^{\prime \prime}$, and $6^{\prime \prime}$.

These products are listed for use in conveying petroleum products, gasoline mixtures and up to $100 \%$ ethanol underground (ULC).

| Table for Use in Classifying Fiberglass Flanges to ASTM D4024 |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Filament Wound (FW) $\qquad$ <br> Compression Molded. $\qquad$ <br> Resin-Transfer Molded $\qquad$ <br> Centrifugally Cast $\qquad$ |  |  |  | Grade |  |  | sure <br> ting <br> sig- <br> ion* | Property Designation |
| Epoxy Resin $\qquad$ <br> Polyester Resin $\qquad$ <br> Furan Resin $\qquad$ |  |  |  | $\begin{array}{r} . . .1 \\ \ldots . . \\ \ldots \\ \ldots . . \end{array}$ |  |  |  |  |
| Integrally-Molded (mfg. on pipe/fitting) <br> Taper to Taper Adhesive Joint $\qquad$ <br> Straight to Taper Adhesive Joint $\qquad$ <br> Straight Adhesive Joint. $\qquad$ | ...... |  |  |  |  |  |  |  |
| *Gauge Pressure (psig) <br> (Flanges must withstand a pressure of 4 times the rating without damage to the flange) |  |  |  | .... |  |  |  |  |
| PROPERTY 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| Burst Pressure (psig) (unspecified) |  | 400 | 600 | 800 | 1000 | 1200 | 1600 | 2000 |
| Sealing Test Pressure (psig) | 75 | 150 | 225 | 300 | 375 | 450 | 600 | 750 |
| Bolt Torque Limit (ft.lbs.) | 20 | 30 | 50 | 75 | 100 | 125 | 150 | 200 |



## APPENDIX A

Geometric Properties: $\quad A=A r e a ; ~ A 1=$ Surface area of solids; $V=$ Volume; $C=C$ ircumference


A = HB



Circle
$\mathbf{A}=\pi \mathrm{R}^{2}$
$\mathbf{C}=\pi \mathbf{D}$
$C=\pi D$
$R=D / 2$


Sector of Circle

$$
\begin{aligned}
\mathrm{A} & =\pi \mathrm{R}^{2} \frac{\alpha}{360} \\
\mathrm{~L} & =\pi \mathrm{R} \frac{\alpha}{180} \\
\alpha & =57.296 \frac{\mathrm{~L}}{\mathrm{R}} \\
\mathrm{R} & =57.296 \frac{\mathrm{~L}}{\alpha}
\end{aligned}
$$



Rectanglular Solid $A 1=2(W L+L H+H W)$ V $=$ WLH


Elliptical Tanks

$$
A 1=2 \pi\left(\begin{array}{c}
A B+H \sqrt{\frac{A^{2}+B^{2}}{2}} \\
V=\pi A B H
\end{array}\right.
$$



Sphere
$A=4 \pi R^{2}$

$$
V=\frac{4 \pi R^{3}}{3}
$$



Cylinder
$A 1=2 \pi R(H+R)$ $\mathrm{V}=\pi \mathrm{HR}^{2}$
For Above Containers:
Capacity in gallons $=\frac{V}{231}$ when $V$ is in cubic inches Capacity in gallons $=7.48 \times V$ when $V$ is in cubic feet

## SUPPORT SPANS

"Three Moment Equation" for a uniformly loaded continuous beam.


$$
\frac{M_{\mathrm{a}} \cdot L_{1}}{E_{1} \cdot I_{1}}+2 \cdot M_{b} \cdot\left(\frac{L_{1}}{E_{1} \cdot I_{1}}+\frac{L_{2}}{E_{2} \cdot I_{2}}\right)+\frac{M_{c} \cdot L_{2}}{E_{2} \cdot I_{2}}+\frac{W_{1} \cdot L_{1}^{3}}{4 \cdot E_{1} \cdot I_{1}}+\frac{W_{2} \cdot L_{2}^{3}}{4 \cdot E_{2} \cdot I_{2}}=0
$$

Where:
$\mathrm{Ma}=$ Internal moment at support $\mathrm{A}, \mathrm{in}-\mathrm{lb}(\mathrm{N}-\mathrm{m})$
$\mathrm{Mb}=$ Internal moment at support B, in-lb(N-m)
$\mathrm{Mc}=$ Internal moment at support C , in- $\mathrm{lb}(\mathrm{N}-\mathrm{m})$
$L_{n}=$ Span " $n$ " length, in(m)
$I_{n}=$ Span " $n$ " area moment of inertia, $\mathrm{in}^{4}\left(\mathrm{~m}^{4}\right)$
$\mathrm{W}_{\mathrm{n}}=$ Span " n " uniformly distributed load, $\mathrm{Ib} / \mathrm{in}(\mathrm{N} / \mathrm{m})$
$\mathrm{E}_{\mathrm{n}}=$ Span " n " modulus of elasticity, $\mathrm{lb} / \mathrm{in}^{2}\left(\mathrm{~N} / \mathrm{m}^{2}\right)$
$n=1,2$
"Fixed-Fixed Beam Equation" for a uniformly loaded beam.

Where:


Maximum Deflection, in(m)
Maximum Moment, in-lb (n-m)

$$
\delta \max :=\frac{W \cdot L^{4}}{384 \cdot E \cdot I}
$$

$$
\operatorname{MImax}:=\frac{\mathrm{WV} \cdot \mathrm{~L}^{2}}{12}
$$

$\mathrm{W}=$ Uniformly distributed load, $\mathrm{Ib} / \mathrm{in}(\mathrm{N} / \mathrm{m})$
$\mathrm{L}=$ Span length in(m)
I = Area moment of inertia, $\mathrm{in}^{4}\left(\mathrm{~m}^{4}\right)$
$\mathrm{E}=$ Modulus of elasticity, $\mathrm{lb} / \mathrm{in}^{2}\left(\mathrm{~N} / \mathrm{m}^{2}\right)$

WATER HAMMER

$$
P:=\rho \cdot\left[\mathrm{Ev} \cdot \mathrm{t} \cdot \frac{\mathrm{E}}{\rho \cdot(\mathrm{t} \cdot \mathrm{E}+\mathrm{D} \cdot \mathrm{Ev})}\right]^{0.5} \cdot \delta \mathrm{~V}
$$

Talbot Equation for calculating the surge pressure due to an instantaneous change in flow velocity.
Where:

$$
\begin{aligned}
\text { P } & =\text { Pressure surge, } \mathrm{lb} / \mathrm{in}^{2}\left(\mathrm{~N} / \mathrm{m}^{2}\right) \\
\mathrm{r} & =\text { Mass density, } \mathrm{lb} / \mathrm{in}^{3}\left(\mathrm{~kg} / \mathrm{m}^{3}\right) \\
\text { En } & =\text { Volume modulus compressibility of fluid, } \mathrm{Ib} / \mathrm{in}^{2}\left(\mathrm{~N} / \mathrm{m}^{2}\right) \\
\mathrm{E} & =\text { Hoop modulus of elasticity of pipe wall, } \mathrm{lb} / \mathrm{in}^{2}\left(\mathrm{~N} / \mathrm{m}^{2}\right) \\
\mathrm{t} & =\text { Pipe wall thickness, in }(\mathrm{m}) \\
D & =\text { Pipe inner diameter, in }(\mathrm{m}) \\
\mathrm{dV} & =\text { Change in velocity, } \mathrm{ft} / \mathrm{sec}(\mathrm{~m} / \mathrm{sec})
\end{aligned}
$$

## GEOMETRIC RELATIONSHIPS FOR MINIMUM BENDING RADIUS



$$
\begin{aligned}
& \delta=R \cdot\left(1-\cos \left(\frac{L}{2 \cdot R}\right)\right) \\
& C=2 \cdot R \cdot \sin \left(\frac{L}{2 \cdot R}\right)
\end{aligned}
$$

Where:
$L=$ pipe length, $\mathrm{ft}(\mathrm{m})$
$\mathrm{R}=$ minimum bend radius, $\mathrm{ft}(\mathrm{m})$
$\delta=$ maximum offset deflection, $\mathrm{ft}(\mathrm{m})$
$\mathrm{C}=$ chord length, $\mathrm{ft}(\mathrm{m})$
(trigonometric functions based on radians)

MINIMUM BENDING RADIUS OFFSET FORMULA


Where:
$\mathrm{X}=$ Run, $\mathrm{ft}(\mathrm{m})$
$Y=0$ Offset, $\mathrm{ft}(\mathrm{m}) \quad \pi)$
$R=$ minimum bend radius, $f(m)$
(trigonometric function based on radians)

## APPENDIX B

Table A. 1 Water Pressure to Feet of Head

| Pressure | Head | Pressure | Head |
| :---: | :---: | :---: | :---: |
| Lb/In ${ }^{2}$ | Feet | Lb/In ${ }^{2}$ | Feet |
| 1 | 2.31 | 100 | 230.90 |
| 2 | 4.62 | 110 | 253.98 |
| 3 | 6.93 | 120 | 277.07 |
| 4 | 9.24 | 130 | 300.16 |
| 5 | 11.54 | 140 | 323.25 |
| 6 | 13.85 | 150 | 346.34 |
| 7 | 16.16 | 160 | 369.43 |
| 8 | 18.47 | 170 | 392.52 |
| 9 | 20.78 | 180 | 415.61 |
| 10 | 23.09 | 200 | 461.78 |
| 15 | 34.63 | 250 | 577.24 |
| 20 | 46.18 | 300 | 692.69 |
| 25 | 57.72 | 350 | 808.13 |
| 30 | 69.27 | 400 | 922.58 |
| 40 | 92.36 | 500 | 1154.48 |
| 50 | 115.45 | 600 | 1385.39 |
| 60 | 138.54 | 700 | 1616.30 |
| 70 | 161.63 | 800 | 1847.20 |
| 80 | 184.72 | 900 | 2078.10 |
| 90 | 207.81 | 1000 | 2309.00 |

Note: One pound of pressure per square inch of water equals 2.309 feet of water at $62^{\circ} \mathrm{F}$. Therefore, to find the feet head of water for any pressure not given in the table above, multiply the pressure pounds per square inch by 2.309.

Table A. 2 Feet of Head of Water to psi

| Head | Pressure | Head | Pressure |
| :---: | :---: | :---: | :---: |
| Feet | Lb/In ${ }^{2}$ | Feet | Lb/In ${ }^{2}$ |
| 1 | 0.43 | 100 | 43.31 |
| 2 | 0.87 | 110 | 47.64 |
| 3 | 1.30 | 120 | 51.97 |
| 4 | 1.73 | 130 | 56.30 |
| 5 | 2.17 | 140 | 60.63 |
| 6 | 2.60 | 150 | 64.96 |
| 7 | 3.03 | 160 | 69.29 |
| 8 | 3.46 | 170 | 73.63 |
| 9 | 3.90 | 180 | 77.96 |
| 10 | 4.33 | 200 | 86.62 |
| 15 | 6.50 | 250 | 108.27 |
| 20 | 8.66 | 300 | 129.93 |
| 25 | 10.83 | 350 | 151.58 |
| 30 | 12.99 | 400 | 173.24 |
| 40 | 17.32 | 500 | 216.55 |
| 50 | 21.65 | 600 | 259.85 |
| 60 | 25.99 | 700 | 303.16 |
| 70 | 30.32 | 800 | 346.47 |
| 80 | 34.65 | 900 | 389.78 |
| 90 | 38.98 | 1000 | 433.00 |

[^36]Table A. 3 Dry Saturated Steam Pressure

| ABS Press., <br> Lb/In ${ }^{2}$ | Temp <br> ${ }^{\circ} \mathrm{F}$ | ABS Press., <br> Lb/In ${ }^{2}$ | Temp <br> ${ }^{\circ} \mathrm{F}$ |
| :---: | :---: | :---: | :---: |
| 0.491 | 79.03 | 30 | 250.33 |
| 0.736 | 91.72 | 35 | 259.28 |
| 0.982 | 101.14 | 40 | 267.25 |
| 1.227 | 108.71 | 45 | 274.44 |
| 1.473 | 115.06 | 50 | 281.01 |
| 1.964 | 125.43 | 55 | 287.07 |
| 2.455 | 133.76 | 60 | 292.71 |
| 5.000 | 162.24 | 65 | 297.97 |
| 10.000 | 193.21 | 70 | 302.92 |
| 14.696 | 212.00 | 75 | 307.60 |
| 15.000 | 213.03 | 80 | 312.03 |
| 16.000 | 216.32 | 85 | 316.25 |
| 18.000 | 222.41 | 90 | 320.27 |
| 20.000 | 227.96 | 100 | 327.81 |
| 25.000 | 240.07 | 110 | 334.77 |

Table A. 4 Specific Gravity of Gases
(At $60^{\circ} \mathrm{F}$ and 29.92 Hg )


Table A. 5 Specific Gravity of Liquids

| Liquid | Temp <br> ${ }^{\circ} \mathrm{F}$ | Specific Gravity |
| :--- | :---: | :---: |
| Water (1 $\mathrm{ft}^{3}$ weighs 62.41 lb.) | 50 | 1.00 |
| Brine (Sodium Chloride 25\%) | 32 | 1.20 |
| Pennsylvania Crude Oil | 80 | 0.85 |
| Fuel Oil No. 1 and 2 | 85 | 0.95 |
| Gasoline | 80 | 0.74 |
| Kerosene | 85 | 0.82 |
| Lubricating Oil SAE 10-20-30 | 115 | 0.94 |

Table A. 6 Weight of Water

| 1 cu. ft. at $50^{\circ} \mathrm{F} \ldots \ldots \ldots \ldots \ldots \ldots$ weighs 62.41 lb. |
| ---: |
| 1 gal. at $50^{\circ} \mathrm{F} \ldots \ldots \ldots \ldots \ldots$ weighs 8.34 lb. |
| $1 \mathrm{cu} . \mathrm{ft}$. of ice $\ldots \ldots \ldots \ldots \ldots$ weighs 57.2 lb. |
| $1 \mathrm{cu} . \mathrm{ft}$. at $39.2^{\circ} \mathrm{F} \ldots \ldots \ldots \ldots \ldots$ weighs 62.43 lb. |
| Water is at its greatest density at $39.2^{\circ} \mathrm{F}$ |

Table A. 7 Conversion Factors

## Pressure

| 1 in. of mercury | $=345.34 \mathrm{~kg} / \mathrm{m}^{2}$ |
| :--- | :--- |
|  | $=0.0345 \mathrm{~kg} / \mathrm{cm}^{2}$ |
|  | $=0.0334 \mathrm{bar}$ |
|  | $=0.491 \mathrm{lb} / \mathrm{in}^{2}$ |
| 1 lb. per sq. in. | $=2.036 \mathrm{in}$ head of mercury |
|  | $=2.309 \mathrm{ft}$ head of water |
|  | $=0.0703 \mathrm{~kg} / \mathrm{cm}^{2}$ |
|  | $=0.0690 \mathrm{bar}$ |
|  | $=6894.76 \mathrm{pascals}$ |
|  | $=1.0$ newton $/ \mathrm{m}^{2}$ |
|  | $=9.8692 \times 10^{-6} \mathrm{atmospheres}$ |
|  | $=1.4504 \times 10^{-4} \mathrm{lb} / \mathrm{in}^{2}$ |
|  | $=4.0148 \times 10^{-3} \mathrm{in}$. head of water |
|  | $=7.5001 \times 10^{-4} \mathrm{~cm}$. head of mercury |
|  | $=1.0200 \times 10^{-5} \mathrm{~kg} / \mathrm{m}^{2}$ |
|  | $=1.0 \times 10^{-5} \mathrm{bar}$ |
|  | $=101,325 \mathrm{pascals}$ |
|  | $=1,013 \mathrm{milibars}$ |
|  | $=14.696 \mathrm{lbs} / \mathrm{in}^{2}$ |

## Temperature

${ }^{\circ} \mathrm{C}$. $=\left({ }^{\circ} \mathrm{F}-32\right) \times 5 / 9$

## Weight of Liquid

1 gal. (U.S.) $\quad=8.34 \mathrm{lb} . \times \mathrm{Sg}$
$1 \mathrm{cu} . \mathrm{ft} . \quad=62.4 \mathrm{lb} . \times \mathrm{Sg}$
$1 \mathrm{lb} . \quad=0.12$ U.S. gal/Sg.

$$
=0.016 \mathrm{ft}^{3} / \mathrm{Sg}
$$

## Flow

| 1 gpm | $=0.134 \mathrm{ft}^{3} / \mathrm{min}$ |
| :--- | :--- |
|  | $=500 \mathrm{lb} / \mathrm{hr} . x \mathrm{Sg}$ |
| $500 \mathrm{lb} / \mathrm{hr}$. | $=1 \mathrm{gpm} / \mathrm{Sg}$ |
| $1 \mathrm{ft}^{3} / \mathrm{min}$ | $=448.8 \mathrm{gal} / \mathrm{hr}$ |

## Work

| 1 Btu (mean) $=$ | 778 ft lb |
| :--- | :--- |
| $=$ | 0.293 watt hr |
| $=$ | $1 / 180$ of heat required to change |
|  | temp of 1 lb water from $32^{\circ} \mathrm{F}$ to |
|  | $212^{\circ} \mathrm{F}$ |
| $=$ | 2545 Btu |
| $=$ | 0.746 kwhr |
| $1 \mathrm{hp}-\mathrm{hr}$ | $=3413 \mathrm{Btu}$ |
| 1 kwhr | $=1.34 \mathrm{hp} \mathrm{hr}$ |

NOTES

# Chemical 

 Resistance Guide79


## Introduction

This guide is intended for use only as a reference in evaluating NOV Fiber Glass Systems piping systems. It should be used for a general indication of chemical resistance. NOV Fiber Glass Systems data indicates that the pipe and fittings listed are suitable for the services as recommended. However, due to varying conditions encountered in usage from plant to plant, the data should be considered as a recommendation and not as a guarantee. NOV Fiber Glass Systems offers a limited warranty of its products, which is in the Terms and Conditions of Sale. This data does not take into account chemical mixtures, thermal-mechanical or associated loading or stress combinations. Accordingly, the end-user of the fiberglass products assumes the responsibility and risk for proper evaluation, selection, use, and performance of the products in its particular application.

## Basis of Chemical Resistance Recommendations

The information contained in this literature is based on corrosion resistance testing, field experience, published information, and NOV Fiber Glass Systems engineering judgment. Corrosion resistance testing includes the pipe, fittings and adhesive used in NOV Fiber Glass Systems piping systems. There are many successful installations that form the basis of the field experience and engineeringjudgmentrecommendations. NOV Fiber Glass Systems products must be installed and used in accordance with proven practice and common sense. Corrosion barrier and total wall thickness may affect service life in aggressive chemical or abrasive applications.

## General Notes

$N R=$ Not Recommended, except for very low concentrations. Contact NOV Fiber Glass Systems Application Engineering for further evaluation.

NT = Not Tested. Contact NOV Fiber Glass Systems Application Engineering for further evaluation.

When no concentration is shown, recommendations apply to any concentration to $100 \%$ or to saturation.

## Spills or Upset Conditions

Flush the system immediately if spills or upsets exposes the piping to chemicals that have not been recommended.

## Solvent Applications

Solvents may separate from the fluid stream in piping with static or low flow rates. The solvents will be concentrated and may damage piping not recommended for $100 \%$ concentrations. Flush the piping system immediately after shutdown to prevent solvent damage. Vent lines carrying solvent vapors can also have high concentrations of liquid solvent due to condensation. The condensation can affect the service life of systems not recommended for full concentrations.

## Unlisted Applications and Combinations of Chemicals

NOV Fiber Glass Systems piping is being used in many applications containing other chemicals, solvents, and combinations of chemicals not listed in this literature. These applications should be reviewed with the factory for evaluations of the chemicals, their concentrations, temperatures, frequency of use, and other factors that may determine our suitability to provide economic service life. Extra care should be taken when there are combinations of chemicals as some combinations may be more aggressive than their constituent parts. Trace amounts of some chemicals can affect the piping service life.

## Process Drains and Combined Waste Systems

Due to the inherent chemical resistance of NOV Fiber Glass Systems piping systems, they are widely used in aggessive process drains and combined waste systems. For these systems and other intermittent conditions, the products may be used outside of the ratings published in this chemical guide. Please contact Applications Engineering for specific recommendations.

## Mixing Chemicals in the Piping System

Careful consideration should be given to the by-products of mixing chemicals. By-products of chemical reactions may aggressively corrode a piping system.

## Abrasive Fluid

Piping is used successfully in many abrasive slurry applications. Products made especially for abrasive applications are available. Products selection is dependent on particle size, percent solids, particle hardness, flow rates and continuous or intermittent usage.

## Regulations \& Standards

Local, state, or federal regulations, or industry standards may govern the use of our products in particular applications and should be reviewed by the customer to assure compliance.

## Trademarks

Bondstrand ${ }^{T M}$, Red Thread ${ }^{\text {TM }}$, Green Thread ${ }^{T M}$ and Centricast ${ }^{T M}$ piping systems and Key-Lock ${ }^{\text {™ }}$ joints are trademark names of NOV Fiber Glass Systems.

| Chemical Substance | Concentration | Red Thread HP <br> Bondstrand 7000 7000M 3000A 2"-6" 2400 Conductive |  | $\begin{aligned} & \text { Bondstrand } \\ & \text { 3000A 8"-16" } \end{aligned}$ |  | $\begin{gathered} \text { Green Thread HP } \\ \text { Bondstrand } \\ 2000 \\ 2000 \mathrm{M} \\ 2400 \\ 4000 \end{gathered}$ |  | $\begin{aligned} & \text { Centricast } \\ & \text { Z-Core } \end{aligned}$ |  | $\begin{aligned} & \text { Centricast } \\ & \text { RB-1520 } \\ & \text { RB-2530 } \end{aligned}$ |  | $\begin{gathered} \text { Centricast } \\ \text { CL-1520 } \\ \text { CL-2030 } \end{gathered}$ |  | $\begin{gathered} \text { Bondstrand } \\ 5000 \\ 5000 \mathrm{M} \end{gathered}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ |
| 1,1,2,2-Tetrachloroethane |  | NR | NR | NR | NR | 120 | 49 | 150 | 66 | NT | NT | NT | NT | NT | NT |
| 1,1,1-Trichloroethane |  | 120 | 49 | 120 | 49 | $125^{(2)}$ | $52^{(2)}$ | 175 | 79 | 120 | 49 | 80 | 27 | NR | NR |
| 2-Butoxyethoxyethanol |  | NT | NT | NT | NT | NT | NT | NR | NR | NR | NR | 80 | 27 | NT | NT |
| 2-Chlorophenol |  | NT | NT | NT | NT | NT | NT | 100 | 38 | NR | NR | NR | NR | NT | NT |
| Acetaldehyde |  | 120 | 49 | 80 | 27 | 120 | 49 | 100 | 38 | 75 | 24 | NR | NR | NR | NR |
| Acetamide |  | NR | NR | NR | NR | NR | NR | 100 | 38 | NR | NR | NR | NR | NT | NT |
| Acetic acid | $\leq 10 \%$ | 150 | 66 | 150 | 66 | 200 | 93 | 200 | 93 | $150{ }^{(2)}$ | $66^{(2)}$ | 175 | 79 | 210 | 99 |
| Acetic acid | 10 $\leq 20 \%$ | 150 | 66 | 150 | 66 | 200 | 93 | 200 | 93 | 150 | 66 | 175 | 79 | 210 | 99 |
| Acetic acid | 20 $50 \%$ | NT | NT | NT | NT | 150 | 66 | 120 | 49 | 100 | 38 | 175 | 79 | 180 | 82 |
| Acetic acid | 50 $575 \%$ | NT | NT | NT | NT | 75 | 24 | 75 | 24 | 75 | 24 | 150 | 66 | 110 | 43 |
| Acetic acid | > $75 \%$ | NR | NR | NR | NR | 75 | 24 | 75 | 24 | 75 | 24 | 100 | 38 | NT | NT |
| Acetic acid, "glacial" |  | NT | NT | NT | NT | 75 | 24 | 75 | 24 | 75 | 24 | NR | NR | NT | NT |
| Acetic anhydride |  | NR | NR | NR | NR | NR | NR | 100 | 38 | NR | NR | NR | NR | NR | NR |
| Acetone | $\leq 1 \%$ | 150 | 66 | 150 | 66 | 150 | 66 | 200 | 93 | 150 | 66 | 150 | 66 | NR | NR |
| Acetone | 1 $10 \%$ | 150 | 66 | 150 | 66 | 150 | 66 | 200 | 93 | 150 | 66 | 150 | 66 | NR | NR |
| Acetone | > $10 \%$ | 100 | 38 | 100 | 38 | 120 | 49 | 200 | 93 | 125 | 52 | NR | NR | NR | NR |
| Acetonitrile |  | NT | NT | NT | NT | NT | NT | 120 | 49 | NR | NR | NR | NR | NR | NR |
| Acetophenone |  | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NR | NR |
| Acetyl chloride |  | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT |
| Acrylic acid | $\leq 25 \%$ | NT | NT | NT | NT | 120 | 49 | 120 | 49 | NT | NT | 100 | 38 | NT | NT |
| Acrylic acid | 25 $\leq 95 \%$ | NT | NT | NT | NT | 100 | 38 | 100 | 38 | NT | NT | 75 | 24 | NT | NT |
| Acrylonitrile |  | NT | NT | NT | NT | NT | NT | 100 | 38 | NT | NT | NT | NT | NR | NR |
| Air "wet or dry" |  | 210 | 99 | 210 | 99 | 250 | 121 | 300 | 149 | 300 | 149 | 200 | 93 | 200 | 93 |
| Allyl alcohol |  | NT | NT | NT | NT | NT | NT | 150 | 66 | 100 | 38 | 75 | 24 | NT | NT |
| Allyl chloride |  | 100 | 38 | 100 | 38 | 120 | 49 | NT | NT | NT | NT | NT | NT | NR | NR |
| Aluminum acetate | <10\% | NT | NT | NT | NT | NT | NT | 275 | 135 | 250 | 121 | 150 | 66 | 150 | 66 |
| Aluminum chloride ${ }^{(4)}$ | Sat'd | 210 | 99 | 210 | 99 | 225 | 107 | 275 | 135 | 250 | 121 | 200 | 93 | 200 | 93 |
| Aluminum chlorohydroxide | <50\% | NT | NT | NT | NT | NT | NT | 150 | 66 | 150 | 66 | NT | NT | NR | NR |
| Aluminum fluoride | Sat'd | NR | NR | NR | NR | NR | NR | 200 | 93 | 200 | 93 | 175 | 79 | NT | NT |


| Chemical Substance | Concentration | Red Thread HP <br> Bondstrand 7000 7000M 3000A 2"-6" 2400 Conductive |  | $\begin{aligned} & \text { Bondstrand } \\ & \text { 3000A 8"-16" } \end{aligned}$ |  |  | d HP <br> nd | $\begin{aligned} & \text { Centricast } \\ & \text { Z-Core } \end{aligned}$ |  | $\begin{gathered} \text { Centricast } \\ \text { RB-1520 } \\ \text { RB-2530 } \end{gathered}$ |  | $\begin{gathered} \text { Centricast } \\ \text { CL-1520 } \\ \text { CL-2030 } \end{gathered}$ |  | $\begin{aligned} & \text { Bondstrand } \\ & 5000 \\ & 5000 \mathrm{M} \end{aligned}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ |
| Aluminum hydroxide | Sat'd | NR | NR | NR | NR | 190 | 88 | 250 | 121 | 250 | 121 | 175 | 79 | 150 | 66 |
| Aluminum nitrate |  | 150 | 66 | 150 | 66 | 205 | 96 | 250 | 121 | 250 | 121 | 175 | 79 | 180 | 82 |
| Aluminum potassium sulfate "alum" | Sat'd | 210 | 99 | 210 | 99 | 225 | 107 | 275 | 135 | 250 | 121 | 200 | 93 | 200 | 93 |
| Aluminum sulfate | Sat'd | 210 | 99 | 210 | 99 | 225 | 107 | 275 | 135 | 250 | 121 | 200 | 93 | 200 | 93 |
| Ammonia gas, "dry, anhydrous" ${ }^{(3)}$ |  | 150 | 66 | 150 | 66 | 225 | 107 | 275 | 135 | $150^{(2)}$ | $66^{(2)}$ | 100 | 38 | 100 | 38 |
| Ammonia gas, "wet" |  | NT | NT | NT | NT | NT | NT | NT | NT | $150^{(2)}$ | $66^{(2)}$ | 100 | 38 | NT | NT |
| Ammonia, liquid |  | NT | NT | NT | NT | NT | NT | NR | NR | NR | NR | NR | NR | NT | NT |
| Ammonium acetate | <65\% | NT | NT | NT | NT | NT | NT | 275 | 135 | 75 | 24 | 75 | 24 | NT | NT |
| Ammonium bicarbonate | 550\% | 180 | 82 | 180 | 82 | 220 | 104 | 200 | 93 | 180 | 82 | 150 | 66 | 150 | 66 |
| Ammonium bicarbonate | Sat'd | 150 | 66 | 150 | 66 | 180 | 82 | 225 | 107 | 225 | 107 | 125 | 52 | NT | NT |
| Ammonium bisulfate | Sat'd | NT | NT | NT | NT | NT | NT | 275 | 135 | 175 | 79 | 150 | 66 | NT | NT |
| Ammonium bisulfate, "black liquor" |  | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | 150 | 66 | NT | NT |
| Ammonium bisulfate, "cook liquor" |  | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | 150 | 66 | NT | NT |
| Ammonium carbonate | 550\% | 150 | 66 | 150 | 66 | 180 | 82 | 225 | 107 | 200 | 93 | 150 | 66 | 100 | 38 |
| Ammonium carbonate | Sat'd | 150 | 66 | 150 | 66 | 205 | 96 | 225 | 107 | 200 | 93 | 150 | 66 | NT | NT |
| Ammonium chloride | <25\% | 150 | 66 | 150 | 66 | 205 | 96 | 225 | 107 | 200 | 93 | 200 | 93 | NT | NT |
| Ammonium chloride | Sat'd | 150 | 66 | 150 | 66 | 205 | 96 | 225 | 107 | 200 | 93 | 200 | 93 | 200 | 93 |
| Ammonium citrate | Sat'd | 200 | 93 | 200 | 93 | 225 | 107 | 275 | 135 | 175 | 79 | 125 | 52 | NT | NT |
| Ammonium fluoride | <25\% | NR | NR | NR | NR | 75 | 24 | 150 | 66 | 150 | 66 | 125 | 52 | NT | NT |
| Ammonium fluoride | Sat'd | NR | NR | NR | NR | 75 | 24 | 100 | 38 | 100 | 38 | 125 | 52 | NT | NT |
| Ammonium hydroxide | <5\% | 120 | 49 | 120 | 49 | 150 | 66 | 200 | 93 | 150 | 66 | 150 | 66 | 150 | 66 |
| Ammonium hydroxide | $5 \leq 10 \%$ | 120 | 49 | 120 | 49 | 150 | 66 | 200 | 93 | 150 | 66 | 150 | 66 | 150 | 66 |
| Ammonium hydroxide | 10 $20 \%$ | 120 | 49 | 120 | 49 | 125 | 52 | 200 | 93 | 150 | 66 | 150 | 66 | 150 | 66 |
| Ammonium hydroxide | 20 $29 \%$ | 120 | 49 | 120 | 49 | 125 | 52 | 200 | 93 | 100 | 38 | 100 | 38 | 100 | 38 |
| Ammonium hydroxide | Sat'd | 120 | 49 | 120 | 49 | 125 | 52 | 175 | 79 | NT | NT | NT | NT | NT | NT |
| Ammonium lauryl sulfate | <30\% | NT | NT | NT | NT | NT | NT | NT | NT | 150 | 66 | 120 | 49 | NT | NT |
| Ammonium molybdate |  | NT | NT | NT | NT | NT | NT | NT | NT | 100 | 38 | 150 | 66 | NT | NT |
| Ammonium nitrate | $\leq 25 \%$ | 210 | 99 | 200 | 93 | 225 | 107 | 275 | 135 | 250 | 121 | 200 | 93 | 200 | 93 |
| Ammonium nitrate | Sat'd | 210 | 99 | 200 | 93 | 225 | 107 | 210 | 99 | 250 | 121 | 175 | 79 | 200 | 93 |


| Chemical Substance | Concentration | Red Thread HP <br> Bondstrand 7000 7000M 3000A 2"-6" 2400 Conductive |  | $\begin{aligned} & \text { Bondstrand } \\ & \text { 3000A 8"-16" } \end{aligned}$ |  |  | d HP <br> nd | $\begin{aligned} & \text { Centricast } \\ & \text { Z-Core } \end{aligned}$ |  | $\begin{gathered} \text { Centricast } \\ \text { RB-1520 } \\ \text { RB-2530 } \end{gathered}$ |  | $\begin{gathered} \text { Centricast } \\ \text { CL-1520 } \\ \text { CL-2030 } \end{gathered}$ |  | $\begin{aligned} & \text { Bondstrand } \\ & 5000 \\ & 5000 \mathrm{M} \end{aligned}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ |
| Ammonium pentaborate | <12\% | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | 120 | 49 | NT | NT |
| Ammonium persulfate | Sat'd | NR | NR | NR | NR | 100 | 38 | 100 | 38 | 100 | 38 | 180 | 82 | 180 | 82 |
| Ammonium phosphate | $\leq 65 \%$ | 150 | 66 | 150 | 66 | 200 | 93 | 225 | 107 | 180 | 82 | 200 | 93 | 150 | 66 |
| Ammonium phosphate | Sat'd | 150 | 66 | 150 | 66 | 200 | 93 | 225 | 107 | 180 | 82 | 150 | 66 | 150 | 66 |
| Ammonium sulfate | Sat'd | 200 | 93 | 200 | 93 | 225 | 107 | 275 | 135 | 250 | 121 | 200 | 93 | 200 | 93 |
| Ammonium sulfide, "bisulfide" | Sat'd | NT | NT | NT | NT | NT | NT | 100 | 38 | 100 | 38 | 120 | 49 | NT | NT |
| Ammonium sulfite |  | NT | NT | NT | NT | NT | NT | 150 | 66 | NR | NR | NR | NR | NT | NT |
| Ammonium thiocyanate | <20\% | 100 | 38 | 100 | 38 | 150 | 66 | NT | NT | 150 | 66 | 190 | 88 | 100 | 38 |
| Ammonium thiocyanate | Sat'd | 100 | 38 | 100 | 38 | 150 | 66 | NT | NT | 150 | 66 | 100 | 38 | 100 | 38 |
| Ammonium thioglycolate | <8\% | NT | NT | NT | NT | NT | NT | NT | NT | 100 | 38 | 90 | 32 | NT | NT |
| Ammonium thiosulfate | Sat'd | 100 | 38 | 100 | 38 | 150 | 66 | NT | NT | 100 | 38 | 90 | 32 | 100 | 38 |
| Amyl acetate |  | 75 | 24 | 75 | 24 | 120 | 49 | 150 | 66 | NR | NR | NR | NR | NR | NR |
| Amyl alcohol |  | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | 100 | 38 | 100 | 38 |
| Amyl chloride |  | NR | NR | NR | NR | NR | NR | 100 | 38 | NR | NR | 100 | 38 | NR | NR |
| Aniline |  | NT | NT | NT | NT | NT | NT | 150 | 66 | 75 | 24 | NR | NR | NR | NR |
| Aniline hydrochloride |  | NT | NT | NT | NT | NT | NT | 100 | 38 | NR | NR | 180 | 82 | NT | NT |
| Aniline sulfate | Sat'd | NR | NR | NR | NR | NR | NR | 100 | 38 | NR | NR | 200 | 93 | NT | NT |
| Antimony pentachloride |  | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | 90 | 32 |
| Antimony trichloride |  | NR | NR | NR | NR | NR | NR | 150 | 66 | 150 | 66 | 200 | 93 | 200 | 93 |
| Aqua regia |  | NR | NR | NR | NR | NR | NR | NR | NR | NR | NR | NR | NR | NR | NR |
| Arsenic acid |  | NT | NT | NT | NT | NT | NT | NT | NT | NR | NR | 100 | 38 | 180 | 82 |
| Arsenious acid |  | NR | NR | NR | NR | NR | NR | 100 | 38 | NT | NT | NT | NT | NT | NT |
| Barium acetate | Sat'd | 150 | 66 | 150 | 66 | 180 | 82 | 275 | 135 | 180 | 82 | 180 | 82 | 150 | 66 |
| Barium bromide |  | NT | NT | NT | NT | NT | NT | NT | NT | 100 | 38 | 200 | 93 | NT | NT |
| Barium carbonate | Sat'd | 210 | 99 | 200 | 93 | 225 | 107 | 275 | 135 | 250 | 121 | 200 | 93 | 200 | 93 |
| Barium chloride | Sat'd | 210 | 99 | 210 | 99 | 225 | 107 | 275 | 135 | 250 | 121 | 200 | 93 | 200 | 93 |
| Barium cyanide |  | NT | NT | NT | NT | NT | NT | NT | NT | 200 | 93 | 150 | 66 | NT | NT |
| Barium hydroxide | $\leq 10 \%$ | 180 | 82 | 180 | 82 | 200 | 93 | 225 | 107 | 210 | 99 | 200 | 93 | 150 | 66 |
| Barium hydroxide | >10\% | NT | NT | NT | NT | NT | NT | 225 | 107 | 200 | 93 | 150 | 66 | NT | NT |


| Chemical Substance | Concentration | Red Thread HP <br> Bondstrand 7000 <br> 7000M <br> 3000A 2"-6" <br> 2400 Conductive |  | $\begin{aligned} & \text { Bondstrand } \\ & \text { 3000A 8"-16" } \end{aligned}$ |  | Gree | d HP | $\begin{aligned} & \text { Centricast } \\ & \text { Z-Core } \end{aligned}$ |  | $\begin{aligned} & \text { Centricast } \\ & \text { RB-1520 } \\ & \text { RB-2530 } \end{aligned}$ |  | $\begin{aligned} & \text { Centricast } \\ & \text { CL-1520 } \\ & \text { CL-2030 } \end{aligned}$ |  | $\begin{aligned} & \text { Bondstrand } \\ & 5000 \\ & 5000 \mathrm{M} \end{aligned}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ |
| Barium nitrate |  | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | 150 | 66 |
| Barium sulfate | Sat'd | NT | NT | NT | NT | NT | NT | 275 | 135 | 250 | 121 | 200 | 93 | 200 | 93 |
| Barium sulfide | Sat'd | 210 | 99 | 210 | 99 | 225 | 107 | 275 | 135 | 250 | 121 | 200 | 93 | NT | NT |
| Beer |  | 210 | 99 | 200 | 93 | 225 | 107 | 250 | 121 | 200 | 93 | 200 | 93 | 150 | 66 |
| Benzaldehyde |  | NR | NR | NR | NR | NR | NR | 200 | 93 | NT | NT | NT | NT | NR | NR |
| Benzene hydrochloric acid, "wet" |  | NR | NR | NR | NR | NR | NR | NR | NR | NR | NR | NR | NR | NT | NT |
| Benzene in kerosene | <5\% | NT | NT | NT | NT | NT | NT | NT | NT | 200 | 93 | 200 | 93 | NT | NT |
| Benzene sulfonic acid | 550\% | NT | NT | NT | NT | NT | NT | 100 | 38 | 100 | 38 | 125 | 52 | 200 | 93 |
| Benzene sulfonic acid | 50 $575 \%$ | NT | NT | NT | NT | NT | NT | 100 | 38 | NR | NR | 100 | 38 | 200 | 93 |
| Benzene sulfonic acid | > $75 \%$ | NT | NT | NT | NT | NT | NT | 75 | 24 | NR | NR | 100 | 38 | 200 | 93 |
| Benzene |  | $120^{(2)}$ | $49^{(2)}$ | $120^{(2)}$ | $49^{(2)}$ | $150{ }^{(2)}$ | $66^{(2)}$ | $180{ }^{(2)}$ | $82^{(2)}$ | 125 | 52 | NR | NR | NR | NR |
| Benzoic acid | Sat'd | 100 | 38 | 100 | 38 | 150 | 66 | 200 | 93 | 200 | 93 | 200 | 93 | 200 | 93 |
| Benzyl alcohol |  | NT | NT | NT | NT | NT | NT | 150 | 66 | NR | NR | NR | NR | NT | NT |
| Benzyl chloride |  | NT | NT | NT | NT | NT | NT | 150 | 66 | NR | NR | NR | NR | NT | NT |
| Benzyltrimethylammonium chloride | <60\% | NT | NT | NT | NT | NT | NT | NT | NT | 150 | 66 | 100 | 38 | NT | NT |
| Biodiesel |  | 210 | 99 | 210 | 99 | 225 | 107 | 275 | 135 | 250 | 121 | 180 | 82 | NT | NT |
| Black liquor, "pulp mill" |  | 150 | 66 | 125 | 52 | 225 | 107 | 230 | 110 | 180 | 82 | 180 | 82 | 180 | 82 |
| Borax |  | 200 | 93 | 200 | 93 | 225 | 107 | 275 | 135 | 250 | 121 | 200 | 93 | 200 | 93 |
| Boric acid |  | 200 | 93 | 200 | 93 | 225 | 107 | 250 | 121 | 200 | 93 | 200 | 93 | 200 | 93 |
| Brass plating solution |  | NT | NT | NT | NT | NT | NT | NT | NT | NR | NR | 150 | 66 | NT | NT |
| Brine " $<20 \%$ salts" |  | 210 | 99 | 190 | 88 | 225 | 107 | 275 | 135 | 250 | 121 | 200 | 93 | 200 | 93 |
| Bromic acid |  | NT | NT | NT | NT | NT | NT | NT | NT | 150 | 66 | NR | NR | NT | NT |
| Brominated phosphate ester |  | NT | NT | NT | NT | NT | NT | NT | NT | NR | NR | NR | NR | NT | NT |
| Bromine, "dry gas" |  | NT | NT | NT | NT | NT | NT | NT | NT | NR | NR | 100 | 38 | NR | NR |
| Bromine, "liquid" |  | NR | NR | NR | NR | NR | NR | NR | NR | NR | NR | NR | NR | NR | NR |
| Bromine, "wet gas" |  | NR | NR | NR | NR | NR | NR | NR | NR | NR | NR | NR | NR | NR | NR |
| Bromine water | $\leq 1 \%$ | 200 | 93 | NT | NT | 200 | 93 | 75 | 24 | 100 | 38 | 100 | 38 | NT | NT |
| Bromine water | $\leq 5 \%$ | NT | NT | NT | NT | NT | NT | 75 | 24 | 100 | 38 | 100 | 38 | NT | NT |
| Bromoform |  | NR | NR | NR | NR | NR | NR | 185 | 85 | NT | NT | NT | NT | NT | NT |


| Chemical Substance | Concentration | Red Thread HP <br> Bondstrand 7000 7000M 3000A 2"-6" 2400 Conductive |  | Bondstrand 3000A 8"-16" |  |  | d HP <br> d | $\begin{aligned} & \text { Centricast } \\ & \text { Z-Core } \end{aligned}$ |  | $\begin{aligned} & \text { Centricast } \\ & \text { RB-1520 } \\ & \text { RB-2530 } \end{aligned}$ |  | $\begin{aligned} & \text { Centricast } \\ & \text { CL-1520 } \\ & \text { CL-2030 } \end{aligned}$ |  | $\begin{aligned} & \text { Bondstrand } \\ & 5000 \\ & 5000 \mathrm{M} \end{aligned}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ |
| Brown stock |  | NT | NT | NT | NT | NT | NT | NT | NT | NR | NR | 100 | 38 | NT | NT |
| Butadiene, "gas" |  | NR | NR | NR | NR | NR | NR | 200 | 93 | 100 | 38 | 100 | 38 | 100 | 38 |
| Butane |  | 75 | 24 | 75 | 24 | 75 | 24 | 100 | 38 | 180 | 82 | 100 | 38 | 100 | 38 |
| Butanol |  | See Butyl alcohol |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Butyl acetate |  | 75 | 24 | 75 | 24 | 150 | 66 | 175 | 79 | 100 | 38 | NR | NR | NR | NR |
| Butyl acrylate |  | NT | NT | NT | NT | NT | NT | NT | NT | NR | NR | NR | NR | NT | NT |
| Butyl alcohol | <10\% | 120 | 49 | 120 | 49 | 150 | 66 | 200 | 93 | 120 | 49 | 120 | 49 | 100 | 38 |
| Butyl alcohol | > $10 \%$ | 120 | 49 | 120 | 49 | 150 | 66 | 200 | 93 | NT | NT | NT | NT | 100 | 38 |
| Butyl benzoate | <70\% | NT | NT | NT | NT | NT | NT | 200 | 93 | NR | NR | NR | NR | NT | NT |
| Butyl benzyl phthalate ${ }^{(4)}$ |  | NT | NT | NT | NT | NT | NT | 125 | 52 | 125 | 52 | 100 | 38 | NT | NT |
| Butyl carbitol diethylene glycol |  | NT | NT | NT | NT | NT | NT | NT | NT | NR | NR | 80 | 27 | NT | NT |
| Butyl cellosolve |  | 150 | 66 | 150 | 66 | 150 | 66 | 175 | 79 | 150 | 66 | 100 | 38 | NR | NR |
| Butyl phthalate |  | NT | NT | NT | NT | NT | NT | 125 | 52 | NT | NT | NT | NT | NT | NT |
| Butylene glycol |  | 150 | 66 | 150 | 66 | 150 | 66 | 250 | 121 | 200 | 93 | 150 | 66 | NT | NT |
| Butyraldehyde |  | NT | NT | NT | NT | NT | NT | 150 | 66 | 150 | 66 | NR | NR | NR | NR |
| Butyric acid | <25\% | 150 | 66 | 150 | 66 | 200 | 93 | 100 | 38 | 150 | 66 | 175 | 79 | 180 | 82 |
| Butyric acid | 25 $550 \%$ | 150 | 66 | 150 | 66 | 200 | 93 | 100 | 38 | 150 | 66 | 150 | 66 | 160 | 71 |
| Cadmium chloride | Sat'd | NT | NT | NT | NT | NT | NT | NT | NT | 220 | 104 | 180 | 82 | NT | NT |
| Cadmium cyanide plating solution |  | NT | NT | NT | NT | NT | NT | NT | NT | NR | NR | 150 | 66 | NT | NT |
| Calcium bisulfate |  | NT | NT | NT | NT | NT | NT | 250 | 121 | 250 | 121 | 180 | 82 | 200 | 93 |
| Calcium bisulfite | Sat'd | NR | NR | NR | NR | NR | NR | 100 | 38 | 200 | 93 | 180 | 82 | 180 | 82 |
| Calcium bromide |  | NT | NT | NT | NT | NT | NT | NT | NT | 210 | 99 | 200 | 93 | NT | NT |
| Calcium carbonate | Sat'd | 150 | 66 | 150 | 66 | 205 | 96 | 275 | 135 | 250 | 121 | 150 | 66 | 180 | 82 |
| Calcium chlorate | Sat'd | 180 | 82 | 125 | 52 | 180 | 82 | 200 | 93 | 200 | 93 | 200 | 93 | 200 | 93 |
| Calcium chloride | Sat'd | 210 | 99 | 210 | 99 | 225 | 107 | 275 | 135 | 250 | 121 | 200 | 93 | 200 | 93 |
| Calcium hydroxide | <15\% | NR | NR | NR | NR | 150 | 66 | 225 | 107 | 200 | 93 | 150 | 66 | 180 | 82 |
| Calcium hydroxide | 15 $550 \%$ | NR | NR | NR | NR | 150 | 66 | NT | NT | 200 | 93 | 150 | 66 | 180 | 82 |
| Calcium hydroxide | >50\% | NR | NR | NR | NR | 150 | 66 | NT | NT | 200 | 93 | 175 | 79 | 180 | 82 |
| Calcium hypochlorite | $\leq 10 \%$ | NT | NT | NT | NT | NT | NT | NT | NT | 100 | 38 | $160^{(1)(8)}$ | $71^{1(1)(8)}$ | 160 | 71 |


| Chemical Substance | Concentration | Red Thread HPBondstrand70007000M3000A 2"-6"2400 Conductive |  | $\begin{aligned} & \text { Bondstrand } \\ & \text { 3000A 8"-16" } \end{aligned}$ |  |  | d HP <br> d | $\begin{aligned} & \text { Centricast } \\ & \text { Z-Core } \end{aligned}$ |  | $\begin{aligned} & \text { Centricast } \\ & \text { RB-1520 } \\ & \text { RB-2530 } \end{aligned}$ |  | $\begin{aligned} & \text { Centricast } \\ & \text { CL-1520 } \\ & \text { CL-2030 } \end{aligned}$ |  | $\begin{aligned} & \text { Bondstrand } \\ & 5000 \\ & 5000 \mathrm{M} \end{aligned}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ |
| Calcium hypochlorite | Sat'd | NR | NR | NR | NR | NR | NR | NR | NR | NR | NR | $160^{(1)(8)}$ | $71^{111(8)}$ | 160 | 71 |
| Calcium nitrate | Sat'd | 150 | 66 | 150 | 66 | 205 | 96 | 275 | 135 | 250 | 121 | 200 | 93 | 200 | 93 |
| Calcium phosphate |  | NT | NT | NT | NT | NT | NT | 250 | 121 | 250 | 121 | 180 | 82 | 200 | 93 |
| Calcium sulfate | Sat'd | 200 | 93 | 200 | 93 | 225 | 107 | 275 | 135 | 250 | 121 | 200 | 93 | 200 | 93 |
| Calcium sulfite | Sat'd | NT | NT | NT | NT | NT | NT | 100 | 38 | 225 | 107 | 180 | 82 | NT | NT |
| Cane sugar liquor | Sat'd | 200 | 93 | 200 | 93 | 225 | 107 | 250 | 121 | 225 | 107 | 180 | 82 | NT | NT |
| Capric acid |  | NT | NT | NT | NT | NT | NT | NT | NT | NR | NR | 80 | 27 | NT | NT |
| Caprylic acid | Sat'd | NT | NT | NT | NT | NT | NT | 225 | 107 | NR | NR | 150 | 66 | NT | NT |
| Carbo wax |  | NT | NT | NT | NT | NT | NT | NT | NT | NR | NR | 150 | 66 | NT | NT |
| Carbolic acid |  | See Phenol |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Carbon dioxide, "dry gas" | (1) | 210 | 99 | 210 | 99 | 225 | 107 | 275 | 135 | 250 | 121 | 200 | 93 | 200 | 93 |
| Carbon dioxide, "wet acidic" | (1) | 150 | 66 | 150 | 66 | 150 | 66 | 200 | 93 | 150 | 66 | 150 | 66 | 160 | 71 |
| Carbon disulfide |  | 120 | 49 | 120 | 49 | 120 | 49 | 150 | 66 | (1) | (1) | NR | NR | NR | NR |
| Carbon monoxide |  | NT | NT | NT | NT | NT | NT | 250 | 121 | 250 | 121 | 200 | 93 | 200 | 93 |
| Carbon tetrachloride |  | 150 | 66 | 125 | 52 | 150 | 66 | 175 | 79 | 100 | 38 | 125 | 52 | NR | NR |
| Carbonic acid |  | 150 | 66 | 150 | 66 | 150 | 66 | 200 | 93 | 150 | 66 | 150 | 66 | 160 | 71 |
| Carboxyethyl cellulose | $\leq 10 \%$ | NT | NT | NT | NT | NT | NT | NT | NT | 75 | 24 | 150 | 66 | NT | NT |
| Carboxymethyl cellulose | $\leq 10 \%$ | NT | NT | NT | NT | NT | NT | NT | NT | 75 | 24 | 150 | 66 | NT | NT |
| Cascade detergent in solution |  | NT | NT | NT | NT | NT | NT | NT | NT | 100 | 38 | 180 | 82 | NT | NT |
| Castor oil |  | 210 | 99 | 210 | 99 | 225 | 107 | 250 | 121 | 200 | 93 | 160 | 71 | 75 | 24 |
| Cellosolve |  | NT | NT | NT | NT | NT | NT | 150 | 66 | NR | NR | NR | NR | NT | NT |
| Chlorinated water |  | See Water, chlorinated |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Chlorinated wax |  | NT | NT | NT | NT | NT | NT | 150 | 66 | 75 | 24 | 125 | 52 | NT | NT |
| Chlorine dioxide | <15\% | NT | NT | NT | NT | 150 | 66 | 150 | 66 | 75 | 24 | 150 | 66 | NT | NT |
| Chlorine dioxide | > $15 \%$ | NT | NT | NT | NT | NT | NT | NR | NR | NR | NR | NT | NT | NT | NT |
| Chlorine gas, "dry" ${ }^{(3)}$ |  | NR | NR | NR | NR | NR | NR | NR | NR | 125 | 52 | 200 | 93 | 200 | 93 |
| Chlorine gas, "wet" (3)(1) |  | NR | NR | NR | NR | NR | NR | NR | NR | 100 | 38 | 200 | 93 | 200 | 93 |
| Chlorine liquid |  | NT | NT | NT | NT | NT | NT | NR | NR | NR | NR | NR | NR | NT | NT |
| Chlorine saturated brine ${ }^{(5)}$ |  | NT | NT | NT | NT | NT | NT | 75 | 24 | NR | NR | NT | NT | NT | NT |


| Chemical Substance | Concentration | Red Thread HP <br> Bondstrand 7000 7000M 3000A 2"-6" <br> 2400 Conductive |  | Bondstrand 3000A 8"-16" |  |  | d HP <br> d | $\begin{aligned} & \text { Centricast } \\ & \text { Z-Core } \end{aligned}$ |  | $\begin{aligned} & \text { Centricast } \\ & \text { RB-1520 } \\ & \text { RB-2530 } \end{aligned}$ |  | $\begin{aligned} & \text { Centricast } \\ & \text { CL-1520 } \\ & \text { CL-2030 } \end{aligned}$ |  | $\begin{aligned} & \text { Bondstrand } \\ & 5000 \\ & 5000 \mathrm{M} \end{aligned}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ |
| Chloroacetic acid | <10\% | 100 | 38 | 100 | 38 | 120 | 49 | 150 | 66 | 100 | 38 | 100 | 38 | 100 | 38 |
| Chloroacetic acid | 10 $25 \%$ | NT | NT | NT | NT | NT | NT | 100 | 38 | 100 | 38 | 100 | 38 | 100 | 38 |
| Chloroacetic acid | 25 $550 \%$ | NT | NT | NT | NT | NT | NT | 100 | 38 | NR | NR | 75 | 24 | 100 | 38 |
| Chloroacetic acid, "glacial" |  | NT | NT | NT | NT | NT | NT | 100 | 38 | NR | NR | NR | NR | NT | NT |
| Chlorobenzene |  | $200{ }^{(2)}$ | $93^{(2)}$ | $200{ }^{(2)}$ | $93^{(2)}$ | $200{ }^{(2)}$ | $93^{(2)}$ | 200 | 93 | NT | NT | NR | NR | NR | NR |
| Chloroform |  | NR | NR | NR | NR | NR | NR | 185 | 85 | $100^{(1)}$ | $38{ }^{(1)}$ | NR | NR | NR | NR |
| Chloromethane |  | See Methyl chloride |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Chloropicrin |  | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT |
| Chlorosulfonic acid |  | NR | NR | NR | NR | NR | NR | 75 | 24 | NR | NR | NR | NR | NR | NR |
| Chrome alum |  | NT | NT | NT | NT | NT | NT | 200 | 93 | 200 | 93 | 180 | 82 | 200 | 93 |
| Chromic acid | <5\% | NR | NR | NR | NR | 120 | 49 | 75 | 24 | 120 | 49 | 100 | 38 | 100 | 38 |
| Chromic acid | $5 \leq 10 \%$ | NR | NR | NR | NR | 120 | 49 | 75 | 24 | 100 | 38 | 100 | 38 | 100 | 38 |
| Chromic acid | 10 $\leq 15 \%$ | NR | NR | NR | NR | NR | NR | 75 | 24 | 75 | 24 | 100 | 38 | 100 | 38 |
| Chromic acid | 15 $520 \%$ | NR | NR | NR | NR | NR | NR | NR | NR | 75 | 24 | 100 | 38 | 100 | 38 |
| Chromic acid | >20\% | NR | NR | NR | NR | NR | NR | NR | NR | NR | NR | NR | NR | NR | NR |
| Chromic flouride |  | NT | NT | NT | NT | NT | NT | NT | NT | 75 | 24 | 75 | 24 | NT | NT |
| Chromium plate |  | NT | NT | NT | NT | NT | NT | NT | NT | NR | NR | 100 | 38 | NT | NT |
| Chromium sulfate | Sat'd | NT | NT | NT | NT | NT | NT | 100 | 38 | 125 | 52 | 180 | 82 | NT | NT |
| Cinnamaldehde | <50\% | NT | NT | NT | NT | NT | NT | NT | NT | NR | NR | NR | NR | NT | NT |
| Cinnamic acid | 550\% | NT | NT | NT | NT | NT | NT | NT | NT | NR | NR | 100 | 38 | NT | NT |
| Cinnamyl alcohol | 550\% | NT | NT | NT | NT | NT | NT | NT | NT | NR | NR | NR | NR | NT | NT |
| Citric acid | <15\% | 210 | 99 | 210 | 99 | 225 | 107 | 225 | 107 | 150 | 66 | 150 | 66 | 200 | 93 |
| Citric acid | Sat'd | 210 | 99 | 210 | 99 | 225 | 107 | 225 | 107 | 200 | 93 | 180 | 82 | 200 | 93 |
| Cobalt chloride |  | NT | NT | NT | NT | NT | NT | NT | NT | 200 | 93 | 180 | 82 | NT | NT |
| Coca-Cola, "syrup" |  | 100 | 38 | 100 | 38 | 150 | 66 | NR | NR | NT | NT | NR | NR | NT | NT |
| Coconut oil |  | 200 | 93 | 200 | 93 | 225 | 107 | 275 | 135 | 100 | 38 | 180 | 82 | NT | NT |
| Copper acetate |  | NT | NT | NT | NT | NT | NT | 200 | 93 | NT | NT | NT | NT | 160 | 71 |
| Copper brite plating, "causticcyanide" |  | NT | NT | NT | NT | NT | NT | 100 | 38 | NR | NR | NR | NR | NT | NT |
| Copper carbonate |  | NT | NT | NT | NT | NT | NT | 200 | 93 | NT | NT | NT | NT | NT | NT |
| Copper chloride | Sat'd | 150 | 66 | 150 | 66 | 205 | 96 | 225 | 107 | 250 | 121 | 200 | 93 | 200 | 93 |


| Chemical Substance | Concentration | Red Thread HPBondstrand70007000 M3000 A 2 "-6"2400 Conductive |  | Bondstrand 3000A 8"-16" |  |  | d HP <br> d | Centricast Z-Core |  | $\begin{aligned} & \text { Centricast } \\ & \text { RB-1520 } \\ & \text { RB-2530 } \end{aligned}$ |  | $\begin{aligned} & \text { Centricast } \\ & \text { CL-1520 } \\ & \text { CL-2030 } \end{aligned}$ |  | $\begin{aligned} & \text { Bondstrand } \\ & 5000 \\ & 5000 \mathrm{M} \end{aligned}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ |
| Copper cyanide | Sat'd | 150 | 66 | 150 | 66 | 205 | 96 | 225 | 107 | 140 | 60 | 200 | 93 | 200 | 93 |
| Copper fluoride | Sat'd | NT | NT | NT | NT | 200 | 93 | 225 | 107 | 250 | 121 | 175 | 79 | NT | NT |
| Copper matte dipping bath |  | NT | NT | NT | NT | NT | NT | 200 | 93 | NR | NR | NR | NR | NT | NT |
| Copper nitrate | Sat'd | 150 | 66 | 150 | 66 | 200 | 93 | 210 | 99 | 200 | 93 | 200 | 93 | 200 | 93 |
| Copper pickling bath, "ferric sulfate" | $\leq 10 \%$ | NR | NR | NR | NR | NT | NT | 150 | 66 | NR | NR | 200 | 93 | NT | NT |
| Copper plating solution, "cyanide based" |  | NT | NT | NT | NT | NT | NT | NT | NT | NR | NR | 150 | 66 | NT | NT |
| Copper plating solution, fluoroborate |  | NT | NT | NT | NT | NT | NT | NR | NR | NR | NR | NR | NR | NT | NT |
| Coppersulfate | Sat'd | 150 | 66 | 150 | 66 | 200 | 93 | 250 | 121 | 200 | 93 | 200 | 93 | 210 | 99 |
| Corn oil |  | 200 | 93 | 200 | 93 | 225 | 107 | 275 | 135 | 200 | 93 | 200 | 93 | NT | NT |
| Corn starch, slurry |  | 200 | 93 | 200 | 93 | 225 | 107 | 275 | 135 | NT | NT | NT | NT | NT | NT |
| Corn sugar/syrup |  | 200 | 93 | 200 | 93 | 225 | 107 | 250 | 121 | 220 | 104 | 180 | 82 | NT | NT |
| Cottonseed oil |  | 200 | 93 | 200 | 93 | 225 | 107 | 275 | 135 | 200 | 93 | 210 | 99 | NT | NT |
| Cresol | <5\% | 75 | 24 | 75 | 24 | 120 | 49 | 200 | 93 | NT | NT | NT | NT | NT | NT |
| Cresol | 5 $\leq 10 \%$ | NR | NR | NR | NR | 75 | 24 | 200 | 93 | NT | NT | NT | NT | NT | NT |
| Cresol | > 10\% | NR | NR | NR | NR | NT | NT | 200 | 93 | NT | NT | NT | NT | NT | NT |
| Cresylic acid |  | NR | NR | NR | NR | NR | NR | 100 | 38 | NR | NR | NT | NT | NR | NR |
| Crude oil, "sweet or sour" |  | 210 | 99 | 210 | 99 | 225 | 107 | 275 | 135 | 250 | 121 | 200 | 93 | 200 | 93 |
| Cupric chloride | <50\% | NT | NT | NT | NT | NT | NT | 200 | 93 | NT | NT | NT | NT | NT | NT |
| Cupric fluoride |  | 150 | 66 | 150 | 66 | 200 | 93 | 250 | 121 | 200 | 93 | 180 | 82 | 200 | 93 |
| Cupric nitrate |  | 180 | 82 | 180 | 82 | 220 | 104 | 250 | 121 | 220 | 104 | 180 | 82 | 200 | 93 |
| Cupric sulfate |  | 180 | 82 | 180 | 82 | 220 | 104 | 250 | 121 | 220 | 104 | 180 | 82 | 200 | 93 |
| Cyclohexane |  | NT | NT | NT | NT | NT | NT | 175 | 79 | NR | NR | 110 | 43 | 120 | 49 |
| Cyclohexanol |  | NT | NT | NT | NT | NT | NT | 200 | 93 | NT | NT | NT | NT | NR | NR |
| Cyclohexanone |  | NT | NT | NT | NT | NT | NT | 125 | 52 | NT | NT | NT | NT | NT | NT |
| Decanoic acid |  | NT | NT | NT | NT | NT | NT | NT | NT | NR | NR | 80 | 27 | NT | NT |
| Detergents, "sulfonated" |  | NT | NT | NT | NT | NT | NT | 275 | 135 | 200 | 93 | 150 | 66 | NT | NT |
| Diacetone alcohol |  | NT | NT | NT | NT | NT | NT | NT | NT | 150 | 66 | NR | NR | NR | NR |
| Diallyl phthalate |  | NT | NT | NT | NT | NT | NT | 150 | 66 | NR | NR | 150 | 66 | 150 | 66 |
| Di-ammonium phosphate | $\leq 65 \%$ | NT | NT | NT | NT | NT | NT | 275 | 135 | 150 | 66 | 150 | 66 | NT | NT |


| Chemical Substance | Concentration | Red Thread HP <br> Bondstrand 7000 7000M 3000A 2"-6" 2400 Conductive |  | $\begin{aligned} & \text { Bondstrand } \\ & \text { 3000A 8"-16" } \end{aligned}$ |  |  | d HP <br> d | $\begin{aligned} & \text { Centricast } \\ & \text { Z-Core } \end{aligned}$ |  | $\begin{gathered} \text { Centricast } \\ \text { RB-1520 } \\ \text { RB-2530 } \end{gathered}$ |  | $\begin{gathered} \text { Centricast } \\ \text { CL-1520 } \\ \text { CL-2030 } \end{gathered}$ |  | $\begin{gathered} \text { Bondstrand } \\ 5000 \\ 5000 \mathrm{M} \end{gathered}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ |
| Dibromophenol |  | NT | NT | NT | NT | NT | NT | 100 | 38 | NR | NR | NR | NR | NT | NT |
| Dibutyl carbitol |  | NT | NT | NT | NT | NT | NT | NT | NT | NR | NR | 75 | 24 | NT | NT |
| Dibutyl ether |  | NT | NT | NT | NT | NT | NT | 125 | 52 | NR | NR | 75 | 24 | NT | NT |
| Dibutyl phthalate |  | 120 | 49 | 120 | 49 | 180 | 82 | 200 | 93 | 200 | 93 | 175 | 79 | 180 | 82 |
| Dibutyl sebacate |  | NT | NT | NT | NT | NT | NT | NT | NT | NR | NR | NR | NR | NT | NT |
| Dicalcium phosphate |  | NT | NT | NT | NT | NT | NT | 150 | 66 | 150 | 66 | 120 | 49 | 120 | 49 |
| Dichloroacetaldehyde |  | NT | NT | NT | NT | NT | NT | 100 | 38 | NR | NR | NR | NR | NR | NR |
| Dichloroacetic acid |  | NT | NT | NT | NT | NT | NT | 100 | 38 | NR | NR | NR | NR | NT | NT |
| Dichlorobenzene |  | 150 | 66 | 150 | 66 | 180 | 82 | 180 | 82 | NT | NT | NT | NT | NR | NR |
| Dichloroethane |  | NT | NT | NT | NT | NT | NT | 185 | 85 | NR | NR | NR | NR | NT | NT |
| Dichloroethylene |  | NT | NT | NT | NT | NT | NT | 185 | 85 | 75 | 24 | NR | NR | NR | NR |
| Dichloromethane (methylene chloride) |  | See Methylene chloride |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Dichloromonomethane |  | NT | NT | NT | NT | NT | NT | 125 | 52 | NT | NT | NT | NT | NT | NT |
| Dichloropropane |  | NT | NT | NT | NT | NT | NT | 185 | 85 | NT | NT | NT | NT | NT | NT |
| Dichloropropionic acid |  | NT | NT | NT | NT | NT | NT | NT | NT | NR | NR | NR | NR | NT | NT |
| Diesel fuel/bio-diesel |  | 210 | 99 | 210 | 99 | 225 | 107 | 275 | 135 | 250 | 121 | 180 | 82 | 150 | 66 |
| Diethanolamine |  | NT | NT | NT | NT | NT | NT | 150 | 66 | NR | NR | NR | NR | NR | NR |
| Diethyl benzene |  | NT | NT | NT | NT | NT | NT | 185 | 85 | NT | NT | NT | NT | NT | NT |
| Diethyl carbonate |  | NT | NT | NT | NT | NT | NT | 100 | 38 | NR | NR | NR | NR | NT | NT |
| Diethyl ether |  | NT | NT | NT | NT | NT | NT | 100 | 38 | NR | NR | NR | NR | NR | NR |
| Diethyl ketone |  | NT | NT | NT | NT | NT | NT | 150 | 66 | NR | NR | NR | NR | NR | NR |
| Diethyl sulfate |  | NT | NT | NT | NT | NT | NT | 100 | 38 | NR | NR | NR | NR | NT | NT |
| Diethylamine |  | NR | NR | NR | NR | NR | NR | 100 | 38 | NR | NR | NR | NR | NT | NT |
| Diethylene glycol |  | 210 | 99 | 150 | 66 | 225 | 107 | 275 | 135 | 200 | 93 | 150 | 66 | 180 | 82 |
| Diethylene triamine | <10\% | NR | NR | NR | NR | NR | NR | 120 | 49 | NT | NT | NT | NT | NT | NT |
| Diethylhexyl phosphoric acid, "20\% kerosene" |  | NT | NT | NT | NT | NT | NT | NT | NT | NR | NR | 150 | 66 | NT | NT |
| Diisobutyl phthalate |  | NT | NT | NT | NT | NT | NT | 175 | 79 | NR | NR | 100 | 38 | NT | NT |
| Diisobutylene |  | NT | NT | NT | NT | NT | NT | 225 | 107 | NR | NR | 80 | 27 | NT | NT |
| Diisopropanolamine (DIPA) |  | NT | NT | NT | NT | NT | NT | 120 | 49 | NR | NR | 110 | 43 | NT | NT |


| Chemical Substance | Concentration | Red Thread HPBondstrand70007000 M3000A 2"-6"2400 Conductive |  | $\begin{aligned} & \text { Bondstrand } \\ & \text { 3000A 8"-16" } \end{aligned}$ |  | $\begin{gathered} \text { Green Thread HP } \\ \\ \text { Bondstrand } \\ 2000 \\ 2000 \mathrm{M} \\ 2400 \\ 4000 \end{gathered}$ |  | $\begin{aligned} & \text { Centricast } \\ & \text { Z-Core } \end{aligned}$ |  | $\begin{gathered} \text { Centricast } \\ \text { RB-1520 } \\ \text { RB-2530 } \end{gathered}$ |  | $\begin{gathered} \text { Centricast } \\ \text { CL-1520 } \\ \text { CL-2030 } \end{gathered}$ |  | $\begin{aligned} & \text { Bondstrand } \\ & 5000 \\ & 5000 \mathrm{M} \end{aligned}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ |
| Dimethyl formamide |  | NR | NR | NR | NR | NR | NR | 100 | 38 | NR | NR | NR | NR | NR | NR |
| Dimethyl morpholine |  | NR | NR | NR | NR | NR | NR | 100 | 38 | NR | NR | NR | NR | NT | NT |
| Dimethyl phthalate |  | 150 | 66 | 100 | 38 | 150 | 66 | 175 | 79 | NR | NR | 125 | 52 | 100 | 38 |
| Dimethylamine |  | NR | NR | NR | NR | NR | NR | NR | NR | NR | NR | NR | NR | NR | NR |
| Dioctyl phthalate (DOP) |  | 150 | 66 | 150 | 66 | 150 | 66 | 175 | 79 | NR | NR | 125 | 52 | NT | NT |
| Dioxane |  | NR | NR | NR | NR | 75 | 24 | 125 | 52 | NT | NT | NT | NT | NT | NT |
| Diphenyl ether |  | NT | NT | NT | NT | NT | NT | 120 | 49 | NT | NT | NR | NR | NR | NR |
| Diphenyl oxide |  | NT | NT | NT | NT | NT | NT | NT | NT | NR | NR | NR | NR | NT | NT |
| Dipotassium phosphate | <50\% | NT | NT | NT | NT | NT | NT | NT | NT | 150 | 66 | 100 | 38 | NT | NT |
| Dipropylene glycol |  | 150 | 66 | 150 | 66 | 200 | 93 | 275 | 135 | 200 | 93 | 150 | 66 | 150 | 66 |
| Disodium methyl arsenate |  | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | 100 | 38 | 100 | 38 |
| Disodium phoshate | < $75 \%$ | NT | NT | NT | NT | NT | NT | 150 | 66 | 150 | 66 | 100 | 38 | NT | NT |
| Distillery stillage |  | NT | NT | NT | NT | NT | NT | 175 | 79 | NT | NT | NT | NT | NT | NT |
| Distillery syrup |  | NT | NT | NT | NT | NT | NT | 175 | 79 | NT | NT | NT | NT | NT | NT |
| Divinyl benzene |  | $100^{(2)}$ | $38^{(2)}$ | $100^{(2)}$ | $38^{(2)}$ | $100^{(2)}$ | $38^{(2)}$ | 175 | 79 | NT | NT | NT | NT | NT | NT |
| Dodecanol |  | See Dodecyl alcohol |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Dodecene |  | NT | NT | NT | NT | NT | NT | NT | NT | NR | NR | 100 | 38 | NT | NT |
| Dodecyl alcohol |  | NT | NT | NT | NT | NT | NT | 225 | 107 | NR | NR | 125 | 52 | NT | NT |
| Dodecyl benzene sulfonic acid |  | NT | NT | NT | NT | NT | NT | NT | NT | 75 | 24 | 100 | 38 | NT | NT |
| Dow Latex 2144 |  | NT | NT | NT | NT | NT | NT | 275 | 135 | NT | NT | NT | NT | NT | NT |
| Dow Latex 560 |  | NT | NT | NT | NT | NT | NT | 275 | 135 | NT | NT | NT | NT | NT | NT |
| Dow Latex 700 |  | NT | NT | NT | NT | NT | NT | 275 | 135 | NT | NT | NT | NT | NT | NT |
| DowanolEE |  | 75 | 24 | 75 | 24 | 75 | 24 | 100 | 38 | NT | NT | NT | NT | NT | NT |
| DowanolEM |  | 75 | 24 | 75 | 24 | 75 | 24 | 100 | 38 | NT | NT | NT | NT | NT | NT |
| Dowfax 9N9-Surfactant |  | NT | NT | NT | NT | NT | NT | 100 | 38 | NT | NT | NT | NT | NT | NT |
| Electrosol | $\leq 5 \%$ | NT | NT | NT | NT | NT | NT | 225 | 107 | 100 | 38 | 75 | 24 | NT | NT |
| Epichlorohydrin |  | NT | NT | NT | NT | NT | NT | 100 | 38 | NT | NT | NT | NT | NT | NT |
| Epoxidized soybean oil |  | NT | NT | NT | NT | NT | NT | 275 | 135 | NR | NR | 150 | 66 | NT | NT |
| Esters, "fatty acids" |  | NT | NT | NT | NT | NT | NT | 275 | 135 | 100 | 38 | 150 | 66 | NT | NT |


| Chemical Substance | Concentration | Red Thread HP$\begin{gathered} \text { Bondstrand } \\ 7000 \\ 7000 \mathrm{M} \\ 3000 \mathrm{~A} 2 "-6 " \\ 2400 \text { Conductive } \end{gathered}$ |  | Bondstrand 3000A 8"-16" |  | Gree <br> Bo | d HP <br> nd | $\begin{aligned} & \text { Centricast } \\ & \text { Z-Core } \end{aligned}$ |  | $\begin{gathered} \text { Centricast } \\ \text { RB-1520 } \\ \text { RB-2530 } \end{gathered}$ |  | $\begin{gathered} \text { Centricast } \\ \text { CL-1520 } \\ \text { CL-2030 } \end{gathered}$ |  | $\begin{gathered} \text { Bondstrand } \\ 5000 \\ 5000 \mathrm{M} \end{gathered}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ |
| Ethanol |  | See Ethyl alcohol |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Ethyl acetate |  | 75 | 24 | 75 | 24 | 120 | 49 | 150 | 66 | NT | NT | NT | NT | NR | NR |
| Ethyl acrylate |  | 120 | 49 | 100 | 38 | 120 | 49 | 150 | 66 | NT | NT | NT | NT | NR | NR |
| Ethyl alcohol | $\leq 10 \%$ | NT | NT | NT | NT | NT | NT | 200 | 93 | NT | NT | $120^{(1)}$ | $49^{(1)}$ | 100 | 38 |
| Ethyl alcohol | > 10\% | 120 | 49 | 120 | 49 | 120 | 49 | 175 | 79 | 125 | 52 | $80^{(1)}$ | $27^{(1)}$ | NR | NR |
| Ethyl amines |  | NR | NR | NR | NR | NR | NR | NT | NT | NR | NR | NR | NR | NT | NT |
| Ethyl benzene |  | 120 | 49 | 120 | 49 | 150 | 66 | 185 | 85 | NT | NT | NT | NT | NR | NR |
| Ethyl bromide |  | NT | NT | NT | NT | NT | NT | 100 | 38 | NT | NT | NT | NT | NT | NT |
| Ethyl cellosolve |  | NT | NT | NT | NT | NT | NT | NT | NT | 100 | 38 | NR | NR | NR | NR |
| Ethyl chloride |  | NT | NT | NT | NT | NT | NT | 100 | 38 | 75 | 24 | NR | NR | NR | NR |
| Ethyl ether |  | $120^{(2)}$ | $49^{(2)}$ | $120^{(2)}$ | $49^{(2)}$ | $120{ }^{(2)}$ | $49^{(2)}$ | 120 | 49 | NT | NT | NT | NT | NR | NR |
| Ethyl sulfate |  | NT | NT | NT | NT | NT | NT | 100 | 38 | NT | NT | NT | NT | NT | NT |
| Ethyl tert-butyl ether (ETBE) |  | NT | NT | NT | NT | NT | NT | 150 | 66 | NT | NT | NR | NR | NR | NR |
| Ethylene chlorohydrin |  | 100 | 38 | 100 | 38 | 150 | 66 | 150 | 66 | 150 | 66 | 100 | 38 | 100 | 38 |
| Ethylene diamine |  | NR | NR | NR | NR | NR | NR | 100 | 38 | NR | NR | NR | NR | NR | NR |
| Ethylene dichloride |  | NT | NT | NT | NT | NT | NT | 185 | 85 | NR | NR | NR | NR | NR | NR |
| Ethylene glycol | $\leq 50 \%$ (in water) | 210 | 99 | 210 | 99 | 225 | 107 | 275 | 135 | 200 | 93 | 200 | 93 | 200 | 93 |
| Ethylene glycol | >50\% | 210 | 99 | 210 | 99 | 225 | 107 | 275 | 135 | 200 | 93 | 200 | 93 | 200 | 93 |
| Ethylenediaminetetraacetic acid |  | NT | NT | NT | NT | NT | NT | NT | NT | 75 | 24 | 100 | 38 | NT | NT |
| Eucalyptus oil |  | NT | NT | NT | NT | NT | NT | NT | NT | 150 | 66 | 140 | 60 | NT | NT |
| Fatty acids | Sat'd | 210 | 99 | 210 | 99 | 225 | 107 | 275 | 135 | 200 | 93 | 200 | 93 | 200 | 93 |
| Ferric acetate | Sat'd | NT | NT | NT | NT | NT | NT | NT | NT | 150 | 66 | 160 | 71 | 180 | 82 |
| Ferric chloride | $\leq 20 \%$ | 170 | 77 | 170 | 77 | 220 | 104 | 275 | 135 | 250 | 121 | 200 | 93 | 200 | 93 |
| Ferric chloride | 20 $560 \%$ | 150 | 66 | 150 | 66 | 205 | 96 | 275 | 135 | 250 | 121 | 200 | 93 | 200 | 93 |
| Ferric chloride | Sat'd | 150 | 66 | 150 | 66 | 205 | 96 | 275 | 135 | 250 | 121 | 200 | 93 | NT | NT |
| Ferric nitrate | Sat'd | 150 | 66 | 150 | 66 | 205 | 96 | 275 | 135 | 250 | 121 | 200 | 93 | 200 | 93 |
| Ferric sulfate | Sat'd | 210 | 99 | 210 | 99 | 225 | 107 | 275 | 135 | 200 | 93 | 200 | 93 | 200 | 93 |
| Ferrous chloride | Sat'd | 210 | 99 | 210 | 99 | 225 | 107 | 275 | 135 | 250 | 121 | 200 | 93 | 200 | 93 |
| Ferrous chloride 5\% HCL |  | NT | NT | NT | NT | NT | NT | NT | NT | 210 | 99 | 175 | 79 | NT | NT |
| Ferrous nitrate | Sat'd | NT | NT | NT | NT | NT | NT | 275 | 135 | 200 | 93 | 200 | 93 | 200 | 93 |


| Chemical Substance | Concentration | Red Thread HP <br> Bondstrand 7000 7000M 3000A 2"-6" 2400 Conductive |  | Bondstrand 3000A 8"-16" |  | $\begin{gathered} \text { Green Thread HP } \\ \text { Bondstrand } \\ 2000 \\ 2000 \mathrm{M} \\ 2400 \\ 4000 \end{gathered}$ |  | $\begin{aligned} & \text { Centricast } \\ & \text { Z-Core } \end{aligned}$ |  | $\begin{aligned} & \text { Centricast } \\ & \text { RB-1520 } \\ & \text { RB-2530 } \end{aligned}$ |  | $\begin{aligned} & \text { Centricast } \\ & \text { CL-1520 } \\ & \text { CL-2030 } \end{aligned}$ |  | $\begin{aligned} & \text { Bondstrand } \\ & 5000 \\ & 5000 \mathrm{M} \end{aligned}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ |
| Ferrous sulfate | Sat'd | 210 | 99 | 210 | 99 | 225 | 107 | 275 | 135 | 200 | 93 | 200 | 93 | 200 | 93 |
| Fertilizer (8-8-8) |  | NT | NT | NT | NT | NT | NT | 275 | 135 | NR | NR | 120 | 49 | NT | NT |
| Fertilizer-urea ammonium nitrate |  | NT | NT | NT | NT | NT | NT | 275 | 135 | 75 | 24 | 120 | 49 | NT | NT |
| Fire fighting foam, "ATC" | 3 or 6\% | NR | NR | NR | NR | NT | NT | NT | NT | NT | NT | NR | NR | NR | NR |
| Fire fighting foam, "AFFF" | 3 or 6\% | NR | NR | NR | NR | NT | NT | NT | NT | NT | NT | NR | NR | NR | NR |
| Flue gas, "dry" ${ }^{(1)}$ |  | 210 | 99 | 210 | 99 | 250 | 121 | 300 | 149 | 300 | 149 | 200 | 93 | 200 | 93 |
| Flue gas, "wet" |  | 200 | 93 | 200 | 93 | 235 | 113 | 275 | 135 | 250 | 121 | 180 | 82 | 180 | 82 |
| Fluoboric acid | Sat'd | NR | NR | NR | NR | NR | NR | 75 | 24 | NT | NT | 150 | 66 | 200 | 93 |
| Fluorine gas, "dry" |  | NT | NT | NT | NT | NT | NT | NT | NT | 75 | 24 | 75 | 24 | NT | NT |
| Fluorine gas, "wet" |  | NT | NT | NT | NT | NT | NT | NT | NT | NR | NR | 150 | 66 | NT | NT |
| Fluorobenzene (phenyl fluoride) |  | NT | NT | NT | NT | NT | NT | 180 | 82 | NT | NT | NT | NT | NT | NT |
| Fluoroboric acid |  | NT | NT | NT | NT | NT | NT | NT | NT | 180 | 82 | 150 | 66 | NT | NT |
| Fluosilicic acid | $\leq 10 \%$ | NR | NR | NR | NR | $100{ }^{(2)}$ | $38^{(2)}$ | 125 | 52 | NR | NR | 80 | 27 | NT | NT |
| Fluosilicic acid | 10 $\leq 25 \%$ | NR | NR | NR | NR | $100{ }^{(2)}$ | $38^{(2)}$ | 125 | 52 | NR | NR | 100 | 38 | NT | NT |
| Fluosilicic acid | 25 $37 \%$ | NT | NT | NT | NT | NT | NT | 150 | 66 | NR | NR | NR | NR | NT | NT |
| Formaldehyde | $\leq 37 \%$ | 75 | 24 | 75 | 24 | $120^{(2)}$ | $49^{(2)}$ | 150 | 66 | 75 | 24 | 75 | 24 | 150 | 66 |
| Formaldehyde | 37 $\leq 40 \%$ | NT | NT | NT | NT | NT | NT | 150 | 66 | 75 | 24 | 75 | 24 | 150 | 66 |
| Formaldehyde | Sat'd | NT | NT | NT | NT | NT | NT | 150 | 66 | NR | NR | NR | NR | NT | NT |
| Formic acid | $\leq 10 \%$ | NR | NR | NR | NR | NR | NR | 120 | 49 | 140 | 60 | 100 | 38 | 180 | 82 |
| Formic acid | 10 $\leq 25 \%$ | NR | NR | NR | NR | NR | NR | 120 | 49 | 100 | 38 | 100 | 38 | 120 | 49 |
| Formic acid | $25 \leq 88 \%$ | NR | NR | NR | NR | NR | NR | 120 | 49 | NT | NT | NT | NT | NT | NT |
| Formic acid |  | NR | NR | NR | NR | NR | NR | 100 | 38 | NT | NT | NT | NT | NT | NT |
| Freon 11 |  | 75 | 24 | 75 | 24 | 75 | 24 | 75 | 24 | 150 | 66 | 75 | 24 | NT | NT |
| Freon 12 or 22 (gas or liquid) |  | NR | NR | NR | NR | 75 | 24 | 75 | 24 | 150 | 66 | 75 | 24 | NT | NT |
| Fuel oil |  | 210 | 99 | 210 | 99 | 225 | 107 | 275 | 135 | 175 | 79 | 200 | 93 | 180 | 82 |
| Fumaric acid | $\leq 25 \%$ | NT | NT | NT | NT | NT | NT | NT | NT | 100 | 38 | 100 | 38 | NT | NT |
| Furfural | $\leq 5 \%$ | NR | NR | NR | NR | NR | NR | 150 | 66 | NR | NR | NR | NR | NT | NT |
| Furfural | 5 $\leq 10 \%$ | NR | NR | NR | NR | NR | NR | 125 | 52 | NR | NR | NR | NR | NT | NT |
| Furfural | > $10 \%$ | NR | NR | NR | NR | NR | NR | 100 | 38 | NR | NR | NR | NR | NT | NT |
| Gallic acid | Sat'd | NT | NT | NT | NT | NT | NT | NT | NT | NR | NR | 125 | 52 | NT | NT |


| Chemical Substance | Concentration | Red Thread HP <br> Bondstrand 7000 <br> 7000M <br> 3000A 2"-6" <br> 2400 Conductive |  | Bondstrand 3000A 8"-16" |  | Gree <br> Bo | d HP <br> nd | $\begin{aligned} & \text { Centricast } \\ & \text { Z-Core } \end{aligned}$ |  | $\begin{aligned} & \text { Centricast } \\ & \text { RB-1520 } \\ & \text { RB-2530 } \end{aligned}$ |  | $\begin{gathered} \text { Centricast } \\ \text { CL-1520 } \\ \text { CL-2030 } \end{gathered}$ |  | $\begin{gathered} \text { Bondstrand } \\ 5000 \\ 5000 \mathrm{M} \end{gathered}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ |
| Gas, natural |  | 210 | 99 | 210 | 99 | 225 | 107 | 275 | 135 | 200 | 93 | 200 | 93 | NT | NT |
| Gasoline |  | 210 | 99 | 210 | 99 | 225 | 107 | 250 | 121 | 150 | 66 | NR | NR | 150 | 66 |
| Gasoline/ethanol mixtures |  | 210 | 99 | 210 | 99 | 225 | 107 | 250 | 121 | 225 | 107 | NR | NR | NT | NT |
| Germanium tetrachloride |  | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT |
| Gluconic acid | <50\% | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | 100 | 38 | 100 | 38 |
| Glucose |  | 210 | 99 | 210 | 99 | 225 | 107 | 275 | 135 | 200 | 93 | 200 | 93 | 200 | 93 |
| Glutaric acid | <50\% | NT | NT | NT | NT | NT | NT | 150 | 66 | 75 | 24 | 100 | 38 | NT | NT |
| Gluteraldehyde | <50\% | NT | NT | NT | NT | NT | NT | 150 | 66 | NR | NR | 75 | 24 | NT | NT |
| Glycerine |  | NT | NT | NT | NT | NT | NT | 275 | 135 | 250 | 121 | 200 | 93 | 200 | 93 |
| Glycerine (aq.) |  | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | 180 | 82 | 200 | 93 |
| Glycol ethylene |  | 210 | 99 | 210 | 99 | 225 | 107 | 275 | 135 | 200 | 93 | 200 | 93 | NT | NT |
| Glycolic acid | $\leq 10 \%$ | NR | NR | NR | NR | NR | NR | 100 | 38 | NR | NR | 75 | 24 | NT | NT |
| Glycolic acid | 10 $570 \%$ | NR | NR | NR | NR | NR | NR | 100 | 38 | NR | NR | 75 | 24 | NT | NT |
| Glyconic acid, (gluconic) | -50\% | NT | NT | NT | NT | NT | NT | 120 | 49 | NT | NT | NT | NT | NT | NT |
| Glyoxal | $\leq 40 \%$ | NT | NT | NT | NT | NT | NT | 125 | 52 | NR | NR | 100 | 38 | NT | NT |
| Glyoxal | Sat'd | NT | NT | NT | NT | NT | NT | 120 | 49 | NR | NR | NR | NR | NT | NT |
| Gold plating solultion |  | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT |
| Green liquor |  | 100 | 38 | 100 | 38 | $205^{(2)}$ | $96^{(2)}$ | 225 | 107 | NT | NT | NT | NT | NR | NR |
| Heptane |  | 200 | 93 | 175 | 79 | 200 | 93 | 225 | 107 | 150 | 66 | 150 | 66 | 180 | 82 |
| Hexamethylenetetramine | <40\% | NT | NT | NT | NT | NT | NT | NT | NT | 100 | 38 | 75 | 24 | NT | NT |
| Hexane |  | $150^{(2)}$ | $66^{(2)}$ | $150^{(2)}$ | $66^{(2)}$ | $150^{(2)}$ | $66^{(2)}$ | 175 | 79 | 125 | 52 | 150 | 66 | 120 | 49 |
| Hexylene glycol |  | NT | NT | NT | NT | NT | NT | 250 | 121 | 150 | 66 | 150 | 66 | NT | NT |
| HF, 2.5\% and HCl, 1.5\% |  | NR | NR | NR | NR | NR | NR | NR | NR | NR | NR | NT | NT | NT | NT |
| Hot stack gases |  | NT | NT | NT | NT | NT | NT | 275 | 135 | NT | NT | NT | NT | NT | NT |
| Hydrated lime (calcium hydroxide) |  | 150 | 66 | 150 | 66 | 200 | 93 | 225 | 107 | 200 | 93 | 175 | 79 | NT | NT |
| Hydraulic fluid | $\leq 60 \%$ | 200 | 93 | 200 | 93 | 225 | 107 | 250 | 121 | 200 | 93 | 100 | 38 | 180 | 82 |
| Hydraulic fluid | >60\% | 200 | 93 | 200 | 93 | 225 | 107 | 250 | 121 | 225 | 107 | 170 | 77 | 180 | 82 |
| Hydraulic oils |  | 210 | 99 | 210 | 99 | 225 | 107 | 275 | 135 | 250 | 121 | 200 | 93 | 200 | 93 |
| Hydrazine |  | NT | NT | NT | NT | NT | NT | NR | NR | NR | NR | NR | NR | NR | NR |
| Hydriodic acid | <40\% | NT | NT | NT | NT | NT | NT | NT | NT | NR | NR | NR | NR | NT | NT |


| Chemical Substance | Concentration | Red Thread HP <br> Bondstrand 7000 7000M 3000A 2"-6" 2400 Conductive |  | Bondstrand 3000A 8"-16" |  | $\begin{gathered} \text { Green Thread HP } \\ \text { Bondstrand } \\ 2000 \\ 2000 \mathrm{M} \\ 2400 \\ 4000 \end{gathered}$ |  | $\begin{aligned} & \text { Centricast } \\ & \text { Z-Core } \end{aligned}$ |  | $\begin{aligned} & \text { Centricast } \\ & \text { RB-1520 } \\ & \text { RB-2530 } \end{aligned}$ |  | $\begin{aligned} & \text { Centricast } \\ & \text { CL-1520 } \\ & \text { CL-2030 } \end{aligned}$ |  | $\begin{aligned} & \text { Bondstrand } \\ & 5000 \\ & 5000 \mathrm{M} \end{aligned}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ |
| Hydrobromic acid | <18\% | NR | NR | NR | NR | $75{ }^{(6)}$ | $24^{(6)}$ | 150 | 66 | 150 | 66 | 100 | 38 | 200 | 93 |
| Hydrobromic acid | 18 $48 \%$ | NR | NR | NR | NR | $75{ }^{(6)}$ | $24^{(6)}$ | 100 | 38 | 100 | 38 | 100 | 38 | 160 | 71 |
| Hydrobromic acid | 48 $\leq 62 \%$ | NR | NR | NR | NR | $75{ }^{(6)}$ | $24^{(6)}$ | 100 | 38 | 100 | 38 | NR | NR | NT | NT |
| Hydrochloric acid | $\leq 1 \%$ | 75 | 24 | 75 | 24 | $205{ }^{(6)}$ | $96^{(6)}$ | 200 | 93 | 200 | 93 | 175 | 79 | 200 | 93 |
| Hydrochloric acid | 1 $\leq 10 \%$ | NT | NT | NT | NT | $205{ }^{(6)}$ | $96^{(6)}$ | 200 | 93 | 200 | 93 | 200 | 93 | 200 | 93 |
| Hydrochloric acid ${ }^{(9)}$ | 10 $20 \%$ | NT | NT | NT | NT | 150 | 66 | 200 | 93 | $200{ }^{(1)}$ | $93^{(1)}$ | 175 | 79 | 200 | 93 |
| Hydrochloric acid ${ }^{(9)}$ | 20 $36 \%$ | NR | NR | NR | NR | 100 | 38 | 150 | 66 | $140^{(1)}$ | $60^{(1)}$ | 150 | 66 | 150 | 66 |
| Hydrochloric acid (36.5\% Muriatic) ${ }^{(9)}$ | 37\% | NR | NR | NR | NR | 75 | 24 | 150 | 66 | 140 | 60 | 150 | 66 | 150 | 66 |
| Hydrocyanic acid | <10\% | NR | NR | NR | NR | NR | NR | 100 | 38 | 120 | 49 | 150 | 66 | NT | NT |
| Hydrocyanic acid (Prussic) | Sat'd | NR | NR | NR | NR | NR | NR | 100 | 38 | NT | NT | NT | NT | NT | NT |
| Hydrofluoric acid | $\leq 1 \%$ | NR | NR | NR | NR | NR | NR | 75 | 24 | NR | NR | 150 | 66 | 150 | 66 |
| Hydrofluoric acid | 1 $\leq 5 \%$ | NR | NR | NR | NR | NR | NR | 75 | 24 | NR | NR | 150 | 66 | 120 | 49 |
| Hydrofluoric acid | $5 \leq 10 \%$ | NR | NR | NR | NR | NR | NR | 75 | 24 | NR | NR | 150 | 66 | 100 | 38 |
| Hydrofluoric acid | 10 $20 \%$ | NR | NR | NR | NR | NR | NR | NR | NR | NR | NR | 100 | 38 | NR | NR |
| Hydrofluoric acid | >20\% | NR | NR | NR | NR | NR | NR | NR | NR | NR | NR | NR | NR | NR | NR |
| Hydrofluosilicic acid |  | See Fluosilicic acid |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Hydrogen bromide, gas (wet) |  | NR | NR | NR | NR | NR | NR | NR | NR | NT | NT | NT | NT | NT | NT |
| Hydrogen chloride, gas (dry) ${ }^{(3)}$ |  | 150 | 66 | 150 | 66 | 150 | 66 | 150 | 66 | NT | NT | NT | NT | 150 | 66 |
| Hydrogen chloride, gas (wet) |  | NR | NR | NR | NR | NR | NR | NR | NR | NR | NR | NT | NT | 150 | 66 |
| Hydrogen fluoride, vapor |  | NR | NR | NR | NR | NR | NR | NR | NR | NR | NR | 180 | 82 | NT | NT |
| Hydrogen peroxide | $0 \leq 10 \%$ | NR | NR | NR | NR | NR | NR | 75 | 24 | 75 | 24 | NR | NR | 150 | 66 |
| Hydrogen peroxide | 10 $30 \%$ | NR | NR | NR | NR | NR | NR | 75 | 24 | NR | NR | NR | NR | 100 | 38 |
| Hydrogen sulfide (dry) ${ }^{(3)}$ |  | 150 | 66 | 150 | 66 | 150 | 66 | 150 | 66 | 250 | 121 | 175 | 79 | 180 | 82 |
| Hydrogen sulfide (wet) | Sat'd | 150 | 66 | 150 | 66 | 150 | 66 | 150 | 66 | 250 | 121 | 175 | 79 | 180 | 82 |
| Hydrosulfite bleach |  | NT | NT | NT | NT | NT | NT | NR | NR | NR | NR | 150 | 66 | NT | NT |
| Hydroxyacetic acid |  | See Glycolic acid |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Hypochlorous acid | $\leq 10 \%$ | NR | NR | NR | NR | NR | NR | NR | NR | NR | NR | NR | NR | NT | NT |
| Hypochlorous acid | 10 $\leq 20 \%$ | NR | NR | NR | NR | NR | NR | NR | NR | NR | NR | NR | NR | NT | NT |
| Hypophosphorous acid | <50\% | NT | NT | NT | NT | NT | NT | NT | NT | NR | NR | 120 | 49 | NT | NT |


| Chemical Substance | Concentration | Red Thread HPBondstrand70007000M3000A 2"-6"2400 Conductive |  | $\begin{aligned} & \text { Bondstrand } \\ & \text { 3000A 8"-16" } \end{aligned}$ |  |  | d HP | $\begin{aligned} & \text { Centricast } \\ & \text { Z-Core } \end{aligned}$ |  | $\begin{aligned} & \text { Centricast } \\ & \text { RB-1520 } \\ & \text { RB- } 2530 \end{aligned}$ |  | $\begin{aligned} & \text { Centricast } \\ & \text { CL-1520 } \\ & \text { CL-2030 } \end{aligned}$ |  | $\begin{aligned} & \text { Bondstrand } \\ & 5000 \\ & 5000 \mathrm{M} \end{aligned}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ |
| Iodine, vapor | Sat'd | 120 | 49 | 80 | 27 | 150 | 66 | 200 | 93 | NR | NR | 100 | 38 | 100 | 38 |
| Isobutanol |  | See Isobutyl alcohol |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Isobutyl alcohol | <10\% | 120 | 49 | 120 | 49 | 120 | 49 | 150 | 66 | 100 | 38 | 100 | 38 | 80 | 27 |
| Isobutyric acid | 550\% | NT | NT | NT | NT | NT | NT | NT | NT | 75 | 24 | 100 | 38 | NT | NT |
| Isocaproic acid |  | NT | NT | NT | NT | NT | NT | NT | NT | 100 | 38 | 75 | 24 | NT | NT |
| Isononyl alcohol |  | NT | NT | NT | NT | NT | NT | NT | NT | 125 | 52 | 115 | 46 | NT | NT |
| Isooctyl adipate |  | NT | NT | NT | NT | NT | NT | NT | NT | NR | NR | NR | NR | NT | NT |
| Isooctyl alcohol |  | NT | NT | NT | NT | NT | NT | NT | NT | 125 | 52 | 75 | 24 | NT | NT |
| Isophthalic acid (liquor) |  | NT | NT | NT | NT | NT | NT | 200 | 93 | NT | NT | 180 | 82 | NT | NT |
| Isopropanol |  | See Isopropyl alcohol |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Isopropyl alcohol | <10\% | 120 | 49 | 120 | 49 | 120 | 49 | 175 | 79 | 150 | 66 | NT | NT | 80 | 27 |
| Isopropyl alcohol | > $10 \%$ | 120 | 49 | 120 | 49 | 120 | 49 | 150 | 66 | 120 | 49 | NT | NT | 80 | 27 |
| Isopropyl ether |  | NT | NT | NT | NT | NT | NT | 150 | 66 | NT | NT | NT | NT | NT | NT |
| Isopropyl myristate |  | NT | NT | NT | NT | NT | NT | NT | NT | 200 | 93 | 75 | 24 | NT | NT |
| Isopropyl palmitate |  | NT | NT | NT | NT | NT | NT | 275 | 135 | 200 | 93 | 200 | 93 | NT | NT |
| Itaconic acid | <25\% | NT | NT | NT | NT | NT | NT | NT | NT | 200 | 93 | 120 | 49 | NT | NT |
| Jet fuel (JP-A, JP-8 ...) |  | 150 | 66 | 150 | 66 | 225 | 107 | 275 | 135 | 250 | 121 | 175 | 79 | 180 | 82 |
| Kerosene |  | 210 | 99 | 210 | 99 | 225 | 107 | 275 | 135 | 250 | 121 | 175 | 79 | 175 | 79 |
| Ketones (general) |  | 100 | 38 | 100 | 38 | 120 | 49 | 150 | 66 | NT | NT | NT | NT | NT | NT |
| Lactic acid |  | 200 | 93 | 200 | 93 | 225 | 107 | 275 | 135 | 200 | 93 | 150 | 66 | 200 | 93 |
| Lasso herbicide |  | NT | NT | NT | NT | NT | NT | NT | NT | NR | NR | NR | NR | NT | NT |
| Latex |  | NT | NT | NT | NT | NT | NT | 275 | 135 | 200 | 93 | 120 | 49 | 120 | 49 |
| Lauric acid | Sat'd | 200 | 93 | 200 | 93 | 225 | 107 | 275 | 135 | 200 | 93 | 150 | 66 | 200 | 93 |
| Lauroyl chloride |  | NT | NT | NT | NT | NT | NT | NT | NT | NR | NR | 120 | 49 | NT | NT |
| Lauryl alcohol |  | NT | NT | NT | NT | NT | NT | NT | NT | 250 | 121 | 150 | 66 | 200 | 93 |
| Lauryl chloride |  | NT | NT | NT | NT | NT | NT | 200 | 93 | 100 | 38 | 200 | 93 | NT | NT |
| Lead acetate | Sat'd | 150 | 66 | 150 | 66 | 200 | 93 | 275 | 135 | 250 | 121 | 200 | 93 | 200 | 93 |
| Lead nitrate | Sat'd | NT | NT | NT | NT | NT | NT | 225 | 107 | NT | NT | NT | NT | 200 | 93 |
| Lead plating solution |  | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT |


| Chemical Substance | Concentration | Red Thread HP$\begin{gathered} \text { Bondstrand } \\ 7000 \\ 7000 \mathrm{M} \\ 3000 \mathrm{~A} 2 \text { "-6" } \\ 2400 \text { Conductive } \end{gathered}$ |  | $\begin{aligned} & \text { Bondstrand } \\ & \text { 3000A8"-16" } \end{aligned}$ |  |  | d HP <br> d | $\begin{aligned} & \text { Centricast } \\ & \text { Z-Core } \end{aligned}$ |  | $\begin{aligned} & \text { Centricast } \\ & \text { RB-1520 } \\ & \text { RB-2530 } \end{aligned}$ |  | $\begin{aligned} & \text { Centricast } \\ & \text { CL-1520 } \\ & \text { CL-2030 } \end{aligned}$ |  | $\begin{aligned} & \text { Bondstrand } \\ & 5000 \\ & 5000 \mathrm{M} \end{aligned}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ |
| Levulinic acid |  | NT | NT | NT | NT | NT | NT | 250 | 121 | 200 | 93 | 200 | 93 | 200 | 93 |
| Lime |  | 180 | 82 | 180 | 82 | 200 | 93 | 225 | 107 | 200 | 93 | 180 | 82 | 180 | 82 |
| Lime slurry (abrasive media) | (1) | 180 | 82 | 180 | 82 | 200 | 93 | 275 | 135 | 225 | 107 | 170 | 77 | 180 | 82 |
| Linseed oil |  | 200 | 93 | 200 | 93 | 225 | 107 | 275 | 135 | 225 | 107 | 200 | 93 | 200 | 93 |
| Lithium bromide | Sat'd | NT | NT | NT | NT | NT | NT | 275 | 135 | 100 | 38 | 200 | 93 | NT | NT |
| Lithium carbonate | Sat'd | NT | NT | NT | NT | NT | NT | NT | NT | 140 | 60 | 100 | 38 | NT | NT |
| Lithium chloride | Sat'd | NT | NT | NT | NT | NT | NT | 275 | 135 | 210 | 99 | 200 | 93 | 200 | 93 |
| Lithium hydroxide | Sat'd | NT | NT | NT | NT | NT | NT | 225 | 107 | NT | NT | NT | NT | 120 | 49 |
| Lithium sulfate | Sat'd | NT | NT | NT | NT | NT | NT | 275 | 135 | 100 | 38 | 200 | 93 | NT | NT |
| Lube oil |  | 200 | 93 | 200 | 93 | 225 | 107 | 250 | 121 | 220 | 104 | 180 | 82 | 180 | 82 |
| Magnesium bisulfate | Sat'd | NT | NT | NT | NT | NT | NT | NT | NT | 200 | 93 | 150 | 66 | NT | NT |
| Magnesium bisulfite | Sat'd | NT | NT | NT | NT | NT | NT | 225 | 107 | 100 | 38 | 150 | 66 | NT | NT |
| Magnesium carbonate | Sat'd | 150 | 66 | 150 | 66 | 200 | 93 | 275 | 135 | 250 | 121 | 175 | 79 | 200 | 93 |
| Magnesium chloride | Sat'd | 210 | 99 | 210 | 99 | 225 | 107 | 275 | 135 | 225 | 107 | 200 | 93 | 200 | 93 |
| Magnesium fluosilicate |  | NT | NT | NT | NT | NT | NT | NT | NT | 225 | 107 | 100 | 38 | NT | NT |
| Magnesium hydroxide | Sat'd | 120 | 49 | 120 | 49 | 205 | 96 | 275 | 135 | 250 | 121 | 150 | 66 | 150 | 66 |
| Magnesium nitrate | Sat'd | 210 | 99 | 210 | 99 | 225 | 107 | 275 | 135 | 250 | 121 | 200 | 93 | 160 | 71 |
| Magnesium phosphate |  | NT | NT | NT | NT | NT | NT | NT | NT | 250 | 121 | 150 | 66 | NT | NT |
| Magnesium sulfate | Sat'd | 210 | 99 | 210 | 99 | 225 | 107 | 275 | 135 | 250 | 121 | 200 | 93 | 200 | 93 |
| Maleic acid |  | NT | NT | NT | NT | NT | NT | 175 | 79 | 150 | 66 | 200 | 93 | 200 | 93 |
| Maleic anhydride |  | 150 | 66 | 150 | 66 | 150 | 66 | 175 | 79 | NT | NT | NT | NT | 120 | 49 |
| Manganese chloride | Sat'd | NT | NT | NT | NT | NT | NT | 250 | 121 | 225 | 107 | 180 | 82 | NT | NT |
| Manganese sulfate |  | NT | NT | NT | NT | NT | NT | NT | NT | 225 | 107 | 200 | 93 | NT | NT |
| Mercaptoacetic acid |  | NT | NT | NT | NT | NT | NT | NT | NT | NR | NR | NR | NR | NT | NT |
| Mercuric chloride | Sat'd | 210 | 99 | 210 | 99 | 225 | 107 | 275 | 135 | 150 | 66 | 200 | 93 | 200 | 93 |
| Mercurous chloride | Sat'd | NT | NT | NT | NT | NT | NT | 275 | 135 | 150 | 66 | 200 | 93 | 200 | 93 |
| Mercury |  | NT | NT | NT | NT | NT | NT | NT | NT | 250 | 121 | 200 | 93 | 200 | 93 |
| Methacrylic acid |  | NT | NT | NT | NT | NT | NT | NT | NT | NR | NR | NR | NR | NR | NR |
| Methane |  | 210 | 99 | 210 | 99 | 235 | 113 | 275 | 135 | 150 | 66 | 140 | 60 | 200 | 93 |
| Methanesulfonic acid |  | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT |


| Chemical Substance | Concentration | Red Thread HPBondstrand70007000 M3000A 2"-6"2400 Conductive |  | $\begin{aligned} & \text { Bondstrand } \\ & \text { 3000A 8"-16" } \end{aligned}$ |  | Gree <br> Bo | d HP <br> nd | $\begin{aligned} & \text { Centricast } \\ & \text { Z-Core } \end{aligned}$ |  | $\begin{aligned} & \text { Centricast } \\ & \text { RB-1520 } \\ & \text { RB- } 2530 \end{aligned}$ |  | $\begin{aligned} & \text { Centricast } \\ & \text { CL-1520 } \\ & \text { CL-2030 } \end{aligned}$ |  | $\begin{aligned} & \text { Bondstrand } \\ & 5000 \\ & 5000 \mathrm{M} \end{aligned}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ |
| Methanol |  | See Methyl alcohol |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Methyl acetate |  | 75 | 24 | 75 | 24 | 120 | 49 | 150 | 66 | NT | NT | NT | NT | NT | NT |
| Methyl alcohol | <80\% | 120 | 49 | 100 | 38 | 150 | 66 | 175 | 79 | 100 | 38 | NR | NR | NR | NR |
| Methyl alcohol | >80\% | 100 | 38 | 100 | 38 | 120 | 49 | 150 | 66 | NT | NT | NT | NT | NR | NR |
| Methyl amine |  | NT | NT | NT | NT | NT | NT | NT | NT | NR | NR | NR | NR | NT | NT |
| Methyl chloride |  | NR | NR | NR | NR | NR | NR | 75 | 24 | NR | NR | NR | NR | NT | NT |
| Methyl ester |  | 75 | 24 | 75 | 24 | 120 | 49 | 100 | 38 | NT | NT | NT | NT | NT | NT |
| Methyl ethyl ketone | <5\% | 120 | 49 | 75 | 24 | 150 | 66 | 175 | 79 | 100 | 38 | NR | NR | NR | NR |
| Methyl ethyl ketone | > 5\% | 100 | 38 | 80 | 27 | 150 | 66 | 175 | 79 | NT | NT | NR | NR | NR | NR |
| Methyl isobutyl alcohol |  | 150 | 66 | 170 | 77 | 180 | 82 | 200 | 93 | 180 | 82 | 120 | 49 | 120 | 49 |
| Methyl isobutyl carbitol |  | NT | NT | NT | NT | NT | NT | 150 | 66 | 100 | 38 | NR | NR | NR | NR |
| Methyl isobutyl ketone |  | 120 | 49 | 120 | 49 | 150 | 66 | 175 | 79 | 150 | 66 | NR | NR | NR | NR |
| Methyl methacrylate |  | NT | NT | 75 | 24 | 100 | 38 | 100 | 38 | NT | NT | NR | NR | NR | NR |
| Methyl propyl ketone |  | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT |
| Methyl styrene |  | 120 | 49 | 120 | 49 | 150 | 66 | 175 | 79 | NT | NT | NT | NT | NT | NT |
| Methyl tert-butyl ether (MTBE) |  | 100 | 38 | 100 | 38 | 120 | 49 | 120 | 49 | 100 | 38 | NR | NR | NR | NR |
| Methylene chloride | (1) | NR | NR | NR | NR | NR | NR | 100 | 38 | NR | NR | NR | NR | NR | NR |
| Mineral oil |  | 210 | 99 | 210 | 99 | 225 | 107 | 275 | 135 | 250 | 121 | 200 | 93 | 200 | 93 |
| Mineral spirits |  | NT | NT | NT | NT | NT | NT | 275 | 135 | NT | NT | NT | NT | NT | NT |
| Monochloro acetic acid |  | NR | NR | NR | NR | NR | NR | 100 | 38 | NR | NR | NR | NR | NT | NT |
| Monochlorobenzene, "MCB" |  | $75^{(2)}$ | $75^{(2)}$ | $75^{(2)}$ | $24^{(2)}$ | $100^{(2)}$ | $38^{(2)}$ | 200 | 93 | NT | NT | NT | NT | NT | NT |
| Monoethanolamine |  | NT | NT | NT | NT | NT | NT | 150 | 66 | NR | NR | NR | NR | NT | NT |
| Motor oil |  | 210 | 99 | 210 | 99 | 225 | 107 | 275 | 135 | 250 | 121 | 200 | 93 | 200 | 93 |
| Muriatic acid |  |  |  |  |  |  |  | See H | ric aci |  |  |  |  |  |  |
| Myristic acid |  | NT | NT | NT | NT | NT | NT | 250 | 121 | 150 | 66 | 175 | 79 | NT | NT |
| Naphtha |  | 210 | 99 | 210 | 99 | 225 | 107 | 275 | 135 | 200 | 93 | 175 | 79 | 180 | 82 |
| Naphthalene |  | 200 | 93 | 200 | 93 | 200 | 93 | 225 | 107 | 150 | 66 | 100 | 38 | 200 | 93 |
| Natural gas |  | 210 | 99 | 210 | 99 | 235 | 113 | 275 | 135 | 150 | 66 | 140 | 60 | 200 | 93 |
| n-dibutylamine |  | NT | NT | NT | NT | NT | NT | 100 | 38 | NT | NT | NT | NT | NT | NT |


| Chemical Substance | Concentration | Red Thread HPBondstrand70007000 M3000A 2"-6"2400 Conductive |  | $\begin{aligned} & \text { Bondstrand } \\ & \text { 3000A 8"-16" } \end{aligned}$ |  | $\begin{gathered} \text { Green Thread HP } \\ \text { Bondstrand } \\ 2000 \\ 2000 \mathrm{M} \\ 2400 \\ 4000 \end{gathered}$ |  | $\begin{aligned} & \text { Centricast } \\ & \text { Z-Core } \end{aligned}$ |  | $\begin{aligned} & \text { Centricast } \\ & \text { RB-1520 } \\ & \text { RB- } 2530 \end{aligned}$ |  | $\begin{aligned} & \text { Centricast } \\ & \text { CL-1520 } \\ & \text { CL-2030 } \end{aligned}$ |  | $\begin{aligned} & \text { Bondstrand } \\ & 5000 \\ & 5000 \mathrm{M} \end{aligned}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ |
| Nickel chloride | Sat'd | 210 | 99 | 210 | 99 | 225 | 107 | 275 | 135 | 250 | 121 | 200 | 93 | 200 | 93 |
| Nickel nitrate | Sat'd | 210 | 99 | 210 | 99 | 225 | 107 | 275 | 135 | 200 | 93 | 200 | 93 | 200 | 93 |
| Nickel plating |  | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT |
| Nickel sulfate | Sat'd | 210 | 99 | 210 | 99 | 225 | 107 | 275 | 135 | 225 | 107 | 200 | 93 | 200 | 93 |
| n-Isopropyl acetate |  | NT | NT | NT | NT | NT | NT | 150 | 66 | NT | NT | NR | NR | NR | NR |
| Nitric acid ${ }^{(7)}$ | $\leq 1 \%$ | 75 | 24 | 75 | 24 | $120^{(6)}$ | $49^{(6)}$ | 150 | 66 | 120 | 49 | 150 | 66 | 150 | 66 |
| Nitric acid | 1 $\leq 5 \%$ | 75 | 24 | 75 | 24 | $100{ }^{(6)}$ | $38^{(6)}$ | 150 | 66 | 120 | 49 | 150 | 66 | 150 | 66 |
| Nitric acid | $5 \leq 10 \%$ | 75 | 24 | 75 | 24 | $100{ }^{(6)}$ | $38^{(6)}$ | 120 | 49 | 120 | 49 | 125 | 52 | 120 | 49 |
| Nitric acid | 10 $20 \%$ | NR | NR | NR | NR | $75^{(6)}$ | $24^{(6)}$ | 75 | 24 | NR | NR | NR | NR | 120 | 49 |
| Nitric acid | 20 $25 \%$ | NR | NR | NR | NR | $75^{(6)}$ | $24^{(6)}$ | 75 | 24 | NR | NR | NR | NR | 100 | 38 |
| Nitric acid | >25\% | NR | NR | NR | NR | NR | NR | NR | NR | NR | NR | NR | NR | NR | NR |
| Nitrilotriacetic acid, "NTA" |  | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT |
| Nitrobenzene |  | NT | NT | NT | NT | NT | NT | 200 | 93 | NR | NR | NR | NR | NT | NT |
| Nitrogen solutions |  | NT | NT | NT | NT | NT | NT | 150 | 66 | NT | NT | 100 | 38 | 100 | 38 |
| n-lauryl alcohol |  | See Lauryl alcohol |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Oakite rust stripper |  | NT | NT | NT | NT | NT | NT | 150 | 66 | 150 | 66 | 100 | 38 | NT | NT |
| Octanoic acid | Sat'd | See Caprylic acid |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Oil sweet crude |  | See Crude oil (sweet or sour) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Oil, lubricating |  | See Lube oil |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Oil, sour crude |  | See Crude oil (sweet or sour) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Oleic acid |  | 200 | 93 | 200 | 93 | 225 | 107 | 275 | 135 | 200 | 93 | 100 | 38 | 200 | 93 |
| Oleum |  | See Sulfuric acid, fuming |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Olive oil |  | 210 | 99 | 210 | 99 | 225 | 107 | 275 | 135 | 200 | 93 | 200 | 93 | 200 | 93 |
| Orange juice |  | 200 | 93 | 200 | 93 | 225 | 107 | 275 | 135 | 250 | 121 | 180 | 82 | 180 | 82 |
| Ortho benzoyl benzoic acid |  | NT | NT | NT | NT | NT | NT | 100 | 38 | 200 | 93 | 200 | 93 | NT | NT |
| Ortho-dichloro benzene, "ODB" | $\leq 10 \%$ | 120 | 49 | 120 | 49 | 150 | 66 | 200 | 93 | NT | NT | NT | NT | NT | NT |
| Oxalic acid | Sat'd | NT | NT | NT | NT | NT | NT | 225 | 107 | 200 | 93 | 200 | 93 | NT | NT |
| Ozone | $\leq 35 \mathrm{ppm}$ | NR | NR | NT | NT | 150 | 66 | (1) | (1) | (1) | (1) | (1) | ${ }^{(1)}$ | NT | NT |
| Ozone | $35 \leq 300 \mathrm{ppm}$ | NR | NR | NT | NT | NR | NR | (1) | (1) | (1) | (1) | (1) | (1) | NT | NT |
| Palmitic acid |  | NT | NT | NT | NT | NT | NT | NT | NT | 150 | 66 | 100 | 38 | 200 | 93 |


| Chemical Substance | Concentration | Red Thread HP$\begin{gathered} \text { Bondstrand } \\ 7000 \\ 7000 \mathrm{M} \\ \text { 3000A 2"-6" } \\ \text { 2400 Conductive } \end{gathered}$ |  | Bondstrand 3000A 8"-16" |  | Green <br> Bo | ad HP <br> nd | $\begin{aligned} & \text { Centricast } \\ & \text { Z-Core } \end{aligned}$ |  | $\begin{aligned} & \text { Centricast } \\ & \text { RB-1520 } \\ & \text { RB-2530 } \end{aligned}$ |  | $\begin{gathered} \text { Centricast } \\ \text { CL-1520 } \\ \text { CL-2030 } \end{gathered}$ |  | $\begin{aligned} & \text { Bondstrand } \\ & 5000 \\ & 5000 \mathrm{M} \end{aligned}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ |
| Perchloric acid | $\leq 10 \%$ | NT | NT | NT | NT | NT | NT | NT | NT | 75 | 24 | 150 | 66 | NT | NT |
| Perchloric acid | 10 $\leq 30 \%$ | NT | NT | NT | NT | NT | NT | NT | NT | 75 | 24 | 75 | 24 | NT | NT |
| Perchloroethylene |  | 150 | 66 | 100 | 38 | $150{ }^{(2)}$ | $66^{(2)}$ | 150 | 66 | 120 | 49 | 75 | 24 | NR | NR |
| Petroleum ether |  | NT | NT | NT | NT | NT | NT | 125 | 52 | NT | NT | NR | NR | NR | NR |
| Phenol | $\leq 1 \%$ | 100 | 38 | 100 | 38 | $150{ }^{(6)}$ | $66^{(6)}$ | 175 | 79 | 150 | 66 | NR | NR | NR | NR |
| Phenol | 1 $55 \%$ | 100 | 38 | 100 | 38 | $150{ }^{(6)}$ | $66^{(6)}$ | 175 | 79 | NR | NR | NR | NR | NR | NR |
| Phenol | 5 $\leq 88 \%$ | NR | NR | NR | NR | NR | NR | $100^{(1)}$ | $38^{(1)}$ | NR | NR | NR | NR | NR | NR |
| Phenol sulfonic acid | 1 $\leq 5 \%$ | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | 200 | 93 | NT | NT |
| Phosphoric acid ${ }^{(7)}$ | $\leq 2 \%$ | 150 | 66 | 100 | 38 | $225{ }^{(6)}$ | $107{ }^{(6)}$ | 200 | 93 | 100 | 38 | 200 | 93 | 200 | 93 |
| Phosphoric acid | 2 $\leq 25 \%$ | 150 | 66 | 75 | 24 | $150{ }^{(6)}$ | $66^{(6)}$ | 150 | 66 | 100 | 38 | 200 | 93 | 200 | 93 |
| Phosphoric acid | 25 $550 \%$ | 150 | 66 | 75 | 24 | $150{ }^{(6)}$ | $66^{(6)}$ | 75 | 24 | 75 | 24 | 200 | 93 | 200 | 93 |
| Phosphoric acid | 50 $\leq 85 \%$ | NT | NT | NT | NT | $75{ }^{(6)}$ | $24^{(6)}$ | NR | NR | NR | NR | 175 | 79 | 200 | 93 |
| Phosphorus oxychloride |  | NR | NR | NR | NR | NR | NR | NR | NR | NR | NR | NR | NR | NR | NR |
| Phosphorus pentoxide | 554\% | NT | NT | NT | NT | NT | NT | NT | NT | 100 | 38 | 200 | 93 | NT | NT |
| Phosphorus trichloride |  | NT | NT | NT | NT | NT | NT | NT | NT | NR | NR | NR | NR | NT | NT |
| Phthalic acid |  | NT | NT | NT | NT | NT | NT | NT | NT | NR | NR | 200 | 93 | NT | NT |
| Phthalic anhydride |  | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | 150 | 66 | 200 | 93 |
| Pickling acid (5\% H2SO4, 0.25\% coal, coal tar inhibitor, water) |  | NT | NT | NT | NT | NT | NT | 150 | 66 | 100 | 38 | 200 | 93 | 200 | 93 |
| Picric acid, alcoholic | 510\% | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NR | NR | 100 | 38 |
| Picric acid | Sat'd | NT | NT | NT | NT | NT | NT | 100 | 38 | NT | NT | NT | NT | 100 | 38 |
| Pine oil |  | NT | NT | NT | NT | NT | NT | NT | NT | 200 | 93 | NR | NR | 150 | 66 |
| Plating solution ( $17 \%$ NiSO4, $5 \%$ NiCl2, 30\% H3BO3, water) |  | 120 | 49 | 120 | 49 | 200 | 93 | 220 | 104 | 200 | 93 | 180 | 82 | 180 | 82 |
| Polyethylene glycol (E-200) |  | 120 | 49 | 120 | 49 | 150 | 66 | 180 | 82 | 150 | 66 | 150 | 66 | 150 | 66 |
| Polyethylene glycol (P-400) |  | 150 | 66 | 150 | 66 | 150 | 66 | 180 | 82 | 150 | 66 | 150 | 66 | 150 | 66 |
| Polyethyleneimine, 10\% |  | NT | NT | NT | NT | NT | NT | NT | NT | NR | NR | 100 | 38 | NT | NT |
| Polyvinyl acetate adhesives |  | NT | NT | NT | NT | NT | NT | NT | NT | 150 | 66 | 120 | 49 | NT | NT |
| Polyvinyl acetate emulsion |  | 100 | 38 | 100 | 38 | 150 | 66 | 150 | 66 | 150 | 66 | 100 | 38 | 100 | 38 |
| Polyvinyl acetate latex, "PVCa" |  | 210 | 99 | 210 | 99 | 225 | 107 | 250 | 121 | 150 | 66 | 100 | 38 | NT | NT |
| Polyvinyl alcohol, "PVA" |  | 150 | 66 | 150 | 66 | 150 | 66 | 175 | 79 | 100 | 38 | 100 | 38 | NT | NT |


| Chemical Substance | Concentration | Red Thread HP$\begin{gathered} \text { Bondstrand } \\ 7000 \\ 7000 \mathrm{M} \\ \text { 3000A 2"-6" } \\ 2400 \text { Conductive } \end{gathered}$ |  | Bondstrand 3000A 8"-16" |  |  | d HP <br> d | $\begin{aligned} & \text { Centricast } \\ & \text { Z-Core } \end{aligned}$ |  | $\begin{aligned} & \text { Centricast } \\ & \text { RB-1520 } \\ & \text { RB-2530 } \end{aligned}$ |  | $\begin{aligned} & \text { Centricast } \\ & \text { CL-1520 } \\ & \text { CL-2030 } \end{aligned}$ |  | $\begin{aligned} & \text { Bondstrand } \\ & 5000 \\ & 5000 \mathrm{M} \end{aligned}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ |
| Polyvinyl chloride latex w/ 35 parts DOP |  | NR | NR | NR | NR | NR | NR | NT | NT | NR | NR | 120 | 49 | NT | NT |
| Potash |  | See Potassium hydroxide |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Potassium alum sulfate | Sat'd | NT | NT | NT | NT | NT | NT | 275 | 135 | 120 | 49 | 200 | 93 | NT | NT |
| Potassium bicarbonate | 550\% | 150 | 66 | 150 | 66 | 200 | 93 | 225 | 107 | 225 | 107 | 150 | 66 | 150 | 66 |
| Potassium bicarbonate | >50\% | NT | NT | NT | NT | NT | NT | NT | NT | 225 | 107 | 100 | 38 | 150 | 66 |
| Potassium bromide | Sat'd | 210 | 99 | 200 | 93 | 225 | 107 | 275 | 135 | 200 | 93 | 100 | 38 | 200 | 93 |
| Potassium carbonate | $\leq 14 \%$ | 200 | 93 | 100 | 38 | 205 | 96 | 275 | 135 | 250 | 121 | 150 | 66 | 150 | 66 |
| Potassium carbonate | 14<50\% | 150 | 66 | 100 | 38 | 205 | 96 | 275 | 135 | 250 | 121 | 150 | 66 | 150 | 66 |
| Potassium carbonate | >50\% | 150 | 66 | 100 | 38 | 205 | 96 | 275 | 135 | 250 | 121 | 150 | 66 | 150 | 66 |
| Potassium chloride | Sat'd | 210 | 99 | 210 | 99 | 225 | 107 | 275 | 135 | 250 | 121 | 200 | 93 | 200 | 93 |
| Potassium cyanide | $\leq 5 \%$ | 210 | 99 | 210 | 99 | 225 | 107 | 275 | 135 | NT | NT | NT | NT | 180 | 82 |
| Potassium dichromate | <10\% | 150 | 66 | 150 | 66 | 200 | 93 | 250 | 121 | 250 | 121 | 200 | 93 | 210 | 99 |
| Potassium dichromate | Sat'd | NT | NT | NT | NT | NT | NT | NT | NT | 250 | 121 | 200 | 93 | 210 | 99 |
| Potassium ferricyanide | Sat'd | 200 | 93 | 200 | 93 | 225 | 107 | 275 | 135 | 250 | 121 | 200 | 93 | 200 | 93 |
| Potassium ferrocyanide | Sat'd | 200 | 93 | 200 | 93 | 225 | 107 | 275 | 135 | 225 | 107 | 200 | 93 | 200 | 93 |
| Potassium fluoride | <30\% | NT | NT | NT | NT | NT | NT | 150 | 66 | NT | NT | NT | NT | 150 | 66 |
| Potassium gold cyanide | $\leq 12 \%$ | NT | NT | NT | NT | NT | NT | NT | NT | 225 | 107 | 100 | 38 | NT | NT |
| Potassium hydroxide | $\leq 25 \%$ | 100 | 38 | 100 | 38 | 150 | 66 | 240 | 116 | 200 | 93 | 125 | 52 | 120 | 49 |
| Potassium hydroxide | 25 5 50\% | 100 | 38 | 100 | 38 | 150 | 66 | 240 | 116 | 200 | 93 | 125 | 52 | 100 | 38 |
| Potassium hydroxide | 50 $575 \%$ | 100 | 38 | 100 | 38 | 150 | 66 | 225 | 107 | NT | NT | NT | NT | 100 | 38 |
| Potassium hypochlorite |  | NT | NT | NT | NT | NT | NT | NR | NR | NR | NR | (12)(8) | (1)(8) | NT | NT |
| Potassium iodide |  | NT | NT | NT | NT | NT | NT | NT | NT | 225 | 107 | 120 | 49 | NT | NT |
| Potassium nitrate | Sat'd | 200 | 93 | 200 | 93 | 225 | 107 | 275 | 135 | 250 | 121 | 200 | 93 | 200 | 93 |
| Potassium permanganate |  | NR | NR | NR | NR | NR | NR | NR | NR | NR | NR | 100 | 38 | 100 | 38 |
| Potassium persulfate | Sat'd | NT | NT | NT | NT | NT | NT | NT | NT | 225 | 107 | 200 | 93 | 180 | 82 |
| Potassium phosphate |  | NT | NT | NT | NT | NT | NT | 200 | 93 | 180 | 82 | 100 | 38 | 100 | 38 |
| Potassium pyrophosphate | <60\% | NT | NT | NT | NT | NT | NT | NT | NT | 225 | 107 | 135 | 57 | NT | NT |
| Potassium sulfate | Sat'd | 210 | 99 | 210 | 99 | 225 | 107 | 275 | 135 | 225 | 107 | 200 | 93 | 180 | 82 |
| Propane |  | $75^{(2)}$ | $24^{(2)}$ | $75^{(2)}$ | $24^{(2)}$ | $75^{(2)}$ | $24^{(2)}$ | 100 | 38 | 150 | 66 | 200 | 93 | 100 | 38 |


| Chemical Substance | Concentration | Red Thread HP <br> Bondstrand 7000 7000M 3000A 2"-6" 2400 Conductive |  | Bondstrand 3000A 8"-16" |  |  | d HP <br> d | $\begin{aligned} & \text { Centricast } \\ & \text { Z-Core } \end{aligned}$ |  | $\begin{aligned} & \text { Centricast } \\ & \text { RB-1520 } \\ & \text { RB-2530 } \end{aligned}$ |  | $\begin{aligned} & \text { Centricast } \\ & \text { CL-1520 } \\ & \text { CL-2030 } \end{aligned}$ |  | $\begin{aligned} & \text { Bondstrand } \\ & 5000 \\ & 5000 \mathrm{M} \end{aligned}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ |
| Propionic acid | $\leq 20 \%$ | NT | NT | NT | NT | NT | NT | 120 | 49 | 100 | 38 | 150 | 66 | NT | NT |
| Propionic acid | 20 5 50\% | NT | NT | NT | NT | NT | NT | 120 | 49 | 100 | 38 | NR | NR | NT | NT |
| Propionic acid | >50\% | NT | NT | NT | NT | NT | NT | 100 | 38 | 100 | 38 | NR | NR | NT | NT |
| Propylene glycol |  | 210 | 99 | 210 | 99 | 225 | 107 | 275 | 135 | 200 | 93 | 200 | 93 | 200 | 93 |
| Prussic acid |  | See Hydrocyanic acid |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Pyridine |  | NT | NT | NT | NT | NT | NT | 125 | 52 | NT | NT | NT | NT | NT | NT |
| Quatenary ammonium salts |  | NT | NT | NT | NT | NT | NT | 150 | 66 | 120 | 49 | 100 | 38 | 100 | 38 |
| Rayon spin bath |  | NT | NT | NT | NT | NT | NT | NT | NT | NR | NR | NR | NR | NT | NT |
| Red liquor |  | NT | NT | NT | NT | NT | NT | NT | NT | NR | NR | 100 | 38 | NT | NT |
| Salicylic acid | Sat'd | NT | NT | NT | NT | NT | NT | NT | NT | 125 | 52 | 125 | 52 | NT | NT |
| Sebacic acid | Sat'd | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT |
| Selenious acid | Sat'd | NT | NT | NT | NT | NT | NT | NT | NT | NR | NR | 200 | 93 | NT | NT |
| Silicic acid |  | NT | NT | NT | NT | NT | NT | NT | NT | 200 | 93 | 125 | 52 | NT | NT |
| Silver nitrate | Sat'd | 150 | 66 | 150 | 66 | 225 | 107 | 275 | 135 | 250 | 121 | 200 | 93 | 200 | 93 |
| Silver plating solution |  | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT |
| Soaps |  | 200 | 93 | 200 | 93 | 225 | 107 | 275 | 135 | 250 | 121 | 200 | 93 | NT | NT |
| Sodium acetate | Sat'd | 150 | 66 | 150 | 66 | 205 | 96 | 225 | 107 | 250 | 121 | 200 | 93 | 200 | 93 |
| Sodium alkyl aryl sulfonates |  | NT | NT | NT | NT | NT | NT | 225 | 107 | 125 | 52 | 150 | 66 | NT | NT |
| Sodium aluminate | Sat'd | 150 | 66 | 150 | 66 | 205 | 96 | 225 | 107 | 200 | 93 | 120 | 49 | NT | NT |
| Sodium aluminum sulfate |  | NT | NT | NT | NT | NT | NT | 275 | 135 | 250 | 121 | 180 | 82 | 200 | 93 |
| Sodium benzoate | Sat'd | 180 | 82 | 180 | 82 | 200 | 93 | 250 | 121 | 250 | 121 | 150 | 66 | 180 | 82 |
| Sodium bicarbonate | $\leq 10 \%$ | 180 | 82 | 180 | 82 | 225 | 107 | 275 | 135 | 250 | 121 | 150 | 66 | 180 | 82 |
| Sodium bicarbonate | 10 $\leq 20 \%$ | 180 | 82 | 180 | 82 | 225 | 107 | 275 | 135 | 250 | 121 | 150 | 66 | 150 | 66 |
| Sodium bicarbonate | Sat'd | 180 | 82 | 180 | 82 | 205 | 96 | 275 | 135 | 250 | 121 | 150 | 66 | NT | NT |
| Sodium bifluoride | Sat'd | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT |
| Sodium bisulfate | Sat'd | 150 | 66 | 150 | 66 | 205 | 96 | 225 | 107 | 250 | 121 | 200 | 93 | 200 | 93 |
| Sodium bisulfite | Sat'd | 200 | 93 | 200 | 93 | 205 | 96 | 250 | 121 | 250 | 121 | 200 | 93 | 200 | 93 |
| Sodium borate | Sat'd | NT | NT | NT | NT | NT | NT | 250 | 121 | 225 | 107 | 200 | 93 | NT | NT |
| Sodium bromate | $\leq 10 \%$ | NT | NT | NT | NT | NT | NT | 125 | 52 | 125 | 52 | 140 | 60 | NT | NT |
| Sodium bromide | Sat'd | 210 | 99 | 210 | 99 | 225 | 107 | 275 | 135 | 200 | 93 | 200 | 93 | 200 | 93 |


| Chemical Substance | Concentration | Red Thread HPBondstrand70007000 M3000A 2"-6"2400 Conductive |  | $\begin{aligned} & \text { Bondstrand } \\ & \text { 3000A 8"-16" } \end{aligned}$ |  | Green <br> Bo | d HP <br> nd | $\begin{aligned} & \text { Centricast } \\ & \text { Z-Core } \end{aligned}$ |  | $\begin{aligned} & \text { Centricast } \\ & \text { RB-1520 } \\ & \text { RB- } 2530 \end{aligned}$ |  | $\begin{aligned} & \text { Centricast } \\ & \text { CL-1520 } \\ & \text { CL-2030 } \end{aligned}$ |  | $\begin{aligned} & \text { Bondstrand } \\ & 5000 \\ & 5000 \mathrm{M} \end{aligned}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ |
| Sodium carbonate | <10\% | 200 | 93 | 200 | 93 | 205 | 96 | 225 | 107 | 250 | 121 | 150 | 66 | 180 | 82 |
| Sodium carbonate | 10 $25 \%$ | 200 | 93 | 200 | 93 | 205 | 96 | 225 | 107 | 250 | 121 | NT | NT | 160 | 71 |
| Sodium carbonate | 25 $50 \%$ | 200 | 93 | 200 | 93 | 205 | 96 | 225 | 107 | 250 | 121 | NT | NT | 160 | 71 |
| Sodium chlorate | <50\% | 210 | 99 | 200 | 93 | 225 | 107 | 200 | 93 | 225 | 107 | 200 | 93 | 180 | 82 |
| Sodium chlorate | Sat'd | 180 | 82 | 180 | 82 | 180 | 82 | 200 | 93 | 225 | 107 | 200 | 93 | NT | NT |
| Sodium chloride | Sat'd | 205 | 96 | 205 | 96 | 225 | 107 | 275 | 135 | 250 | 121 | 200 | 93 | 200 | 93 |
| Sodium chlorite | $\leq 25 \%$ | NT | NT | NT | NT | NT | NT | NT | NT | 125 | 52 | 100 | 38 | NT | NT |
| Sodium chlorite | Sat'd | NR | NR | NR | NR | NR | NR | NT | NT | NT | NT | NT | NT | NT | NT |
| Sodium chloroacetate |  | NT | NT | NT | NT | NT | NT | NT | NT | NR | NR | 100 | 38 | NT | NT |
| Sodium chromate | Sat'd | NT | NT | NT | NT | NT | NT | NT | NT | 150 | 66 | 200 | 93 | NT | NT |
| Sodium cyanide | <6\% | NT | NT | NT | NT | NT | NT | 250 | 121 | 250 | 121 | 200 | 93 | 200 | 93 |
| Sodium cyanide | Sat'd | NT | NT | NT | NT | NT | NT | NT | NT | 250 | 121 | 200 | 93 | 200 | 93 |
| Sodium dichromate | $\leq 10 \%$ | 180 | 82 | 180 | 82 | 200 | 93 | NT | NT | 250 | 121 | 200 | 93 | 200 | 93 |
| Sodium dichromate | Sat'd | NT | NT | NT | NT | NT | NT | NT | NT | 250 | 121 | 200 | 93 | NT | NT |
| Sodium diphosphate |  | NT | NT | NT | NT | NT | NT | NT | NT | 210 | 99 | 200 | 93 | NT | NT |
| Sodium dodecylbenzenesulfonate |  | NT | NT | NT | NT | NT | NT | NT | NT | 175 | 79 | 160 | 71 | NT | NT |
| Sodium ferricyanide | Sat'd | 200 | 93 | 200 | 93 | 225 | 107 | 275 | 135 | 250 | 121 | 200 | 93 | 200 | 93 |
| Sodium ferrocyanide | Sat'd | 200 | 93 | 200 | 93 | 225 | 107 | 275 | 135 | 250 | 121 | 200 | 93 | 200 | 93 |
| Sodium fluoride | Sat'd | 150 | 66 | 150 | 66 | 150 | 66 | 200 | 93 | 200 | 93 | 150 | 66 | NT | NT |
| Sodium fluorosilicate | Sat'd | NT | NT | NT | NT | NT | NT | NT | NT | 150 | 66 | 120 | 49 | NT | NT |
| Sodium hexametaphosphate | Sat'd | NT | NT | NT | NT | NT | NT | NT | NT | 150 | 66 | 100 | 38 | NT | NT |
| Sodium hydrosulfide | Sat'd | NT | NT | NT | NT | NT | NT | NT | NT | NR | NR | 100 | 38 | 100 | 38 |
| Sodium hydroxide ${ }^{(7)}$ | $\leq 1 \%^{(1)}$ | $100^{(6)}$ | $38^{(6)}$ | $100^{(6)}$ | $38^{(6)}$ | $150{ }^{(6)}$ | $66^{(6)}$ | 200 | 93 | 200 | 93 | 180 | 82 | 100 | 38 |
| Sodium hydroxide | $2 \leq 30 \%$ | NR | NR | NR | NR | $150{ }^{(6)}$ | $66^{(6)}$ | $200^{(2)}$ | $93^{(2)}$ | 200 | 93 | 150 | 66 | 100 | 38 |
| Sodium hydroxide | 30 $\leq 50 \%$ | NR | NR | NR | NR | $150{ }^{(6)}$ | $66^{(6)}$ | 240 | 116 | 200 | 93 | 200 | 93 | 150 | 66 |
| Sodium hydroxide | Sat'd | NR | NR | NR | NR | 150 | 66 | 240 | 116 | 200 | 93 | NT | NT | NT | NT |
| Sodium hypochlorite | $\leq 5.25 \%$ | NR | NR | NR | NR | NR | NR | NR | NR | NR | NR | $N R^{(1)(8)}$ | $N R^{11 /(8)}$ | $140^{(11) 8)}$ | $60^{(1)(8)}$ |
| Sodium hypochlorite (stable) | $10 \leq 18 \%$ | NR | NR | NR | NR | NR | NR | NR | NR | NR | NR | NR | NR | NR | NR |
| Sodium lauryl sulfate | Sat'd | NT | NT | NT | NT | NT | NT | NT | NT | 200 | 93 | 160 | 71 | NT | NT |


| Chemical Substance | Concentration | Red Thread HP <br> Bondstrand 7000 <br> 7000M <br> 3000A 2"-6" <br> 2400 Conductive |  | $\begin{aligned} & \text { Bondstrand } \\ & \text { 3000A8"-16" } \end{aligned}$ |  | Green Thread HP |  | $\begin{aligned} & \text { Centricast } \\ & \text { Z-Core } \end{aligned}$ |  | $\begin{aligned} & \text { Centricast } \\ & \text { RB-1520 } \\ & \text { RB- } 2530 \end{aligned}$ |  | $\begin{aligned} & \text { Centricast } \\ & \text { CL-1520 } \\ & \text { CL-2030 } \end{aligned}$ |  | $\begin{gathered} \text { Bondstrand } \\ 5000 \\ 5000 \mathrm{M} \end{gathered}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ |
| Sodium metabisulfite (sodium bisulfite) |  | 150 | 66 | 150 | 66 | 205 | 96 | 250 | 121 | 250 | 121 | 200 | 93 | NT | NT |
| Sodium monophosphate | Sat'd | NT | NT | NT | NT | NT | NT | NT | NT | 210 | 99 | 200 | 93 | NT | NT |
| Sodium nitrate | Sat'd | 200 | 93 | 200 | 93 | 225 | 107 | 275 | 135 | 250 | 121 | 200 | 93 | 200 | 93 |
| Sodium nitrite | Sat'd | 200 | 93 | 200 | 93 | 225 | 107 | 275 | 135 | NT | NT | NT | NT | 200 | 93 |
| Sodium oxalate | Sat'd | NT | NT | NT | NT | NT | NT | NT | NT | 210 | 99 | 200 | 93 | NT | NT |
| Sodium permanganate | <60\% | NR | NR | NR | NR | NR | NR | NR | NR | NR | NR | 100 | 38 | 100 | 38 |
| Sodium peroxide |  | NT | NT | NT | NT | NT | NT | NT | NT | NR | NR | NR | NR | NT | NT |
| Sodium persulfate | <20\% | NR | NR | NR | NR | 75 | 24 | NT | NT | NT | NT | NT | NT | NT | NT |
| Sodium phosphate | Sat'd | NT | NT | NT | NT | NT | NT | NT | NT | 200 | 93 | 200 | 93 | NT | NT |
| Sodium silicate | Sat'd | NT | NT | NT | NT | 200 | 93 | 225 | 107 | 150 | 66 | 200 | 93 | 200 | 93 |
| Sodium sulfahydrate (NaHS) | $\leq 45 \%$ | NT | NT | NT | NT | 140 | 60 | NT | NT | NT | NT | NT | NT | NT | NT |
| Sodium sulfate, "soda ash" | Sat'd | 200 | 93 | 200 | 93 | 225 | 107 | 275 | 135 | 250 | 121 | 200 | 93 | NT | NT |
| Sodium sulfide | $\leq 15 \%$ | 210 | 99 | 200 | 93 | 225 | 107 | 250 | 121 | 150 | 66 | 200 | 93 | 150 | 66 |
| Sodium sulfide | 15\% 5 Sat'd | NT | NT | NT | NT | NT | NT | NT | NT | 200 | 93 | 200 | 93 | NT | NT |
| Sodium sulfite | Sat'd | 200 | 93 | 200 | 93 | 205 | 96 | NT | NT | 200 | 93 | 200 | 93 | 200 | 93 |
| Sodium tartate |  | NT | NT | NT | NT | NT | NT | NT | NT | 225 | 107 | 200 | 93 | NT | NT |
| Sodium tetraborate | Sat'd | NT | NT | NT | NT | NT | NT | NT | NT | 200 | 93 | 150 | 66 | NT | NT |
| Sodium thiocyanate | <57\% | NT | NT | NT | NT | 200 | 93 | 225 | 107 | 175 | 79 | 150 | 66 | 200 | 93 |
| Sodium thiosulfate | Sat'd | NT | NT | NT | NT | 150 | 66 | 200 | 93 | 150 | 66 | 150 | 66 | 200 | 93 |
| Sodium tripolyphosphate | Sat'd | NT | NT | NT | NT | NT | NT | 225 | 107 | 200 | 93 | 200 | 93 | NT | NT |
| Sodium xylene sulfonate | Sat'd | NT | NT | NT | NT | NT | NT | NT | NT | 125 | 52 | 175 | 79 | NT | NT |
| Sorbitol solutions |  | NT | NT | NT | NT | NT | NT | 225 | 107 | 200 | 93 | 160 | 71 | NT | NT |
| Sour crude oil |  | See Crude oil (sweet or sour) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Soybean fatty acid |  | NT | NT | NT | NT | NT | NT | 275 | 135 | NT | NT | NT | NT | NT | NT |
| Soybean oil (soya oil) |  | NT | NT | NT | NT | NT | NT | 275 | 135 | 225 | 107 | 200 | 93 | NT | NT |
| Stannic chloride | Sat'd | 150 | 66 | 150 | 66 | 205 | 96 | 225 | 107 | 200 | 93 | 200 | 93 | 200 | 93 |
| Stannic sulfate |  | 200 | 93 | 200 | 93 | 225 | 107 | 250 | 121 | 225 | 107 | 180 | 82 | 200 | 93 |
| Stannous chloride | Sat'd | 150 | 66 | 150 | 66 | 205 | 96 | 225 | 107 | 140 | 60 | 200 | 93 | 200 | 93 |
| Steam condensate |  | See (water, steam condensate) |  |  |  |  |  |  |  |  |  |  |  |  |  |


| Chemical Substance | Concentration | Red Thread HPBondstrand70007000 M3000A 2"-6"2400 Conductive |  | $\begin{aligned} & \text { Bondstrand } \\ & \text { 3000A 8"-16" } \end{aligned}$ |  | $\begin{gathered} \text { Green Thread HP } \\ \\ \text { Bondstrand } \\ 2000 \\ 2000 \mathrm{M} \\ 2400 \\ 4000 \end{gathered}$ |  | $\begin{aligned} & \text { Centricast } \\ & \text { Z-Core } \end{aligned}$ |  | $\begin{aligned} & \text { Centricast } \\ & \text { RB-1520 } \\ & \text { RB- } 2530 \end{aligned}$ |  | $\begin{aligned} & \text { Centricast } \\ & \text { CL-1520 } \\ & \text { CL-2030 } \end{aligned}$ |  | $\begin{aligned} & \text { Bondstrand } \\ & 5000 \\ & 5000 \mathrm{M} \end{aligned}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ |
| Stearic acid |  | 200 | 93 | 200 | 93 | 225 | 107 | 275 | 135 | 150 | 66 | 200 | 93 | 200 | 93 |
| Strontium chloride |  | NT | NT | NT | NT | NT | NT | 225 | 107 | 200 | 93 | 200 | 93 | 200 | 93 |
| Styrene |  | 75 | 24 | 75 | 24 | 75 | 24 | 185 | 85 | NT | NT | NT | NT | 100 | 38 |
| Succinonitrile |  | NT | NT | NT | NT | NT | NT | 120 | 49 | NR | NR | 70 | 21 | NT | NT |
| Sugar solutions |  | NT | NT | NT | NT | NT | NT | 275 | 135 | 250 | 121 | 180 | 82 | 180 | 82 |
| Sugar, beet or cane liquor | Sat'd | NT | NT | NT | NT | NT | NT | 275 | 135 | 200 | 93 | 100 | 38 | NT | NT |
| Sugar, sucrose | Sat'd | NT | NT | NT | NT | NT | NT | 275 | 135 | 225 | 107 | 200 | 93 | NT | NT |
| Sulfamic acid | $0 \leq 10 \%$ | 100 | 38 | 100 | 38 | 150 | 66 | 150 | 66 | 125 | 52 | 200 | 93 | 180 | 82 |
| Sulfamic acid | 10 $25 \%$ | 100 | 38 | 100 | 38 | 150 | 66 | 150 | 66 | 125 | 52 | 150 | 66 | 180 | 82 |
| Sulfamic acid | >25\% | NT | NT | NT | NT | NT | NT | NT | NT | NR | NR | 150 | 66 | NT | NT |
| Sulfanilic acid | Sat'd | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT |
| Sulfate liquor |  | NT | NT | NT | NT | NT | NT | NT | NT | NR | NR | 200 | 93 | NT | NT |
| Sulfated detergents | Sat'd | NT | NT | NT | NT | NT | NT | 225 | 107 | 200 | 93 | 200 | 93 | 150 | 66 |
| Sulfite liquor |  | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | 200 | 93 | 200 | 93 |
| Sulfur chloride |  | NT | NT | NT | NT | NT | NT | NT | NT | NR | NR | 200 | 93 | NR | NR |
| Sulfur dioxide, gas (dry) ${ }^{(3)}$ |  | 150 | 66 | 150 | 66 | 150 | 66 | 150 | 66 | 150 | 66 | 200 | 93 | 200 | 93 |
| Sulfur dioxide, gas (wet) ${ }^{(3)}$ |  | NT | NT | NT | NT | NT | NT | NT | NT | 150 | 66 | 200 | 93 | NT | NT |
| Sulfur trioxide |  | 75 | 24 | 75 | 24 | 100 | 38 | 180 | 82 | NR | NR | 160 | 71 | 160 | 71 |
| Sulfur trioxide, air, dry |  | NT | NT | NT | NT | NT | NT | NT | NT | NR | NR | 200 | 93 | 160 | 71 |
| Sulfuric acid | $\leq 2 \%$ | 75 | 24 | 75 | 24 | $180^{(6)}$ | $82^{(6)}$ | 200 | 93 | 200 | 93 | 180 | 82 | 200 | 93 |
| Sulfuric acid | 2 $55 \%$ | NT | NT | NT | NT | $180^{(6)}$ | $82^{(6)}$ | 200 | 93 | 200 | 93 | 180 | 82 | 200 | 93 |
| Sulfuric acid | $5 \leq 10 \%$ | NT | NT | NT | NT | $100^{(6)}$ | $38^{(6)}$ | 200 | 93 | 200 | 93 | 180 | 82 | 200 | 93 |
| Sulfuric acid | 10 $\leq 20 \%$ | NT | NT | NT | NT | $100{ }^{(6)}$ | $38^{(6)}$ | 150 | 66 | 150 | 66 | 180 | 82 | 200 | 93 |
| Sulfuric acid | 20 $\leq 25 \%$ | NT | NT | NT | NT | $100{ }^{(6)}$ | $38^{(6)}$ | 150 | 66 | 100 | 38 | 180 | 82 | 180 | 82 |
| Sulfuric acid | 25 $500 \%$ | NR | NR | NR | NR | $100^{(6)}$ | $38^{(6)}$ | 150 | 66 | 100 | 38 | 160 | 71 | 180 | 82 |
| Sulfuric acid | $50 \leq 70 \%$ | NR | NR | NR | NR | $70^{(6)}$ | $21^{(6)}$ | 150 | 66 | NR | NR | 160 | 71 | 120 | 49 |
| Sulfuric acid | $70 \leq 98 \%$ | NR | NR | NR | NR | NR | NR | 120 | 49 | NR | NR | NR | NR | NR | NR |
| Sulfuric acid | > 98\% | NR | NR | NR | NR | NR | NR | 100 | 38 | NR | NR | NR | NR | NR | NR |
| Sulfuric acid, fuming, oleum |  | NR | NR | NR | NR | NR | NR | 100 | 38 | NR | NR | NR | NR | NT | NT |
| Sulfurous acid | $\leq 6 \%$ | NT | NT | NT | NT | NT | NT | 75 | 24 | (1) | ${ }^{(1)}$ | 120 | 49 | 100 | 38 |


| Chemical Substance | Concentration | Red Thread HPBondstrand70007000M3000A 2"-6"2400 Conductive |  | $\begin{aligned} & \text { Bondstrand } \\ & \text { 3000A 8"-16" } \end{aligned}$ |  |  | d HP | $\begin{aligned} & \text { Centricast } \\ & \text { Z-Core } \end{aligned}$ |  | $\begin{aligned} & \text { Centricast } \\ & \text { RB-1520 } \\ & \text { RB- } 2530 \end{aligned}$ |  | $\begin{aligned} & \text { Centricast } \\ & \text { CL-1520 } \\ & \text { CL-2030 } \end{aligned}$ |  | $\begin{aligned} & \text { Bondstrand } \\ & 5000 \\ & 5000 \mathrm{M} \end{aligned}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ |
| Sulfurous acid | 6 $\leq 10 \%$ | NT | NT | NT | NT | NT | NT | 75 | 24 | NT | NT | 100 | 38 | 100 | 38 |
| Superphosphoric acid |  | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT |
| Tall oil |  | NT | NT | NT | NT | NT | NT | 225 | 107 | 150 | 66 | 210 | 99 | 200 | 93 |
| Tannic acid | <15\% | 210 | 99 | 210 | 99 | 225 | 107 | 275 | 135 | 200 | 93 | 200 | 93 | 200 | 93 |
| Tannic acid | Sat'd | 210 | 99 | 210 | 99 | 225 | 107 | 250 | 121 | 200 | 93 | 200 | 93 | 200 | 93 |
| Tartaric acid | Sat'd | 210 | 99 | 210 | 99 | 225 | 107 | 275 | 135 | 250 | 121 | 200 | 93 | NT | NT |
| Terephthalic acid | $\leq 25 \%$ | NT | NT | NT | NT | NT | NT | NT | NT | 100 | 38 | NR | NR | NT | NT |
| Tert-amyl methyl ether (TAME) |  | NT | NT | NT | NT | NT | NT | 125 | 52 | NT | NT | NR | NR | NR | NR |
| Tetrachloroethane 1, 1, 2, 2 |  | See 1,1,2,2-Tetrachloroethane |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Tetrachloroethylene |  | NT | NT | NT | NT | NT | NT | 175 | 79 | NT | NT | NT | NT | NR | NR |
| Tetraethyl lead |  | NT | NT | NT | NT | NT | NT | NT | NT | 100 | 38 | NR | NR | 100 | 38 |
| Tetrahydrofuran-THF |  | NT | NT | NT | NT | NT | NT | 100 | 38 | NT | NT | NT | NT | NT | NT |
| Tetrapotassium pyrophosphate | <60\% | NT | NT | NT | NT | NT | NT | NT | NT | NR | NR | 150 | 66 | NT | NT |
| Tetrasodium ethylene-diamine | Sat'd | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT |
| Tetrasodium ethylenediaminetetraacetic $A$ |  | NT | NT | NT | NT | NT | NT | NT | NT | 150 | 66 | 150 | 66 | NT | NT |
| Thioglycolic acid | $\leq 10 \%$ | NT | NT | NT | NT | NT | NT | NT | NT | NR | NR | NR | NR | NT | NT |
| Thionyl chloride, vents |  | NT | NT | NT | NT | NT | NT | 120 | 49 | NT | NT | NT | NT | NT | NT |
| Thionyl chloride |  | NT | NT | NT | NT | NT | NT | NT | NT | NR | NR | NR | NR | NT | NT |
| Tin(II) chloride |  | See Stannous chloride |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Tin plating ${ }^{(1)}$ |  | NR | NR | NR | NR | NR | NR | NT | NT | NR | NR | 200 | 93 | NT | NT |
| Titanium chloride |  | NT | NT | NT | NT | NT | NT | NT | NT | 175 | 79 | 175 | 79 | NT | NT |
| Titanium dioxide |  | NT | NT | NT | NT | NT | NT | NT | NT | 200 | 93 | 175 | 79 | NT | NT |
| Tobias acid ${ }^{(1)}$ |  | NT | NT | NT | NT | NT | NT | NT | NT | NR | NR | 200 | 93 | NT | NT |
| Toluene |  | 200 | 93 | 125 | 52 | 200 | 93 | 200 | 93 | 150 | 66 | NR | NR | NR | NR |
| Toluene sulfonic acid |  | NT | NT | NT | NT | NT | NT | NT | NT | NR | NR | 80 | 27 | NT | NT |
| Tomato catsup |  | 210 | 99 | 210 | 99 | 225 | 107 | 250 | 121 | 250 | 121 | 200 | 93 | 200 | 93 |
| Tomato puree |  | 210 | 99 | 210 | 99 | 225 | 107 | 250 | 121 | 250 | 121 | 200 | 93 | 200 | 93 |
| Transformer oil |  | 210 | 99 | 210 | 99 | 225 | 107 | 275 | 135 | 250 | 121 | 200 | 93 | 200 | 93 |
| Transformer oil (chloro-phenyl types) |  | NT | NT | NT | NT | NT | NT | 100 | 38 | NT | NT | NT | NT | NT | NT |


| Chemical Substance | Concentration | Red Thread HPBondstrand70007000M3000A 2"-6"2400 Conductive |  | Bondstrand 3000A 8"-16" |  | $\begin{gathered} \text { Green Thread HP } \\ \text { Bondstrand } \\ 2000 \\ 2000 \mathrm{M} \\ 2400 \\ 4000 \end{gathered}$ |  | $\begin{aligned} & \text { Centricast } \\ & \text { Z-Core } \end{aligned}$ |  | $\begin{aligned} & \text { Centricast } \\ & \text { RB-1520 } \\ & \text { RB-2530 } \end{aligned}$ |  | $\begin{aligned} & \text { Centricast } \\ & \text { CL-1520 } \\ & \text { CL-2030 } \end{aligned}$ |  | $\begin{aligned} & \text { Bondstrand } \\ & 5000 \\ & 5000 \mathrm{M} \end{aligned}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ |
| Transformer oil (mineral oil type) |  | 210 | 99 | 210 | 99 | 225 | 107 | 275 | 135 | 225 | 107 | 200 | 93 | 200 | 93 |
| Tributyl phosphate |  | NT | NT | NT | NT | NT | NT | NT | NT | NR | NR | 150 | 66 | NT | NT |
| Trichloroacetic acid | <50\% | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT |
| Trichloroethane 1,1,1 |  | See 1,1,1-Trichloroethane |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Trichloroethylene |  | 120 | 49 | 100 | 38 | 120 | 49 | 150 | 66 | 150 | 66 | NR | NR | NR | NR |
| Trichloromonofluoromethane |  | NT | NT | NT | NT | NT | NT | 120 | 49 | NT | NT | NT | NT | NT | NT |
| Trichloronitromethane |  | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT |
| Trichlorophenol |  | NT | NT | NT | NT | NT | NT | 100 | 38 | NR | NR | NR | NR | NT | NT |
| Trichlorophenoxyacetic acid |  | NT | NT | NT | NT | NT | NT | NT | NT | NR | NR | NR | NR | NT | NT |
| Tricresyl phosphate |  | NT | NT | NT | NT | NT | NT | NT | NT | NR | NR | 150 | 66 | NT | NT |
| Tridecylbenzene sulfonate |  | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT |
| Triethanolamine |  | 150 | 66 | 150 | 66 | $150^{(2)}$ | $66^{(2)}$ | 150 | 66 | 100 | 38 | 100 | 38 | NR | NR |
| Triethylamine |  | NR | NR | NR | NR | 100 | 38 | 100 | 38 | 100 | 38 | NR | NR | NR | NR |
| Triethylene glycol |  | NT | NT | NT | NT | NT | NT | NT | NT | NR | NR | 100 | 38 | NT | NT |
| Trimethylene chlorobromide |  | NT | NT | NT | NT | NT | NT | 150 | 66 | NT | NT | NT | NT | NT | NT |
| Triphenyl phosphite |  | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | 120 | 49 | 120 | 49 |
| Tripropylene glycol |  | NT | NT | NT | NT | NT | NT | NT | NT | NR | NR | 150 | 66 | NT | NT |
| Trisodium phosphate | <25\% | 150 | 66 | 150 | 66 | 200 | 93 | 225 | 107 | 200 | 93 | 200 | 93 | 210 | 99 |
| Trisodium phosphate |  | 100 | 38 | 100 | 38 | 200 | 93 | 225 | 107 | 150 | 66 | 200 | 93 | 210 | 99 |
| Tung oil |  | NT | NT | NT | NT | NT | NT | NT | NT | 200 | 93 | 100 | 38 | NT | NT |
| Turpentine |  | 100 | 38 | 100 | 38 | 100 | 38 | 150 | 66 | 75 | 24 | 100 | 38 | NR | NR |
| Tween surfactant |  | NT | NT | NT | NT | NT | NT | NT | NT | NR | NR | 125 | 52 | NT | NT |
| Urea formaldehyde resin |  | NT | NT | NT | NT | NT | NT | NT | NT | 150 | 66 | 120 | 49 | NT | NT |
| Urea | 550\% | 200 | 93 | 150 | 66 | 200 | 93 | 225 | 107 | 150 | 66 | 150 | 66 | 150 | 66 |
| Urea | >50\% | 200 | 93 | 150 | 66 | 200 | 93 | 225 | 107 | 150 | 66 | 125 | 52 | 150 | 66 |
| Vegetable oils |  | NT | NT | NT | NT | NT | NT | 275 | 135 | 225 | 107 | 210 | 99 | NT | NT |
| Vinegar, 300 grain,"acetic acid" |  | NR | NR | NR | NR | 120 | 49 | 120 | 49 | 100 | 38 | 100 | 38 | 200 | 93 |
| Vinyl ester resin, 45\% styrene |  | NT | NT | NT | NT | NT | NT | 150 | 66 | NT | NT | NT | NT | NT | NT |
| Vinyl acetate |  | NR | NR | NR | NR | NR | NR | 120 | 49 | 75 | 24 | NR | NR | NR | NR |


| Chemical Substance | Concentration | Red Thread HP <br> Bondstrand 7000 <br> 7000M <br> 3000A 2"-6" <br> 2400 Conductive |  | $\begin{aligned} & \text { Bondstrand } \\ & \text { 3000A 8"-16" } \end{aligned}$ |  | Gree Bo | HP <br> nd | $\begin{aligned} & \text { Centricast } \\ & \text { Z-Core } \end{aligned}$ |  | $\begin{aligned} & \text { Centricast } \\ & \text { RB-1520 } \\ & \text { RB-2530 } \end{aligned}$ |  | $\begin{gathered} \text { Centricast } \\ \text { CL-1520 } \\ \text { CL-2030 } \end{gathered}$ |  | $\begin{aligned} & \text { Bondstrand } \\ & 5000 \\ & 5000 \mathrm{M} \end{aligned}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ |
| Vinyltoluene |  | 80 | 27 | 80 | 27 | 80 | 27 | 200 | 93 | NT | NT | NT | NT | NT | NT |
| Water, brine |  | 210 | 99 | 210 | 99 | 225 | 107 | 275 | 135 | 212 | 100 | 175 | 79 | 200 | 93 |
| Water, chlorinated | $0 \leq 200 \mathrm{ppm}$ | 100 | 38 | 100 | 38 | 125 | 52 | 275 | 135 | 200 | 93 | 200 | 93 | 150 | 66 |
| Water, chlorinated | $200 \leq 2000 \mathrm{ppm}$ | NR | NR | NT | NT | NT | NT | 150 | 66 | 100 | 38 | 150 | 66 | 110 | 43 |
| Water, chlorinated | $2000 \leq 3500$ ppm | NR | NR | NR | NR | NR | NR | 125 | 52 | NR | NR | 150 | 66 | 110 | 43 |
| Water, chlorinated | Sat'd | NR | NR | NR | NR | NR | NR | 75 | 24 | NR | NR | 150 | 66 | 150 | 66 |
| Water, chlorinated brine |  | NT | NT | NT | NT | NT | NT | 150 | 66 | 120 | 49 | 150 | 66 | 150 | 66 |
| Water, deionized |  | 200 | 93 | 200 | 93 | 205 | 96 | 275 | 135 | 212 | 100 | 175 | 79 | 180 | 82 |
| Water, demineralized |  | 200 | 93 | 200 | 93 | 205 | 96 | 275 | 135 | 250 | 121 | 200 | 93 | 200 | 93 |
| Water, distilled |  | 200 | 93 | 200 | 93 | 205 | 96 | 275 | 135 | 212 | 100 | 175 | 79 | 200 | 93 |
| Water, fresh |  | 200 | 93 | 200 | 93 | 225 | 107 | 275 | 135 | 212 | 100 | 175 | 79 | 200 | 93 |
| Water, hard |  | 200 | 93 | 200 | 93 | 225 | 107 | 275 | 135 | 212 | 100 | 175 | 79 | 200 | 93 |
| Water, pH 2-13 |  | 210 | 99 | 210 | 99 | 225 | 107 | 275 | 135 | 212 | 100 | 175 | 79 | 200 | 93 |
| Water, reverse osmosis |  | 200 | 93 | 200 | 93 | 225 | 107 | 275 | 135 | 212 | 100 | 175 | 79 | 200 | 93 |
| Water, salt |  | 210 | 99 | 210 | 99 | 225 | 107 | 275 | 135 | 250 | 121 | 175 | 79 | 200 | 93 |
| Water, sea |  | 210 | 99 | 210 | 99 | 225 | 107 | 275 | 135 | 250 | 121 | 175 | 79 | 200 | 93 |
| Water, steam condensate |  | (1) | (1) | (1) | (1) | $225{ }^{(1)}$ | $107^{(1)}$ | 250 | 121 | NR | NR | NR | NR | 200 | 93 |
| White liquor (pulp mill) |  | NT | NT | NT | NT | NT | NT | 275 | 135 | NT | NT | NT | NT | 150 | 66 |
| Xylene |  | 200 | 93 | 125 | 52 | 205 | 96 | 200 | 93 | 125 | 52 | NR | NR | NR | NR |
| Zinc acetate |  | NT | NT | NT | NT | NT | NT | 200 | 93 | 180 | 82 | 180 | 82 | 180 | 82 |
| Zinc bromide |  | NT | NT | NT | NT | NT | NT | NT | NT | 250 | 121 | 200 | 93 | NT | NT |
| Zinc chlorate | Sat'd | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT |
| Zinc chloride | 550\% | 200 | 93 | 200 | 93 | 225 | 107 | 250 | 121 | 250 | 121 | 200 | 93 | NT | NT |
| Zinc chloride | >50\% | 200 | 93 | 200 | 93 | 225 | 107 | 250 | 121 | 225 | 107 | 180 | 82 | 200 | 93 |
| Zinc electrolyte |  | NT | NT | NT | NT | NT | NT | NT | NT | NR | NR | 150 | 66 | NT | NT |
| Zinc nitrate | Sat'd | 200 | 93 | 200 | 93 | 200 | 93 | 250 | 121 | (1) | (1) | 200 | 93 | NT | NT |
| Zinc phosphate |  | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | 180 | 82 | 200 | 93 |
| Zinc plating solution ${ }^{(1)}$ |  | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT | NT |
| Zinc sulfate | Sat'd | 70 | 21 | 70 | 21 | 70 | 21 | 275 | 135 | 250 | 121 | 200 | 93 | 200 | 93 |

## Footnotes

1. Contact NOV Fiber Glass Systems Application Engineering for further review and recommendations.
2. Based on limited service and test data, could be serviceable at higher temperatures. Contact NOV Fiber Glass Systems Application Engineering for consideration of higher temperature service.
3. Avoid service conditions where dry gasses such as chlorine or sulfur dioxide may condense to liquids inside fiberglass piping systems. Furthermore, liquid chlorine and sulfur dioxide should not be confused with solutions mixed with water.
4. Pneumatic conveyance of dry chemicals is not recommended. Contact NOV Fiber Glass Systems Application Engineering for further review.
5. These recommendations represent chemical compound saturation concentrations at atmospheric pressure. Higher concentrations or super saturation caused by higher pressure in a closed system may increase corrosion. Contact NOV Fiber Glass Systems Application Engineering for further review.
6. All grooved adapters, Bondstrand Key-Lock connections and 8" and larger Green Thread reducer bushings are not recommended for this service. Furthermore, exposed glass fibers at machined surfaces and/or threads must be covered with a protective coating of adhesive during installation. An adhesive may be used in place of thread locking compound in these services.
7. For very low caustic and acidic concentrations in water use the recommendations under "Water, pH 2-13".
8. Requires the use of RP-106 adhesive.
9. Not recommended for service temperatures above the chemical compounds boiling point at the operating pressure.

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# Red Thread ${ }^{\text {TM }} \mathrm{HP}$, Green Thread ${ }^{\text {Tm }} \mathrm{HP}$, and Silver Streak ${ }^{\text {TM }}$ 

Pipe Installation Handbook

Matched Tapered
Bell \& Spigot Joints

## Matched Tapered Bell \&Spigot Joints

This fabrication manual is offered to assist you in the proper fabrication and installation procedures when assembling your NOV Fiber Glass Systems piping system.
Ifyou do not find the answer to your questions in the manual, feel free to contact us or your local distributor.
Our products must be installed and used in accordance with sound, proven practice and common sense.
The information supplied by NOV Fiber Glass Systems in its literature must be considered as an expression of guidelines based on field experience rather than a warranty for which the company assumes responsibility. We offer a limited warranty of its products in the Terms and Conditions of Sale. The information contained in the literature and catalogs furnished cannot ensure, of itself, a successful installation and is offered to customers subject to these limitations and explanations.

Installing fiberglass pipe is easier than installing carbon steel, stainless steel, and lined steel due to its light weight. Learning the proper methods to prepare and make-up bell \& spigot joints can help ensure the reliability and long-term performance of your piping system.

We offer the TQI Plus (ASME B31.3) Fabrication and Assembly certification program. Qualified Field Service Representatives train fabrication and assembly crews, conduct and supervise fabrication work, and inspect work in progress.

For complete information concerning these training seminars, contact your local distributor or NOV Fiber Glass Systems.

## SAFETY

The safety alert symbol indicates an important safety message. When you see this symbol, be alert to the possiblity of personal injury

## CAUTION

As this pipe may carry hazardous material and/or operate at a hazardous pressure level, you must follow instructions in this manual to avoid serious personal injury or property damage. In any event, improper installation can cause injury or damage. In addition, installers should read and follow all cautions and warnings on adhesive kits, heat packs, propane torches, etc. to avoid personal injury. Also, observe general safety practices with all saws, tools, etc. to avoid personal injury. Wear protective clothing when necessary. Make sure work surfaces are clean and stable and that work areas are properly ventilated.

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## Section 1

Pipe Products

Pipe Grades
Fittings
Adhesives
Fabrication Accessories
Joining Systems

## Description of pipe products

The performance characteristics of a fiberglass pipe system depend on several important elements including the resin and curing agent, as well as the manufacturing process and type and thickness of the pipe's corrosion barrier.

NOV Fiber Glass Systems' piping systems are manufactured using epoxy, vinyl ester, or isophthalic polyester resin systems. All are heat cured for optimum chemical resistance and physical properties. Match your temperature, pressure and chemical resistance requirements to the piping system.

## Pipe Grades

## Red Thread HP

Epoxy pipe grade that provides long service life, lightweight and corrosion resistance. Used for light chemical services in salts, solvents and pH 2 to 13 solutions up to $210^{\circ} \mathrm{F}$ and pressures to 25 bar ( 362 psig ). Available in $2^{\prime \prime}-42^{\prime \prime}$ pipe sizes. T.A.B. (Threaded and Bonded bell \& spigot) is the primary joining method for 2"-6" diameter pipe. Matched tapered bell \& spigot joining method is used for 8"-42" pipe.

## Green Thread HP

Epoxy pipe with 15-20 mil resin-rich liner that provides excellent chemical resistance to dilute acids and caustics. Rated for temperatures up to $230^{\circ} \mathrm{F}\left(110^{\circ} \mathrm{C}\right.$ ) and pressures to $40 \mathrm{bar}(580$ psi). Matched tapered bell \& spigot connection is provided on all 1"-42" pipe sizes.

## Silver Streak

Custom filament wound pipe is specially designed for abrasive and corrosive services found in flue gas desulfurization. It is a proprietary blend of epoxy resin and abrasion-resistant additives. Rated for temperatures to $225^{\circ} \mathrm{F}$ and 225 psig. Available in 2"-24" pipe sizes.

## Fittings

All fittings are black in color. Green Thread fittings may be used with Red Thread and Green Thread pipe. Be sure to use the correct grade of pipe and fittings for your service. Consult Fittings \& Accessories Bulletins for pressure rating limits on various fittings. The lowest rated fitting determines the system pressure rating.

Most compression-molded fittings have a center line dot or cross which will assist you in making measurements.


Photo 1
Fittings

## Adhesives

Our adhesives are formulated for specific use with the companion pipe grades. Use only the recommended adhesive with each pipe grade-do not mix systems! Standard adhesives are a two-component system (Parts A and B) which must be mixed prior to use. Detailed instructions for adhesives are provided with each kit. Read these instructions thoroughly and follow the recommended procedures. The cure time and pot-life of the adhesive is dependent on temperature. Refer to the adhesive instructions. Ambient temperatures above $100^{\circ}$ F require extra care by the fabricator to assure sufficient working time of the adhesive. Refer to Adverse Weather Recommendations on page 23.

## Adhesive Selection

Standard adhesive kits are designed to be used with specific piping systems as shown in Table 2.

## Adhesive Working Life

Working life or pot life is the time it takes for the adhesive to harden in the mixing can. Refer to Table 1 below.

## Table 1

Adhesive Estimated Pot Life

| Pipe Resin <br> Systems | Adhesive | Pot Life @ 70 <br> (min.) | Pot Life @ 90 <br> (min.) |
| :--- | :--- | :--- | :--- |
| Epoxy | 2000 | 20 | 12 |
| Epoxy | 8000 | 15 | 8 |

NOTE:
Pot life is the time available for fabrication. Times may vary depending upon temperature, humidity, quantity mixed, etc.
Table 2
Adhesive Selection (refer to Bulletin ADH4000 for more information)

| Use with these Piping Systems | Max. <br> Temp. | Kit \# | Number of Bonds per Kit |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 1 | $11 / 2$ | 2 | 3 | 4 | 6 | 8 | 10 | 12 | 14 | 16 | 18 | 20 | 24 | 30 | $\begin{aligned} & 36 "- \\ & 42 " \end{aligned}$ |
| Red Thread HP <br> Green Thread HP <br> Silver Streak | $\begin{aligned} & 230^{\circ} \mathrm{F} \\ & \left(110^{\circ} \mathrm{C}\right) \end{aligned}$ | 8014 | 45 | 27 | 21 | 15 | 8 | 5 | 3 | 2 | 1 |  |  | 1/2 |  |  |  |  |
|  |  | 8024 | 20 | 12 | 9 | 6 | 4 | 2 | 1 |  |  |  |  |  |  |  |  |  |
|  |  | 8069 |  |  |  |  |  | 8 | 4 | 3 | 2 | 2 | 1 |  | 1/2 | 1/2 |  |  |
|  |  | 8036 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 1/2 | 1/2 |

Ambient temperature, adhesive working life and number of crewmen should be considered when ordering adhesive. For long runs of 8" and larger pipe, one kit per joint is recommended

## Fabrication Accessories

## Heat Collars and Heat Blankets

We offer high temperature heat collars and silicone heat blankets for use in curing of adhesive joints. The blankets and collars have a pre-set thermostat which controls the temperature of the unit. See page 60 for heat collar cure times for adhesive joint fabrications.


Photo 2
Heat Collar


Photo 3
Heat Blanket

## Heat Gun

High wattage electric heat guns are also available to heat adhesive joints. The heat guns are 1600 watt capacity.


Photo 4
Heat Gun

## Heat Packs

A heat pack unit consisting of ties and reactants in a plastic bag attached to foil paper is also available. Heat packs will cure joints within one hour.

## Tapering Tools

Matched tapered joints require various tools for making the tapered spigot in the field (RT, GT, SS). Refer to Table 6 on page 40 for selection of proper tapering tool.

## Come-Along

Specifically designed hydraulic come-alongs are available for 8"-42" piping systems (RT, GT, SS). Especially useful for long straight runs of pipe.


## Ratchet-Type Cable Come-Along

Kit consists of two manual cable puller come-alongs and one strap clamp kit. It is a mechanical aid used to join larger diameter piping. The come-along is most useful for 8 "-16" pipe sizes to aid in the alignment and landing of the spigot end into the bell.


Photo 6
Ratchet-Type Cable Come-Along

## Strap Clamp Kit

We offer Strap Clamp Kits that can be used in conjunction with come-alongs for bonding 8"-16" fittings. Strap clamp kits consist of two strap clamps and four $D$ belts.


## Joining Systems

## Bell and Spigot Joint

The adhesive bonded, tapered bell and spigot joint is a primary joining method for the following products:
1"-42" Green Thread piping and pipe to fittings
2"-42" Red Thread piping and pipe to fittings
2"-24" Silver Streak pipe to fittings
Pipe is supplied with one end tapered (the spigot) and the other end belled (integral bell or factory bonded coupling) to accept a tapered spigot. The joint is made by applying adhesive which, when cured, is compatible with the piping systems for joint strength and corrosion resistance.

## T.A.B. (Threaded and Bonded) Joint

The T.A.B. joint is the primary joining method for the following product:

2"-6" Red Thread piping and pipe to couplings.
The joining system combines both threads and adhesives on the bonding surfaces. The mechanical locking action of these promotes positive makeup which prevents back out during adhesive curing. Standard tapered bell fittings are used with this system.


Figure 1
Bell and Spigot Joint


Figure 2
T.A.B. (Threaded and Bonded) Joint

## Section 2

Site Considerations

Storage and Handling
Tools, Equipment and Supplies
Suggested Crew Setup and Assembly
Recommendations for Fabrication in Adverse Weather Conditions
Buried Recommendations
Anchors, Guides and Supports

## SiteConsiderations

## Storage and Handling

## Pipe and Fittings

Fiberglass reinforced pipe, fittings, and adhesives require special storage and handling. Care should be taken in transporting, unloading, handling, and storing products to prevent impact and other damage.

When transporting pipe, the spacers under and between the pipe joints must be of sufficient width to avoid point loading, which could produce cracking or buckling damage. A minimum offour spacers should be used for supporting 14" and larger 40' long pipe joints. More spacers should be used for smaller pipe or if pipe is stacked over eight feet high.

Due to its light weight, lifting equipment is usually not required for 1" - 6" pipe. When lifting equipment is required, use nylon slings or chokers. Do not allow chains or cables to contact the pipe during transport or handling. If a pipe or fabrication is more than 20 feet long, use at least two support points.
For storage, a board (2" $\times 4$ " minimum) should be placed under each layer of pipe approximately every ten feet. The intent is to support the pipe and distribute the load evenly. The pipe should also be braced on either side of the pipe rack to prevent unnecessary pipe movement. Avoid placing pipe on sharp edges, narrow supports, or other objects that could cause damage to the pipe wall. When storing pipe directly on the ground, select a flat area free of rocks and other deb ris that could damage the pipe. Stack pipe a maximum of 8'. Our pipe is furnished factory packaged in compact, easy-to-handle bundles complete with protective end caps. Leave these caps in place until installation time to protect the pipe ends as well as to prevent dirt or other material from getting into the pipe. Fittings are packaged in cardboard boxes and should be stored in a dry area. Iffittings are removed from the boxes, protect machined bells and spigots from exposure to direct sunlight.
If the protection on the pipe ends are damaged or removed, cover
immediately with corrugated cardboard and/or heavy duty black plastic.
The pipe can be damaged when joints or bundles of pipe are dropped during handling or shipping. Severe localized impact blows may result in damage to the fiberglass reinforced structure in the pipe wall. Before installation, inspect the pipe's outer surface for any damage.

Do not use damaged pipe unless inspected and approved by a NOV Fiber Glass Systems' representative. If impact damage occurs, the damaged areas may be recognized by a star type fracture on the pipe. Pipe that has been damaged should have a length cut away approximately one foot either side of the impacted site.

## NOTE:

Do not allow the bell end of the pipe to support any pipe weight.
Do not allow deformation of the pipe due to supports or straps.

## Adhesive

Refer to adhesive instructions included in each kit for storage life recommendations.

Safety Data Sheets (SDS) are available at nov.com/fgs.

## Tools, Equipment and Supplies

## Requirements for Installation

For maximum efficiency, the following tools and equipment are recommended prior to any installation:

- Pipe Stands, Jacks, Chain Vise, Come-along \& strap clamp kit
- Hand Tools
- Level, Marking Pen, Tape Measure, Pipe Wrap
- Hacksaw (22-28 teeth/inch)
- Tapering tool (See pages 38-40)
- Shop hammer, 3 lbs, and a 2x4 block of wood (for 1"-6" RT, GT, SS)
- Power Tools
- Power tapering tools (See pages 38-40)
- Circular power saw with a grit edge abrasive blade aluminum oxide, carbide or diamond
- Jigsaw with carbide abrasive blade or fine-tooth metal cutting blade
- Heat gun, heat blanket or collar
-T.A.B. wrenches (for 2"-6" T.A.B. joint piping systems)
- Expendables
- Clean, Dry, Lint-Free Shop Cloths
- Sandpaper Disc/Emery Cloth (80-120 grit for RT, GT, SS)
- Impermeable gloves
- Chemical splash goggles

NOTE: You must use the proper tool for tapering each size and type of pipe (see pages 38-40).

## Equipment for Cool Weather (Below $70^{\circ}$ F) pipe assembly:

- Heat source
- Portable torch with spreader tip, or
- Portable electric heat lamp, or
- Industrial hot air gun
- A means of maintaining adhesive kits at $70^{\circ}-80^{\circ} \mathrm{F}$ :
-A box with a 25 watt light bulb, or
- Inside of a warm vehicle with the heat running.
- Heat assisted curing
- Electric heating collars or blankets
- Chemical heat packs

WARNING: Be sure there are no flammable material or gas present when using any type of heating device.

Additional equipment for 8"-42" pipe assembly (RT, GT, SS):

- Manual or hydraulic come-alongs for 8" - 16"
- Hydraulic come-alongs for 18"-42"
- Strap clamp kit for 8" - 16"
-Strap Clamp kit and manual come alongs 8" - 16" /HP 32 - HP 40 systems
- Sledge hammer, 10-16 lbs., and a $4 \times 4$ block of wood


## Additional equipment for applying saddles:

- Power sander with 24-60 grit sanding disc
- Hose clamps.


## Table 2.1

Suggested labor times for Bell $\times$ Spigot Piping Systems

| Pipe <br> Size | Setup ${ }^{(1)}$ | Scribe \& Cutting Hand/power | Hand Tapering | Power Tapering | Joint Makeup (7,8) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| in | min | min/jt | min/jt | min/jt | min |
| 1 | 3 | 1.33/1.25 | 1 | $0.25^{(2)}$ | 1 |
| $11 / 2$ | 3 | 1.33/1.25 | 1.5 | $0.25{ }^{(2)}$ | 1 |
| 2 | 3 | 1.50/1.25 | 2 | 0.25 | 1.5 |
| 3 | 3 | 2.0/1.33 | 3 | 0.25 | 2 |
| 4 | 4 | 5.0/2.5 | 4 | 0.25 | 3 |
| 6 | 5 | 7.0/3.0 | 5 | $2.5{ }^{(2,3)}$ | 4 |
| 8 | 7 | 4.5/3.5 | 22 | $8.0^{(4,5,9)}$ | 5 |
| 10 | 7 | NA/5.0 | 35 | $10.0^{(5,9)}$ | 6 |
| 12 | 8 | NA/5.0 | 40 | $12.0^{(5,9)}$ | 8 |
| 14 | 9 | NA/5.0 | NA | $12.0^{(5,9)}$ | 10 |
| 16 | 10 | NA/6.0 | NA | $12.0{ }^{(5,9)}$ | 14 |
| 18 | 12 | NA/8.0 | NA | $25.0^{(6,9)}$ | 14 |
| 20 | 12 | NA/8.0 | NA | $28.0^{(6,9)}$ | 20 |
| 24 | 15 | NA/12.0 | NA | $30.0^{(6,9)}$ | 30 |
| 30 | 18 | NA/15.0 | NA | $60.0^{(9,11)}$ | 36 |
| 36 | 24 | NA/20.0 | NA | $70.0{ }^{(9,11)}$ | 40 |
| 42 | 30 | NA/24.0 | NA | $90.0^{(9,11)}$ | 45 |

## Suggested Labor Times for Bell x Spigot Piping Systems

${ }^{(1)}$ These numbers are based on installations using experienced crews in typical installation conditions. They do not include extreme weather conditions, time used for gathering supplies and tools, break time, manpower issues, etc. Assume 6 hours of productive labor for every 8 hours worked. Adjustment factors should be applied to these base units to compensate for prevailing production and job conditions. Because of all the variables involved, NOV Fiber Glass Systems is not responsible for any differential between these numbers and actual results.
${ }^{(2)} 2000$ series Power Tools
${ }^{(3)}$ 2"-6" Hand Tapering Tool
${ }^{(4)}$ Individual Tapering Tool
${ }^{(5)}$ 8"-16" Taper/ScarfTool
${ }^{(6)}$ 18"-24" Taper Tool
${ }^{(7)}$ Each joint makeup calculation includes cleaning, sanding, applying adhesive and proper engagement. Allow three minutes formixing adhesive.
${ }^{(8)}$ The units (time) listed above are based on using experienced crews on fitting intensive runs. For straight run pipe, contact your local representative.
${ }^{(9)}$ Time doubles for HP 25 products.
${ }^{(10)}$ Includes set up for hydraulic or manual come-along and setting pipe stand levels.
${ }^{(11)}$ Use the 30"- 42" taper tool.

## Suggested Crew Setup and Assembly

Manpower requirements change depending on whether the installation is simple, consisting of long, straight runs, or complex. It also depends on pipe size, installation temperature, and other similar influences. Following are some general guidelines that are applicable to most installations. If you have any questions, please contact an NOV Fiber Glass Systems representative for information.

## Suggested Crew Size for 1"-6" straight long pipe runs

A three-worker crew is the minimum recommended crew size. A four-worker crew is sometimes more efficient, even when installing 1" - 6" diameter pipe.

| Man \# | Crew Description |
| :--- | :--- |
| $\mathbf{1}$ | Clean/prep/align <br> Removes end caps, sands and cleans joint and aligns pipe for <br> bonding. |
| $\mathbf{2}$ | Adhesive mixer/bonder <br> Mixes adhesive and applies to bell and spigot. |
| $\mathbf{3}$ | Assembly man <br> Helps make up joint and checks for lock up. |
| $\mathbf{4}$ | Pre-heat/prep/supplies <br> (optional through 4"; recommended on 6") <br> Pre-heats joints and helps keep pipe aligned. Also applies heat <br> collars during cool weather. (All help in moving supplies and <br> equipment from joint to joint.) |

Suggested Crew Size for 8"-42" straight long pipe runs
A six or seven crew members is recommended.

| Man \# | Crew Description |
| :--- | :--- |
| $\mathbf{1}$ | Clean/prep/align <br> Removes end caps, sands and cleans joint and aligns pipe for <br> bonding. |
| $\mathbf{2}$ | Adhesive mixer/bonder <br> Mixes adhesive and applies to bell and spigot. Marks insertion <br> depth and determines when joint is locked up. Assists with come- <br> along. |
| $\mathbf{3}$ | Adhesive mixer/bonder <br> Helps \#2 with adhesive and assists with come-along. |
| $\mathbf{4}$ | Pre-heat/alignment man <br> Pre-heats joints, helps align joints and assists with come-along. |
| $\mathbf{5}$ | Alignment man <br> Sets level of pipe and aligns joint for proper insertion; directs <br> tractor driver. |
| $\mathbf{6}$ | Truck driver/Supply man (optional) <br> Drives supply truck and assists with all aspects of installation. <br> Also coordinates heat collars during cool weather and ice chest <br> during hot weather. |
| $\mathbf{7}$ | Tractor Operator <br> Operates side boom tractor, track hoe or backhoe. <br> (All help in moving supplies and equipment from joint to joint.) |

In more complex pipe assemblies, the crew size will depend on the amount of tapering and prefabrication needed. In most cases, a three-worker crew is the minimum for any size piping installation. In some instances (small jobs with only a few joints) only one or two crewmen will be required.

## Recommendations for Fabrication in Adverse Weather Conditions

The piping can be installed in adverse weather conditions when the necessary precautions are taken.

Actual work will often be more quickly completed in high temperature conditions. Low temperatures can increase the work time 20\%-35\% over normal shop conditions. A similar increase is common for high moisture conditions.

## Hot Weather Installation Tips

Hot weather conditions, temperatures above $90^{\circ} \mathrm{F}$, will greatly reduce the working time of the adhesive. The following steps are recommended when fabricating in hot weather conditions:

1. Avoid direct sunlight on the joining surfaces.
2. Store adhesive in a cool area.
3. Keep mixed adhesive in an ice chest with sealed bag of ice or ice pack.

## Cold Weather Installation Tips

Adhesive cure time is directly related to the temperature. Colder temperatures result in longer cure times.

CAUTION: Overheating the adhesive could result in pre-mature exotherm.

The following steps should be used when fabricating in colder temperatures:

1. Adhesive kits should be placed in a warm room for six to twelve hours before application in order to reach temperatures of $80^{\circ} \mathrm{F}-100^{\circ} \mathrm{F}$. This will make mixing much easier and speed cure times. Or use a box with a 25 watt light bulb to warm adhesive kits.
2. When possible, piping should be bonded indoors into sub-assemblies. The warmer conditions of these areas will allow faster cure times.
3. Pre-warm bonding surfaces to $80^{\circ} \mathrm{F}-100^{\circ} \mathrm{F}$ when temperature falls below $70^{\circ} \mathrm{F}$.
4. A heat gun, collar or blanket may be used to obtain a faster cure time. Apply a layer of fiberglass insulation or a welding blanket around the heat collars or blankets when installation temperatures are below $50^{\circ} \mathrm{F}$.

## Extreme Moisture

Adhesive Joints - If fittings or pipe have moisture on the bonding surface, wipe them dry prior to sanding and if within safety guidelines use some type of heat to complete drying.

- Sand pipe or fittings immediately before applying the adhesive to bond the joint. Sand surfaces until a fresh, dry surface is present, then remove dust with a clean dry cloth, and apply adhesive.
- Cure per the previous recommendations for normal, extreme heat or extreme cold temperatures.


## Buried Installations

These are general guidelines only. For more details see Engineering and Piping Design Guide.

## Minimum Bending Radius Layout



Where:

$$
\mathrm{X}=\text { Run, } \mathrm{ft}(\mathrm{~m})
$$

$Y=$ Offset, $\mathrm{ft}(\mathrm{m}) \quad \pi$ )
$\mathrm{R}=$ minimum bend radius, $\mathrm{ft}(\mathrm{m})$
(trigonometric function based on radians)

Offset Bending Allowance for Green \& Red Thread HP 16/HP 25 Pipe (contact Applications Engineering for 30" - 42")

| Pipe <br> Size | X <br> Straight Run |  | Y Offset for HP 16 |  | $\mathbf{Y}$ <br> Offset for HP 25 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | ft | m | ft | m | ft | m |
| 2 | 20 | 6.1 | 2 | 0.6 | 2 | 0.6 |
|  | 40 | 12.2 | 10 | 3.0 | 8 | 2.4 |
| 3 | 40 | 12.2 | 6 | 1.8 | 5 | 1.5 |
|  | 60 | 18.3 | 16 | 4.9 | 12 | 3.7 |
| 4 | 40 | 12.2 | 5 | 1.5 | 4 | 1.2 |
|  | 80 | 24.4 | 23 | 7.0 | 17 | 5.2 |
| 6 | 40 | 12.2 | 3 | 0.9 | 3 | 0.9 |
|  | 80 | 24.4 | 15 | 4.6 | 11 | 3.4 |
|  | 120 | 36.6 | 34 | 10.4 | 26 | 7.9 |
|  | 160 | 48.8 | 67 | 20.4 | 49 | 14.9 |
| 8 | 80 | 24.4 | 11 | 3.4 | 9 | 2.7 |
|  | 120 | 36.6 | 25 | 7.6 | 20 | 6.1 |
|  | 160 | 48.8 | 47 | 14.3 | 36 | 11.0 |
|  | 200 | 61.0 | 78 | 23.8 | 58 | 17.7 |
| 10 | 80 | 24.4 | 9 | 2.7 | 7 | 2.1 |
|  | 120 | 36.6 | 20 | 6.1 | 16 | 4.9 |
|  | 160 | 48.8 | 36 | 11.0 | 28 | 8.5 |
|  | 200 | 61.0 | 59 | 18.0 | 45 | 13.7 |
| 12 | 80 | 24.4 | 7 | 2.1 | 6 | 1.8 |
|  | 120 | 36.6 | 17 | 5.2 | 13 | 4.0 |
|  | 160 | 48.8 | 32 | 9.8 | 24 | 7.3 |
|  | 200 | 61.0 | 51 | 15.5 | 38 | 11.6 |
| 14 | 80 | 24.4 | 6 | 1.8 | 5 | 1.5 |
|  | 120 | 36.6 | 15 | 4.6 | 12 | 3.7 |
|  | 160 | 48.8 | 28 | 8.5 | 21 | 6.4 |
|  | 200 | 61.0 | 44 | 13.4 | 33 | 10.1 |
| 16 | 80 | 24.4 | 5 | 1.5 | 4 | 1.2 |
|  | 120 | 36.6 | 13 | 4.0 | 10 | 3.0 |
|  | 160 | 48.8 | 23 | 7.0 | 18 | 5.5 |
|  | 200 | 61.0 | 36 | 11.0 | 28 | 8.5 |


| Pipe <br> Size | $\mathbf{X}$ <br> Straight Run |  |  | Y <br> Offset for HP 16 |  | Y <br> Offset for HP 25 |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :---: |
| 18 | $\mathbf{f t}$ | $\mathbf{m}$ | $\mathbf{f t}$ | $\mathbf{m}$ | $\mathbf{f t}$ | $\mathbf{m}$ |  |
|  | 80 | 24.4 | 5 | 1.5 | 4 | 1.2 |  |
|  | 120 | 36.6 | 11 | 3.4 | 9 | 2.7 |  |
|  | 160 | 48.8 | 19 | 5.8 | 16 | 4.9 |  |
|  | 200 | 61.0 | 31 | 9.5 | 25 | 7.6 |  |
| 24 | 80 | 24.4 | 4 | 1.2 | 4 | 1.2 |  |
|  | 120 | 36.6 | 10 | 3.0 | 8 | 2.4 |  |
|  | 160 | 48.8 | 17 | 5.2 | 15 | 4.6 |  |
|  | 200 | 61.0 | 27 | 8.2 | 23 | 7.0 |  |
|  | 80 | 24.4 | 3 | 0.9 | 3 | 0.9 |  |
|  | 120 | 36.6 | 8 | 2.4 | 7 | 2.1 |  |
|  | 160 | 48.8 | 16 | 4.9 | 12 | 3.7 |  |
|  | 200 | 61.0 | 25 | 7.6 | 19 | 5.8 |  |

## Table 3

Burial Depths*

| Product | Minimum |  | Maximum |  |
| :--- | :--- | :--- | :--- | :--- |
|  | $\mathbf{f t}$ | $\mathbf{m}$ | $\mathbf{f t}$ | $\mathbf{m}$ |
| 1"-4" Red Thread HP16/HP 25 | 2 | 0.6 | 15 | 4.6 |
| 6"-24" Red Thread HP16/HP 25 | 3 | 0.9 | 15 | 4.6 |
| 1"-12" Green Thread HP16/HP 25 | 2 | 0.6 | 15 | 4.6 |
| $14 "-24$ " Green Thread HP16/HP 25 | 3 | 0.9 | 15 | 4.6 |
| 1" - 12" Silver Streak | 2 | 0.6 | 15 | 4.6 |
| $14 "-24 "$ Silver Streak | 3 | 0.9 | 15 | 4.6 |

* Based on a 1000 psi composite constrained modulus. Contact the factory for detailed information for your specific application.
NOTE: Contact NOV Fiber Glass Systems' Applications Engineering for HP 32 \& HP 40 systems.


## Burial Depth:

Minimum burial depth in unpaved areas for pipe subjected to vehicular loads depends on pipe grade, pipe size, vehicle axle weight, and the bedding material. With a standard legal axle load of $34,000 \mathrm{lbs}$., the minimum depth of cover (from the top of the pipe to the surface) for moderately compacted non-clay bearing soils is shown in Table 3.

Maximum burial depth is dependent on the backfill material. For moderately compacted soils that do not contain large amounts of highly expansive clays, the maximum burial depth is shown in Table 3.


The pipe should always be buried below the frost line.
Trench Preparation - Final bedding of the trench must be as uniform and continuous as possible. Before backfilling, fill all gaps under the pipe with proper bedding material. Avoid sharp bends and sudden changes in slope. It is important to remove all sharp rocks, cribbage, or other foreign objects that could come in contact with the piping.

Bedding Requirements - Fiberglass pipe can be damaged by point contact or wear with the trench bottom and walls, improper bedding materials, or adjacent pipe. Use recommended bedding material a minimum of 6 inches thick at the bottom, sides, and top of the piping (refer to Table 4). Adjacent pipes should be spaced the greater of 6 inches or one pipe diameter. The piping can be laid directly on the trench bottom if the native soil meets the requirements of a recommended bedding material (refer to Table 4). In some situations, the trench bottom can be "scratched" such that a natural cradle of dirt is formed. Never


Areas "a" must firmly support pipe haunches

## Table 4

Recommended Bedding Materials

| Bedding Material | Compaction Proctor <br> Density |
| :--- | :---: |
| Crushed rock or pea gravel 3/4" maximum size | Not Required |
| Coarse-grained sand or soil with little or no fines | $75-85 \%$ |
| Coarse-grained sand or soil with more than 12\% <br> fines | $85-95 \%$ |
| Sand or gravel with more than 30\% coarse- <br> grained particles | $85-95 \%$ |
| Sand or gravel with less than 30\% coarse- <br> grained particles | Greater than 95\% |

lay fiberglass piping directly against native rock or shale. Always use dry, unfrozen bedding materials that do not contain foreign objects or debris. Never use water flood for compaction. Slurries can be used that are intended for burial of flexible piping systems. When using slurries, care must be taken to prevent floating or deformation of the piping.
Pipe Support- Fiberglass pipe is flexible and requires the support of the bedding material to keep the pipe round in burial applications. It is very important that a recommended bedding material is properly compacted around the entire circumference of the pipe. (Refer to Table 4) Tamp the bedding material under the bottom half of the piping to prevent voids or areas of low compaction. Vibratory or similar tamping equipment can drive

small stones or debris into the pipe wall if they are present in the bedding material. Avoid striking the pipe with tamping equipment as the pipe may be fractured.

High Water Tables or Vacuum - Consult factory for recommendations.

Road Crossings - When laying fiberglass pipe under road crossings, it may be necessary to pass the pipe through conduit to protect the pipe. Pad the pipe to prevent rubbing or point loads against the conduit.

## Wall Penetrations

Where the pipe goes through or passes under a concrete structure, precautions must be taken to prevent bending or point loading of the pipe due to settling. A minimum 2" thick pad of

resilient material should be wrapped around the pipe to provide flexibility and prevent contact with the concrete. If bolts are used in the resilient material, care should be taken that the bolts, nuts, or washers cannot come into point load contact with the pipe. Bedding depth under the pipe should be increased to a minimum of 12 " or one pipe diameter, whichever is greater, for one pipe joint length away from the concrete.

Timing-Test and cover the pipe as soon as possible to reduce the chance of damage to the pipe, floating of the pipe due to flooding, or shifting of the line due to cave-ins.
Two Point Lifting of Red Thread \& Green Thread HP Series
Piping The Lift Points table provides the locations for safe two point lifting with straps at least 4 inches in width. The cantilever

## Lift Points

| Nominal Size | Pipe Lengths (ft) |  | Cantilever <br> Lengths (ft) |  | Mid-Span Lengths (ft) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | Number | Length | Min. | Max. | Min. | Max. |
| 8 | 3 | 120 | 24 | 26 | 68 | 72 |
| 10 | 3 | 120 | 20 | 28 | 64 | 80 |
| 12 | 3 | 120 | 22 | 31 | 58 | 76 |
| 14 | 3 | 120 | 22 | 31 | 58 | 76 |
| 16 | 3 | 120 | 20 | 35 | 50 | 80 |
| 18 | 3 | 120 | 19 | 36 | 48 | 82 |
| 20 | 4* | 160 | 31 | 37 | 86 | 98 |
| 24 | 4* | 160 | 30 | 40 | 80 | 100 |
| 30 | 4* | 160 | 30 | 40 | 80 | 100 |
| 36 | 4* | 160 | 30 | 40 | 80 | 100 |
| 42 | 4* | 160 | 30 | 40 | 80 | 100 |

* The same cantilever length applies for 3 pipe lengths.

lengths are critical and should be followed without exception. Lifting and moving of the pipe should be performed by smooth motions. Avoid aggressive jerking or rough movement of pipe during installation.


## Anchors, Guides and Supports

Pipe Hangers-Pipe hangers such as those shown are often used to support pipe in buildings and pipe racks. However, the use of too many hangers in succession can result in an unstable line when control valves operate, and during pump start-up and shutdown. To avoid this condition, the designer should incorporate auxiliary guides periodically in the line to add lateral
 and axial stability.
Pipe Guides-Guides are rigidly fixed to the supporting structure and allow the pipe to move in the axial direction only. Proper guide placement and spacing are important to ensure proper movement of expansion joints or loops and to prevent buckling of the line.


The guiding mechanism should be loose so it will allow free axial movement of the pipe. " $U$ " bolts, double-nutted so they cannot be pulled down tight, are often utilized for guides.

Primary and secondary guides, i.e.,
 those immediately adjacent to expansion joints, are spaced more closely than intermediate guides. Refer to Engineering \& Piping Design Manual, for details.

Piping entering expansion joints or expansion loops require additional guides. Refer to Engineering \& Piping Design Manual for details.

Pipe Supports - Piping supports for the pipe should be spaced at intervals as shown in the product bulletins.

NOTE: Properly spaced supports do not alleviate the need for guides as recommended in the preceding
 section. Supports that make only point contact or that provide narrow supporting areas should be avoided. Some means of increasing the supporting area should be used; sleeves made from half of a coupling or pipe are suitable. Support pumps, valves and other heavy equipment independent of the pipe. Refer to pump and valve connection instructions on page 80.

Pipe Anchors - Pipe anchors divide a pipeline into individual expanding sections. In most applications, major pieces of connected equipment, such as pumps and tanks, function as anchors. Additional anchors are usually located at valves, near changes in direction of the piping, at blind ends of pipe, and at major branch connections. Provisions for expansion should be designed into each of the individual pipe sections.


Refer to Engineering \& Piping Design Guide, for a thorough discussion on supports, anchors and guides.

# Section 3 

General Installation Instructions

Read This First

Cutting Fiberglass Pipe

## Installation Statement

## Important-Read this First

Before beginning the actual assembly procedures, read and make sure all installers thoroughly understand the following instructions.

All bonding surfaces must be clean, dry and factory fresh in appearance before applying adhesive. When end caps have been lost, surfaces will weather and result in loss of bond strength. When surfaces are weathered, re-taper (RT, GT, SS) spigots to achieve a factory fresh appearance. (Note: T.A.B. couplings that have weathered must be replaced.)

Matching tapered bell and spigot joints require a very thin adhesive bond line for maximum strength and durability.
The adhesive used with tapered joints is very strong when used in bond lines a few thousandths of an inch thick. The same adhesive may be brittle in thick sections resulting in poor bond strength. To achieve a thin bond line, the matched tapered angles of the joint are designed to mechanically "lock-up" when wedged together.

Using mechanical force assures "lock up" and a thin bond line. Hammering a wooden block placed against the bell end of pipe, or using mechanical devices such as come-alongs should be used to "lock up" the joint.
NOTE: For T.A.B. joints, special T.A.B. wrenches are required to achieve the mechanical lock up in the joint.

Adverse weather conditions require special precautions when bonding pipe. (See page 24, Recommendations for Fabrication in Adverse Weather Conditions) The adhesive is very viscous (thick) when cool or when applied to cool pipe. The thick adhesive can actually be stiff enough to prevent joint "lock up." When the adhesive is hot or when it is applied to hot pipe, the available working time may be significantly reduced. For Installers new to fiberglass it is strongly recommended that the system be hydrotested within the first 2500 ' or 50 joints.

## Matched tapered bell and spigot joints that are not "locked

 up" can fail prematurely.
## Cutting Fiberglass Pipe

NOV Fiber Glass Systems' pipe should be cut using one of the methods referred to under Tools and Equipment on page 18.

1. Measure pipe, remembering to allow for spigot and fitting dimensions.
2. Scribe a cutting guide around the pipe to ensure a perpendicular cut for proper fit.
3. Hold the pipe firmly but not to the point of crushing. If chain vises or other mechanical holding devices are used, care should be taken to prevent crushing or point loading of the pipe. To prevent damage to the pipe, 180 degree sections of pipe can be used for protective covers.
4. Saw the pipe as smoothly as possible. The pipe ends should be square within $1 / 8$ inch.


NOTE: For integral joint (IJ) bell ends, the bell end must be cut off before tapering. Measure the O.D. of the pipe near the bell end until you see the O.D. start to get larger. Cut the pipe at this point. Depending on pipe size the distance from the end of the bell can vary anywhere from 12 " to 36 ".

## Section 4

## Fabrication of

 Red Thread HP, Green Thread HP and Silver Streak Pipe and FittingsTapering Pipe
Tapering Tool Reference Chart Joint Assembly
Close Tolerance Piping
Joint Prep
Adhesive Mixing

Take-Off Dimensions
1"x6" Bell x Spigot Joints
8"x36" Bell x Spigot Joints
T.A.B. Joints

Joint Cure and Heat Collars
Repairs

## Tapering Pipe

Various tools are available from NOV Fiber Glass Systems for making the tapered spigot in the field.

To reproduce a standard taper, the tapering tool must be marked or adjusted. The process varies depending on the tool being used and the product being tapered. Please refer to individual tool instructions for tapering.

Refer to Table 6 on page 40 for specific bulletin number and proper taper angle for each size and type of pipe. Do not taper over the bell end of integral joint pipe. See page 36 for cutting instructions.

1"-6" Tool - A hand-held tool that can be adapted for power when a large number of tapers is necessary. Different piping systems require different mandrels.

Model 2100/ 2102/2106 Tool - Power tool for tapering and scarfing Red Thread and Red Thread IIA piping.
Model 2300/2306 Tool - Power tool especially designed for tapering 1" - 6" Green Thread piping.

8", 10", or 12" Tapering Tool - These tools are designed for manual or power (i.e., Ridgid ${ }^{\circledR} 300$ or 700 power drive or equal) operation; there is a tool for each size pipe.

NOTE: Red Thread and Green Thread mandrels can be purchased separately and used on this tool.


1"-6" Tool


Model 2100/2101 Tool


Model 2300/2306 Tool


Model 2106/2306 Tool


8 ", 10 " or 12 " Tapering Tool

2"-12" Remote Power Tool-Tapers 2"-12" pipe. Must change angle for 8 " and larger pipe. Recommended for $6 "$ tapers.
Additional material will be needed for 8" and larger tools: Sturdy work bench (preferably with a metal top) or stand to hold the tool. Strap Clamp kit to restrain pipe while tapering.

8"-16" Taper/Scarf Tool - This is an electrically powered tapering tool. When using the 8 "-16" tool you must find a method to secure the pipe. This can be done with strap clamps, a heavy duty table for short sections or HD pipe stands for full lengths.
18"-24" Tapering Tool-This is an electrically powered tapering tool. The tool comes with different size mandrels to taper 18"-24" pipe.
Note for HP 32 pipe: For 2"-6" pipe, use the 2"-12" Remote Power Tool. For 8"-16" pipe, use the 8"-16" Single Point


2"-12" Remote Power Tool


8"-16" Taper/Scarf Tool


18"-24" Tapering Tool Taper tool. The 2"-12" Remote Power Tool can taper 8"-12" pipe if necessary but the 8"-16" tool is preferred for those sizes.

Note for HP 40 pipe: For 2"-16" pipe, taper angle is $13 / 4$ degree.

Table 5
Extension Cord Length*

| Wire Size AWG | Maximum Length (ft) |
| :---: | :---: |
| 12 | 20 |
| 10 | 30 |
| 8 | 50 |

*The 8"-24" single point taper tools may not operate properly with an extension cord over 25 '.

Table 6
Tapering, Scarfing and Cutting Tool Reference Chart

| Tool | Product | Tool Taper Angle | Bulleting \# | Comments |
| :---: | :---: | :---: | :---: | :---: |
| 1" - 6" Hand Tapering | $\begin{aligned} & \text { RT } \\ & \text { GT } \end{aligned}$ | $\begin{aligned} & 1^{\prime \prime}=3^{\circ} ; 1 \frac{1}{2}=21 / 2^{\circ} \\ & 2^{\prime \prime}-6^{\prime \prime}=1^{3 / 4^{\circ}} \end{aligned}$ | TLS 6600 | Specify product to receive correct mandrels. Order scarfing adapter kit for secondary containment power adapter separate. Uses Ridgid 700 or equivalent power drive with a Ridgid 774 adapter. |
| 2100 Power | RT | $13 / 4^{\circ}$ | TLS 2000 | Tapers 2" \& 3"; Scarfs 3" \& 4" |
| 2102 Power | RT | $13 / 4^{\circ}$ | TLS 2000 | Tapers 2"-4"; Scarfs 3" |
| 2300 Power | GT | $13 / 4^{\circ}$ | TLS 2000 | Tapers 2"-4" |
| 2106/2306 Power | RT/GT | $13 / 4^{\circ}$ | TLS 2000 | The 2106 tapers 2"-6" RT. The 2306 tapers 2"-6" GT. The tools are interchangeable between RT/GT. Mandrels can be purchased separate. |
| 2700 Power | SS | $13 / 4^{\circ}$ | TLS 2000 | Tapers 2"-4" Silver Streak |
| 8" Tapering Tool | RT/GT | 0 or $1^{\circ}$ | TLS 6608 Taper TLS 6609 Scarf | Tapers and scarfs 8" Red Thread and Green Thread |
| 10" \& 12" Taper or Scarfing Tool | RT/GT | 0 or $1^{\circ}$ | TLS 6612 Taper TLS 6613 Scarf | Tapers and scarfs. Order scarfing adapter kit for Secondary Containment. Uses Ridgid 700 or equivalent power drive with a Ridgid 774 adapter. |
| 8 "-16" or 18 "-26" Single Point Taper Tool | 8"-26" RT, GT, SS | $1^{\circ}$ or $1^{3} 4^{\circ}$ | TLS 6622 TLS 6621 | Tapers or scarfs 8"-16" RT, GT, SS. Scarfs 8"-12" GT, or $8^{\prime \prime}-16$ " secondary containment. |
| 2"-12" Remote Power Tool | RT, GT, SS | $\begin{aligned} & 2^{\prime \prime}-6 "-1^{3 / 4^{\circ}} \\ & 8^{\prime \prime}-12^{\prime \prime}-1^{\circ} \end{aligned}$ | TLS 6601 | Tapers 2"-12" pipe. Must change angle for 8" and larger pipe. |
| 30"-42" Taper Tool | RT, GT, SS | $13 / 4{ }^{\circ}$ | TLS 6636 | Taper 30', 36", and 42" |

## Joint Prep for Red Thread, Green Thread and Silver Streak

All bonding surfaces must be clean and dry before bonding.

- For T.A.B. joints, clean with an acceptable solvent and clean rag. Wire brushes may also be used for cleaning T.A.B. surfaces; however, they must be clean and free of oily contaminates.
- All bonding surfaces must be clean and dry before bonding. For T.A.B. joints clean with an acceptable solvent and a clean rag. Never sand T.A.B.XT.A.B. surfaces.
- For smooth tapers, sandpaper or solvent (or both) may be used. Sand just light enough to remove any contaminates.
- Use caution as over-sanding can change the taper angle or end dimension, and create flat spots on the spigot.
- When surfaces have weathered, sand or retaper spigots and sand bells to achieve a factory fresh appearance. Cut at least 1" from spigots before retapering. T.A.B. couplings must be replaced.
- Bonding surfaces must be dry, so be sure all solvent has evaporated before applying adhesive.

When ambient temperature is below $70^{\circ} \mathrm{F}$, pre warm the bonding surfaces. Use a hot air gun, propane torch or other clean burning heat source that has a spreader type tip, and apply heat uniformly to bell and spigot until warm to the touch. Check temperature by touching bonding surfaces with the back of your hand. Do not touch with the front of your hand as this may contaminate the joint. If hot to the touch, let cool before applying adhesive. When using a torch to preheat, warm the bell first. It is thicker and will hold heat longer. If an electric heating collar is used to pre warm, place the joint together dry, then heat the O.D. of the bell to avoid contaminating the spigot. Do not use chemical heat packs to prewarm. $\triangle$ Warning: Do not use propane torch around flammable gases or liquids.

NOTE: Use of a solvent as a cleaning method is optional.
WARNING: Before using heating devices or open flames be sure all safety checks and regulations are followed. Do not use if flammable gases or liquids are present.

Some alternate cleaning solvents are acetone, methylene chloride, and methyl ethyl ketone. After cleaning, be sure any residual solvent has evaporated before applying adhesive. DO NOT USE SOLVENTS THAT LEAVE AN OILY FILM ON THE BONDING SURFACES. Only use fresh solvent directly from the manufacturer's container. Do not use dirty solvent or solvent poured in a secondary bucket.

!WARNING: Some degreasers and solvents are extremely flammable. Do not smoke or use near an open flame. Wear eye protection. Be sure to read warning labels on containers. Do not use alcohole as most alcohol contains water and could contaminate the joint.
Never use gasoline, turpentine, or diesel fuel to clean joints.
Solvent containers may be under pressure. Use caution when removing inner seals, especially in warm weather. Use with adequate ventilation.
Close Tolerance Piping - The tapered bell and spigot system employed by FGS can be readily used to achieve dimensional accuracy where required by a particular pipe layout. When the installation is such that close tolerances must be maintained, you must follow these instructions. You must accurately reproduce tapers (spigots) in the field with the field tapering tools. This provides a means of achieving dimensional accuracy.
Calculation to Achieve a Desired Length - Most close tolerance installations are made to prints calling out CL to CL (center line to center line) dimensions.
When fabricating to these dimensions, follow these procedures per the figure below.


1. Obtain the center line to face dimension (A) of fittings to be used from Tables 8 or 9 on pages 46-50.
2. Create an insertion gauge by cutting a short section of pipe; 12 " long for small diameters and 18 " long for larger diameters. Taper the pipe using the instructions supplied with each tool. Check dry insertion. The insertion length should be within $\pm 1 / 8$ " of a factory spigot insertion. NEVER USEA FACTORY TAPER FORA GAUGE.
3. Obtain insertion length (IL) by inserting the gauge (made with the tool being used) into a fitting and measuring. (NOTE: Measure each end of each fitting, because the insertion may vary for each bell.) You can prepare and use a short nipple as a standard insertion gauge.

NOTE: You must prepare a new gauge if you change tapering tools or make any changes to the tool you are using.) Always add a make-up dimension (refer to Table 7) to this measurement, since the adhesive will act as a lubricant and allow greater penetration than when the surfaces are dry. Measure each end of each fitting with your gauge.

Table 7
Approximate Make-up Dimensions HP 16/HP 25 (M)*

| Pipe Diameter, in | Approximate Make-up <br> Dimensions*, in |
| :---: | :---: |
| 1 and $11 / 2$ | $1 / 16$ |
| 2 | $1 / 8$ |
| 3 and 4 | $3 / 16$ |
| 6 | $1 / 4$ |
| 8 | $3 / 8$ |
| 10 and 12 | $5 / 8$ |
| 14 | $3 / 4$ |
| 16 | 1 |
| 18 | $11 / 4$ |
| 20 | $11 / 2$ |
| 24 | $13 / 4$ |

4. To achieve a specified CL to CL dimension, the length of pipe to cut is equal to the CL to CL distance minus the sum of the center line to face dimension of the fittings ("A" dimension) plus the sum of the measured insertion lengths (IL) plus the sum of the make-up allowance $(M)$, or length of pipe to cut = $\left(C_{L}\right.$ to $\left.C_{L}\right)-(A+A)+(I L+I L)+(M+M)$.

*CAUTION: Make-up dimensions depend on the tightness of the dry fit. If the field developed dimensions vary, use field developed dimensions.

NOTE: Use field dimensions for HP 32/HP 40 systems.

## Adhesive Mixing

When the weather is cool or the adhesive has been stored in a cool environment (below $70^{\circ} \mathrm{F}$ ), pre warm the adhesive kits. (Do not heat above $100^{\circ} \mathrm{F}$ !)

1. For epoxy empty all of the contents of the hardener bottle into the can of base adhesive.
2. Mix all of the base epoxy adhesive with all of the hardener. NEVER ATTEMPT TO SPLIT A KIT. Cut through the adhesive with the edge of the mixing stick to assist in mixing the two components.
3. Mix until the adhesive has a uniform color and a consistent flow off the mixing stick. Wipe down the sides, bottom, and under the rim of the can with the mixing stick to assure complete mixture.
Complete information and safety precautions are packaged with each adhesive kit. Review all safety precautions thoroughly before mixing the adhesive.

ADHESIVE DISPOSAL: Once the adhesive and hardener have been mixed and reacted, nothing can be extracted, and it is
classified as non-hazardous material. Dispose of in a normal manner as other solid waste. Excess adhesive and hardener can be mixed, allowed to react, and disposed of as above. If extra jars of adhesive or hardener have accumulated without the other component to mix and react, contact your regional manager. Hardener jars, when empty are not subject to EPA regulation and can be disposed of in a normal manner. These guidelines are based on federal regulations. State and local regulations and ordinances should be reviewed.

Table 8.0
Take-off Dimensions for RT, GT, Fittings (Contact Company for SS Dimensions)


| Size | $45^{\circ}$ Elbow | $90^{\circ}$ Elbow | Tee | Later |  | Cross | M/FW* | M/FW* | *Flanges <br> M-Molded FW-Filament Wound |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | A | A | A | A | B | A | B | C |  |
| 1 | 23/8 | 23/4 | 23/4 | 37/8 | 21/2 | 23/4 | $13 / 4$ | $3 / 4$ |  |
| $11 / 2$ | 27/8 | 33/8 | $33 / 8$ | 51/4 | $31 / 4$ | 33/8 | $13 / 4$ | $3 / 4$ | Dimensions are used to calculate pipe length requirements to meet pipeline center line to center line dimensions. |
| 2 | 25/8 | 33/8 | 33/8 | 65/8 | 23/4 | 33/8 | 21/4/21/8 | 3/4 |  |
| 3 | 33/4 | 45/8 | 45/8 | $73 / 4$ | 41/4 | 45/8 | 25/8 | $13 / 8$ |  |
| 4 | 37/8 | 51/8 | 51/8 | 9 | $43 / 8$ | 51/8 | 25/8/31/2 | $13 / 8$ |  |
| 6 | 43/8 | 61/8 | 61/8 | 121/2 | 53/4 | 61/8 | $3 / 33 / 4$ | $11 / 2$ |  |
| 8 | 81/8 | 115/8 | 115/8 | 161/4 | 73/8 | 115/8 | 4 | $13 / 4$ |  |
| 10 | 85/8 | 13 | 13 | 195/8 | $83 / 4$ | 131/8 | 43/4 | 2 |  |
| 12 | 91/2 | 14 | 14 | 243/4 | $113 / 4$ | 14 | 5 | 21/4 |  |
| 14 | 121/2 | 19 | 19 | 321/2 | 153/4 | 16 | 31/8 | 21/2 |  |
| 16 | $131 / 4$ | 201/4 | 201/4 | $353 / 4$ | $173 / 4$ | 171/4 | $31 / 8$ | 21/2 |  |

Table 8.1a
Dry insertion depths for standard Red Thread HP 16 and Green Thread HP 16 pipe and fittings

| Size | $90^{\circ} \& 45^{\circ}$ <br> Degree <br>  <br> Tees |  | Crosses |  | Laterals |  | Molded Flanges |  | FW Flanges |  | Couplings |  | Integral Joints |  | The $X$ values are the nominal dry spigot insertions used to set up tapering tools. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | X-RT | X-GT | X-RT | X-GT | X-RT | X-GT | X-RT | X-GT | X-RT | X-GT | X-RT | X-GT | X-RT | X-GT |  |
| 1 | - | 1 | - | 1 | - | 1 | NA | 1 | - | 1 | - | - | - | $11 / 4$ | The tolerances for dry insertion are $\pm 1 / 8^{\prime \prime}$ for 1 "- 6 " and $\pm 1 / 4$ " for 8 "-16""pipe sizes. The final insertion referred to as the wet locked up position will be larger than the $X$ dimension. Do not use these dry insertion depths for close tolerance piping calculations. |
| $11 / 2$ | - | 1 | - | 1 | - | 1 | - | 1 | - | 11/8 | - | - | - | $11 / 2$ |  |
| 2 | $11 / 2$ | $11 / 2$ | 11/2 | 15/8 | 11/2 | 15/8 | $11 / 2$ | 15/8 | $11 / 2$ | 15/8 | - | - | $13 / 4$ | $11 / 2$ |  |
| 3 | 15/8 | 17/8 | $15 / 8$ | $17 / 8$ | 15/8 | 17/8 | $11 / 2$ | 17/8 | 17/8 | 2 | - | - | $13 / 4$ | $13 / 4$ |  |
| 4 | $11 / 2$ | 17/8 | 11/2 | $17 / 8$ | 11/2 | 17/8 | $13 / 4$ | 17/8 | $17 / 8$ | 25/8 | - | - | 21/8 | $17 / 8$ |  |
| 6 | 21/8 | 23/8 | 21/8 | $23 / 8$ | 21/8 | 23/8 | $21 / 4$ | 21/2 | 21/2 | 21/2 | - | - | 23/8 | $21 / 8$ |  |
| 8 | 33/4 | $31 / 4$ | $31 / 4$ | 27/8 | $31 / 4$ | 27/8 | 25/8 | 2114 | $33 / 8$ | $33 / 8$ | $37 / 8$ | $37 / 8$ | 37/8 | $33 / 8$ |  |
| 10 | 37/8 | 35/8 | $31 / 4$ | 3 | 31/8 | 27/8 | 33/4 | 33/8 | 3 | 3 | $33 / 4$ | 33/8 | $33 / 4$ | $33 / 8$ |  |
| 12 | 4 | $33 / 4$ | 35/8 | $31 / 4$ | $31 / 4$ | 3 | $33 / 4$ | $33 / 8$ | 3 | 3 | 37/8 | 35/8 | $37 / 8$ | $35 / 8$ |  |
| 14 | 61/8 | 6 | 35/8 | 35/8 | 35/8 | 35/8 | - | - | 21/4 | 23/8 | $43 / 8$ | $41 / 4$ | $43 / 8$ | $41 / 4$ |  |
| 16 | 61/8 | $61 / 8$ | $37 / 8$ | $37 / 8$ | 37/8 | 37/8 | - | - | 17/8 | 2 | $41 / 2$ | $41 / 2$ | $41 / 2$ | $41 / 2$ |  |

## Table 8.2

Take off and nominal dry insertion dimensions for Silver Streak piping systems.
Refer to Silver Streak bulletin or www.nov.com/fgs for more information.

| Size | Coupled/Mitered | Filament Wound |
| :---: | :---: | :---: |
| in | in | in |
| 2 | $17 / 8$ | $25 / 8$ |
| 3 | $23 / 8$ | $27 / 8$ |
| 4 | 2 | $31 / 8$ |
| 6 | $27 / 8$ | $2^{3 / 3} 4$ |
| 8 | $31 / 2$ | $51 / 4$ |
| 10 | $43 / 8$ | $51 / 8$ |
| 12 | $47 / 8$ | $63 / 8$ |
| 14 | $51 / 2$ | $41 / 2$ |
| 16 | $61 / 4$ | $5 \frac{5}{2}$ |

## Table 8.3

Dry insertion depth " $X$ " for Stub Ends

| Size | Green Thread | Red Thread ${ }^{(1)}$ | Red Thread <br> T.A.B. |
| :---: | :---: | :---: | :---: |
| in | in | in | in |
| 2 | $21 / 8$ | $21 / 8$ | $17 / 8$ |
| 3 | $27 / 8$ | $21 / 4$ | $17 / 8$ |
| 4 | $21 / 4$ | $17 / 8$ | $17 / 8$ |
| 6 | $33 / 8$ | $31 / 4$ | 3 |

${ }^{(1)}$ Smooth Taper as built in field
${ }^{(2)}$ Factory T.A.B. spigot

## Table 9a

Take off dimensions for RT/GT HP 25 products. X dimensions are nominal dry insertion lengths. Pipe must be driven together and fully locked up to assure full joint strength. Actual insertions should be $+1 / 4$ " for 8 " and larger joints. Insertion depths are for tool set up only. Do not use insertion depths ( $x$ ) for close tolerance piping. Refer to joint assembly instructions for complete information on joint lock up

| Size | $45^{\circ}$ Degree Elbows (Long Radius) (in) |  |  | 90́ Degree Elbows (Long Radium) (in) |  |  | Tee <br> (in) |  |  | FW Flanges (in) |  | Van <br> Stone <br> Flanges <br> (in) | Coupling (in) |  | Integral Joint <br> (in) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | A | X-RT | X-GT | A | X-RT | X-GT | A | X-RT | X-GT | X-RT | X-GT |  | X-RT | X-GT | X-RT | X-GT |
| 1 | - | - |  | - | - |  | - | - |  | - | - | - | - | - | - | - |
| $11 / 2$ | - | - |  | - | - |  | - | - |  | - | $11 / 8$ | - | - | - | - | - |
| 2 | - | - | 21/2 | - | - | $21 / 2$ | - | - | 21/2 | - | $13 / 4$ | - | - | - | - | - |
| 3 | - | - | 23/4 | - | - | $23 / 4$ | - | - | 23/4 | - | 27/8 | - | - | - | - | - |
| 4 | - | - | 3 | - | - | 3 | - | - | 3 | - | $31 / 4$ | - | - | - | - | - |
| 6 | - | - | 23/4 | - | - | $23 / 4$ | - | - | 23/4 | - | 35/8 | - | - | - | - | - |
| 8 | 121/2 | 6 | 51/8 | 191/2 | 6 | 51/8 | $131 / 2$ | 6 | 51/8 | - | 33/8 | $61 / 4$ | 53/4 | 51/4 | 45/8 | 41/8 |
| 10 | 141/2 | $61 / 2$ | 61/2 | 231/4 | $61 / 2$ | 61/2 | 153/4 | $61 / 2$ | $61 / 2$ | - | 5 | 7 | $51 / 2$ | $51 / 4$ | 53/4 | 53/8 |
| 12 | 161/2 | 7 | 7 | 27 | 7 | 7 | 173/4 | 7 | 7 | - | 55/8 | 73/4 | 61/8 | 57/8 | $61 / 4$ | 6 |
| 14 | 173/4 | 53/4 | 53/4 | 30 | 53/4 | 53/4 | 191/2 | 53/4 | 53/4 | - | 45/8 | 8 | 53/4 | $51 / 4$ | 6 | 53/8 |
| 16 | 20 | - | 53/4 | 34 | 53/4 | 53/4 | 211/2 | 53/4 | 53/4 | - | $41 / 2$ | 9 | 63/8 | 51/8 | 63/8 | 51/8 |
| 18 | 247/8 | - | 107/8 | 40 | - | - | 263/8 | - | - | - | 73/8 | 101/2 | - | - | - | - |
| 20 | 295/8 | - | 125/8 | $471 / 4$ | - | - | $311 / 4$ | - | - | - | 8 | 121/2 | - | - | - | - |
| 24 | 357/8 | - | 155/8 | 57 | - | - | 35 | - | - | - | 103/8 | 151/2 | - | - | - | - |

Table 9b
Dry insertion depth for Green Thread HP 32 fittings

| Size | $90^{\circ} \& 45^{\circ}$ Degree Elbows \& Tees | FW Flanges |
| :---: | :---: | :---: |
| in | X-GT | X-GT |
| $1^{*}$ | - | - |
| $11 / 2^{*}$ | - | - |
| 2* | - | - |
| 3* | - | - |
| 4* | - | - |
| 6* | - | - |
| 8* | - | - |
| 10* | - | - |
| 12* | - | - |
| 14 | $81 / 8$ | 63/4 |
| 16 | 95/8 | 8 |
| 18 | 101/8 | $83 / 8$ |
| 20 | 117/8 | 10 |
| 24 | 15 | $123 / 4$ |

* These sizes are rated to HP 40. See Table 9c for HP 40 insertion depths.


## Table 9c

Dry insertion depth for Green Thread HP 40 fittings

| Size | $90^{\circ}$ \& $\mathbf{4 5}^{\circ}$ Degree <br> Elbows \& Tees | FW Flanges |
| :---: | :---: | :---: |
| in | X-GT | X-GT |
| 1 | - | - |
| $11 / 2$ | - | - |
| 2 | $21 / 2$ | $13 / 4$ |
| 3 | $31 / 8$ | $21 / 2$ |
| 4 | $33 / 4$ | $31 / 8$ |
| 6 | $43 / 8$ | $35 / 8$ |
| 8 | $73 / 8$ | $65 / 8$ |
| 10 | $81 / 2$ | $75 / 8$ |
| 12 | $97 / 8$ | $83 / 4$ |

## Installing 1"-6" joints with a block of wood and a hammer

When ambient temperature is below $70^{\circ} \mathrm{F}$, pre warm the bonding surfaces. Use a hot air gun, propane torch or other clean burning heat source that has a spreader typetip, and apply heat uniformly to bell and spigot until warm to the touch. Check temperature by touching bonding surfaces with the
 back of your hand. Do not touch with the front of your hand as this may contaminate the joint. If hot to the touch, let cool before applying adhesive. When using a torch to preheat, warm the bell first. It is thicker and will hold heat longer. If an electric heating collar is used to pre warm, place the joint together dry, then heat the O.D. of the bell to avoid contaminating the spigot. Do not use chemical heat packs to pre warm. $\triangle$ WARNING: Do not use propane torch around flammable gases and liquids.
Brush adhesive on both the bell and spigot bonding surfaces, applying a thin uniform coating to each. To minimize contamination, apply adhesive to the bell first. Adhesive should always be worked into the machined surface by applying pressure during application. This will "wet out" the machined surface and maintain the required thin bond line. Be sure that adhesive is deep down into the bell past the insertion depth and that all machined taper surfaces on the spigot and the cut end of the pipe are uniformly covered. Excess adhesive will make the joint more difficult to lock.


Align and lock the joint. For 2" or smaller pipe, insert the spigot into the bell until surfaces touch, then push and turn at the same time until a lock is achieved. Only a quarter to a half turn is usually needed. On 3"-6" diameter pipe or on fittings, pushing and turning to lock the joint is impractical and driving force must be used. A hammer may be used to assist in joint lock-up. Place a $2 \times 4$ board flat across the bell. The first few raps should be light to
prevent any tendency of the joint to back out.

If the adhesive or the pipe surfaces are cool, push and hold
 for a few seconds to allow time for the adhesive to start flowing out of the tapered joint.

Check lock up by moving a free end of the pipe in an up and down or side to side motion. The movement must be sufficient to move the joint being checked. No movement should be visible in the joint. If any movement exists, the joint is not properly locked up. Avoid excess movement as this could damage the spigot.

## For installing 8" - 16" fittings and pipe with manual comealongs and strap clamps, the following recommendations

 should be followed:- Strap clamps should only be tightened by hand. Do not use cheater bars or wrenches to tighten them for the clamps may be overstressed.
- The clamps should be covered to prevent flying debris should a clamp failure occur.
- If the strap slips on the pipe surface, Emery cloth placed between the strap and pipe will increase the frictional resistance to slipping. Abrasive powders such as Ajax ${ }^{\circledR}$ or Comet ${ }^{\circledR}$ powdered cleaners will likewise increase the resistance to slippage.
- Only use on pipe joint sizes 8" - 16".

Hydraulic come-alongs are required on all matched tapered joint sizes 18 " and larger. When pipe joints are pulled together with come-alongs, they must be vibrated during joint make up. The vibrating reduces the joints resistance to movement.

## Installing 8" - 16" HP 16 and HP 25 products using an FGS

 Hydraulic Come-along. (See manual TLS6618) Hydraulic Come-alongs are recommended for long pipe runs. All threaded parts should be checked before every use to ensure engagement of threads to prevent tool damage and possible physical injury.The operator should be positioned in a safe position to the side of the pipe. The hydraulic pump is supplied with a pressure gauge to allow monitoring of the loads. Do not exceed the recommended loads.

One strap clamp is supplied with each come along kit. A Strap Clamp kit or bolt up style metallic fitting clamps are available on request.
The 8" - 16" hydraulic come-alongs are supplied with wedge style pipe clamps. Attach the clamps and drive the wedges on tight. Clean and prep the bonding surfaces and apply adhesive. Stab the joint together by hand and attach come-along chains. Use the hand pump and apply the required pressure from table 10. As the joint is pulled together use a 5 lb dead blow hammer (supplied with the come-along) to vibrate the joint hitting it 360 degree around the IJ head or fitting. Keep pressure on the joint until all of the adhesive has squeezed out and there is not forward movement seen at the joint. With full pressure on, hit across the joint three times. When the pressure drop is 200 psig or less, the joint is considered locked up. After the pipe has been properly supported, you may remove the come along and clamps and move to the next joint immediately. Come along pressure must be left on until all pipe movement, blocking up, etc. is finished and the pipe is secure.

## Table 10

Hydraulic Come-Along Pressures

| Pipe Grade | Pipe Size | Hydraulic Pressure |
| :---: | :---: | :---: |
|  | in | psig |
| RT, GT, SS | $8-10$ | $1500-1750$ |
|  | $12-16$ | $1750-2000$ |
| HP 16 Products | $18-42$ | $1500-2600$ |
|  | $8-12$ | 2000 |
|  | $14-16$ | 2500 |
|  | $18-24$ | 3000 |
|  | $30-36$ | 4500 |
|  | 42 | 5000 |

## Joint Support During Cure

During joint assembly, the uncured bonded joint MUST be supported at all times until the adhesive is fully cured. Blocks, sand bags or skids may be used to support the pipe during installation. At least two supports are required for each pipe length. Place the supports 5' from each end. After the joint has been pulled together and locked up, leave the come-along pressure on until the supports have been placed under the pipe
and the pipe is heading in the right direction/orientation. If the middle of the pipe starts to sag, place supports under them as well. Excess movement across the joint before it has cured could result in damage to the pipe spigots. After the joint has been supported properly you may remove the clamps and go to the nextjoint.

## Installing 18"-42"Pipe and Fittings with Hydraulic Come-Along

Hydraulic come-alongs are required for 18 " an larger products. The operator should be in a safe position to the side of the pipe.
Check all threaded parts before each use to ensure full engagement of the threads and prevent tool damage and possible physical injury. The hydraulic pump is supplied with a pressure gauge to monitor the pressure loads. Steel fitting clamps and $11 / 4$ " bolts are shipped with each come-along unit. Do not over pressurize as this could lead to joint back out.
Bolt up style pipe and fitting clamps are available in 18" - 42" sizes. The fitting clamps are narrower than the pipe clamps. The come -along clamps are supplied with a small hook on the handle. This hook is designed to hold the two clamps together while the bolts are tightened. The use of an impact wrench and a portable air compressor is recommended. Basic wrenches can be used but add time to the process.
Place the clamps approximately 3 ' from the end of the joint on both sides. Screw the cylinder base extension to the cylinders. and place between the clamps. Tighten bolt tight to prevent slippage. Place a bolt through the cylinder base with no threads and tighten. Connect chain thru the cylinder bases. Prep joint and apply adhesive. Using a tractor or side boom slowly stab the joint together. Tighten chains and hang through the "claw" on the cylinders. Apply the required pressure from Table 10. As the joint is pulled together use a 5 lb dead blow hammer (supplied with the come-along) to vibrate the joint hitting it 360 degree around the IJ head or fitting. Keep pressure on the joint until all of the adhesive has squeezed out and there is not forward movement seen at the joint. With full pressure on hit across the joint three times. When the pressure drop is 300 psig or less, the joint is considered locked up.
When installing $18^{\prime \prime}-24$ " it is recommended that the come-alongs be left on for approximately 5 minutes before releasing comealong pressure to ensure lock up and the pipe has been properly supported.

When installing 30" - 42" joint the clamps must be left on until the joint is fully cured per the required cure time.
Ratchet-Type Cable Come-alongs are recommended when it is not practical to use hydraulic come alongs. Strap clamp kits or special fitting collars are available for use with the manual come alongs. Only use on 8" - 16"products.

Strap clamps should only be tightened by hand. DO NOT use cheater bars or wrenches to tighten them as this could result in personal injury.


The clamps should be covered to prevent flying debris should a clamp fail.
If the straps slip on the slick pipe or fitting surface, emery cloth placed between the strap and the pipe or fitting will increase the frictional resistance to slipping. Abrasive powders such as Ajax or Comet may also be used under the straps to help prevent sliding.
Two cable come-alongs are required to make up a joint. The come-alongs should be positioned on opposite sides of the pipe joint to achieve a straight pull. The come-alongs are attached to the pipe via heavy-duty strap clamp kits or metallic pipe clamps.. These straps/clamps should be placed far enough away from the joint to allow the positioning and use of the come-alongs. They are generally placed 24" - 36" away from the joint, one on each side of the joint but actual placement requirements will be governed by the size of the come-alongs.
Clean and prep the joint and apply the adhesive. Gently stab the joint together. The two come-alongs should be tightened at the same time to maintain a straight joint while pulling the joint together. Vibrating of the pipe by rapping the fitting bell or coupling surface with a 5 \# dead blow hammer will reduce the frictional resistance in the joint being pulled together. The load on the cables should be held firm until the joints are aligned and completely locked up. The joint is considered locked up when no forward movement is noted. After a joint is made up, do not aggressively move the pipe and joint until the adhesive is completely cured. Relieve tension on cables before attempting to removestrap clamps.
Operation of cable come-alongs should be in accordance with the device manufacturer's instructions.

## Installing 18" - 30" Green Thread Flanges

1. Install the flange onto the spigot without adhesive to determine the dry-fit measurement. Use a dead blow hammer to force the flange onto the pipe spigot. See Photo \#8
2. If the spigot extends through the bell dry you will need to cut the end of the spigot off. Scribe a cutting guide around the pipe spigot that sticks through the flange face. See Photo \#9
3. Remove the flange from the pipe spigot.
4. To calculate the additional amount to be removed due to wet overdry insertion refer to Table 11 and the appropriate pipe diameter, draw a new scribe line on the pipe spigot. See Photo \#10
5. Saw the pipe spigot off at the scribe line drawn. See Photo \#11
6. Saw the spigot off as smoothly as possible. Sand the new spigot face to remove jagged edges. See Photo \#12
7. Sand the spigot and flange I.D. using a heavy grit sand paper. Clean the bonding surfaces with acetone.


Photo \#8


Photo \#9


Photo\#10


Photo\#11

Allow bonding surfaces to dry completely. See Photo \#13. Refer to standard cleaning/joint prep practices in this manual.
8. Bond the flange to the pipe spigot using a comealong and the appropriate pressure from Table 11.


Photo \#12


Photo \#13 serrated flange face and the O-ring groove using a cutting agent.
11. Allow to gel and then post cure according to Table 13.


Photo \#14


Photo \#15

Table 11

| Size |  | Spigot Removal |  | Come-Along Pressure |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| in | $\mathbf{m m}$ | in | $\mathbf{m m}$ | psi | MPa |
| 18 | 450 | 1.00 | 25.4 | $2500-2750$ | $17.2-19.0$ |
| 20 | 500 | 1.00 | 25.4 | $2500-2750$ | $17.2-19.0$ |
| 24 | 600 | 1.25 | 31.75 | $2500-2750$ | $17.2-19.0$ |
| 30 | 750 | 1.50 | 38.1 | $2750-3000$ | $19.0-20.7$ |

## Installing 2" - 16" HP 32 and HP 40 Products

For 2" - 6" sizes use the sames methods referred to in the HP 16/ HP 25 system. Because the 8"-16" HP 32/HP 40 systems have a steeper $13 / 4$ taper angle vs the 1 degree on the HP 16/HP 25 system, hydraulic come-alongs are not required. Use FGS approved strap clamp kits (these can be purchased through FGS) or rubber lined riser clamps fitted to the pipe OD. Place clamps approximately 3 ' from the end of the joint and tighten securely where they will not slip. A gritty cleaning powder such as Ajax or Comet may be used under the straps if they start slipping. Attach ratchet or chain style come alongs rated to a minimum of 2000 lbs to the strap or riser clamps on each side of the joint. Clean and prep the joint and apply adhesive. Stab the joint together by hand and attach the come along. Slowly pull the joint together. A 5 lb dead blow or rubber hammer may be used to help vibrate the joint as it is being pulled together. Firmly hit the joint 360 degrees around the IJ head or fitting. Keep pressure on the joint until the adhesive has squeezed out and there is no forward movement seen. For all HP 32 and HP 40 systems, the come-alongs must be left on until the joint is fully cured.
Saddles and Reductions (HP 16) - The recommended adhesives for RT or GT systems are ZC-275 or PSX 60. To develop full strength of an adhesive bonded joint, it is important to properly prepare the bonding surfaces as recommended in the following paragraphs. Heat curing the saddle joint reduces cure time, improves the chemical
 resistance as well as the ultimate strength of the bond.

Position the saddle on the pipe and mark around the saddle base. Use a sander or sanding tool ( 24 to 40 grit) to remove all surface gloss from the pipe O.D. where the saddle is to be bonded. (For large diameter pipe, a disc sander is usually more practical.) Use circular or random pattern motion during sanding to eliminate grooves on the pipe surface. After sanding, position the saddle on the pipe and mark the hole to be cut in the pipe. Cut a hole the same size as the saddle outlet using a pilot drill and circular hole or saber saw. Do not force the cutter or it will fray the edges of the hole excessively. Clean all bonding surfaces as required.

Apply a thick coat of adhesive to the O.D. of the pipe and the I.D. of the saddle, and the edges of the pipe wall exposed by the hole. Place the saddle over the hole and clamp with two hose clamps or a strap clamp. The clamps may be left on after the joint is cured.
Using a large screw driver, hand tighten the hose clamps alternately until secure and adhesive squeezes out all the way around the saddle. This will ensure that the pipe O.D. conforms to the saddle run. To cure a saddle it is recommended that two
 heating collars be used, one on each side of the saddle "run". An alternate method is to use a box lined with industrial heavy duty foil and an industrial heat gun. When using the foil method cut a 12 " section of 2" pipe and insert heat gun in the end to prevent over heating. Allow adhesive to cure before bonding in the side run.
Installing Reducer Bushings - Install reducer bushings using a block of wood and a hammer and the same procedures as for bell and spigot pipe. The wood block should be sized to allow the reducer bushing to be counter-sunk in the bell. Some reducer bushings will be counter-sunk before they are actually locked up. For maximum chemical resistance with 8 " and larger Green Thread reducer bushings, coat all machined surfaces with adhesive just before assembly.
Making Short Nipples - To make short nipples, be sure the overall length is equal to two insertion lengths plus a minimum of ½" (gap between mating fittings).

The most common way is to:

1. Cut off an existing section of pipe from the bell end that is long enough to be securely contained in a pipe vise or clamped to a table.
2. Use a factory taper or set your taper tool up and taper one end of a longer section of pipe. Cut pipe with taper to the required length you want your pipe nipple to be. Jam the tapered end in to the bell of the pipe in step 1 . Be sure it is secure enough to hold the pipe nipple without spinning.
3. Taper the pipe. The same method "loose bell method" can be used with the 2000 series box tools. Never hold your hand over the end of the pipe when working with the box tools."

## T.A.B. Joints (Threaded and Bonded)

Two T.A.B. wrenches are recommended for 2 " and 3 " and are required for 4 " and 6" T.A.B.xT.A.B. joints. T.A.B to smooth connections do not require T.A.B. wrenches. Prep bonding area and mix adhesive. Spread adhesive over both

T.A.B. connections. Stab joint together and start thread engagement by hand and turn until hand tight. Place T.A.B. wrenches 12 " away from the bonding area. Using the T.A.B. wrenches screw together until firm. Check lock up by moving the joint up and down. No movement should be visible at the joint.

## Joint Cure

Ambient Cure-Cure time is the time required for the adhesive in the assembled joint to harden. Cure time depends on the type of adhesive and the ambient temperature, as shown in Table 12.
You can shorten cure time by applying heat. Although all of the adhesives will cure at ambient temperatures above $70^{\circ}$ F, it is recommended they be heat-cured at temperatures of at least $275^{\circ} \mathrm{F}$ to maximize physical properties and corrosion resistance. See page 43 for instructions for using heat collars for heat-curing joints.
High Temperature Heat Collar (Table 13) - Refer to bulletin for complete operating instructions.

NOTE: Do not bend or fold heating collar as this may break the heating elements and cause the collar to work improperly or not at all.

## Pipe and Fittings:

1. Use the same size heating collar as the pipe size you are installing, with the exception of flanges. Do not use a heating collar that is designed for a larger size pipe.
2. With the uninsulated flap on the bottom (next to the fitting), carefully wrap the heating collar around the joint. Feed the strap through the square ring. $\triangle$ CAUTION: The uninsulated flap is extremely hot when the collar is on. DO NOT TOUCH with bare hands.
3. Tighten the straps until the heating collar is snug against the joint.

## Flanges:

1. For 1 ", $1 \frac{1}{2}$ " and 2 " flanges, an industrial heat gun may be used to cure the joint. Be sure that the end of the gun is at least six inches from the opening of the flange.
2. For 3" through 16" flange joints, use a heating collar that is one pipe size smaller. Remove the straps from the heating collar.
3. Carefully turn the collar inside out with the heated area facing the I.D. of the pipe. Place the heating collar in the I.D. of the flange. A split ring of pipe may be used to hold the collar in place while the joint is curing.
Allow the joint to return to ambient temperature before applying stress to the joint.

NOTE: High Temperature electric heating collars are designed to fit around fittings, and will overlap on pipe joints and couplings. Exceeding the recommended cure time on pipe joints where the heating collar overlaps may shorten the life of the heating collar and/or damage the pipe.

## Table 12

Adhesive Ambient Cure Time

| Adhesive Type | Temperature, ${ }^{\circ} \mathbf{F}$ | Cure Time, hr |
| :---: | :---: | :---: |
| 2000 | 110 | 1 |
|  | 90 | 3 |
|  | 80 | 4 |
|  | 70 | 9 |
|  | 8000 | 60 |
|  |  | 16 |
|  |  | 24 |
|  |  | 1 |
|  | 80 | 2 |
|  | 70 | 6 |
|  | 60 | 12 |
|  | 50 | 18 |

Table 13
Adhesive Cure Time for Electric Heating Collars

| Pipe System \& Adhesive Grade | Pipe Size | Cure Time (minutes) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Pipe ${ }^{(1)}$ | Fitting ${ }^{(2)}$ | Flange | HP 20/HP 25 | HP 32/HP 40 |
| Red Thread <br> Green Thread <br> Silver Streak <br> 2000 or 8000 <br> Series Adhesive | 1-6 | 15 | 20 | 15 | N/A | N/A |
|  | 8 | 20 | 20 | 20 | 30 | 60 |
|  | 10 | 30 | 30 | 30 | 35 | 60 |
|  | 12 | 30 | 30 | 30 | 40 | 90 |
|  | 14 | 35 | 35 | 35 | 45 | 90 |
|  | 16 | 40 | 40 | 40 | 60 | 90 |
|  | $18^{(3)}$ | 90 | 90 | 90 | 120 | N/A |
|  | $20^{(3)}$ | 90 | 90 | 90 | 120 | N/A |
|  | $24^{(3)}$ | 90 | 90 | 90 | 120 | N/A |
|  | $30^{(4)}$ | 120 | 120 | 90 | N/A | N/A |
|  | $36^{(4)}$ | 120 | 120 | 90 | N/A | N/A |

The use of insulation is required below $40^{\circ} \mathrm{F}$ to prevent heat loss.
NOTE: These cure times are for environments warmer than $70^{\circ} \mathrm{F}$. If cooler, see "Cold Weather Installation Tips" or consult NOV Fiber Glass Systems. Adhesives will cure in 24 hours at ambient temperatures of $70-100^{\circ} \mathrm{F}$.
${ }^{(1)}$ Includes sleeve couplings.
${ }^{(2)} 1^{\prime \prime}, 11 / 2$ " \& 2" flanges require the use of an industrial heat gun. Air temperatures inside the flange should be no greater than $400^{\circ} \mathrm{F}$ and no less than $250^{\circ} \mathrm{F}$.
${ }^{(3)}$ Below $50^{\circ}$, the heating collars should be wrapped in insulation to reduce heat loss and are required below 40 F .
${ }^{(4)} 18$ " and larger heat collars require multiple plug 20 amp power outlets.

Heat Packs - Heat packs that cure joints in approximately one hour are also available. Refer to bulletin for complete instructions that are included with each kit. Observe all safety precautions listed on the instruction sheets that accompany the heat packs.

CAUTION: The adhesive bead will cure faster than the adhesive in the joint. It is important that the joint not be pressurized until it has been subjected to the proper time-temperature cycle. A temperature versus time to pressure curve is indicated in the instructions packaged with each adhesive kit.

## Repairs for Red Thread, Green Thread \& Silver Streak Piping Systems

Contact a NOV Fiber Glass Systems field service rep for HP 32/HP 40 repairs.Fiberglass piping systems HP 16/HP 25 are repaired by cutting out a fitting or a damaged section of pipe and replacing it with new material.

CAUTION: Always determine exactly what fluid has been in the piping system as it may be flammable. Contact may be harmful to humans. Take necessary precautions.
Always use the same pipe grade, fittings, and adhesive on new parts as is in the existing system. Do not mix pipe grades.

## Inspecting for Potential Causes of Joint Failure

Joint Back Out - If the bead is no longer next to the edge of the bell, the joint backed out before the adhesive cured.

Cocked Joint - If a joint is cocked or misaligned, there will usually be a large gap between the bell and spigot on one side.

Improperly Cured Joint - If the adhesive bead is soft or flexible, the adhesive is not sufficiently cured.

Weathered Joint - If the machined area appears yellow, the joint may have been exposed to UV degradation.

## Repairing Weather Damage

If machined surfaces of pipe or fittings are exposed to direct sunlight prior to installation, a loss of joint bonding strength may occur. If ultraviolet exposure is greater than two hours, the following steps must be taken:

1. For exposed spigot ends, use 60 to 80 grit sand paper or Emery cloth and lightly sand to remove UV degradation. If UV degradation is too severe, cut 1" from the end of the pipe and retaper.
2. For exposed bell ends (pipe or fittings), sand thoroughly until the entire surface appears fresh. Hand sanding with 40 grit sandpaper is recommended. Use a light sanding operation to prevent changing the taper angle.
NOTE: Couplings or integral bells with T.A.B. threads that have been overexposed must be replaced.

## Repairing Minor Damage

For damaged areas less than one inch in diameter in light chemical orwater service.

Flanged Systems - If possible, simply replace the entire flanged length. Otherwise, cut out the damaged section, then bond new flanges to the remaining pipe ends according to recommended procedures. Next, fabricate a new flange-by-flange spool to the length required. Bolt in the new pipe section.

Flanged fittings should be removed from the system when damaged and replaced with a new fitting.

Tapered Systems - Make a patch to cover damaged area.

1. Cut a length of good pipe to adequately cover the damaged area and extend 3 "-4" on either side of the damaged area.
2. Slit this"patch" lengthwise twice and remove a section so that
 about three-fourths of the circumference remains for 1 "-4" pipe and one-half the circumference for 6 " and larger pipe.
3. Thoroughly sand the inner surface of the patch and sand a corresponding area on the pipe around the damaged section.
4. Clean the bonding surfaces, then apply a thick coating of adhesive to both surfaces,
 snap the patch in place, and apply pressure with hose clamps. The clamps may be left on or removed after curing.

## Repairing Extensive Damage

When the damaged area in the pipe wall is larger than one inch in diameter, or for repair of pipe in severe chemical service that requires a lined product, follow these instructions:

1. When damage is local (less than one inch long, but more than two inches around the circumference of the pipe), check to see if there is enough slack in the pipe to cut out the damaged section, re-taper the cut ends, and bond a sleeve coupling between the tapered ends.
2. When damage is extensive (too large for replacement by a single sleeve coupling), cut out the damaged section, taper the cut ends, and install two sleeve
 couplings and a pipe nipple. This procedure requires sufficient slack in the line to make the final joint by lifting the pipe (or moving the pipe to one side) to engage the bell and spigot joint.
3. If the line cannot be moved sufficiently to install a sleeve coupling or a sleeve coupling spool piece, taper both ends of the pipe and install flanges.
4. If it is impossible to taper the pipe in the ditch, you can install a new section of pipe by over wrapping the plain cut ends.
a. Clean an area large enough for installers to work on both sides and under the pipe. Cut out the damaged section of pipe and measure the gap. Cut a section of good pipe that is not more than one-half inch shorter than the length to be replaced ( $1 / 4$ " maximum gap on each end).
b. Sand the ends of the pipe to remove all resin gloss. Align the replacement pipe section with the pipeline and block up all sections to maintain alignment. All sections must be rigid so they will not move during the over wrapping procedure. Tack welds should be used by placing 1" $\times 2$ " patches of glass cloth and adhesive (four patches spaced at $90^{\circ}$ intervals around the pipe). See Overwrapping.

## Repairing Leaking Joints

Repair Coupling for HP Tapered Products - Repair couplings are available from NOV Fiber Glass Systems for most applications. These couplings may be used on Red Thread HP 16, Green Thread HP 16, Silver Streak and Bondstrand 3000/3200 piping services up to $200^{\circ}$ F. Contact your local FGS representative for recommendations for severe chemical services or
 temperatures above $200^{\circ} \mathrm{F}$.

For the 2" through 10" RT, GT and SS products Bondstrand Maintenance Repair Couplings can be used for services up to 150 psig. For 12 " products the pressure is rated up to 125 psig. For sizes 4" - 12" Red Thread FM Maintenance Coupling Kits may be used on RT, RTFM, GT, SS for a pressure rating up to 200 psig as long as ZC 275 adhesive is used. For installation guidance and instructions please review installation bulletin INS2004.
Overwrapping - If a joint leaks because of improper installation, you can repair it by over wrapping with glass cloth and resin. The temperature in the work area should be $70^{\circ} \mathrm{F}-90^{\circ} \mathrm{F}$. Be sure to protect the over wrap from the sun. System must be open
to atmosphere to prevent pressure from building and blowing through wrap.

1. Use FGS 10 oz. glass cloth. Components for the epoxy overwrap are available in the 8088 repair kit (see Table 14).
2. Use a grinder or sander with
 coarse grit to remove gloss five inches on either side of the joint.
3. Bevel the shoulder to blend in with the pipe wall and add putty to make a smooth transition from fitting to pipe. The length of this putty should be held to a minimum, because the putty has limited pressure capabilities.
CAUTION: There must not be any pressure on the line or any fluid leaking from the joint when performing this procedure.
4. Re-sand and clean surfaces including bevel.
5. Thoroughly mix the adhesive and hardener with the stir stick until there is a uniform color and a consistent flow off the stir stick.

NOTE: Cure time is the time before the line can be tested. Times may vary depending upong temperature, humidity, etc.
6. Using a paint brush, apply the mixed adhesive to all sanded areas.
7. Each piece of glass cloth must be slightly longer than the previous piece, because the O.D. of the pipe becomes larger as you add glass cloth. Cut the first piece to allow for two inches of overlap. When this length is no longer sufficient to overlap at least one-half inch on the ends, determine a new length with two inches of overlap.
8. Center a piece of glass cloth over the joint. Pull on the cloth while positioning it and wet it out by painting with adhesive. Brush to remove any trapped air bubbles in the wrap. Start at one end of the cloth and work around the
 circumference, wetting the cloth with resin. Work the cloth
away from the starting end and from the center of the cloth to the sides. The cloth must be thoroughly wetted with adhesive, but do not spend a lot of time in one area as the cloth will wet out (lose its shiny, white appearance) with time. By the time the cloth has been worked down smoothly with no air beneath it, most of it will be wetted out. An alternate method would be to place a section of clean cardboard or kraft paper on a work table/section of plywood adjacent to the joint to be wrapped. Spread the dry glass out on the table. Wet out each layer by pouring a small amount of adhesive on the glass and spreading it out with the wooden mixing stick or the brush. Be sure the glass is wet out thoroughly but not saturated (dripping). Use the same adhesive to wet out the prepped pipe/fitting surface. Center wet glass over the damaged area or the center of the joint and carefully pull tension around the joint with enough pressure to squeeze out adhesive. Work out any air under the wrap by pushing it out to the side.
9. To prevent thick sections or humps in the over wrap, center the next piece of glass cloth on the joint starting from a new point on the circumference. Never do more than 12 layers at once time. For joints that require more than 12 layers split the procedure into two or more stages. Allow to cure and cool. Lightly sand the glossy areas and repeat Step 8 until all layers are applied.
10. Should the overwrap start to give off heat, discontinue wrapping and let the joint cure and cool with a fan. Sand the cured layers to remove the gloss before restarting the over wrap procedure.
11. Pay particular attention to the bottom of the over wrap as this is the area that may sag and is most difficult to see. Excessive adhesive use may cause this condition.
12. In temperatures above $90^{\circ}$ F, protect the over wrap from direct sunlight with some type of sun shade.

Table 14
Weldfast 8088 Overwrap Repair Kits

|  | $\stackrel{\bullet}{\sim}$ | $\begin{aligned} & 10 \\ & \underset{0}{0} \end{aligned}$ | $\rightarrow$ | $\checkmark$ | $\checkmark$ | N | $\stackrel{?}{\sim}$ | $\sim$ | $m$ | $\checkmark$ | 10 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $$ | $\stackrel{\bullet}{N}$ | $\stackrel{n}{\sim}$ | $\stackrel{N}{\stackrel{N}{N}}$ | $\rightarrow$ | $\stackrel{?}{i}$ | － | $\stackrel{n}{\sim}$ | N | $m$ | $\checkmark$ | $\stackrel{\sim}{\dot{\circ}}$ | ம | $\stackrel{\square}{\sim}$ |
|  | $\cdots$ | $\stackrel{\circ}{*}$ | $\overline{6}$ | $\overline{\%}$ | $\bar{\infty}$ | $\cdots$ | $\bar{\infty}$ | $\cdots$ | $\left\|\begin{array}{cc} i & \overline{0} \\ \infty & -1 \\ \frac{\pi}{n} & \frac{\omega}{6} \\ \frac{\pi}{\sigma} & \frac{\lambda}{\sigma} \\ \frac{\pi}{\sigma} \end{array}\right\|$ |  |  |  |  |  |
|  | シ | $\underset{\downarrow}{ }$ | $\overline{6}$ | $\overline{6}$ | $\overline{\bar{v}}$ | $\bar{\infty}$ | $\bar{\infty}$ | $\bar{\infty}$ | $\cdots$ | $\cdots$ | $\bar{\infty}$ | $\begin{aligned} & \overline{0} \\ & \stackrel{1}{1} \end{aligned}$ | $\begin{aligned} & \overline{0} \\ & \end{aligned}$ | $\begin{aligned} & \overline{0} \\ & \stackrel{1}{1} \end{aligned}$ |
| $$ | $\bullet$ | 6 | $\bullet$ | N | N | の | $\underset{\sim}{N}$ | $\stackrel{1}{7}$ | $\stackrel{\infty}{\sim}$ | $\stackrel{\ominus}{\mathrm{N}}$ | $\stackrel{m}{N}$ | $\stackrel{\ominus}{\sim}$ | $\stackrel{\square}{\sim}$ | ৷ |
|  | $\checkmark$ | ナ | $\bullet$ | $\bullet$ | $\bullet$ | $\bullet$ | $\infty$ | 윽 | $\underset{\sim}{\sim}$ | $\underset{\sim}{\underset{-}{2}}$ | $\underset{-1}{6}$ | $\stackrel{\infty}{\sim}$ | 아N | $\stackrel{\checkmark}{\sim}$ |
| $\stackrel{0}{\circ} \stackrel{\sim}{\sim}$ | $\stackrel{\rightharpoonup}{-1}$ | $\begin{aligned} & = \\ & \underset{-}{\prime} \end{aligned}$ | $\bar{\sim}$ | $\overline{\mathrm{m}}$ | － | $\overline{6}$ | $\cdots$ | $\bar{O}$ | $\stackrel{\underset{\sim}{\sim}}{\sim}$ | $\underset{\underset{-}{*}}{\stackrel{\rightharpoonup}{*}}$ | $\overline{\mathrm{o}}$ | $\stackrel{\bar{\infty}}{\infty}$ | $\begin{aligned} & \overline{\mathrm{O}} \\ & \hline \end{aligned}$ | $\stackrel{\bar{\star}}{+}$ |

NOTE：An 8088L（Large）repair kit is available for 8＂and larger over wraps．A 2088 over wrap kit is available for applications with temperatures at or below $200^{\circ} \mathrm{F}$ ．
${ }^{(1)}$ For $1^{\prime \prime}-6$＂sizes use the 8088 S kit．For 8 ＂through 16 ＂sizes use 8088 L Glass is also available in bulk 125 yard rolls in widths of 8 ＂， $91 / 4^{\prime \prime}$ and 12 ＂and can be used with any 8000 series or 2000 series adhesive．
${ }^{(2)}$ Stagger 8 ＂wide glass to the $10 "$ required width．
${ }^{(3)}$ Stagger 8 ＂or $91 / 4^{\prime \prime}$ wide glass to 10 ＂stagger 12 ＂wide glass to 13 ＂required width．
${ }^{(4)}$ Stagger $8^{\prime \prime}$ or $91_{4}$＂wide glass to $10^{\prime \prime}$ and $12^{\prime \prime}$ wide glass to the $16^{\prime \prime}$ required width．

## Section 5

## Installation <br> Considerations

## Hydrotesting

Testing
System Start-Up
Water Hammer
Fliberglass Flanges
Connecting to Other Systems
Painting Plpe

$\triangle$These procedures must be followed in order to avoid serious personal injury or property damage. Failure to do so will result in loss of warranty, and buyer, installer, or any employee, agent, or representative thereof, assumes the risk of any damage or injury to person or property.

## Hydrotest Frequency

Hydro tests should be performed on sections of the installation as they are completed to ensure installation procedures are satisfactory. The first hydro test should be performed early during a system assembly to ensure installation techniques are providing the performance required. Long pipe line installations should be hydro tested before 2,500 feet have been installed. Fitting intensive systems as found in industrial systems should be hydro tested before 50 joints have been installed.
Hydrostatic testing should be performed to evaluate the structural integrity of a new or modified piping system. Hydro test pressures must meet any local jurisdiction or code requirements and not exceed the hydro test pressure limits for the particular product.

## Safety Precautions

Before hydro testing, supports, anchors and guides must be in place prior to testing an above ground system. A buried piping system must be properly bedded and have sufficient backfill cover between joints to hold the pipe in place. The joints should be left uncovered forvisual inspection during test. Never stand over or at the end of a line that is under pressure.

Locate pressure gauges away from the end of the pipe. A pressure gauge with the test pressure at midscale is recommended. When filling the system for hydro testing, open vents to prevent entrapment of air in the system. Then close the vents and slowly pressurize to the test pressure.

## Hydro Test Procedures

In order to provide a high degree confidence in the piping system, FGS recommends a 10 cycle hydro test at 1.5 times the design operating pressure not to exceed the recommendations in the product data bulletins ranging from 1.25 to 1.5 . Be sure you do not exceed the maximum rating of any other element in the
piping system such as valves, expansion joints, various seals and gaskets that may have a lower pressure rating than the fiberglass. The maximum static rating can be found in bulletins CI1200, CI1225, Cl1300, CI 1320, Cl1325, Cl 1330, Cl1340, CI1350, Cl1351, Cl 1360 and CI 1370

## Filling the Line

When filling the system for hydro testing, open high point vents to prevent entrapment of air. High point vents can be made from saddles, tees or flanges with a valve connection. For systems that do not have high point vents it is recommended that soft pipeline pigs be used to remove trapped air. If air is trapped in the system and you have a failure, catastrophic damage could occur.

## Hydro Test Start Up

Allow the temperature to stabilize before starting test.
Slowly increase pressure to recommended pressure. Initial pressurization should be gradual to prevent pressure surges or water hammer.

## Hydrotest

The hydro test pressurization cycle may be repeated up to ten times from 0 psig (or city water or static head pressure) to the test pressure to provide an additional degree of confidence in the piping system. The intermediate pressure cycles should be held a minimum of 5 to 10 minutes. The final pressurization should be held for a period of one to two hours to allow the system to stabilize and slow leaks or pressure drops to be detected. The pressure may be lowered as deemed necessary by the on-site safety engineers prior to a full visual inspection of the piping system after the final pressure cycle.

Monitor the test pressure closely to avoid over pressurization. Pipe lines exposed to the sun can heat up quickly resulting in a pressure rise. If this happens bleed the line to original test pressure. The reverse is possible if the line is exposed to cold temperatures. If left under pressure over night during cold weather the water may cool resulting in a system pressure drop. Allow the water to warm back up to original input temperature before assuming a leak.

## Checking The Line For Leaks

Walk the line to check for leaks. Do not stand orwalk near the top or end of the line. Generally you are looking for moist spots under the joints. Brown kraft paper under the joints can help ease the visual ability to spot a leak. Do not repair a leak while the system is pressurized.

## De-Pressuring The Line

Upon completion of hydro test, slowly open vents and drains to relieve the pressure on the system. Be sure you open vents to allow for complete drainage of the system and prevent a vacuum type failure. If the drain is open and the vents are closed the system could create a vacuum resulting in damage to the pipe.

It is highly recommended that piping systems operating at $150^{\circ} \mathrm{F}$ or higher and/or have a critical medium, should be tested to the maximum allowable test pressures as determined in the previous paragraphs.
Air Testing: Hydrostatic test should be used instead of air or compressed gas if possible. When air or compressed gas is used for testing, tremendous amounts of energy can be stored in the system. If a failure occurs, the energy may be released catastrophically, which can result in property damage and personal injury. In cases where system contamination or fluid weight prevents the use of hydrostatic test, an air test may be used with extreme caution. To reduce the risk of air testing, use the table below to determine maximum pressure. When pressurizing the system with air or compressed gas, the area surrounding the piping must be cleared of personnel to prevent injury. Hold air pressure for one hour, then reduce the pressure to one half the original. Personnel can then enter the area to perform soap test of all joints. Again, extreme caution must be exercised during air testing to prevent property damage or personnel injury. If air or compressed gas testing is used, NOV Fiber Glass Systems will not be responsible for any resulting injury to personnel or damage to property, including the piping system. Air or compressed gas testing is done entirely at the discretion and risk of management at the job site.

| Pipe Size | $\mathbf{1 " - 6 " ~}$ | 8"-12" | $\mathbf{1 4 " - 4 2 " ~}$ |
| :--- | :---: | :---: | :---: |
| psig | 25 | 15 | 10 |

## System Operation and Startup

On any pressurized piping system, initial start-ups should be gradual to prevent pressure surges which may damage or weaken the piping.

One method is to slowly fill the system while bleeding the air before starting any pumps or opening valves connected to pressurized piping. An alternate method is to start the centrifugal pump against a closed, adjacent valve; then slowly open the valve to gradually build up system pressure. The air should be bled off while the line is filling as in the first method.

For positive displacement pumps, consult NOV Fiber Glass Systems' Engineering for recommendations.

## Water Hammer - Avoiding Problems

Water Hammer is pressure surge in a piping system that causes a violent movement of the system. Usually this pressure surge is caused by a sudden valve closing, electrical outage, pump failure, or some other out-of-the ordinary situation. The pressure surge is usually brief, but damage can be severe. In FRP piping, water hammer usually results in failed fittings due to pipe system movement. Careful location of supports, anchors and guides during design will help control movement of the piping during water hammers. Reducing the pressure surges by installing slow operating valves, a pump bypass or surge protectors in the system is recommended.

Air in a system can also cause water hammer. Be sure to bleed air out of the piping prior to full pressure operation. Any pipe system which moves suddenly, creates a lot of noise, or is unstable, may be influenced by water hammer.

## Fiberglass Flanges

Before bonding the flange onto the pipe, make sure the bolt holes line up with the mating bolt holes on the other system. Do not bolt the flange before bonding, unless insertion depth of the spigot is previously checked to be certain that the spigot does not bottom out or extend through the flange. The use of flat washers on all nuts and bolts is required. The maximum allowable torque is indicated on each flange and is also shown in Tables 15 and 16.

## Connecting to Flat-Face Flanges:

Fiberglass flanges may be joined to flat-face flanges at the recommended torque levels when using proper gaskets.

## Connecting to Raised-Face Steel Flanges:



Filament Wound Flanges
Figure 8.3

When connecting to a raised-face steel flange, one of the following must be utilized:

Option 1 - Use filament wound fiberglass flanges,
Option 2 -Use molded fiberglass flanges and machine the steel flange face until it is flat or use a metal spacer ring to fill the void between the raised-face steel flange and the fiberglass flat-face flange (normally more difficult than machining the steel flange face). If metal spacer rings are not available, it is acceptable to use spacer rings made from materials that are at least as hard as the fiberglass flange.

Option 3 - Use metal back-up rings behind molded fiberglass flanges (See Figs. 8.4 and 8.5).


Compression Molded Flanges
Figure 8.4

| Back-Up Ring Thickness |  |
| :---: | :---: |
| Pipe Size | Ring Thickness |
| $1^{\prime \prime}-12^{\prime \prime}$ | $9 / 16^{\prime \prime}$ |



Interlocking Laminated

Figure 8.5

## Connecting to Lug or Wafer Valves:

Most lined valves need a flat surface to seal against and a sealing surface that is close to their own I.D. to properly seat the lining. Unlined valves with sealing components in the face are in the same category as lined valves.

Sometimes the sealing ridges on the valve face can fall in the wrong place for the grooves in fiberglass flange faces, or they can be too close to the I.D. to seal. When connecting to valves with other than flat-faced flanges, follow these recommendations:

1) For unlined lug and wafervalves without integral seals, use filament wound flanges with no back-up rings or molded flanges with metal back-up rings. (See Fig. 8.3, 8.4, and 8.5)
2) For lug and wafer valves that are lined or have integral seals, use a $1 / 4$ " steel spacer plate with an I.D. equal to Schedule 40 steel or as required by the valve manufacturer. (See Fig. 8.6).


Figure 8.6

## Summary

- Molded flanges are designed to be used against flat-face flanges. When joining to raised-face flanges and lug or wafer valves, steel back-up rings should be used, or spacers fabricated from any material capable of preventing the flange face from bending.
- Filament wound flanges may be mated to raised-face flanges and lug or wafer valves with no back-up rings or spacers if the bolt torque limits shown in Tables 15, and 16 are not exceeded.
- When using lug and wafer valves with integral seals, it may be necessary to use a $1 / 4$ " thick steel flange between the valve and the fiberglass flange to achieve a proper seal. A $1 / 8$ " thick full-face gasket should be used between the steel flange face and the fiberglass flange.


## Standard Bolting Conditions

NOV Fiber Glass Systems' flanges are designed to meet ANSI B16.5 bolt hole standards. For RT, GT \& SS, full-face gasket materials, $1 / 8$ " thick, with a Shore A hardness of 60 to 70 durometer, are recommended.

Flat gaskets made from Teflon ${ }^{\oplus}$ and PVC usually have high durometer ratings and are not acceptable.

Table 15
Stub End Flanges

| Size <br> in | Number ${ }^{(1)}$ of <br> Bolts | Machine $^{(2)}$ <br> Bolt Size | Stud <br> Size | Bolt <br> ft-lb |
| :---: | :---: | :---: | :---: | :---: |
| 2 | 4 | $5 / 8-11 \times 3$ | $5 / 8-11 \times 4$ | 66 |
| 3 | 4 | $5 / 8-11 \times 41 / 2$ | $5 / 8-11 \times 51 / 2$ | 66 |
| 4 | 8 | $5 / 8-11 \times 41 / 2$ | $5 / 8-11 \times 51 / 2$ | 66 |
| 6 | 8 | $3 / 4-10 \times 5$ | $3 / 4-10 \times 6$ | 150 |

${ }^{(1)}$ ANSI B16.5 Class 150 lb . bolt hole standard.
${ }^{(2)}$ Bolt lengths are nominal. When joining our flanges to flanges of other material or manufacturer products, bolt lengths must be calculated.

## Table 16

Bolt, Washer \& Torque Requirements for RT/GT HP 16, SS Flanges \& Flanged Fittings ${ }^{(1)}$, ANSI B16.5 Class 150

| Flange Size in | Number of Bolts ${ }^{(3)}$ | Machine Bolt ${ }^{(2)}$ Size | Stud Bolt ${ }^{(2)}$ Size | Maximum <br> Allowable <br> Torque ft-lb |
| :---: | :---: | :---: | :---: | :---: |
| 1 | 4 | $1 / 2-13 \times 3$ | $1 / 2-13 x 4$ | 25 |
| $11 / 2$ | 4 | $1 / 2-13 \times 3$ | $1 / 2-13 x 4$ | 25 |
| 2 | 4 | $5 / 8-11 \times 3$ | 5/8-11x4 | $30^{(4)}$ |
| 3 | 4 | $5 / 8-11 \times 41 / 2$ | $5 / 8-11 \times 51 / 2$ | $30^{(4)}$ |
| 4 | 8 | $5 / 8-11 \times 41 / 2$ | $5 / 8-11 \times 51 / 2$ | $30^{(4)}$ |
| 6 | 8 | $3 / 4-10 \times 5$ | $3 / 4-10 \times 6$ | $30^{(4)}$ |
| 8 | 8 | $3 / 4-10 \times 51 / 2$ | $3 / 4-10 \times 61 / 2$ | 100 |
| 10 | 12 | $7 / 8-9 x 6$ | $7 / 8-9 \times 71 / 2$ | 100 |
| 12 | 12 | $7 / 8-9 \times 61 / 2$ | $7 / 8-9 \times 71 / 2$ | 100 |
| 14 | 12 | $1-8 \times 7$ | $1-8 \times 8$ | 100 |
| 16 | 16 | $1-8 \times 7$ | $1-8 \times 8$ | 100 |
| 18 | 16 | $11 / 8-7 \times 71 / 2$ | $11 / 8-7 \times 83 / 4$ | 200 |
| 20 | 20 | $11 / 8-7 \times 71 / 2$ | $11 / 8-7 \times 83 / 4$ | 200 |
| 24 | 20 | $11 / 4-7 \times 73 / 4$ | $11 / 4-7 \times 91 / 2$ | 200 |

${ }^{(1)}$ Most flanged fittings are available with molded flanges. Filament wound flanges are available on request.
${ }^{(2)}$ Bolt lengths are nominal. When joining our flanges to flanges of other material or manufacturers products, bolt length must be calculated.
${ }^{(3)} 1^{\prime \prime}-24$ " flanges are ANSI B16.5 Class 150 lb . bolt hole standard.
${ }^{(4)} \mathrm{HD}$ filament wound flanges are available in 2 " -6 " sizes with a maximum allowed torque of 100 ft . lbs.

## Recommended Bolt Torquing Sequence for NOV Fiber Glass

 Systems' FlangesBefore bonding the flange onto the pipe, make sure the bolt holes line up with the mating bolt holes on the other system. Do not bolt the flange before bonding unless insertion depth of the spigot is previously checked to be certain that the spigot does not bottom out or extend through the flange. Certain flanged fittings have recessed bolt holes to provide clearance for bolt installation during assembly. The number and depth of the recesses are shown in Table 17 for standard fittings. To determine the bolt length and size requirements see Table 16. The required bolt length must account for the recess depth and mating flange thickness. Stud bolts are recommended for ease of assembly and the use of washers under nuts is required.

## Table 17

Recessed Bolt Hole Data for Flanged Fittings

| Flange Size in | Recess <br> Depth in | Washer O.D. in | Number of Recessed Holes |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | $\begin{gathered} 45^{\circ} \\ \text { Elbows } \end{gathered}$ | $\begin{gathered} 90^{\circ} \\ \text { Elbows } \end{gathered}$ | Tees |
| 3 | $1 / 4$ | 15/16 | 4 | - | - |
| 8 | $1 / 2$ | $11 / 2$ | 4 | 4 | 8 |
| 10 | 5/8 | $13 / 4$ | 4 | 4 | 8 |
| 12 | $3 / 4$ | $13 / 4$ | 4 | 4 | 8 |
| 14 | $1 / 2$ | 2 | 4 | - | - |
| 16 | $1 / 2$ | 2 | 4 | - | - |




## Connecting to Other Systems

It is often necessary to connect a fiberglass piping to another piping system or make a connection that will not be possible using flanges. Two types of adapters are available: bell or spigot by grooved ends and bell or spigot by threaded ends.

## Adapters

NOTE: When using adapters with spigot ends, it may be necessary to cut off a portion of the factory pipe bell if the groove or threads are not fully exposed.

## A. Grooved Adapters

RT, GT, SS Product: Do not use couplings designed for plastic or cement-lined steel as they can
 leak due to a difference in groove dimensions. Grooved adapters are machined to ES Cut Groove dimensions. Use standard high pressure (Victaulic Style HP70ES) coupling or equivalent.

## B. Threaded Adapters

When using threaded adapters, thread them into the other system before bonding onto fiberglass
 pipe. Otherwise, unless a union is used, it may be impossible to turn the adapter into the mating thread. Use soft set, nonmetallic thread lubricant or two wraps of plumber's tape. CAUTION: Do not over-tighten. Tighten the adapters as if they were brass or other soft material.

## NOTES:

1. The use of NOV Fiber Glass Systems' adhesive to bond a steel or metal pipe into a fiberglass flange is not recommended.
2. If mating a fiberglass system to steel, the preferred method is with flanges. Terminate the old system with their flange and bolt our flange on the new system.
3. Be sure to check the anchors, guides, and supports of an existing system to avoid transfer of any stresses or thermal expansion loads into the fiberglass system.
4. Do not try to cut or machine threads in fiberglass pipe or fittings.

## Special Bolting Conditions

It is often necessary to mate fiberglass flanges with other components which do not have a full flat-face surface such as raised face flanges, butterfly or check valves having partial linerfacings, and Van Stone flange hubs. The addition of a
 hard spacer ring or steel back-up ring placed between the raised face and the outer edge of the flange to form a full flat face on the mating flange is recommended. The purpose of the spacer is to fill the gap outside the raised face to prevent bolt loads from bending and breaking the fiberglass flange.

Pump \& Equipment Connection - Fiberglass pipe connections to pumps or other equipment that involve vibration, shock loads or other mechanical movements should include flexible connectors. These flexible connectors allow for the absorption of vibration and eliminate the placing of undue strain on the pipe and fittings. A bellows-type expansion joint is recommended.

Painting Pipe - All piping O.D. surfaces should be clean and dry before painting. Use a fast-drying solvent such as acetone or trichloroethylene to clean the O.D. of RT, GT, or SS. For longer lasting results the O.D. should be thoroughly sanded or sand blasted. If sand blasting, be careful not to cut or groove the pipe O.D. with an aggressive spray. Fiberglass pipe can be painted with any good quality epoxy ester or two-part epoxy paint. Contact your local paint supplier for a detailed recommendation.

## Section 6

 Helpful Information ConversionsConversions

Decimal Equivalents of Fractions
Definition of Terms
How to Read Flanged or Reducing Fittings
How to Figure a $45^{\circ}$ Offset

|  | Metric Units | U.S. Equivalents |
| :--- | :--- | :--- |
| Lengths | 1 millimeter | 0.03937 inch |
|  | 1 centimeter | 0.3937 inch |
|  | 1 meter | 39.37 inches <br> or 1.094 yards |
|  | 1 kilometer | 1093.61 yards <br>  <br>  |
|  | 1 or 0.6214 mile |  |

## Decimal Equivalents of Fraction

| inches | Decimal of an inch | inches | Decimal of an inch |
| :---: | :---: | :---: | :---: |
| 1/64 | 0.015625 | 29/64 | 0.453125 |
| 1/32 | 0.03125 | 15/32 | 0.46875 |
| 3/64 | 0.046875 | $31 / 64$ | 0.484375 |
| $1 / 20$ | 0.05 | 1/2 | 0.5 |
| 1/16 | 0.0625 | 33/64 | 0.515625 |
| 1/13 | 0.0769 | 17/32 | 0.53125 |
| 5/64 | 0.078125 | 35/64 | 0.546875 |
| 1/12 | 0.0833 | 9/16 | 0.5625 |
| 1/11 | 0.0909 | 37/64 | 0.578125 |
| 3/32 | 0.09375 | 19/32 | 0.59375 |
| 1/10 | 0.1 | 39/64 | 0.609375 |
| 7/64 | 0.109375 | 5/8 | 0.625 |
| 1/9 | 0.111 | 41/64 | 0.640625 |
| 1/8 | 0.125 | 21/32 | 0.65625 |
| 9/64 | 0.140625 | 43/64 | 0.671875 |
| 1/7 | 0.1429 | 11/16 | 0.6875 |
| 5/32 | 0.15625 | 45/64 | 0.703125 |
| 1/6 | 0.1667 | 23/32 | 0.71875 |
| 11/64 | 0.171875 | 47/64 | 0.734375 |
| 3/16 | 0.1875 | 3/4 | 0.75 |
| 1/5 | 0.2 | 49/64 | 0.765625 |
| 13/64 | 0.203125 | 25/32 | 0.78125 |
| 7/32 | 0.21875 | 51/64 | 0.796875 |
| 15/64 | 0.234375 | 13/16 | 0.8125 |
| $1 / 4$ | 0.25 | 53/64 | 0.828125 |
| 17/64 | 0.265625 | 27/32 | 0.84375 |
| 9/32 | 0.28125 | 55/64 | 0.859375 |
| 19/64 | 0.296875 | 7/8 | 0.875 |
| 5/16 | 0.3125 | 57/64 | 0.890625 |
| 21/64 | 0.328125 | 29/32 | 0.90625 |
| 1/3 | 0.333 | 59/64 | 0.921875 |
| 11/32 | 0.34375 | 15/16 | 0.9375 |
| 23/64 | 0.359375 | 61/64 | 0.953125 |
| 3/8 | 0.375 | $31 / 32$ | 0.96875 |
| 25/64 | 0.390625 | 63/64 | 0.984375 |
| 13/32 | 0.40625 | 1 | 1.0 |
| 7/16 | 0.4375 |  |  |

## Definition of Terms

Adapter - A fitting used to join two pieces of pipe, or two fittings, which have different joining systems.
Adhesive - A material formulated to bond together pipe and fittings resulting in high strength and corrosion resistant fabrications.

Anchors - Device to positively restrain the movement of the pipe against all lateral and axial forces.

Bell and Spigot - A joining system in which two truncated conical surfaces come together and bond adhesively. The bell is the female end. The spigot is the male end.

Bushing - A fitting used to join two different sizes of pipe by reducing the size of the female end of the joint. Joints may come threaded ortapered.

Catalyst-See hardener.
Collar-See coupling.
Compressive Force - The force that occurs when a pipe is subjected to crushing loads. Axial compressive forces occur when a piping system is anchored to restrain thermal growth.
Compression Molding - A process for making fittings in which a molding compound is formed and cured into the finished part configuration through pressure and heat in a die.
Concentric Reducer - A pipe fitting used to join two different sizes of pipe while maintaining the same center line.
Contact Molding - A process for making fittings in which cut pieces of fiberglass reinforcement are laid on a mold, saturated with resin, and cured to the finished part shape.
Coupling (collar) - A short heavy wall cylindrical fitting used to join two pieces of the same size pipe in a straight line. The coupling always has female connection ends which can be bell, threaded or a mechanical joining method.
Cure - The hardening of a thermoset resin system by the action of heat or chemical action.

Cure Stages - Stages describe the degree to which a thermoset resin has cross-linked. Three stages, in order of increasing cross linking, include B stage, gelled, fully cured.

Cure Time - The time required for a thermoset material to react and develop full strength. The time is dependent upon the temperature of the material.
Curing Agent - See hardener.
Cut and Mitered Fittings - Fittings manufactured by cutting, assembling and bonding pipe sections into a desired configuration. The assembled product is then over wrapped with resin-impregnated roving or glass cloth, to provide added strength.

Epoxy Resin - A thermosetting resin, usually made from Bisphenol A and epichlorhydrin, cured by a variety of agents such as anhydrides and amines. These resins contain cyclic ether groups. See thermoset.

FRP - Fiberglass Reinforced Plastic.
Filament Wound -A manufacturing method for pipe and fittings in which resin impregnated continuous strand roving wraps around a mandrel to achieve high reinforcement concentration and precise filament placement.
Fillers (extender, pigments, inerts; i.e., sand, etc.) Materials added to a resin which do not affect the cure of the resin but may influence the physical properties of the resin system.

Fitting Types-The classification of fittings by the method of manufacture; i.e., molded, cut and mitered, filament wound, contact molded.

Gel Time - The time it takes for a resin system to harden to a rubber-like state.

Guide - Device that allows free axial movement of the pipe, but restrains lateral movement.

Hand Lay-Up - The forming of resin and fiberglass into finished pipe products or fittings by manual procedures. These procedures include overwrap techniques, contact molding, hand molding and others.
Hardener (accelerator, catalyst, curing agent, promoter) Chemicals added to the resin, single or in combination, which speed up the hardening process, or cause hardening to occur.

Heat Blanket or Heat Collar - An electrical device used to heat a fabrication to reduce cure time.

Hydrostatic Test - A pressure test of a completed fabrication to confirm good quality. Typically, the system is filled with water and held at the selected pressure while checking for leaks.
Impact Resistance - The ability of a part to absorb a striking blow without damage.
Joining (connecting systems) - Any of a variety of methods for connecting two separate components of a piping system together. Included are bell and spigot, threaded and coupled, mechanical devices, etc.
Joint - A term used to describe an individual length of pipe or the actual joining mechanism; i.e., adhesive bonded bell and spigot, threaded and coupled, etc.)
Liner - A generic term used to describe the interior surface in pipe. Generally, liners are resin-rich regions from 0.005 to 0.100 in. thick. Liners may be reinforced with fibrous material such as veil or mat. Liners can provide extra corrosion protection for severe chemical service. They also form a leak barrier (elastomer bladder). The manufacturer may add a liner before, during, or after construction of the pipe wall depending on the manufacturing process.
Lock-Up -A bell and spigot joint engaged sufficiently to eliminate pivot action in the joint.
Matrix - The material used to bind reinforcement and fillers together. This material may be thermoplastic or thermosetting and dictates to a large extent the temperature and chemical service conditions allowable for a pipe or fitting.
Mechanical Force - Physical exertion of power used to achieve lock-up in tapered bell and spigot joints.
Molded Fittings - Pipe fittings formed by compressing resin, chopped fiber and other ingredients in a mold under heat and pressure.
Molding - Any of several manufacturing methods where pressure or compression molding shapes resin and reinforcing materials into final products.

Polyester Resin - Any of a large family of resins which are normally cured by cross linking with styrene. The physical and chemical properties of polyester resins vary greatly. Some have excellent chemical and physical properties while others do not. Vinyl esters are a specific type of polyester resin. Other polyester resins with properties suitable for use in the manufacture of fiberglass pipe include: isophthalic Bisphenol A fumarate and HET acid polyesters. Each type of resin has particular strengths and weaknesses for a given piping application.
Pot Life - The time available to use thermoset adhesives after the reactive materials have been mixed.

Pressure Rating - The maximum anticipated long term operating pressure a manufacturer recommends for a given product. Also referred to as working pressure, pressure class or design pressure.

Reinforcement - Typically, fibers of glass, carbon or synthetic material used to provide strength and stiffness to a composite material.

The type of fiber used as reinforcement plays a major role in determining the properties of a composite, as does the fiber diameter and the type of sizing used. Terms relating to the physical form of the reinforcement include:

Chopped Fiber - Continuous fibers cut into short (0.125 to 2.0 in.) lengths.

Filament - A single fiber of glass; e.g., a mono filament.
Mats - Coarse fabric sheets made from chopped strands randomly placed and held together by resin binders.

Milled Fibers - Glass fibers, ground or milled, into short (0.032 to $0.125-\mathrm{in}$.) lengths.

Roving - A collection of one or more filaments wound into a cylindrical package. The typical form of glass fiber used in the manufacture offilament wound pipe.
Veil - Surfacing mat of porous fabric made from glass or synthetic filaments. Used to provide a resin rich layer or liner.

Yarn - Glass fiber filaments twisted together to form textiletype fibers.

Yield - The number of yards of material made from one pound of the product.

Resin (polymer) - As applied to fiberglass pipe, resin is the polymer or plastic material used to bind the glass fibers together.
Resin - The polymer (liquid plastic) material which hardens with cure to provide a solid form, holding the fiberglass reinforcement in place. Resins provide the corrosion resistance in FRP parts.
Saddle - A fitting which is bonded to the exterior of a pipe to make a branch connection.

Shelf Life - The storage time for a material until it becomes unusable.

Socket Joint - A joining system in which two straight cylindrical surfaces come together and bond adhesively.

Spacers - Wooden strips used to support pipe during storage and handling.
Stress - The force per unit of cross sectional area. Measured in pounds per square inch (psi). This should not be confused with hydraulic pressures, measured as psig or psia, which can induce stress.

Support Spacing (span) - The recommended maximum distance between pipe supports to prevent excessive pipe deformation (bending).
Surge Pressure - A transient pressure increase due to rapid changes in the momentum of flowing fluids. Water hammer is one type of surge pressure. Rapid opening or closing of valves often result in a surge pressure or water hammer.
Thermal Conductivity - The rate at which a material (pipe) transmits heat from an area of high temperature to an area of lower temperature. Fiberglass pipe has low thermal conductivity.
Thermal Expansion - The increase in dimensions of a material (pipe) resulting from an increase in temperature. A decrease in temperature results in thermal contraction.

Thermoset - A polymeric resin cured by heat or chemical additives. Once cured, a thermoset resin becomes essentially infusible, (cannot be re-melted) and insoluble. Thermosetting resins used in pipe generally incorporate reinforcements. Typical thermosets include:

- Vinyl esters • Novolac or epoxy Novolac
- Epoxies •Unsaturated polyesters

Thrust Forces - Commonly used to describe the forces resultant from changes in direction of a moving column of fluid. Also used to describe the axial or longitudinal end loads at fittings, valves, etc., resultant from hydraulic pressure.

Torque - Used to quantify a twisting moment (torsion) in pipe. Torque is measured as a force times the distance from the force to the axis of rotation. Torque is expressed in foot-pounds (ft-lb) or inch-pounds (in-lb).
Two Holing - A method of aligning flanges onto pipe or fittings so that the bolt circle will mate with the adjoining flange.
Vinyl Ester-A premium resin system with excellent corrosion resistance. Vinyl ester exhibits high versatility, temperature resistance and excellent corrosion resistance to acids.

Water Hammer - Pressure surges in a piping system caused by sudden change in fluid velocity, such as operation of a valve, pump, or other component.
Working Life - Same as POT LIFE.

## How to Read Flanged or Reducing Fittings



Lateral
Run x Run x Branch


Cross
Run x Run x Branch x Branch

The above sequence should be used when describing fitting outlets. Drawings or sketches showing outlet types, locations, sizes and dimensional requirements are required for more complicated fitting configurations.

## How to Figure a $45^{\circ}$ Offset



True Length $=$ offset $\times 1.414$
Offset $=$ true length $\times .707$
Examples:
IF: offset = 12"
$12^{\prime \prime} \times 1.414=16.968=1^{\prime}-5^{\prime \prime}$
true length = 1'-5"
(to nearest 1/16")
IF: true length $=24 "$
$24 \times .707=16.968=1^{\prime}-5 "$
offset length $=1^{\prime \prime}-5^{\prime \prime}$
(to nearest $1 / 16^{\prime \prime}$ )

Notes:
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## Fiber Glass Systems

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INS1000ENG March 2017

## Fiber Glass Systems

## Pipe Installation Handbook

## Straight Socket and Butt \& Wrap Joints

- CENTRICAST ${ }^{\text {TM }}$ PRODUCTS

CL-1520
CL-2030
RB-1520
RB-2530

- $\mathrm{F}^{-\mathrm{CHEM}^{\text {TM }}}$
- Z-CORE ${ }^{\text {TM }}$


# NOV FIBER GLASS SYSTEMS PIPE INSTALLATION HANDBOOK 

## Straight Socket Joints and Butt \& Wrap Joints

This fabrication manual is offered to assist you in the proper fabrication and installation procedures when assembling your NOV Fiber Glass Systems piping system.

If you do not find the answer to your questions in the manual, feel free to contact your Regional Manager, local distributor, or the factory.

The products must be installed and used in accordance with sound, proven practice and common sense.

The information supplied in our literature must be considered as an expression of guidelines based on field experience rather than a warranty for which we assume responsibility. NOV Fiber Glass Systems offers a limited warranty of its products in the Terms and Conditions of Sale. The information contained in the literature and catalogs furnished cannot ensure, of itself, a successful installation and is offered to customers subject to these limitations and explanations.

It is our policy to improve its products continually. Therefore, the company reserves the right, without notice, to change specifications and/or design at any time without incurring an obligation for equipment previously sold. Descriptions contained in this catalog are for the purpose of identification and neither limit nor extend the standard product limited warranty set forth in the Terms and Conditions of Sale and Trade Customs.

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CL = Centricast Plus CL-2030 or Centricast CL-1520 Piping Systems RB = Centricast Plus RB-2530 or Centricast RB-1520 Piping Systems ZC = Z-Core Piping Systems FC = F-Chem Piping Systems

## FABRICATION AND INSTALLATION ASSISTANCE

Installing fiberglass pipe is easier than installing carbon steel, stainless steel and lined steel due to light weight. Learning the proper methods to prepare and make-up socket or butt \& wrap joints can help ensure the reliability and long-term performance of your piping system.

We offer the TQI Plus (ASME B31.3) Fabrication and Assembly certification program. Qualified Field Service Representatives train fabrication and assembly crews, conduct and supervise fabrication work, and inspect work in progress.

For complete information concerning these training seminars, contact your local distributor or Regional Manager.

## CAUTION

As this pipe may carry hazardous material and/or operate at a hazardous pressure level, you must follow instructions in this manual to avoid serious personal injury or property damage. In any event, improper installation can cause injury or damage. In addition, installers should read and follow all cautions and warnings on adhesive kits, heat packs, propane torches, etc. to avoid personal injury. Also, observe general safety practices with all saws, tools, etc. to avoid personal injury. Wear protective clothing when necessary. Make sure work surfaces are clean and stable and that work areas are properly ventilated.

> Safety Data Sheets (SDS) are available on our web site at www.nov.com/fgs.

## PART I <br> PIPE PRODUCTS

## DESCRIPTION OF PIPE PRODUCTS

The performance characteristics of a fiberglass pipe system depend on several important elements including the resin and curing agent, as well as the manufacturing process and type and thickness of the pipe's corrosion barrier.

Our piping systems are manufactured using epoxy, vinyl ester, or isophthalic polyester resin systems. All are heat cured for optimum chemical resistance and physical properties. Match your temperature, pressure and chemical resistance requirements to the piping system.

## Fiberglass piping systems offer:

a. Smooth iron pipe size O.D.
b. Used with standard IPS pipe hangers
c. High strength for long spans
d.Excellent corrosion resistance
e.Lightweight
f. Complete line of fittings and accessories available
g. Costs can be optimized by selecting pipe grades for specific services
h. Full vacuum capability in premium grades
i. Easy to repair if damaged

## Centrifugally Cast Pipe

Centrifugally cast FRP pipe (Centricast) consists of reinforcement fabric layers saturated with thermosetting resin, then cured in a casting machine. Cast pipe features a pure resin interior barrier for maximum corrosion resistance. The glass fabric gives the pipe its structural strength and the resin provides the corrosion resistance. Pipe is available in premium epoxy (ZC), epoxy (RB) and vinyl ester (CL) resin grades.
a.Sizes 1" - 14" diameter
b. Straight socket adhesive joint method
c. No special fabrication tools required
d. 10 mil resin-rich exterior resistant to UV attack

## Filament Wound Pipe

Our filament wound pipe begins with resin-saturated fiberglass or other man-made materials as an inner liner or corrosion barrier. The liner is then covered with a resin impregnated filament wound matrix of fiberglass. The matrix is applied under controlled tension in a predetermined pattern to the specified wall thickness.

Custom Filament Wound Product (F-Chem) is available in epoxy, vinyl ester, isophthalic polyester and fire retardant resin grades.
a. Sizes 1"-72" diameter
b. Joining methods include:

- Plain end butt and wrap
- Matched tapered bell \& spigot
c. No special fabrication tools required


## PIPE GRADES

## CENTRICAST PLUS RB-2530

Highly corrosion resistant epoxy pipe grade handles most caustics, salts, solvents, many acids and chemical process solutions up to $250^{\circ} \mathrm{F}$, 100 mil pure resin corrosion barrier. Pipe has durable heavy wall construction for long spans, great impact resistance, tensile, bending and compressive strengths.


## CENTRICAST RB-1520

Epoxy pipe grade recommended for many caustics, acids, salts, solvents and chemical process solutions up to $250^{\circ} \mathrm{F}, 50$ mil pure resin corrosion barrier. Pipe has long spans, integral socket joints, and low thermal expansion loads for the lowest installed cost.

## Z-CORE

Premium epoxy pipe with proprietary resin for outstanding corrosion resistance to aggressive solvents and strong acids, including $98 \%$ sulfuric acid. Rated for temperatures up to $275^{\circ} \mathrm{F}, 100$ mil resin-rich liner. Heavy wall construction for great impact resistance, long spans and low thermal expansion.

## CENTRICAST PLUS CL-2030

Highly corrosion resistant vinyl ester pipe grade used for over 25 years in the harshest hot acid, chlorine, and other chemical services up to $200^{\circ} \mathrm{F}$, 100 mil pure resin corrosion barrier also provides impact and abrasion resistance. Pipe has high strength heavy wall construction.


## CENTRICAST CL-1520

Vinyl ester pipe grade used for many hot acid, chlorine and corrosive chemical services up to $200^{\circ} \mathrm{F}$, 50 mil pure resin corrosion barrier. Long spans, integral socket joints, and low thermal expansion loads provide for a low installed cost system.

## F-CHEM and F-CHEM AR*

Custom filament wound construction offers more flexibility in resin systems, corrosion barriers and wall thickness than our standard products. Let us assist you in selecting the right pipe for a specific application.
*AR grade is manufactured for added
 abrasion resistance.

## FITTINGS

Fittings are color coded. Epoxy Fittings: RB fittings are brown; Z-Core fittings are dark green or black. Vinyl Ester Fittings: CL fittings are off-white. Be sure to use the correct grade of pipe and fittings for your service. Consult Bulletins for pressure rating limits on various fittings. Be sure your system pressure requirements do not exceed the lowest rated component fittings.

Most compression-molded fittings have a center line dot or cross which will assist you in making measurements. Take-off dimensions for most standard fittings are shown in Tables 6 on page 21. The positive stop or "land" in the socket helps you make exact fabrications.


## ADHESIVES

Adhesives are formulated for specific use with the companion pipe grades. Use only the recommended adhesive with each pipe grade - do not mix systems! Standard adhesives are a two-component system (Parts A and B) which must be mixed prior to use. CL-200 Quick Set (QS) adhesives are available for reduced cure time where necessary. Detailed instructions for adhesives are provided with each kit. Read these instructions thoroughly and follow the recommended procedures. The pot life and cure time of the adhesive is dependent on temperature; refer to pages 6, 28, 30, and 36. Ambient temperatures above $100^{\circ} \mathrm{F}$ require extra care by the fabricator to assure sufficient working time of the adhesive. Refer to Adverse Weather Recommendations on page 11.

## ADHESIVE SELECTION

Standard adhesive kits are designed to be used with specific piping systems as shown below.

TABLE 1. Adhesive Selection

$\left.$| Use with <br> these <br> piping systems | Kit <br> Number${ }^{(1)(2)(3)}$ |
| :---: | :---: | :---: |$\quad$| Maximum |
| :---: |
| Service |
| Temperature | \right\rvert\,

## Notes:

1. Although all of the adhesives will cure at ambient temperatures above $70^{\circ} \mathrm{F}$, it is recommended they be heat-cured at temperatures of at least $275^{\circ} \mathrm{F}$ to maximize physical properties and corrosion resistance. See pages 27-30 for instructions for using heat blankets or collars for heat-curing joints.
2. For complete detailed instructions on using adhesive, refer to the step-by-step instruction bulletin included in the adhesive kits.
3. Refer to Chemical Resistance Guide, for adhesive chemical resistance rating.
4. Quick-set adhesive for use when faster cure time is required and the ambient temperature is below $90^{\circ} \mathrm{F}$. Weldfast CL-200-QS is the same as Weldfast CL-200 except a third component, Part C, has been added to the kit.

## ADHESIVE WORKING LIFE

Working life or pot life is the time it takes for the adhesive to harden in the mixing can. Refer to Table 2.

| TABLE 2. Adhesives Estimated Pot Life |  |  |  |
| :---: | :---: | :---: | :---: |
| Pipe Resin <br> Systems | Adhesive | Pot Live <br> @ 70 <br> (min.) <br> (see note) | Pot Live <br> @ 90⿳⺈ <br> (min.) <br> (see note) |
| Epoxy | 275 | $30-40$ | $15-25$ |
| Vinyl Ester | 200 | $20-30$ | $6-12$ |
| Vinyl Ester | 200 QS | $7-15$ | $4-7$ |
| Vinyl Ester | Butt Weld* | $20-40$ | $8-15$ |

NOTE: Pot life is the time available for fabrication. Times may vary depending upon temperature, humidity, etc.

* Based on 16 ml of catalyst per quart of resin.

| TABLE 3. Approximate Number of Bonds per Kit |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Pipe Size (in.) |  |  |  |  |  |  |  |  |  |
|  | 1 | $11 / 2$ | 2 | 3 | 4 | 6 | 8 | 10 | 12 | 14 |
| Number of Joints | 12 | 10 | 8 | 5 | 3 | 2 | 1 | $1 / 2$ | $1 / 2$ | $1 / 3$ |

## FABRICATION ACCESSORIES

## Heat Blankets and Heat Collars:

 Silicone heat blankets and high temperature heat collars are offered for use in curing of adhesive socket joints. The blankets and collars have a pre-set thermostat which controls the temperature of the unit. See pages 27-30 for instructions and cure times for adhesive joint fabrications.


Heat Guns: High wattage electric heat guns are also available to heat adhesive joints. The heat guns are 1600 watt capacity.

JOINING SYSTEMS

## Socket Joint:

Straight socket adhesive joints have positive stop lands for precise makeup.


## Butt \& Wrap Joint:

Two pieces of plain end pipe or pipe and fittings are butted together, then several layers of resin saturated mat or woven roving are wrapped
 around the area and cured. Highly reliable joint in critical service applications.

# PART II <br> SITE CONSIDERATIONS 

## STORAGE AND HANDLING

## Pipe and Fittings

Fiberglass reinforced pipe, fittings, and adhesives require special storage and handling. Care should be taken in transporting, unloading, handling, and storing products to prevent impact and other damage.

When transporting pipe, the spacers under and between the pipe joints must be of sufficient width to avoid point loading, which could produce cracking or buckling damage. A minimum of four spacers should be used for supporting 14" and larger 40' long pipe joints. More spacers should be used for smaller pipe or if pipe is stacked over eight feet high.

Due to its light weight, lifting equipment is usually not required for 1"-14" pipe. When lifting equipment is required, use nylon slings or chokers. Do not allow chains or cables to contact the pipe during transport or handling. If a pipe or fabrication is more than 20 feet long, use at least two support points.

For storage, a board ( $2 \times 4$ minimum) should be placed under each layer of pipe approximately every five feet. The intent is to support the pipe and distribute the load evenly. The pipe should also be braced on either side of the pipe rack to prevent unnecessary pipe movement. Avoid placing pipe on sharp edges, narrow supports, or other objects that could cause damage to the pipe wall. When storing pipe directly on the ground, select a flat area free of rocks and other debris that could damage the pipe.

Pipe is furnished factory packaged in compact, easy-to-handle bundles complete with protective end caps. Leave these caps in place until installation time to protect the pipe ends as well as to prevent dirt or other material from getting into the pipe. Fittings are packaged in cardboard boxes and should be stored in a dry area. If fittings are removed from the boxes, protect machined bells and spigots from exposure to direct sunlight.

Pipe can be damaged when joints or bundles of pipe are dropped during handling or shipping. Severe localized impact blows may result in damage to the fiberglass reinforced structure in the pipe wall. Before installation, inspect the pipe's outer surface and inner surface (if possible) for any damage. Do not use damaged pipe unless inspected and approved by a company representative. If impact damage occurs, the damaged areas may be recognized by a star type fracture on the interior of cast pipe or the exterior of filament wound pipe. Pipe that has been damaged should have a length cut away approximately one foot either side of the damaged or cracked area.

## Note:

Do not allow the bell end of the pipe to support any pipe weight.

Do not allow deformation of the pipe due to supports or straps.

## Adhesive

We recommend adhesives be stored in a dry area where temperatures do not exceed $80^{\circ}$ F. Refer to adhesive instructions included in each kit for storage life recommendations. Vinyl ester adhesives are particularly susceptable to damage caused by high temperature storage.

## TOOLS, EQUIPMENT and SUPPLIES <br> REQUIRED FOR INSTALLATION

For maximum efficiency, the following tools and equipment are recommended prior to any installation:

- Fab Tables, Pipe Stands, Jacks \& Vise
- Hand Tools
- Level - Marking Pen - Tape Measure - Pipe Wrap
- Hacksaw (22-28 teeth/inch)
- Power Tools
- 1" or 2" drum sander
- Disk sander
- Circular power saw with a grit edge abrasive blade, aluminum oxide, carbide or diamond.
- Band Saw with 16-22 teeth/inch at speeds of 200-600 ft./min.
- Saber saw with carbide-tipped blade
- Chop saw with aluminum oxide blade
- Heat gun and heat blanket may be required
- Expendables
- Impermeable Gloves
- Chemical Splash Goggles
- Clean, Dry, Lint-Free Shop Cloths
- Sandpaper Disc/Emery Cloth (36-60 grit)

We suggest securing an area where work can be planned, staged, and quickly executed more efficiently. Power tools greatly reduce the time required to sand pipe and fittings prior to bonding.

Equipment for Cool Weather (Below $70^{\circ} \mathrm{F}$ ) pipe assembly:

- Heat source
- Portable torch with spreader tip, or
- Portable electric heat lamp, or
- Industrial heat gun
- A means of maintaining adhesive kits at $70^{\circ}-80^{\circ} \mathrm{F}$ :
- A box with a 25 watt light bulb, or
- Inside of a vehicle.
- Heat assisted curing
- Electric heating collars or blankets
- Chemical heat packs


## RECOMMENDATIONS FOR FABRICATION IN ADVERSE WEATHER CONDITIONS

FRP piping can be installed in adverse weather conditions when the necessary precautions are taken. Actual work will often be more quickly completed in high temperature conditions. Low temperatures can increase the work time $20 \%-35 \%$ over normal shop conditions. A similar increase is common for high moisture conditions.

## Hot Weather Installation Tips

Hot weather conditions, temperatures above $90^{\circ} \mathrm{F}$, will greatly reduce the working time of the adhesive. The following steps are recommended when fabricating in hot weather conditions:

1. Avoid direct sunlight on the joining surfaces.
2. Store adhesive in a cool area.
3. Keep mixed adhesive in an ice chest with sealed bag of ice or ice pack.
4. Refer to the field fabrication instructions supplied in adhesive kit for the proper amount of catalyst in vinyl ester kits.
5. Butt weld laminates must be "staged" by applying no more than four layers of fabmat at a time. Staging prevents excess exothermic heat. Sand the bonding surface after each stage has gelled and cooled to less than $120^{\circ} \mathrm{F}$.

## Cold Weather Installation Tips

Adhesive cure time is directly related to the temperature. Colder temperatures result in longer cure times.

The following steps should be used when fabricating in colder temperatures:

1. Adhesive kits should be placed in a warm room for six to twelve hours before application in order to reach temperatures of $80^{\circ} \mathrm{F}-100^{\circ} \mathrm{F}$. This will make mixing much easier and speed cure times. Or use a box with a 25 watt light bulb to warm adhesive kits.
2. When possible, piping should be bonded indoors into subassemblies. The warmer conditions of these areas will allow faster cure times.
3. Pre-warm bonding surfaces to $80^{\circ} \mathrm{F}-100^{\circ} \mathrm{F}$ when temperature falls below $70^{\circ} \mathrm{F}$.
4. Refer to the field fabrication instructions supplied in the adhesive kit for the proper amount of catalyst for vinyl ester kits.
5. A heat gun, collar or blanket may be used to obtain a faster cure time. Apply a layer of fiberglass insulation or a welding blanket around the heat collars or blankets when installation temperatures are below $50^{\circ} \mathrm{F}$.

## Extreme Moisture

## Adhesive Joints

- If fittings or pipe have moisture on the bonding surface, wipe them dry prior to sanding.
- Sand pipe or fittings immediately before applying the adhesive to bond the joint. Sand surfaces until a fresh, dry surface is present, then remove dust with a clean dry cloth, and apply adhesive.
- Cure per the previous recommendations for normal, extreme heat or extreme cold temperatures.


## Laminate Joints

- Keep the glass fabric dry, as resins will not saturate wet fabric. Discard glass fabric which has been wet or exposed to rain, as moisture can remove the bonding agent.
- In high humidity environments, keep the glass fabric in the plastic wrap until ready to use.
- If it is raining, move the work to a shelter, or construct a temporary shelter.
- Bonding surfaces must be sanded immediately prior to application of the resin to the pipe or fitting. Sand or grind until a fresh, dry surface is present, then wipe off the dust and apply resin.
- Saturate the fabric with the resin and apply a coat of resin to the sanded surface prior to applying the fabric.
- Refer to recommendations for conditions of extreme heat, cold, or normal conditions for curing.
- When a laminate requires staging, repeat the above precautions for each step.
- Moisture will not affect the cured laminate joint.


## BURIAL RECOMMENDATIONS

These are general guidelines only. For more details see Engineering and Piping Design Guide.
A. Burial Depth

1. Minimum Burial Depth

Minimum depth in unpaved areas for pipe subjected to vehicular loads depends on pipe type, pipe size, vehicle axle weight, and the bedding material. With a standard legal axle load of $34,000 \mathrm{lbs}$., the minimum depth of cover (from the top of the pipe to the surface) for moderately compacted non-clay bearing soils is shown in Table 4.

The pipe should always be buried below the frost line.
2. Maximum Burial Depth

Maximum burial depth is dependent on the backfill material. For moderately compacted soils that do not contain large amounts of highly expansive clays, the maximum burial depth is shown in Table 4.

| TABLE 4. Burial Depths* |  |  |
| :--- | :---: | :---: |
| Product | Minimum <br> (ft.) | Maximum <br> (ft.) |
| Centricast CL-1520 | 2 | 20 |
| Centricst CL-2030 | 2 | 20 |
| Centricast RB-1520 | 2 | 20 |
| Centricst RB-2530 | 2 | 20 |
| Z-Core | 2 | 20 |
| F-Chem Custom Piping** | $3-5$ | $12-20$ |

* Based on 1000 psi soil modulus. Refer to Engineering \& Piping Design Guide, for detailed information for your specific application.
** F -Chem is designed for specific burial applications according to AWWA M45.


## B. Trench Preparation

Final bedding of the trench must be as uniform and continuous as possible. Before backfilling, fill all gaps under the pipe with proper bedding material. Avoid sharp bends and sudden changes in slope. It is important to remove all sharp rocks, cribbage, or other foreign objects that could come in contact with the piping.

C. Bedding Requirements

Fiberglass pipe can be damaged by point contact or wear with the trench bottom and walls, improper bedding materials, or adjacent pipe. Use recommended bedding material a minimum of 6 inches thick at the bottom, sides, and top of the piping (refer to Table 5). Adjacent pipes should be spaced the greater of 6 inches or one pipe diameter. The piping can be laid directly on the undisturbed trench bottom if the native soil meets the requirements of a recommended bedding material (refer to Table 5). Never lay fiberglass piping directly against native rock or shale. Always use dry, unfrozen bedding materials that do not contain foreign objects or debris. Never use water flood for compaction. Slurries can be used that are intended for burial of flexible piping systems. When using slurries, care must be taken to prevent floating or deformation of the piping.


TABLE 5. Recommended Bedding Materials

| Bedding Material | Compaction <br> Proctor Density |
| :---: | :---: |
| Crushed rock or pea gravel $3 / 4 "$ <br> maximum size | Not Required |
| Coarse-grained sand or soil with <br> little or no fines | $75-85 \%$ |
| Coarse-grained sand or soil with <br> more that 12\% fines | $85-95 \%$ |
| Sand or gravel with more than <br> $30 \%$ coarse-grained particles | $85-95 \%$ |
| Sand or gravel with less than <br> $30 \%$ coarse-grained particles | Greater <br> than $95 \%$ |

## D. Pipe Support

Fiberglass pipe is flexible and requires the support of the bedding material to keep the pipe round in burial applications. It is very important that a recommended bedding material is properly compacted around the entire circumference of the pipe. (Refer to Table 5) Tamp the bedding material under the bottom half of the piping to prevent voids or areas of low compaction. Vibratory or similar tamping equipment can drive small stones or debris into the pipe wall if they are present in the bedding material. Avoid striking the pipe with tamping equipment as the pipe may be fractured.

Consult the factory if the pipe will be subject to vacuum or high water tables.

E. Road Crossings

When laying fiberglass pipe under road crossings, it may be necessary to pass the pipe through conduit to protect the pipe. Pad the pipe to prevent rubbing or point loads against the conduit.

F. Wall Penetrations

Where the pipe goes through or passes under a concrete structure, precautions must be taken to prevent bending or point loading of the pipe due to settling. A minimum 2" thick pad of resilient material should be wrapped around the pipe to provide flexibility and prevent contact with the concrete. If bolts are used in the resilient material, care should be taken that the bolts, nuts, or washers cannot come into point load contact with the pipe. Bedding depth under the pipe should be increased to a minimum of 12 " or one pipe diameter, whichever is greater, for one pipe joint length away from the concrete.

G. Timing

Test and cover the pipe as soon as possible to reduce the chance of damage to the pipe, floating of the pipe due to flooding, or shifting of the line due to cave-ins.
A. Pipe Hangers

Pipe hangers such as those shown are often used to support pipe in buildings and pipe racks. However, the use of too many hangers in succession can result in an unstable line when control valves operate, and during pump start-up and shutdown.
 To avoid this condition, the designer should incorporate auxiliary guides in the line to add lateral stability.
B. Pipe Guides

Guides are rigidly fixed to the supporting structure and allow the pipe to move in the axial direction only. Proper guide placement and spacing are important to ensure proper movement of expansion joints or loops and to prevent buckling of the line.

The guiding mechanism should be loose so it will allow free axial movement of the pipe. "U" bolts, double-nutted so they cannot be pulled down tight, are often utilized for guides.


Pipe entering expansion joints or expansion loops requires additional guides. Refer to Engineering \& Piping Design Manual, for details.
C. Pipe Supports:

Piping supports for pipe should be spaced at intervals as shown in the pipe product bulletins.

Note: Properly spaced supports do not alleviate the need for
 guides as recommended in the preceding section. Supports that make only point contact
or that provide narrow supporting areas should be avoided. Some means of increasing the supporting area should be used; sleeves made from half of a coupling or pipe are suitable. Support pumps, valves and other heavy equipment independent of the pipe. Refer to pump and valve connection instructions on page 48.
D. Pipe Anchors:

Pipe anchors divide a pipeline into individual expanding sections. In most applications, major pieces of connected equipment, such as pumps and tanks, function as anchors. Additional
 anchors are usually located at valves, near changes in direction of the piping, at blind ends of pipe, and at major branch connections. Provisions for expansion should be designed into each of the individual pipe sections.

Do not install more than one expansion joint or expansion loop between two anchors.

Do not anchor pipe by applying external pressure as point loads, such as a "U"-bolt, directly to the bare pipe.

Refer to Engineering \& Piping Design, for a thorough discussion on supports, anchors and guides.

## CUTTING PIPE

Pipe should be cut using one of the methods referred to under Tools and Equipment on page 10.

1. Measure pipe, remembering to allow for spigot and fitting dimensions.
2. Scribe a cutting guide around the pipe to ensure a perpendicular cut for proper fit.
3. Hold the pipe firmly but not to the point of crushing. If chain vises or other mechanical holding devices are used, care should be taken to prevent crushing or point loading of the pipe. To prevent damage to the pipe, 180 degree sections of the pipe
 can be used for protective covers.
4. Saw the pipe as smoothly as possible. The pipe ends should be square within $1 / 8$ inch.

## NOTES:

a. Centricast pipe should be above $55^{\circ} \mathrm{F}$ when cutting. Preheat with a heat blanket if ambient temperature is below $55^{\circ} \mathrm{F}$.
b. Z-Core pipe should be warmed to a minimum ID temperature of $100^{\circ} \mathrm{F}$ prior to cutting using a heat blanket. c. Inspect the inside diameter of the pipe after cutting to be sure it has not been damaged by saw cracking or during handling.

## ASSEMBLY LAYOUT

Refer to Table 6 on page 21 for "Take-Off Dimensions" for socket joint fittings or Tables 8 and 9 on pages 22-23 for F-Chem fittings. The method for calculation is similar to the method for any other piping system:
a. Determine the required finished length of the pipe spool sections from the drawing.
b. Subtract the take-off dimension for each fitting in the spool section.
c. Cut the pipe to the length determined as the take-off dimension (b. above).
d. As a double check, dry fit the pipe and fitting(s) to confirm the finished length is correct.
e. Mark the cut pipe lengths with the pipe spool identification number from the blueprint to avoid later confusion. Many pipe lengths can be cut at one time to allow improved efficiency in pipe fabrication.

Consult Fittings \& Accessories Bulletins for complete fitting dimensions and other data.
TABLE 6. Take-off Dimensions for CL, RB \& ZC Socket Fittings
Pipe stop to fittings' center line dimensions. The dimensions are used to calculate pipe length requirements to meet pipeline center line to center line dimensions.


| Size | Fig. 265C $45^{\circ}$ Elbow |  | Fig. 255C 90́․ Elbow | $\begin{gathered} \hline \text { Fig. } 275 \mathrm{C} \\ \text { Tee } \end{gathered}$ |  | Fig. 266C |  | Fig. 285C Cross | $\begin{gathered} \text { Fig. 257C } \\ \text { LR } 90^{\circ} \text { Elbow } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | PM | HLU |  | PM | HLU | A | B |  |  |
| In. | In. | In. | In. | In. | In. | In. | In. | In. | In. |
| 1 | 15/16 | 9/16 | 15/16 | 15/16 | 25/16 | - | - | - | 313/16 |
| $11 / 2$ | 1 | 15/16 | 17/16 | 17/16 | $2^{11 / 16}$ | - | - | - | $411 / 16$ |
| 2 | 17/16 | 11/16 | 2 | 2 | $2^{11 / 16}$ | 511/16 | 13/16 | 13/8 | 411/16 |
| 3 | 15/16 | 13/16 | 25/8 | 25/8 | 311/16 | 71/8 | 11/8 | 23/16 | 515/16 |
| 4 | 21/4 | $23 / 16$ | $31 / 4$ | 31/4 | $411 / 16$ | 93/16 | 7/8 | $31 / 2$ | 73/16 |
| 6 | 215/16 | $33 / 16$ | 43/16 | 43/16 | 63/16 | 15\%16 | 55/16 | 43/16 | 9 |
| 8 | - | 35/16 | $47 / 8$ | - | 51/16 | $18^{11 / 16}$ | 55/16 | 53/16 | 12 |
| 10 | - | $311 / 16$ | - | - | $83 / 16$ | 227/16 | 67/16 | 83/16 | $13^{11 / 16}$ |
| 12 | - | $4^{11 / 16}$ | - | - | 93/16 | 2715/16 | 75/16 | 93/16 | $163 / 16$ |
| 14 | - | 53/8 | - | - | 95/8 | - | - | - | 18 |

TABLE 8. Take-off Dimensions for 14" - 72" F-Chem Plain End \& Flanged Fittings


< ©


Plain End Eccentric


Flanged Concentric

## TABLE 9. Take-off Dimensions for 14" - 72" F-Chem Plain End \& Flanged Reducers

| Size (inch) |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{A} \mathbf{B}$ | $\mathbf{C}$ | $\mathbf{D}$ | $\mathbf{E}$ | $\mathbf{F}$ | $\mathbf{G}$ | $\mathbf{H}$ |
| $14 \times 10$ | 10 | 10 | $141 / 4$ | 16 | $183 / 4$ | 21 |
| $14 \times 12$ | 5 | 10 | 17 | 19 | $183 / 4$ | 21 |
| $16 \times 12$ | 10 | 10 | 17 | 19 | $213 / 4$ | $231 / 2$ |
| $16 \times 14$ | 5 | 12 | $183 / 4$ | 21 | $213 / 4$ | $231 / 2$ |
| $18 \times 14$ | 10 | 12 | $183 / 4$ | 21 | $223 / 4$ | 25 |
| $18 \times 16$ | 5 | 12 | $211 / 4$ | $231 / 2$ | $223 / 4$ | 25 |
| $20 \times 16$ | 10 | 12 | $211 / 4$ | $231 / 2$ | 25 | $271 / 2$ |
| $20 \times 18$ | 5 | 12 | $223 / 4$ | 25 | 25 | $271 / 2$ |
| $24 \times 18$ | 15 | 12 | $223 / 4$ | 25 | $291 / 2$ | 32 |
| $24 \times 20$ | 10 | 12 | 25 | $271 / 2$ | $291 / 2$ | 32 |
| $30 \times 20$ | 25 | 12 | 25 | $271 / 2$ | 36 | $383 / 4$ |
| $30 \times 24$ | 15 | 12 | $291 / 2$ | 32 | 36 | $383 / 4$ |
| $36 \times 24$ | 30 | 12 | $291 / 2$ | 32 | $423 / 4$ | 46 |
| $36 \times 30$ | 15 | 15 | $383 / 4$ | 36 | $423 / 4$ | 46 |
| $42 \times 30$ | 30 | 15 | $383 / 4$ | 36 | $491 / 2$ | 53 |
| $42 \times 36$ | 15 | 15 | $423 / 4$ | 46 | $491 / 2$ | 53 |

## PART III SOCKET JOINT FABRICATION

Straight socket adhesive joints are designed for:

1. High strength
2. Easy, quick fabrications
3. Minimum of tools and procedures
4. High reliability

The adhesives provide reinforcement in the bond area and are designed to prevent void areas. There are only a few important procedures, but you must follow them correctly to achieve a good bond. (Note: Follow complete detailed instructions supplied with each adhesive kit.)

## PREPARATION OF 1"-14" CL, ZC \& RB PIPE AND FITTINGS FOR BONDING

Key requirements for a good bond are:

1. $\mathbf{C L}, \mathbf{Z C}$ and RB piping: Measure the length of the socket, add $1 / 2^{\prime \prime}$ and thoroughly sand the pipe OD with $36-60$ grit material until there are no glossy areas. Resand the fittings sockets with 36-60 grit material to thoroughly clean the bond area. A clean, rough surface provides a bond area for good adhesion. Do not use a flapper wheel to sand pipe OD or fitting socket. Use a clean, dry rag or paper towel to remove sanding dust. Do not use solvents. Do not use compressed air to blow sanding dust off the prepared ends as it may contain


Disk power sander for large diameter pipe. Use 36-60 grit abrasive.
bond strength.
"Shoe Shine" method using Emery cloth of 36-60 grit abrasive.


High speed die grinder for sanding sockets. Use drum with 36-60 grit abrasive.

## Never sand the joint surfaces more than two (2) hours before making the joint.

2. Thoroughly mix the adhesive until the color is consistent. A poor mix may result in a leaky connection. Do not mix less than a full kit or try to estimate partial quantities.
3. Thoroughly wet-out the fitting socket (see note 1 for 1" -2 " joint) by working a thin layer (approx. $1 / 16^{\prime \prime}$ ) of adhesive into the bonding
 surface of the fitting. In a similar manner, apply a generous layer ( $1 / 8$ " minimum) onto the pipe's OD. Also coat the cut end of the pipe to prevent chemical attack. Caution: Do not continue to use the adhesive once it has begun to set up in the can.
4. Push the fitting smoothly, straight onto the pipe. Do not turn, twist, or work the fitting as that could pull
 air into the joint and create a void area. Slight rotation (approx. $1 / 22^{\prime \prime}$ ) after insertion is acceptable for fitting alignment. Be sure there is squeeze-out all around the hub of the fitting.
5. Refer to page 29 for
 ambient temperature joint cure. Do not move the joint during the gelling period of the cure cycle. Movement can cause out-of-plumb fitting alignment and a leaky joint. Though not required, heat cure is highly recommended for piping systems carrying fluids at temperatures above $120^{\circ} \mathrm{F}$. Refer to pages $27-31$ for heat curing.

Warning: Do not use the heat blanket or collar on the CL or RB joints until the adhesive fillet is gelled and firm to the touch.

Note: 1", $\mathbf{1}^{1 / 2 ", ~ \& ~ 2 " ~ C e n t r i c a s t ~ P i p e ~-~ S m a l l ~ d i a m e t e r ~}$ adhesive socket joints may be obstructed by excessive adhesive if the following instructions are not followed. Apply adhesive to the fitting socket forcing it into the sanded surface. Make sure all of the bonding surfaces are completely coated with adhesive. Remove the adhesive with the applicator leaving only a very thin film to wet all the bonding surfaces.

Any excessive adhesive left in the fittings socket will be forced into the pipe during joining and may obstruct fluid flow in the system. Wet the end of the pipe leaving a small bead of adhesive. The adhesive will prevent chemical attack of the pipe end. Apply a thin film of adhesive to the pipe forcing it into the sanded bonding surface. Next coat the bonding area of the pipe only with adhesive at least $1 / 4$ " thick. Make sure there is not excessive adhesive on the end of the pipe or in the pipe bore before placing the fitting on the pipe.

## JOINT CURE

## A. Ambient Cure

Cure time is the time required for the adhesive in the assembled joint to harden. Cure time depends on the type of adhesive and the ambient temperature, as shown in Table 10.

Heat Assist Gel: Place an industrial heat gun (1600 watt) approximately 6 " away from the fitting and point at the socket. Continuously rotate slowly around the fitting until the bead is firm to the touch.
Heat Cure: We recommend heat curing all Z-CORE joints with electric heating blanket for maximum joint strength, corrosion resistance, accelerated assembly time, or if the ambient temperature falls below $70^{\circ} \mathrm{F}$. See pages $28-31$ for Instructions for Using Heat Blankets and Collars.

| TABLE 10. Adhesive Ambient Cure Time |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Adhesive Type | Cure time (hrs.) based on temperature ( ${ }^{\circ} \mathrm{F}$ ) |  |  |  |  |  |
|  | 40-50 | 51-60 | 61-70 | 71-80 | 81-90 | 91-100 |
| $\begin{gathered} \text { Epoxy: } \\ 275 \end{gathered}$ | $\mathrm{N} / \mathrm{R}$ | N/R | N/R | 24 | 24 | 24 |
| Vinyl Ester: $\begin{gathered} C L-200^{(1)} \\ \text { CL-200QS } \end{gathered}$ | $\begin{aligned} & N / R \\ & N / R \end{aligned}$ | $\begin{aligned} & N / R \\ & N / R \end{aligned}$ | $\mathrm{N} / \mathrm{R}$ 4 | 24 2 | 24 1 | 24 $N / R$ |

(1) Heat cure highly recommended for piping systems carrying fluids above $120^{\circ} \mathrm{F}$.
(2) Times will be longer a colder temperatures and shorter at higher temperatures.
$N / R=$ Not recommended.

ADHESIVE DISPOSAL: Once the adhesive and hardener have been mixed and reacted, nothing can be extracted, and it is classified as non-hazardous material. Dispose of in a normal manner as other solid waste. Hardener jars, when empty are not subject to EPA regulation and can be disposed of in a normal manner. These guidelines are based on federal regulations. State and local regulations and ordinances should be reviewed.

## INSTRUCTIONS FOR USING HEAT BLANKET AND CONTROLLER

Caution: Refer to Heat Blanket Instructions for complete operating instructions

- Use only with 120 volt power outlet. Special 240 volt heat collars are available.
- Blanket should not be used in wet conditions.
- Tears, cuts or punctures in the blanket can create a potential safety hazard.

1. Use only the proper size heat blanket for the pipe being joined. See Table 11 on page 29.
2. Wrap the blanket around the joint placing the thermistor side out and the smoother side of the blanket down against the joint. Wrap around the joint until reaching the overlap. Once the blanket starts to overlap, place the tail of the blanket through the slit in the thick end of the blanket and pull it tight. The entire joint should be covered now and the small amount of blanket left should be laid out off of the thermistor. Now run the straps around the pipe, put them through their respective slots, and then pull tight. This will ensure a tight-fighting heat blanket providing you with the best cure.
Note: Check heat blanket temperature to be sure it is heating properly.
3. Flange joints require heating from the inside. First, lay the blanket flat with the thermistor down. Next, roll up the blanket from the tail so that once rolled up, the thermistor is facing out towards the inside of the pipe. Insert the blanket into the pipe or fitting to the depth of the adhesive joint. Leave the cord and the remaining part of the blanket exposed. The blanket may be held in position against the ID of the joint being heated by inserting a short section of smaller FRP pipe inside the rolled blanket.
4. Avoid excess flexing of the blanket. Abnormal flexing can cause breakage and shorten the service life of the blanket. DO NOT crease the heat blanket.
5. DO NOT use cleaning solvents. Solvents penetrate the rubber and damage the heating wires.
6. DO NOT carry or move the blanket by lifting it with the cord alone. Support the weight of the blanket separately from the cord to avoid abusing the cord-to-blanket connection.

Improper sizing or use of the heat blankets can cause excess heating which can damage both the piping and heat blankets.

| TABLE 11. Heat Blanket Models |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Pipe Size | 1 "-3" | $4 "-8 "$ | $10 "-14 "$ | $16 "-20 "$ |
| Model | B | C | D | E |

## Heat Blanket Cure Time

High temperature heat collars are to be used to cure Z-Core, CL and RB Centricast pipe and fittings bonded with ZC-275 and CL-200 series adhesive. The adhesive must be gelled before applying heat blankets. The use of high temperature heating blankets maximizes the strength and the corrosion resistance of the joint. The recommended cure times varies with pipe size as shown in Table 12. These cure times are valid for fabrication in environments between $70^{\circ} \mathrm{F}$ and $100^{\circ} \mathrm{F}$. Please refer to Part II, Site Considerations, Adverse Weather Conditions for adverse environmental considerations.

| TABLE 12. Heat Blanket <br> Cure Times |  |  |
| :---: | :---: | :---: |
| Adhesive <br> Grades | Pipe <br> Size | All Joints <br> \& Fittings <br> (hours) |
| ZC-275 | 1 "-14" | 1 |
| CL-200 | $1 "-14 "$ | $1 / 2$ |

Based on controller style heat blanket

The cure time refers to the time a powered heat blanket must remain on the joint being cured. Once the cure time has been reached the blanket may be removed. The joint will be structurally sound and may be moved as required to further the piping system assembly. The joint should be allowed to cool to ambient temperature prior to hydro testing.


#### Abstract

INSTRUCTIONS FOR USING HIGH TEMPERATURE HEAT COLLAR (Refer to Heat Collar Bulletin for complete operating instructions.)


Note: Allow adhesive to gel before applying heating collar.

- Do not bend or fold heating collar as this may break the heating elements and cause the collar to work improperly or not al all.
For Pipe and Fittings:

1. Use the same size heating collar as the pipe size you are installing, with the exception of flanges. Do not use a heating collar that is designed for a larger size pipe. See Table 14 on page 31.
2. With the un-insulated flap on the bottom (next to the fitting), carefully wrap the heating collar around the joint. Feed the strap through the square ring. Caution: The un-insulated flap is extremely hot when the collar is on. DO NOT TOUCH with bare hands.
3. Tighten the straps until the heating collar is snug against the joint.
For Flanges:
4. For 1 ", $1 \frac{1}{2}$ " and 2 " flanges, an industrial heat gun may be used to cure the joint. Be sure that the end of the gun is at least six inches from the opening of the flange.
5. For $3^{\prime \prime}$ through 16 " flange joints, use a heating collar that is one pipe size smaller than the product you are working with. Remove the straps from the heating collar.
6. Carefully turn the collar inside out with the heated area facing the I.D. of the pipe. Place the heating collar in the I.D. of the flange. A split ring of pipe may be used to hold the collar in place while the joint is curing.
For Saddles:
7. Place the heating collar over the saddle outlet. During cool weather, a wind shield is recommended to keep heat on the joint. Saddles must be heat cured for two hours.
Allow the joint to return to ambient temperature before applying stress to the joint.

Note: High Temperature electric heating collars are designed to fit around fittings, and will overlap on pipe joints and couplings. Exceeding the recommended cure time on pipe joints where the heating collar overlaps may shorten the life of the heating collar and/or damage the pipe.
The use of insulation may be necessary below $40^{\circ} \mathrm{F}$ to prevent heat loss.

## High Temperature Heat Collars Cure Times

High temperature heat collars are to be used to cure Z-Core and RB series Centricast pipe and fittings bonded with ZC 275 series epoxy adhesive. The adhesive must be gelled before applying heat collars. The use of high temperature heating collars maximizes the strength and the corrosion resistance of the joint. The recommended cure times varies with pipe size as shown in Table 13. These cure times are valid for fabrication in environments between $70^{\circ} \mathrm{F}$ and $100^{\circ} \mathrm{F}$. Please refer to Part II, Site Considerations, Adverse Weather Conditions for adverse environmental considerations.

## TABLE 13. High Temperature Heat Collar Cure Times

| Pipe <br> Size | All Joints \& Fittings <br> (hrs.) |
| :---: | :---: |
| $1^{\prime \prime}-6^{\prime \prime}$ | $1 / 2$ |
| $8^{\prime \prime}-14^{\prime \prime}$ | 1 |

TABLE 14. High Temperature Heat Collar Models (For use with ZC and RB pipe only)

| Pipe Size | Model Number |  |
| :---: | :---: | :---: |
|  | 110 VAC | $\mathbf{2 4 0}$ VAC |
| $1^{\prime \prime}$ | $005990-500-0$ | $005990-500-1$ |
| $1 \frac{1 / 2 "}{2 "}$ | $005990-501-0$ | $005990-501-1$ |
| $2^{\prime \prime}$ | $005990-502-0$ | $005990-502-1$ |
| $3 "$ | $005990-503-0$ | $005990-503-1$ |
| $4 "$ | $005990-504-0$ | $005990-504-1$ |
| $6 "$ | $005990-505-0$ | $005990-505-1$ |
| $8 "$ | $005990-506-0$ | $005990-506-1$ |
| $10 "$ | $005990-507-0$ | $005990-507-1$ |
| $12 "$ | $005990-508-0$ | $005990-508-1$ |

The cure time refers to the time a powered heat collar must remain on the joint being cured. Once the cure time has been reached the collar may be removed. The joint will be structurally sound and may be moved as required to further the piping system assembly. The joint should be allowed to cool to ambient temperature prior to hydro testing.

# PART IV <br> BUTT \& WRAP JOINT FABRICATION 

## Surface / End Preparation

Note: It is essential to good fabrication that pipe and fitting surfaces be sanded, clean, dry, and free of oil, grease, and solvent contamination.

1. Prepare both ends of the pipe, or pipe and fitting to be joined, by sanding the bonding surfaces with 36 to 60 grit abrasive. The sanded area should extend at least $1 / 2$ " beyond the widest layer of glass.
Example: 14" Pipe Size.
The widest layer of fiberglass is
 8 ", therefore, sand the pipe ends to a distance of $41 / 2$ " from each cut end.
2. Never sand the joint surfaces more than two (2) hours before making the joint.
3. Wipe the sanded area with a clean, dry, lint-free cloth, and avoid touching the surfaces with bare hands or dirty gloves. Do not use solvents.


Interior Surface Preparation
For 24 " and larger piping, where accessible, use a die grinder to sand the interior surface of the pipe $3^{\prime \prime}$ from the joint ends. This will provide a proper bonding surface for applying the veil, mat, and resin to the pipe's interior surface.

## Sealing and Securing The Pipe Ends

Coat the sawed ends of the pipe and/or fittings with catalyzed resin or Weldfast CL-200 Adhesive before joining the ends. Mix Weldfast CL-200 per the instructions in the Weldfast Kit. Sealing the pipe ends protects the fiberglass reinforcement from chemical attack.


## Hot Patches

Hot patches are used to prevent joint movement during the Field Weld procedure. Hot patches are small pieces of Fabmat, approximately 4 " x 6 ", which are included in the Field Weld Kit. Two (2) patches should be used on pipe up to 20" diameter, and three (3) patches on all pipe larger than 20 ". Only a small amount of resin is required to apply hot patches. Mix one pint of resin with 12 ml . of catalyst. Saturate the patches with the catalyzed resin, and apply to the piping with the mat side to
 the pipe.

The hot patches need to harden before applying joint filler. Heat may be applied to accelerate hardening of the catalyzed resin.


## Joint Filler

Weldfast CL-200 adhesive is used to fill gaps and voids caused by uneven saw cuts and differences in pipe outside diameters.

Mix according to the instructions provided in the Weldfast Kit. Apply enough catalyzed adhesive to fill all of the gaps and provide smooth transitions where the pipes join. Let the adhesive harden and re-sand the joining surfaces before applying the Field Weld resin and glass. Heat may be applied to accelerate hardening of the adhesive.

## Mixing The Standard Lay-Up Resin

1. Measure the recommended amount of catalyst using the graduated measuring beaker. See the Cure Times Chart on page 37.
2. Pour the measured catalyst into 1 quart of vinyl ester resin and stir until completely blended. When the resin is properly blended, the color will consistent and will start to foam.

The standard mix of resin is 16 ml . of catalyst for each quart of vinyl ester resin. After the first quart of resin is mixed and a layer of fiberglass has been applied, it may be evident that the ratio of catalyst should be changed to allow more or less working time. If more working time is required, use as little as 13 ml . of catalyst to each quart of resin. This will normally double the pot life and the curing time. If a quicker cure is required, use up to 22 ml . of catalyst for each quart of resin. This will shorten the pot life and cure time.

IMPORTANT NOTE! Never use less than 13 ml . or more than 22 ml . of catalyst for each quart of resin. "Smoking" or "crazing" of a joint indicates an over-catalyzed resin. Joints made with over catalyzed resin will be structurally weak, provide poor chemical resistance, and should not be used.

Inside Corrosion Barrier (24" Diameter and Larger Piping)


Application Diagram - (24" Diameter and Larger Piping)


Inside corrosion barriers improve the structural and chemical integrity of the pipe. When possible, always make inside corrosion barriers when joining large diameter pipe, using the following procedures:

1. Wet the sanded surface of the piping interior with a light coat of catalyzed resin.
2. Arranging the materials

on a flat surface or table top, pre-wet two layers of 4 " wide, fiberglass mat, and one layer of veil. Be sure the veil is the top layer.
3. Apply the pre-wetted layers, centering the glass over the joint. Be sure the veil is toward the center of the pipe.


## Fab-Mat Layers Per Packing List

$\square$

Application Diagram (Smaller Than 24" Diamerter Piping)

5" Veil
4" Mat


## Exterior Corrosion Barrier (Smaller Than 24" Diameter Piping)

 If an inside corrosion barrier cannot be made, a corrosion barrier must be made on the exterior joining surfaces of the piping, using the following procedures:1. Wet the sanded surface of the piping exterior with a light coat of catalyzed resin.
2. Arranging the materials on a flat surface or table top, pre-wet two layers of 4" wide fiberglass mat, and one
 layer of veil. Be sure the veil is the top layer.
3. Apply the pre-wetted layers, centering the glass over the joint. Be sure the veil is against the pipe.

## Applying the Fiberglass Reinforcement

Apply all the fiberglass layers, as supplied in the Field Weld Kit, for the pressure rating and size of the pipe being joined. Start with the narrowest Fabmat at the pipe surface and proceed to the widest Fabmat. (See Application Diagram for the proper sequence and staging of fiberglass strips to be laid-up.)


Pre-wet with resin, a layer of fiberglass on a table or flat surface. Pick up the wetted layer of fiberglass and place it over the joint. Apply each layer of Fabmat with the mat side down. As each layer is applied, roll out the wrinkles or trapped air with the 3 " paint roller.

The catalyzed resin should be continuously worked into the glass until it begins to gel (warms and begins to harden). No more than 4 layers of Fabmat should be applied before the resin is allowed to gel. After each stage has gelled and cooled, sand lightly to remove any burrs before additional layers are applied. Do not move the piping until the joint has hardened and cooled.

## Mixing and Applying The Finish Coat

After all the layers of fiberglass have been applied to the joint, and the joint has gelled or semi-hardened, apply a final coat of catalyzed resin using the $3^{\prime \prime}$ paint roller or a brush. This finish coating is in a separate container marked "Finish Coat Resin." This resin should be catalyzed using the same procedure as for the standard lay-up resin. If less than one quart of Finish Coat Resin is required, reduce the recommended amounts of
 catalyst proportionately.

Application of the special Finish Coat Resin is critical to developing a chemical resistant piping surface and joint.

> ADHESIVE DISPOSAL: Once the adhesive and hardener have been mixed and reacted, nothing can be extracted, and it is classified as non-hazardous material. Dispose of in a normal manner as other solid waste. Excess adhesive and hardener can be mixed, allowed to react, and disposed of as above. If extra jars of adhesive or hardener have accumulated without the other component to mix and react, contact your Regional Manager. Hardener jars, when empty are not subject to EPA regulation and can be disposed of in a normal manner. These guidelines are based on federal regulations. State and local regulations and ordinances should be reviewed.

## JOINT CURE

The minimum required cure time is 24 hours at $70^{\circ} \mathrm{F}$. Inadequate joint strength will result if the catalyzed resin is cured at temperatures less than $60^{\circ} \mathrm{F}$. Heat cure at $200^{\circ} \mathrm{F}$ to $275^{\circ} \mathrm{F}$ will accelerate cure time and increase joint strength.

Heat cure is highly recommended for piping systems carrying fluids at temperatures above $120^{\circ} \mathrm{F}$. Before pressurizing the piping system, or moving the piping, cure the joint. See the Cure Times Chart below.

Note: See pages 48-50 for hydrostatic testing and system start-up procedure.

TABLE 14. VINYL ESTER BUTT WELD KIT CURE TIMES

| Temp <br> $\left({ }^{\circ}\right.$ F) | Part A <br> Shelf Life <br> (months) | Part B <br> Shelf Life <br> (months) | Pot <br> Life <br> (min.) | Gel <br> (ime <br> $($ min. $)$ | Joint <br> Cure <br> Time <br> (hours) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $40-49$ | 6 | 12 | $\mathrm{~N} / \mathrm{R}$ | $\mathrm{N} / \mathrm{R}$ | $\mathrm{N} / \mathrm{R}$ |
| $50-59$ | 5 | 12 | $\mathrm{~N} / \mathrm{R}$ | $\mathrm{N} / \mathrm{R}$ | $\mathrm{N} / \mathrm{R}$ |
| $60-69$ | $3-4$ | 12 | $20-40$ | $25-45$ | 36 |
| $70-79$ | $3-4$ | 12 | $20-40$ | $25-45$ | 24 |
| $80-89$ | $2-3$ | 9 | $15-35$ | $18-38$ | 24 |
| $90-100$ | $1-2$ | 4 | $8-15$ | $10-18$ | 16 |
| $200-250$ | - | - | - | - | $2-4$ |

# PART V <br> INSTALLATION CONSIDERATIONS 

## FLANGE \& FITTING ALIGNMENT

As with any piping system, flanges must be set for proper alignment of bolt patterns and fittings must be set to be plumb. Arrangement of the work pieces before adhesive bonding is the key to easy fabrication.

1. Level the pipe on the work table or pipe stands.
2. Dry-fit components to check dimensions.
3. Layout levels, plumb bobs that will be needed.
4. Follow the recommended procedures in sanding, adhesive mixing and bonding.
5. Immediately after inserting the pipe into the fitting socket, adjust the fabrication for correct alignment. For example, a flange may need to be rotated slightly for correct bolt hole alignment. About $1 / 2^{\prime \prime}$ of rotation on a flange should be the limit of movement. The same applies for plumbing an elbow. Excessive movement can create entrapped air and a leak path when the system is pressurized.
6. Hold the fabrication rigid - no movement - until the adhesive gels. This may require tape, pipe supports, or shims.
7. Check the fabrication during the gel stage to be sure it has not been bumped or moved.
8. Thoroughly heat-cure the joint before applying pressure.

Note: If a fabrication has been moved so that the bond is questionable, pull it apart and re-fabricate. If the adhesive is fresh and soft, simply re-apply adhesive to the pipe and fitting. If the adhesive has begun to gel, it is probably easier to let it cure, sand it off and re-do the entire joint procedure.

Pipe Alignment: Proper alignment is one of the most important tasks performed by the pipe fitter. If done correctly, installation will be much easier and the piping system will be properly fabricated. If alignment is poor, however, fit-up will be difficult and the piping system may not function properly.

Methods of alignment vary widely throughout the trade. The procedure in this manual will enable you to obtain good alignment.

Pipe-To-Pipe: Bond pipe lengths together with coupling. Take a long straight edge and place on top of pipes. Measure several locations to make sure both pipes are parallel with the
straight edge. Adjust pipes as needed. Move straight edge to the side of the pipes and repeat measurements. Correct alignment by moving pipes as needed. Hold pipes rigid until adhesive is gelled.

## 90 Degree Elbow-To-Pipe:

Install fitting on pipe to close visual alignment. Center square on top of pipe. Center second square on elbow's alternate face. Move elbow until squares are aligned. Hold rigid until adhesive is gelled.

Alternate Method: Use same procedure to bond fitting to pipe. Level pipe in stand. Place spirit level on elbow's alternate face and adjust if needed. Move spirit level to opposite direction and rotate to level. Hold rigid until adhesive is gelled.

## 45 Degree Elbow-To-Pipe:

Install fitting on pipe to close visual alignment. Follow procedure described above; squares will cross. To obtain correct 45 degree angle, align the same numbers on the inside scale of the tilted square and adjust fitting to conform. Hold rigid until adhesive is gelled.

Alternate Method: Use same procedure to bond pipe and fitting. Center spirit level on pipe. Next, center 45 degree spirit level on face of elbow and move elbow until 45 degree bubble is centered. Hold rigid until adhesive is gelled.

Tee-To-Pipe: Place square on tee as illustrated. Center rule on top of pipe. Blade of square should be parallel with pipe. Check by measuring with rule at several points along the pipe. Move square 90 degrees to side of pipe and recheck
 plumb by measuring with rule along side of pipe. Hold rigid until adhesive is gelled.

## Flange-To-Pipe:

Step 1 Level pipe in stands or vise. Step 2 Install flange on pipe to close visual alignment. Align top two holes of flange with spirit level. Move flange until bubble is centered.
Step 3 Use spirit level to adjust flange face to be vertical or plumb. Step 4 Rotate assembly 90 degrees and repeat Step 3.
Step 5 Hold rigid until adhesive is gelled.


## Alternate Method:

Step 1 Install flange on pipe to close visual alignment. Align top two holes of flange with spirit level. Move flange until bubble is centered.
Step 2 Center square on face of flange. Center rule on top of pipe. Move flange until square and pipe are parallel.
Step 3 Center square on face of flange. Center rule on side of pipe
 and align as in Step 2.
Step 4 Hold rigid until adhesive is gelled.

## FLANGES

## FLANGE GASKET \& O-RING REQUIREMENTS

For RB, CL, \& ZC, full-face gasketing materials, $3 / 16^{\prime \prime}$ thick, with a Shore A hardness of 60 to 70 durometer, are recommended. F-Chem flanges require full-face gasketing material $1 / 4$ " thick or O-ring seals depending on pressure ratings. Refer to Table 15.

Flat gaskets made from Teflon ${ }^{\circledR}$ and PVC usually have high durometer ratings and are not acceptable.

TABLE 15. Gasket \& O-Ring Requirements for F-Chem Stub Flanges \& Flanged Fittings

| Pipe Size (in.) | Pressure Rating (psig) | Gasket ${ }^{(1)}$ |  | O-Ring ${ }^{(2)}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{aligned} & \text { I.D. } \\ & \text { (in.) } \end{aligned}$ | $\begin{aligned} & \text { O.D. } \\ & \text { (in.) } \end{aligned}$ | Cross <br> Section | I.D. |
| 14 | $\begin{gathered} 50-100 \\ 125-150 \end{gathered}$ | $143 / 16$ - | 21 - | $.275$ | $15.475$ |
| 16 | $\begin{gathered} 50-100 \\ 125 \end{gathered}$ | $16^{3} 16$ | 23112 | $.275$ | $17.455$ |
| 18 | $\begin{gathered} 50-100 \\ 125 \end{gathered}$ | $183 / 16$ - | 25 - | $.275$ | $19.455$ |
| 20 | $\begin{gathered} 50-75 \\ 100 \end{gathered}$ | $203 / 16$ - | $271 / 2$ - | $.275$ | $21.629$ |
| 24 | $\begin{gathered} 50-75 \\ 100 \end{gathered}$ | $243 / 16$ - | 32 - | $.275$ | $26.129$ |
| 30 | $\begin{gathered} 50-75 \\ 100 \end{gathered}$ | $303 / 16$ - | $383 / 4$ - | $.375$ | $31.975$ |
| 36 | $\begin{gathered} 50-75 \\ 100 \end{gathered}$ | $363 / 16$ - | 46 | $.375$ | $36.180$ |
| 42 | $\begin{gathered} 50 \\ 75-100 \end{gathered}$ | $42 \text { 3/16 }$ | $53$ | $.375$ | $44.620$ |
| 48 | $\begin{gathered} 50 \\ 75-100 \end{gathered}$ | 481116 - | $591 / 2$ - | $.500$ | $50.680$ |
| 54 | 50-75 | - | - | . 500 | 56.770 |
| 60 | 50-75 | - | - | . 750 | 62.590 |
| 72 | 50-75 | - | - | . 750 | 75.340 |

(1) Use ANSI 16.1 class 125 lb drilling gasket with a hardness of 50 to 70 durometer on the Shore A scale.
(2) Use O-Ring with a hardness of 50-70 durometer on the Shore A scale.

## STANDARD BOLTING CONDITIONS

Flanges meet OD, bolt circle diameter, number of holes and bolt hole diameter dimensions for ANSI B16.1, 125 lb . cast iron sizes 1"-72" and ANSI B16.5, 150 lb . steel for 1"-24" diameters.

## Notes:

1. Standard Bolt Description:

Diameter - Threads per inch x length.
2. Bolt lengths are nominal. When joining flanges to flanges of other material or manufacturers, the bolt length must be calculated.
3. Use two washers with each bolt. Use SAE standard washers under all nuts and bolt heads up to 48" size. Use USS wrought washers for 54 " and larger sizes.
4. Bolt torque based on National Course threads.
5. ANSI B16.1, 125 lb and ANSI B16.5, 150 lb . flange dimensional designs are identical for sizes 1-24".

TABLE 16. Bolt, Washer \& Torque Requirements for CL, RB, ZC Flanges \& Fabricated Flanged Fittings

| Flange Size (in.) | No. of Bolts | Machine Bolt Size | Stud Bolt Size | Maximum Allowable <br> Torque ft. lbs. <br> Dry/Lubricated |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |
| 1 | 4 | $1 / 2-13 \times 3$ | $1 / 2-13 \times 31 / 2$ | 10/10 |
| $11 / 2$ | 4 | $1 / 2-13 \times 31 / 2$ | $1 / 2-13 \times 4$ | 20/15 |
| 2 | 4 | $5 / 8-11 \times 31 / 2$ | $5 / 8-11 \times 41 / 2$ | 50/35 |
| 3 | 4 | $5 / 8-11 \times 31 / 2$ | $5 / 8-11 \times 41 / 2$ | 50/35 |
| 4 | 8 | $5 / 8-11 \times 41 / 2$ | $5 / 8-11 \times 5$ | 50/35 |
| 6 | 8 | $3 / 4-10 \times 41 / 2$ | $3 / 4-10 \times 51 / 2$ | 50/35 |
| 8 | 8 | $3 / 4-10 \times 51 / 2$ | $3 / 4-10 \times 61 / 2$ | 50/35 |
| 10 | 12 | $7 / 8-9 \times 8$ | $7 / 8-9 x 9$ | 50/35 |
| 12 | 12 | $7 / 8-9 \times 8$ | $7 / 8-9 \times 9$ | 50/35 |
| 14 | 12 | $1-8 \times 101 / 2$ | 1-8×12 | 50/35 |
| Integral Flanged Fittings |  |  |  |  |
| 1 | 4 | $1 / 2-13 \times 3$ | $1 / 2-11 \times 31 / 2$ | 10/10 |
| $11 / 2$ | 4 | $1 / 2-13 \times 31 / 2$ | $1 / 2-13 \times 4$ | 20/15 |
| 2 | 4 | $5 / 8-11 \times 31 / 2$ | $5 / 8-11 \times 41 / 2$ | 30/20 |
| 3 | 4 | 5/8-11x31/2 | $5 / 8-11 \times 41 / 2$ | 30/20 |
| 4 | 8 | $5 / 8-11 \times 41 / 2$ | 5/8-11x5 | 30/20 |

TABLE 17. Bolt, Washer \& Torque Requirements for Van Stone-Type Flanges

| Flange Size (in.) | Backing <br> Flange <br> Material | No. of Bolts | Machine <br> Bolt <br> Size | Stud <br> Bolt <br> Size | Max. Allowable Torque (ft.lbs.) |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Dry/Lubricated |
| 2 | FRP | 4 | 5/8-11x5 | 5/8-11x51/2 | 50/35 |
| 3 |  | 4 | 5/8-11x5 | $5 / 8-11 \times 51 / 2$ | 50/35 |
| 4 |  | 8 | 5/8-11x5 | 5/8-11x6 | 50/35 |
| 6 |  | 8 | $3 / 4-10 \times 51 / 2$ | $3 / 4-10 \times 61 / 2$ | 50/35 |
| 2 | Steel | 4 | 5/8-11x4 | 5/8-11x41/2 | 50/35 |
| 3 |  | 4 | $5 / 8-11 \times 4$ | $5 / 8-11 \times 41 / 2$ | 50/35 |
| 4 |  | 8 | $5 / 8-11 \times 4$ | $5 / 8-11 \times 41 / 2$ | 50/35 |
| 6 |  | 8 | $3 / 4-10 \times 4$ | $3 / 4-10 \times 5$ | 50/35 |

TABLE 18. Bolt, Washer \& Torque Requirements for F-CHEM Flanges \& Flanged Fittings

| $\begin{array}{\|l\|} \hline \text { Pipe } \\ \text { Size } \\ \text { (in) } \\ \hline \end{array}$ | $\begin{aligned} & \text { Pressure } \\ & \text { Rating } \\ & \text { (psig) } \end{aligned}$ | No. of Bolt Holes | $\begin{gathered} \text { Machine } \\ \text { Bolt } 1 \text { (1) } \\ \text { Size } \end{gathered}$ | Stud Bolt (1) Size | Bolt Torque (ft. lbs.) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | (Nom) | (Max) |
|  | 50 | 12 | 1-8x41/2 | 1-8x6 | 75 | 100 |
|  | 75 | 12 | 1-8x5 | 1-8x6 | 85 | 110 |
| 14 | 100 | 12 | 1-8x5 | 1-8x7 | 90 | 120 |
|  | 125 | 12 | $1-8 \times 51 / 2$ | 1-8x7 | 50 | 100 |
|  | 150 | 12 | 1-8×6 | 1-8x7 | 50 | 100 |
|  | 50 | 16 | $1-8 \times 41 / 2$ | 1-8×6 | 75 | 100 |
| 16 | 75 | 16 | 1-8x5 | 1-8x6 | 85 | 110 |
| 16 | 100 | 16 | $1-8 \times 51 / 2$ | 1-8x7 | 90 | 120 |
|  | 125 | 16 | 1-8x6 | 1-8x7 | 50 | 100 |
|  | 50 | 16 | 1188-7x5 | 11/8-7x6 | 75 | 100 |
| 18 | 75 | 16 | $11 / 8-7 \times 51 / 2$ | $11 / 8-7 \times 7$ | 85 | 110 |
| 18 | 100 | 16 | 118 -7x6 | $1118-7 \times 7$ | 90 | 120 |
|  | 125 | 16 | $11 / 8-7 \times 61 / 2$ | 1118-7x8 | 50 | 100 |
|  | 50 | 20 | 1188-7x5 | $11 / 8-7 \times 7$ | 90 | 120 |
| 20 | 75 | 20 | $11 / 8-7 \times 51 / 2$ | $11 / 8-7 \times 7$ | 105 | 140 |
|  | 100 | 20 | 11/8-7x6 | $11 / 8-7 \times 8$ | 75 | 125 |
|  | 50 | 20 | $11 / 4-7 \times 51 / 2$ | $11 / 4 / 7 \times 7$ | 90 | 120 |
| 24 | 75 | 20 | 11/4-7x6 | 1114-7x8 | 105 | 140 |
|  | 100 | 20 | $11 / 4-7 \times 61 / 2$ | $1114-7 \times 8$ | 75 | 125 |
|  | 50 | 28 | $11 / 4-7 \times 6$ | $11 / 4-7 \times 8$ | 105 | 140 |
| 30 | 75 | 28 | $11 / 4.7 \times 61 / 2$ | 1114-7x8 | 120 | 160 |
|  | 100 | 28 | $11 / 4-7 \times 7$ | 1114-7x9 | 75 | 125 |
|  | 50 | 32 | $11 / 2-6 \times 61 / 2$ | 11/2-6x9 | 105 | 140 |
| 36 | 75 | 32 | $11 / 2-6 \times 71 / 2$ | 1½-6x9 | 120 | 160 |
|  | 100 | 32 | 1112-6x8 | 11/2-6x10 | 100 | 150 |
|  | 50 | 36 | 112/2-6x7 | 1112-6x9 | 120 | 160 |
| 42 | 75 | 36 | 1112-6x8 | 11/2-6x10 | 100 | 150 |
|  | 100 | 36 | $11 / 2-6 \times 81 / 2$ | $11 / 2-6 \times 10$ | 100 | 150 |
|  | 50 | 44 | $11 / 2-6 \times 71 / 2$ | 1112-6x9 | 120 | 160 |
| 48 | 75 | 44 | 112-6x8 | 1112-6x10 | 100 | 150 |
|  | 100 | 44 | 1112-6x9 | 1112-6x11 | 100 | 150 |
| 54 | 50 | 44 | $13 / 4-5 \times 8$ | 13/4-5x10 | 100 | 175 |
| 54 | 75 | 44 | 13/4-5x9 | 13/4-5x11 | 100 | 175 |
| 60 | 50 | 52 | $13 / 4-5 \times 81 / 2$ | 13/4-5x11 | 100 | 175 |
| 60 | 75 | 52 | $13 / 4-5 \times 91 / 2$ | 13/4-5x12 | 100 | 175 |
| 72 | 50 | 60 | $13 / 4-5 \times 91 / 2$ | $13 / 4-5 \times 11$ | 125 | 200 |
| 72 | 75 | 60 | $13 / 4-5 \times 11$ | $13 / 4-5 \times 13$ | 125 | 200 |

(1) Special bolt lengths are required for blind flanges.

Recommended Bolt Torquing Sequence for Flanges




SPECIAL
FLANGE
BOLTING CONDITIONS
Often it is necessary to mate flanges with components that do not have a full flat face surface such as raised face flanges, butterfly or check valves with partial liner facings, and Van Stone flange hubs. The addition of a hard spacer ring or steel backup ring placed between the raised face and the outer edge of the flange to form a full flat face on the mating flange is recommended. The purpose of the spacer is to fill the gap outside the raised face to prevent bolt loads from bending and breaking the flange. Spacer rings are not required if a Van Stone-type flange is used when connecting to raised face flanges, valves or pumps.


| Back-up Ring Thickness |  |
| :---: | :---: |
| Pipe Size | Ring Thickness |
| $1^{\prime \prime}-12^{\prime \prime}$ | $9 / 16^{\prime \prime}$ |

Compression Molded Flanges
FIGURE 8.4

## CONNECTING TO OTHER PIPING SYSTEMS

It is often necessary to connect our piping to another piping system or make a connection which will not be possible using flanges. Threaded connections are offered - primarily for instruments, thermo wells, etc. Select the appropriate fitting from the Fittings \& Accessories Bulletins. Victaulic-type grooved adapters are also available for use with Series 77 coupling in certain sizes.

## Threaded Joints

1. Before making any threaded joints, be sure all bonded joints are fully cured.
2. Apply thread lubrication to both male and female threads. A material which remains soft for the life of the joint is preferred. Be sure the thread lube is suitable for the fluid service.
3. Tighten the joint to seal. Do not over-torque. FRP threads should be handled carefully - as if they are brass.

## Notes:

1. The use of adhesive to bond a steel or metal pipe into a flange is not recommended.
2. If mating our piping system to steel or other FRP system, the preferred method is with flanges. Terminate the old system with the other FRP flange and bolt our flange on the new system.
3. Be sure to check the anchors, guides, and supports of an existing system to avoid transfer of any stresses or thermal expansion loads into the system.
4. Do not try to thread pipe or fittings. This is very difficult and risky. Purchase the required factory part.

Tips: If no thread lube is available, the use of Weldfast Part "A" will usually be acceptable. Two wraps of Teflon ${ }^{\circledR}$ tape may also be used in lieu of thread lubricant.

## Pump \& Equipment Connection

Pipe connections to pumps or other equipment that involve vibration, shock loads or other mechanical movements should include flexible connectors. These flexible connectors allow for the absorption of vibration and eliminate the placing of undue strain on the pipe and fittings. A bellows-type expansion joint is recommended, although rubber hose has also been used with success.

## HYDROSTATIC TESTING AND SYSTEM STARTUP

Hydrostatic Testing: When possible, piping systems should be hydrostatically tested prior to being put into service. Care should be taken when testing, as in actual installation, to avoid water hammer.

All anchors, guides and supports must be in place prior to testing the line. To hydrostatically test the line, observe the following:

Water is usually introduced into the system through a oneinch diameter or smaller pipe. Provision for bleeding air from the system should be made. Water should be introduced at the lowest point in the system and the air bled off through a partially open valve or loose flange at all high points in the system. Slowly close the valve, and bring the system gradually up to the desired pressure.

Test pressure should not be more than $1-1 / 2$ times the working pressure of the piping system, and never exceed $1-1 / 2$ times the rated operating pressure of the lowest rated component in the system. When testing is completed open all of the high point air bleeds before draining the piping. This will prevent vacuum collapse of the pipe.

For systems with severe chemical or temperature applications, a cyclic test may replace the static test. Contact us for recommendations.

## Warnings:

Air Testing: Hydrostatic test should be used instead of air or compressed gas if possible. When air or compressed gas is used for testing, tremendous amounts of energy can be stored in the system. If a failure occurs, the energy may be released catastrophically, which can result in property damage and personal injury. In cases where system contamination or fluid weight prevents the use of hydrostatic test, air test may be used with extreme caution. To reduce the risk of air testing,
use the table below to determine maximum pressure. When pressurizing the system with air or compressed gas, the area surrounding the piping must be cleared of personnel to prevent injury. Hold air pressure for one hour, then reduce the pressure to one half the original. Personnel can then enter the area to perform soap test of all joints. Again, extreme caution must be exercised during air testing to prevent property damage or personnel injury. If air or compressed gas testing is used, we will not be responsible for any resulting injury to personnel or damage to property, including the piping system. Air or compressed gas testing is done entirely at the discretion and risk of management at the job site.

For larger diameters, contact Fiber Glass Systems.

| Pipe Diameter |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $1{ }^{\prime \prime}$ | 11/2" | 2" | 3" | 4" | 6" | 8" | 10" | 12" | 14" |
| psig | 25 | 25 | 25 | 25 | 25 | 25 | 14 | 9 | 6 | 5 |

System Start-Up: On any pressurized piping system, the initial start-up should be gradual to prevent excessive loads and pressure surges which may damage or weaken the piping.

One method is to slowly fill the system while bleeding off all air before starting any pumps or opening valves into pressurized piping. An alternate method is to start the centrifugal pump against a closed, adjacent valve; then slowly open the valve to gradually build up system pressure. The air should be bled off while the line is filling as in the first method.

For positive displacement pumps, consult Engineering for recommendations.

## WATER HAMMER - AVOIDING PROBLEMS

Water hammer is a term generally used to describe situations where a pressure surge in the piping system causes violent movement of the system. Usually this pressure surge is caused by a sudden valve closing, electrical outage, pump failure, or some other out-of-the ordinary situation. The pressure surge is usually brief, but damage can be severe. In FRP piping, water hammer usually results in broken fittings due to pipe system movement caused by pressure. Insufficient system anchors, guides and supports allow excessive movement of the piping and creates fitting breaks.

If you suspect water hammer, consult with the project engineer as soon as possible to eliminate the problem. This may require installing slow operating valves, a pump bypass or surge protectors in the system.

More anchors, guides or supports may need to be added. If you can easily move the piping by pushing on it, changes in the pipe support arrangement to restrict movement probably need to be made.

Air in a system can also cause water hammer. Bleed air out of the piping prior to full pressure operation. Any pipe system which moves suddenly, creates a lot of noise, or generally seems unstable is a candidate for problems due to water hammer.

## PART VI SYSTEM REPAIR \& MODIFICATION

Should a leak occur during pressure testing or start up of the piping system, the normal procedure to repair is to cut out a fitting or a damaged section of pipe and replace it with new material.

Determine the fluid that has been in the piping system before beginning repairs to avoid contact with chemicals.

Systems often require modification, added instrumentation, or new branches. Components are available to easily accomplish this.

Always use the same pipe grade, fittings, and adhesive on new parts as is in the existing system. Do not mix pipe grades. If you have questions about the chemical service, pipe grade selection, existing system operating conditions, or other matter, call your local Distributor or Regional Manager.

## Notes:

1. Most leaks in a piping system are due to poor fabrication or improper installation (i.e., not properly anchored, guided or supported).
2. When making repairs, be sure all surfaces to be bonded are dry, clean and thoroughly sanded. Good adhesive connections cannot be made on wet or contaminated surfaces.

## REPLACING DAMAGED PIPE

Pipe leaks through the pipe wall are usually the result of physical damage to the pipe from impact, vacuum, excessive bending, or other abusive conditions. The damaged section should always be replaced by using the following procedures:

Flanged Systems: If possible, replace the entire flanged length. Otherwise, cut out the damaged section and bond new flanges to the remaining pipe ends according to recommended procedures. Next, fabricate a new flange-by-flange spool to the length required. Bolt in the new pipe section.

Flanged fittings should be removed from the system when damaged and replaced with a new fitting.
Attempt to find the cause of the damage and take corrective action. Solve the problem; don't just replace a part.

Socket/Bonded Systems: Cut out the section of pipe which leaks, making sure cuts are square. Dry the pipe ends. Cut a new length of pipe to the same length as that which was cut out. Use split repair couplings to adhesive bond the new pipe into place.

1. Before fabricating connection, all seepage or fluid at the joint area must be eliminated.
2. Sand the outer surface of the pipe thoroughly for a distance of at least 1 " on either side of the anticipated contact area of the coupling, using 36 to 60 grit abrasive. Sand the inner and outer surface and mating edges of the inner two-piece coupling and sand the inner surface and mating edges of the outer two-piece coupling.
3. Brush away all the dust from the sanded areas taking care not to contaminate the sanded surfaces. Do not use a solvent wipe.
4. Slide the hose clamp over one of the pipe ends and out of the way of the joint area.
5. Mix the adhesive in accordance with the instructions provided with the adhesive kit.
6. Coat the inner and outer surfaces and mating edges of the inner coupling with a thin layer of adhesive and set aside.
7. Coat the inner surface and mating edges of the outer coupling with a thin layer of adhesive and set aside.
8. Coat the cut edges of the pipe with a thin layer of adhesive.
9. Coat the sanded outer surfaces of the mating pipe sections with a thin layer of adhesive.
10. Place the two-piece inner coupling on the pipe joint, centered over the butted pipe ends.
11. Place the two-piece outer coupling over the inner coupling with the seam rotated 90 degrees away from the seam of the inner coupling.

12. Place the hose clamp over the center of the outer coupling and tighten.
13. Remove the excessive adhesive.
14. Heat cure the adhesive in accordance with the instructions found in the adhesive kit.


Alternate Method: Use Flanges to install a new section of pipe. Cut out the damaged pipe length. Bond flanges to the remaining pipe ends using proper procedures. Fabricate a flange-by-flange spool to the required length and bolt into place.

## REPLACING DAMAGED FITTINGS

In socket adhesive systems which develop a leak in either a fitting or the socket joint area of a fitting, it will usually be necessary to cut out the leaking part and replace it.

When possible, anchors, guides and supports should be loosened and some movement allowed during fabrication. Use couplings to install new pipe stubs and the new required fitting. Where the system is very rigid, it may be necessary to use flanges to allow bolting in of the replacement part. Also, if fittings are close-coupled, a series of fittings may have to be removed and replaced. Certainly, this is not desired, and an alternate overwrap method might be considered; see page 58.

## Procedures to be followed are:

1. Determine the best location to cut the pipe section which contains the leak. Leave enough pipe length to make socket joints per the recommended procedures.
2. Dry the system.
3. If you can move the pipe ends, use couplings to bond the new part into place. Otherwise, use split repair couplings, similar to the procedures below.

Alternate Method: If the piping arrangement does not allow the use of couplings, bond flanges to the pipe ends and bolt the replacement fitting or section into place.


## OVERWRAP

A leaking fitting, pipe or joint can be over wrapped with a resin and glass lay-up. This requires resin, catalyst, fiberglass reinforcement, tools, and a clean, dry work area. Many times an overwrap is the preferred method, particularly when fittings are in a close, complex manifold or assembly. Custom overwrap kits are available for each pipe size and pressure classification. Contact Fiber Glass Systems.

Application Procedure: Before making the over-wrap, read these instructions carefully.

1. Sand the surface area thoroughly for an equal distance on each side of the leak. The sanded surface should extent at least $1 / 2^{\prime \prime}$ beyond the widest layer of glass supplied with the kit. Remove all surface glazes, paint, oil, grease, scale, moisture, or other foreign material to ensure proper bonding of the resin material to the surface.
2. Use the applicator brush to remove all dust from the sanded area.
3. If repairing a socket joint, use the Weldfast adhesive supplied in the kit to form a tapered bead as shown in this sketch.


The bead will provide a smooth transition from fitting to pipe.
4. Lay out the precut fabmat and surfacing veil on a flat, clean, dry surface (i.e., cardboard, plywood, etc.).
5. Add contents of Part "B" tube(s) to container of Part "A" (resin). Using one of the wooden stirrers, mix the contents thoroughly for at least one minute.
6. Use the applicator brush to apply a liberal, even coating of the resin mixture to the entire sanded surface.
7. Using the $3^{\prime \prime}$ roller, thoroughly saturate the fabmat laid out on your working surface. Apply wet-out fabmat to the joint to be overlaid placing the mat side down. Using the $3^{\prime \prime}$ roller, continue to roll out the material until all entrapped air has been rolled out and the fabmat is contoured smoothly to the surface.
8. For joint sizes 4 " and larger, repeat step \#7 above.
9. Place surfacing veil over the fabmat and, again using the 3 " roller, apply a liberal amount of resin and work out all air as in step \#7.

Be sure that the pipe surface is thoroughly wet out with catalyzed resin.

## Some guidelines on the overwrap are:

1. The overwrap should be equally spaced on each side of the point of the leak.
2. The overwrap should be around the entire circumference of the pipe or fitting.
3. The pressure rating and pipe diameter will determine the overwrap thickness. Consult Fiber Glass Systems' Technical Services to determine specific information about design of the overwrap.
4. The resin system of the overwrap should be compatible with the resin system of the existing pipe or fittings.
5. Cure the overwrap completely before pressure testing.

## TEMPORARY FIXES

Pipe Leaks: The use of a conventional metal pipe clamp is a good method for containing a small leak.

Socket Leaks: Materials are available in the marketplace for making "ace bandage" types of over wraps.

Fitting Leaks: A pinhole type leak can sometimes be stopped by applying a thickness of adhesive over a dry, sanded area.

Caution: If hazardous materials or high pressures are present, replace the damaged pipe or fitting at once. Do not try a temporary repair. Make a permanent repair as soon as possible.

## TAPPING INTO A LINE

The two most common methods for adding a branch or tapping into an existing line are the use of a tee or saddle. Saddles are often rated for lower pressure than the pipe; check the rating of the system versus the saddle. Consult Fittings \& Accessories Bulletins.

Generally, the use of flanges to install a new tee is preferred.

## Installing a Flanged Tee:

1. Cut the pipe, leaving enough pipe to bond flanges onto the existing pipe ends.

2. Using recommended procedures, and with the system dry, bond flanges to the existing pipe ends. Be sure your measurements are exact for the new fitting to fit correctly. Cure the adhesive.

3. Install the new tee.


The procedure for installing an adhesive socket tee will be the same as for replacing a damaged socket fitting (see page 53).

Saddles: Bonding a Saddle onto pipe is similar to making a regular adhesive socket joint. The preferred method is:

1. Lay out the required dimensions. Mark the area to be sanded by positioning the saddle on the pipe and marking the pipe.
2. Sand the entire area where the saddle will bond to the pipe. A power sander or die grinder will save time. Refer to page 24 procedures concerning pipe and fitting preparation. Also, sand the bonding surface of the saddle.

3. Locate the center of the branch hole.
a. Saddle with a cement socket outlet (1"-14"). Cut a hole the same size as the saddle outlet using a hole saw with pilot drill. Do not force the cutting tool as
 this will make a rough hole.
b. Saddles with an IP thread outlet ( $1 / 4$ " -1 "). Prepare the surface as above. Install the saddle prior to drilling the hole. After saddle connection has cured, place a thin metal sleeve in the outlet to protect the threads, drill out the opening and coat the cut edges with adhesive. This eliminates clogging the smaller outlets with the adhesive when the saddle is pressed into position.

4. Generous amounts of adhesive must be applied to the pipe and the underside of the saddle; coat the cut edges of the hole in the pipe. Press the saddle over the hole and press into place. Use two hose clamps to tightly band the saddle onto the pipe.
5. Tighten the clamps so that the adhesive is squeezed out around the saddle. Dress the edges and clean the squeezed adhesive out of the branch as best as you can.
6. Cure the fabrication per the adhesive recommendations. The clamps can either be removed or remain on after the cure is completed.
7. Pipe or fittings in the branch run can now be fabricated.

## PART VII <br> HELPFUL INFORMATION CONVERSIONS

| Centigrade | Fahrenheit | Centigrade | Fahrenheit |
| :---: | :---: | :---: | :---: |
| -200 | -328.0 | 24 | 75.2 |
| -100 | -148.0 | 25 | 77.0 |
| -90 | -130.0 | 26 | 78.8 |
| -80 | -112.0 | 27 | 80.6 |
| -70 | -94.0 | 28 | 82.4 |
| -60 | -76.0 | 29 | 84.2 |
| -50 | -58.0 | 30 | 86.0 |
| -40 | -40.0 | 31 | 87.8 |
| -30 | -22.0 | 32 | 89.6 |
| -20 | -4.0 | 33 | 91.4 |
| -10 | 14.0 | 34 | 93.2 |
| 0 | 32.0 | 35 | 95.0 |
| 1 | 33.8 | 36 | 96.8 |
| 2 | 35.6 | 37 | 98.6 |
| 3 | 37.4 | 38 | 100.4 |
| 4 | 39.2 | 39 | 102.2 |
| 5 | 41.0 | 40 | 104.0 |
| 6 | 42.8 | 41 | 105.8 |
| 7 | 44.6 | 42 | 107.6 |
| 8 | 46.4 | 43 | 109.4 |
| 9 | 48.2 | 44 | 111.2 |
| 10 | 50.0 | 45 | 113.0 |
| 11 | 51.8 | 46 | 114.8 |
| 12 | 53.6 | 47 | 116.6 |
| 13 | 55.4 | 48 | 118.4 |
| 14 | 57.2 | 49 | 120.2 |
| 15 | 59.0 | 50 | 122.0 |
| 16 | 60.8 | 51 | 123.8 |
| 17 | 62.6 | 52 | 125.6 |
| 18 | 64.4 | 53 | 127.4 |
| 19 | 66.2 | 54 | 129.2 |
| 20 | 68.0 | 55 | 131.0 |
| 21 | 69.8 | 56 | 132.8 |
| 22 | 71.6 | 57 | 134.6 |
| 23 | 73.4 | 58 | 136.4 |

CONVERSIONS, Cont'd

| Centigrade | Fahrenheit | Centigrade | Fahrenheit |
| :---: | :---: | :---: | :---: |
| 59 | 138.2 | 94 | 201.2 |
| 60 | 140.0 | 95 | 203.0 |
| 61 | 141.8 | 96 | 204.8 |
| 62 | 143.6 | 97 | 206.6 |
| 63 | 145.4 | 98 | 208.4 |
| 64 | 147.2 | 99 | 210.2 |
| 65 | 149.0 | 100 | 212.0 |
| 66 | 150.8 | 110 | 230 |
| 67 | 152.6 | 120 | 248 |
| 68 | 154.4 | 130 | 266 |
| 69 | 156.2 | 140 | 284 |
| 70 | 158.0 | 150 | 302 |
| 71 | 159.8 | 160 | 320 |
| 72 | 161.6 | 170 | 338 |
| 73 | 163.4 | 180 | 356 |
| 74 | 165.2 | 190 | 374 |
| 75 | 167.0 | 200 | 392 |
| 76 | 168.8 | 210 | 410 |
| 77 | 170.6 | 212 | 414 |
| 78 | 172.4 | 220 | 428 |
| 79 | 174.2 | 230 | 446 |
| 80 | 176.0 | 240 | 464 |
| 81 | 177.8 | 250 | 482 |
| 82 | 179.6 | 260 | 500 |
| 83 | 181.4 | 270 | 518 |
| 84 | 183.2 | 280 | 536 |
| 85 | 185.0 | 290 | 554 |
| 86 | 186.8 | 300 | 572 |
| 87 | 188.6 | 310 | 590 |
| 88 | 190.4 | 320 | 608 |
| 89 | 192.2 | 330 | 626 |
| 90 | 194.0 | 340 | 644 |
| 91 | 195.8 | 350 | 662 |
| 92 | 197.6 |  |  |
| 93 | 199.4 |  |  |

## CONVERSIONS, Cont'd

|  | Metric Units | U.S. Equivalents |
| :---: | :---: | :---: |
| Lengths | 1 millimeter <br> 1 centimeter <br> 1 meter <br> 1 kilometer | ...0.03937 inch ...0.3937 inch . . 39.37 inches or 1.094 yards . . 1093.61 yards or 0.6214 mile |
| Areas | 1 square millimeter <br> 1 square centimeter <br> 1 square meter <br> 1 square kilometer | . . . 0.00155 square inch <br> . . . 0.155 square inch <br> . . 10.764 square feet or 1.196 sq. yards <br> . . . 0.3861 square mile |
| Volumes | 1 cubic millimeter <br> 1 cubic centimeter <br> 1 liter <br> 1 cubic meter | . . . 0.000061 cubic inch <br> . . . 0.061 cubic inch <br> . . . 61.025 cubic inches <br> . . .35.314 cubic feet or 1.3079 cubic yards |
| Capacities | $\begin{aligned} & 1 \text { milliliter (0.001 liter) } \\ & 1 \text { liter . . . . . . . . . . . } \\ & 1 \text { liter . . . . . . . . . . . . } \\ & 1 \text { liter. . . . . . . . . } \end{aligned}$ | . . . 0.0338 U.S. fluid ounce <br> . . . 2.1134 U.S. liquid pints <br> ... 1.0567 U.S. liquid quarts <br> . . 0.2642 U.S. gallon |
| Weights | 1 gram . . . . . . . . . . . <br> 1 kilogram(1000 grams | . . . 0.03527 avoir. ounce or 15.4324 grains <br> 2.2046 avoir. pounds |
|  | U.S. System Units | Metric Equivalents |
| Lengths | 1 inch 2 | 25.4 millimeters or 2.54 centimeters |
|  | 1 foot . . . . . . . . . . . 0 | 0.3048 meter |
|  | 1 yard ............ 0 | 0.9144 meter |
|  | 1 mile . . . . . . . . . . . 1 | 1.6093 kilometers |
| Areas | 1 square inch . . . . . . 6 | 645.16 square millimeters or 6.452 square centimeters |
|  | 1 square foot . . . . . 0 | 0.0929 square meter |
|  | 1 square yard ..... 0 | 0.8361 square meter |
|  | 1 square mile . . . . . 2 | 2.59 square kilometers |
| Volumes | 1 cubic inch . . ..... 1 | 16,387.2 cubic millimeters or 16.3872 cubic centimeters |
|  | 1 cubic foot. . . . . . . 0 | 0.02832 cubic meter |
|  | 1 cubic yard . . . . . . 0 | 0.7646 cubic meter |
| Capacities | 1 U.S. fluid ounce .. 2 | 29.573 milliliters |
|  | 1 U.S. liquid pint . . . 0 | 0.47317 liter |
|  | 1 U.S. liquid quart . . 0 | 0.94633 liter |
|  | 1 U.S. gallon . ..... 3 | 3.78533 liters |
| Weights | 1 grain . . . . . . . . . . 0 | 0.0648 gram |
|  | 1 avoir. ounce. . . . . . 2 | 8.35 grams |
|  | 1 avoir. pound ..... 0 | 0.4536 kilogram |
|  | 1 Troy ounce . . . . . 3 | 31.1035 grams |

## DECIMAL EQUIVALENTS OF FRACTIONS

| Inches | Decimal of an Inch | Inches | Decimal of an Inch |
| :---: | :---: | :---: | :---: |
| 1/64 | . 015625 | 29/64 | . 453125 |
| 1/32 | . 03125 | 15/32 | . 46875 |
| 3/64 | . 046875 | $31 / 64$ | . 484375 |
| $1 / 20$ | . 05 | 1/2 | . 5 |
| 1/16 | . 0625 | $33 / 64$ | . 515625 |
| 1/13 | . 0769 | 17/32 | . 53125 |
| 5/64 | . 078125 | 35/64 | . 546875 |
| 1/12 | . 0833 | 9/16 | . 5625 |
| 1/11 | . 0909 | $37 / 64$ | . 578125 |
| $3 / 32$ | . 09375 | 19/32 | . 59375 |
| 1/10 | . 10 | 39/64 | . 609375 |
| 7/64 | . 109375 | 5/8 | . 625 |
| 1/9 | . 111 | $41 / 64$ | . 640625 |
| 1/8 | . 125 | ${ }^{21} 32$ | . 65625 |
| \% 64 | . 140625 | $43 / 64$ | . 671875 |
| 1/7 | . 1429 | $11 / 16$ | . 6875 |
| 5/32 | . 15625 | $45 / 64$ | . 703125 |
| 1/6 | . 1667 | 23/32 | . 71875 |
| 11/64 | . 171875 | 47/64 | . 734375 |
| 3/16 | . 1875 | $3 / 4$ | . 75 |
| 1/5 | . 2 | 49/64 | . 765625 |
| 13/64 | . 203125 | 25/32 | . 78125 |
| 7/32 | . 21875 | $51 / 64$ | . 796875 |
| 15/64 | . 234375 | 13/16 | . 8125 |
| $1 / 4$ | . 25 | 53/64 | . 828125 |
| 17/64 | . 265625 | $27 / 32$ | . 84375 |
| $9 / 32$ | . 28125 | 55/64 | . 859375 |
| 1964 | . 296875 | 7/8 | . 875 |
| 5/16 | . 3125 | 57/64 | . 890625 |
| 21/64 | . 328125 | 29/32 | . 90625 |
| 1/3 | . 333 | 59/64 | . 921875 |
| 11/32 | . 34375 | 15/16 | . 9375 |
| 23/64 | . 359375 | $61 / 64$ | . 953125 |
| $3 / 8$ | . 375 | $31 / 32$ | . 96875 |
| 25/64 | . 390625 | ${ }^{63} 64$ | . 984375 |
| 13/32 | . 40625 | 1 | 1.0 |
| 7/16 | . 4375 |  |  |

## CONVERSION CONSTANTS



## FEET HEAD OF WATER TO PSI

| Feet Head | Pounds Per Square Inch | Feet Head | Pounds Per Square Inch |
| :---: | :---: | :---: | :---: |
| 1 | . 43 | 100 | 43.31 |
| 2 | . 87 | 110 | 47.64 |
| 3 | 1.30 | 120 | 51.97 |
| 4 | 1.73 | 130 | 56.30 |
| 5 | 2.17 | 140 | 60.63 |
| 6 | 2.60 | 150 | 64.96 |
| 7 | 3.03 | 160 | 69.29 |
| 8 | 3.46 | 170 | 73.63 |
| 9 | 3.90 | 180 | 77.96 |
| 10 | 4.33 | 200 | 86.62 |
| 15 | 6.50 | 250 | 108.27 |
| 20 | 8.66 | 300 | 129.93 |
| 25 | 10.83 | 350 | 151.58 |
| 30 | 12.99 | 400 | 173.24 |
| 40 | 17.32 | 500 | 216.55 |
| 50 | 21.65 | 600 | 259.85 |
| 60 | 25.99 | 700 | 303.16 |
| 70 | 30.32 | 800 | 346.47 |
| 80 | 34.65 | 900 | 389.78 |
| 90 | 38.98 | 1000 | 433.00 |

Note: One foot of water at $62^{\circ} \mathrm{F}$ equals .433 pound pressure per square inch. To find the pressure per square inch for any feet head not given in the table above, multiply the feet head by .433 .

## USEFUL FORMULAS

## Geometric Properties: $\quad \mathrm{A}=$ Area; $\mathrm{A} 1=$ Surface area of solids; $\mathrm{V}=$ Volume; $\mathrm{C}=$ Circumference


$A=\frac{B H}{2}$


Circle
$A=\pi R^{2}$
$\mathrm{C}=\pi \mathrm{D}$
$\mathrm{R}=\mathrm{D} / 2$


Sector of Circle

$$
\begin{aligned}
& A=\pi R^{i} \frac{\alpha}{360} \\
& \mathrm{~L}=\pi \mathrm{R} \frac{\alpha}{180} \\
& \alpha=57.296 \frac{\mathrm{~L}}{\mathrm{R}} \\
& \mathrm{R}=57.296 \frac{\mathrm{~L}}{\alpha}
\end{aligned}
$$



Rectanglular Solid $A 1=2(W L+L H+H W)$ $V=W L H$


Elliptical Tanks
$A 1=2 \pi\left(A B+H \sqrt{\frac{A^{2}+B^{2}}{2}}\right)$ $V=\pi A B H$


Cylinder
$A 1=2 \pi R(H+R)$
$V=\pi H R^{2}$
For Above Containers:
Capacity in gallons $=\frac{\mathrm{V}}{231}$ when V is in cubic inches Capacity in gallons $=7.48 \times \mathrm{V}$ when V is in cubic feet

## DEFINITION OF TERMS

ACCELERATOR - Any of a number of chemicals added to the resin, singly or in combination, which speed the hardening process or cause the hardening to occur (hardener, catalyst, curing agent, promoter).
ADAPTER - A fitting used to join two pieces of pipe, or two fittings, which have different joining systems.
ADHESIVE - A material formulated to bond together pipe and fittings resulting in high strength and corrosion resistant fabrications.
BELL AND SPIGOT - A joining system in which two truncated conical surfaces come together and bond adhesively. The bell is the female end. The spigot is the male end.
BUSHING - A fitting used to join two different sizes of pipe by reducing the size of the female end of the joint. Joints may come threaded or tapered.
CATALYST - See hardener.
CENTRIFUGAL CASTING - A process for making pipe in which the resin, fiberglass reinforcement and other ingredients are placed into the interior of a spinning steel rotary mold, forming the pipe through centrifugal force and the application of heat.
COLLAR - See coupling.
COMPRESSION MOLDING - A process for making fittings in which a molding compound is formed and cured into the finished part configuration through pressure and heat in a die. COMPRESSIVE FORCE - The force that occurs when opposing loads act on a material, crushing, or attempting to crush it. In pipe, circumferential compressive forces result from external collapse pressure, or heating of an end-restrained fiberglass pipe.
CONCENTRIC REDUCER - A pipe fitting used to join two different sizes of pipe while maintaining the same center line in both.
CONTACT MOLDING - A process for making fittings in which cut pieces of fiberglass reinforcement are laid on a mold, saturated with resin, and cured to the finished part shape.
COUPLING (collar) - A short heavy wall cylindrical fitting used to join two pieces of the same size pipe in a straight line. The coupling always has female connection ends which can be bell, threaded or a mechanical joining method.
CURE - The hardening of a thermoset resin system by the action of heat or chemical action.

CURE STAGES - Stages describe the degree to which a thermoset resin has crosslinked. Three stages, in order of increasing cross linking, include B-stage, gelled, fully cured.
CURE TIME - The time required for a thermoset material to react and develop full strength and material properties. The time is dependent upon the temperature of the material.
CURING AGENT - See hardener.
CUT AND MITERED FITTINGS - Fittings manufactured by cutting, assembling and bonding pipe sections into a desired configuration. The assembled product is then over wrapped with resin-impregnated roving or glass cloth, to provide added strength.
EPOXY RESIN - A thermosetting resin, usually made from Bisphenol A and epichlorhydrin, cured by a variety of agents such as anhydrides and amines. These resins contain cyclic ether groups. See thermoset.
FRP - Fiberglass Reinforced Plastic.
FABMAT - A combination of woven roving and chopped strand mat held together with resin binders. Usually used for making contact molded fittings and butt weld joints.
FILAMENT WOUND - A manufacturing method for pipe and fittings in which resin impregnated continuous strand roving wraps around a mandrel to achieve high reinforcement concentration and precise filament placement.
FILLERS (extender, pigments, inerts; i.e., sand, etc.) -
Materials added to a resin which do not affect the cure of the resin but may influence the physical properties of the resin system.
FITTING TYPES - The classification of fittings by the method of manufacture; i.e., molded, cut and mitered, filament wound, contact molded.
GEL TIME - The time it takes for a resin system to harden to a rubber-like state.
HAND LAY-UP - Any number of methods of forming resin and fiberglass into finished pipe products by manual procedures. Hand lay-up products do not usually exhibit optimum strength of the reinforcing material since the fibers do not lie oriented for maximum performance. These procedures include overwrap techniques, contact molding, hand molding and others.
HARDENER (accelerator, catalyst, curing agent, promoter) -
Any of a number of chemicals added to the resin, single or in combination, which speed up the hardening process, or cause hardening to occur.

HEAT BLANKET or HEAT COLLAR - An electrical device used to heat a fabrication to reduce cure time.
HYDROSTATIC TEST - A pressure test of the completed fabrication to confirm good quality. Typically, the system is filled with water and held at the selected pressure while checking for leaks.
IMPACT RESISTANCE - The ability of a part to absorb a striking blow without damage.
JOINING (connecting systems) - Any of a variety of methods for connecting two separate components of a piping system together. Included are bell and spigot, threaded and coupled, mechanical devices, etc.
JOINT - A term used to describe an individual length of pipe or the actual joining mechanism; (i.e., adhesive bonded bell and spigot, threaded and coupled, etc.)
LINER - A generic term used to describe the interior surface in pipe. Generally, liners are resin-rich regions from 0.005 to 0.100 in. thick. Liners may be reinforced with fibrous material such as veil or mat. Liners can provide extra corrosion protection for severe chemical service. They also form a leak barrier (elastomer bladder). The manufacturer may add a liner before, during, or after construction of the pipe wall depending on the manufacturing process.
MATRIX - The material used to bind reinforcement and fillers together. This material may be thermoplastic or thermosetting and dictates to a large extent the temperature and chemical service conditions allowable for a pipe or fitting.
MOLDED FITTINGS - Pipe fittings formed of compressing resin, chopped fiber and other ingredients in a mold under heat and pressure.
MOLDING - Any of several manufacturing methods where pressure or compression molding shapes resin and reinforcing materials into final products.
OVER WRAP - A method of repair or joining in which fiberglass reinforcement and resin are fabricated over the selected area.
POLYESTER RESIN - Any of a large family of resins which are normally cured by cross linking with styrene. The physical and chemical properties of polyester resins vary greatly. Some have excellent chemical and physical properties while others do not. Vinyl esters are a specific type of polyester resin. Other polyester resins with properties suitable for use in the manufacture of fiberglass pipe include: isophthalic Bisphenol A fumarate and HET acid polyesters. Each type of resin has particular strengths and weaknesses for a given piping application.

POT LIFE - The time available to use thermoset adhesives after the reactive materials have been mixed.
PRESSURE RATING - The maximum anticipated long-term operating pressure a manufacturer recommends for a given product. Also referred to as working pressure, class or design pressure.
PROMOTER - See hardener.
REINFORCEMENT - Typically, fibers of glass, carbon or synthetic material used to provide strength and stiffness to a composite material. The type of fiber used as reinforcement play a major role in determining the properties of a composite, as does the fiber diameter and the type of sizing used. Terms relating to the physical form of the reinforcement include:

Chopped Fiber - Continuous fibers cut into short ( 0.125 to 2 in.) lengths.
Filament - A single fiber of glass; e.g., a mono filament.
Mats - Coarse fabric sheets made from chopped strands randomly placed and held together by resin binders.
Milled Fibers - Glass fibers, ground or milled, into short ( 0.032 to 0.125 in .) lengths.
Roving - A collection of one or more strands wound into a cylindrical package. The typical form of glass fiber used in the manufacture of filament wound pipe.
Veil - Surfacing mat of porous fabric made from filaments. Used to provide a resin rich layer or liner.
Yarn - Glass fiber filaments twisted together to form textile-type fibers.
Yield - The number of yards of material made from one pound of the product.
Resin (polymer) - As applied to fiberglass pipe, resin is the polymer or plastic material used to bind the glass fibers together.
RESIN - The polymer (liquid plastic) material which hardens with cure to provide a solid form, holding the fiberglass reinforcement in place. Resins provide the corrosion resistance in FRP parts.
SADDLE - A fitting which is bonded to the exterior of a pipe to make a branch connection.
SHELF LIFE - The storage time for a material until it becomes unusable.
SOCKET JOINT - A joining system in which two straight cylindrical surfaces come together and bond adhesively.

STRESS - The force per unit of cross sectional area. Measured in pounds per square inch (psi). This should not be confused with hydraulic pressures, measured as psig or psia, which can induce stress.
SUPPORT SPACING (span) - The recommended maximum distance between pipe supports to prevent excessive pipe deformation (bending).
SURGE PRESSURE - A transient pressure increase due to rapid changes in the momentum of flowing fluids. Water hammer is one type of surge pressure. Rapid opening or closing of valves often result in a surge pressure or water hammer.
THERMAL CONDUCTIVITY - The rate at which a material (pipe) transmits heat from an area of high temperature to an area of lower temperature. Fiberglass pipe has low thermal conductivity.
THERMAL EXPANSION - The increase in dimensions of a material (pipe) resulting from an increase in temperature. A decrease in temperature results in thermal contraction.
THERMOSET - A polymeric resin cured by heat or chemical additives. Once cured, a thermoset resin becomes essentially infusible, (cannot be re-melted) and insoluble. Thermosetting resins used in pipe generally incorporate reinforcements. Typical thermosets include:

- Vinyl esters - Novolac or epoxy Novolac
- Epoxies - Unsaturated polyesters

THRUST FORCES - Commonly used to describe the forces resultant from changes in direction of a moving column of fluid. Also used to describe the axial or longitudinal end loads at fittings, valves, etc., resultant from hydraulic pressure.
TORQUE - Used to quantify a twisting force (torsion) in pipe. Torque is measured as a force times the distance from the force to the axis of rotation. Torque is expressed in footpounds (ft-lb) or inch-pounds (in-lb).
TWO HOLING - A method of aligning flanges onto pipe or fittings so that the bolt circle will mate with the adjoining flange.
VINYL ESTER - A premium resin system with excellent corrosion resistance. Vinyl ester exhibits high versatility, temperature resistance and excellent corrosion resistance to acids.
WATER HAMMER - Pressure surges in a piping system caused by sudden operation of a valve, pump, or other component.

## HOW TO READ FLANGED OR REDUCING FITTINGS

TEE


Run $x$ Run $x$ Branch ( $\mathrm{A} \times \mathrm{BxC}$ )


LATERAL
(AxBxC)
Run x Run x Branch


CROSS (AxBxCxD)
Run x Run x Branch X Branch

The above sequence should be used when describing fitting outlets. Drawings or sketches showing outlet types, locations, sizes and dimensional requirements are required for more complicated fitting configurations.

## HOW TO FIGURE A $45^{\circ}$ OFFSET



True Length $=$ offset $\times 1.414$
Offset $=$ true length $\times .707$

## EXAMPLES:

offset = 12"
$12 " \times 1.414=16.968=1^{\prime}-5 "$ true length = $1^{\prime}-5{ }^{\prime \prime}$
(to nearest $1 / 16^{\prime \prime}$ )
true length $=24 "$
$24 \times .707=16.968=1^{\prime}-5 "$ offset length = $1^{\prime}-5{ }^{\prime \prime}$ (to nearest $1 / 16^{\prime \prime}$ )

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## Introduction

Installation instructions for adhesive bonded 30"-42" diameter Tapered Bell \& Spigot joints. Installation training and certification is required for all bonders. Qualified on-site supervision of initial installation is recommended to ensure proper field practices are followed.

## Field Checks

- Piping components should be visually inspected for physical damage


## Bonding Environment

## Hot Weather Recommendations

- A cool area is recommended for long-term storage of adhesive kits. Storage temperatures between $70-80^{\circ} \mathrm{F}\left(21-27^{\circ} \mathrm{C}\right)$ are ideal.
- When field temperatures exceed $90^{\circ} \mathrm{F}\left(32^{\circ} \mathrm{C}\right)$, store adhesive kits in ice chest with bagged ice or freezer pack. Remove adhesive kits just prior to use.
- Protect joints from direct sunlight to minimize heating of material and ultraviolet exposure.


## Cold Weather Recommendations

- A warm area is recommended for long-term storage of adhesive kits. Storage temperatures between $70-80^{\circ} \mathrm{F}\left(21-27^{\circ} \mathrm{C}\right)$ are ideal.
- When the field temperature falls below $70^{\circ} \mathrm{F}\left(21^{\circ} \mathrm{C}\right)$, warm bond surfaces with a propane torch or another clean burning heat source. The surfaces should be warm to the touch but not hot. If the bond surface is too hot when adhesive is applied, it will set up prematurely. A bonder should be able to comfortably place the back of their hand on the bond surface. A torch should be used only to warm the bonding surface, not to force cure an adhesive joint.
- All bonded joints must be heat cured with electric heating collars.
- Freshly bonded joints should be heat cured when field temperatures are expected to fall rapidly. Heat curing reduces the cure time and the chances of pipeline contraction pulling the joint apart.
- Note:When temperatures fall below $32^{\circ} \mathrm{F}\left(0^{\circ} \mathrm{C}\right)$, it is recommended that all joints (when possible) be made in a portable, heated work space. The use of a portable kerosene heater (torpedo style) is also recommended during extreme cold weather to help maintain ambient temperature inside the pipe.


## Joint Preparation \& Assembly

Bonding surfaces require light sanding with 40-80 grit paper or Emery cloth within two hours before adhesive application. Mix the adhesive in accordance with the applicable adhesive bulletin. The adhesive must be brushed on with mild pressure onto the bell \& spigot bonding surfaces to ensure a thorough wetting.

The adhesive layer on the leading edge of the spigot should be slightly thicker than the other areas. Apply a thin coat of adhesive to the spigot end to coat exposed glass fibers.

During cool weather (below $70^{\circ} \mathrm{F}\left(21^{\circ} \mathrm{C}\right)$, both the adhesive and bond surfaces should be warmed to improve the spread ability of the adhesive. Once warmed both surfaces will cool rapidly.
As the adhesive cools it will become thicker; therefore, it should be applied quickly using two installers per bell and two installers per spigot.

The working area around the joint may need to be covered to protect from sunlight, precipitation, wind and frigid weather. The weight of the pipe requires the use of a side boom tractor, crane or large excavator to move the pipe.

## Insertion Depth Reference Marks

- Using a permanent marker, draw on the pipe a set of reference marks 24 inches from the spigot end of the pipe.
- The reference marks are positions used to determine the insertion depth of an assembled joint. During joint assembly the distance from the bell end to the reference marks should be measured and recorded in a quality record when possible.


## Joint Installation

A pipe joint is made by lifting the pipe and carefully inserting the spigot into the bell until the spigot is seated in the bell. The joint should then be checked for proper alignment meaning the joint should be straight. If the joint is not aligned, the pipe must be maneuvered as required to align the pipe joint. A hydraulic come-along is required to complete the joint make-up. Attach the hydraulic come-alongs as instructed in the Come-Along Instructions.

The joint is pulled into final position by simultaneously pumping the two come-along hydraulic cylinders. The cylinder pressures should be increased slowly to the pressures listed in manual TLS6619 (come alongs)while vibrating the joints. The joint should be vibrated by two installers impacting the sides of the bell with 5 lb . dead blow hammers. The vibrating should continue after come-along's pressure has been reached. The vibrations and come-along's loads will cause the joint to pull together until made up. The cylinder pressure should not exceed 5,000 psig at any time.
As the joint pulls together, the hydraulic cylinder pressure will tend to drop during the process requiring additional strokes on the hydraulic pump to maintain the come-along's pressure. The joint will be made up when the pressure drop becomes negligible ( 300 psi or less with three sharp blows of the dead blow hammer) and it is obvious the joint is no longer moving together. This can be confirmed by repeatedly measuring the distance from the face of the bell to the reference mark on the pipe spigot and comparing to previous measurements. Verify the hydraulic cylinders have not bottomed out giving the illusion of a made-up joint. The final insertion depth should be recorded for the quality records.

Excessive adhesive squeezed out of tapered joints, both on the I.D. and the O.D., should be removed. An electric heating collar is required and may be applied to the bell surface immediately. Leave the come-alongs in place for one hour.

These instructions apply to integral bell/spigot pipe, coupling/spigot pipe and fitting/spigot pipe joints.

## Flange Installation

A flange pull-beam must be constructed to attach the come-along chains and pull the flange onto the pipe spigot. A steel channel $6 x$ 13 and 54 inches in length should be fabricated with two holes each large enough for a come-along chain to fit through. Locate the holes to clear the outer diameter of the flange by a minimum of $1 / 2^{\prime \prime}$.
Start by verifying the bell and spigot tapers are in spec using the factory gauges. Proceed by drawing a reference mark on the pipe with a permanent marker 18 inches from the end of the pipe spigot. Prepare the pipe spigot and flange bonding surfaces and then mix the adhesive. Pre-warm joints if necessary and apply adhesive to bell and spigot. Adhesive application methods are detailed above.

Lift and position the flange onto the spigot until it seats. Verify alignment of the flange onto the spigot. If properly aligned, then measure the distance from the face of the flange to the reference mark on the pipe spigot and record as the initial insertion depth.

Attach the hydraulic come-along collars to the pipe and connect the hydraulic cylinders, per the instruction for come-alongs to the collars and the pull-beam. Place two $4 \times 4$ or larger hardwood timbers between the pull-beam and the face of the flange. The timbers must be located outside the inner diameter of the flange to prevent interference with the spigot should it protrude beyond the face of the flange. The timbers should be smooth to protect the flange face from damage. The use of a $1 / 4$ " thick rubber pad between the flange and the timbers is recommended.

Increase the come-along pressure slowly to the pressures recomended in TLS6619 (come alongs) while vibrating the flange. The sides of the flange should be vibrated by two installers impacting the side of the flange with 5 lb . dead blow hammers. The come-along pressure will tend to drop during this process requiring additional strokes on the hydraulic pump to maintain come along pressure. The joint will be made up when the pressure drop becomes negligible ( 300 psi or less with three sharp blows of the dead blow hammer) and it is obvious the joint is no longer moving together. This can be confirmed by repeatedly measuring the distance from the face of the flange to the reference mark on the pipe spigot and comparing to previous measurements. Verify the hydraulic cylinders have not bottomed out giving the illusion of a made-up joint. The final insertion should be recorded for the quality records.
Any adhesive on the pipe surface behind the flange joint must be removed to allow the Van Stone bolt ring to seat flush against the flange.

During installation the pipe spigot may protrude beyond the face of the flange. Any spigot protrusion must be machined flush with the flange face by cutting or grinding. Should the spigot not protrude any squeezed out adhesive at the end of the spigot should be formed into a fillet.

Use standard bolt tightening sequence for 30 "-42" flanges. (Refer to Matched Taper Joint Installation.) Maximum bolt torque is 400 ft -lbs.

## Adhesive Cure

## Electric Heat Collar Use

All bonded joints must be heat cured. Ensure the electric heating collars are in good working order prior to using. It is good practice to verify they are functioning properly at the end of each cure cycle.

Wrap heat collars over the surface of joint covering entire bonded area. Cure flanges from inside the pipe by turning the heat collar inside out. A narrow split ring of fiberglass pipe may be used to hold the heat collar in place against the inner surface of the pipe.
When ambient temperatures fall below $50^{\circ} \mathrm{F}\left(10^{\circ} \mathrm{C}\right)$ heat collars should be insulated for better heating efficiency. A 2-inch thick glass wool blanket or other insulating material with an $R$ value of 7 or greater is recommended. The open ends of pipe and fittings should be blocked to prevent heat loss due to air flow.
On some fittings and pipe joints, the heating collar may overlap. When this occurs, place a cut section of 2" FRP pipe between the two heat collar layers that are overlapped and place a special cut section of $1 / 16^{\prime \prime}$ thick silicone rubber between the pipe and the heating collar. This will help prevent discoloration of the pipe.

When heat collars left on too long or the overlaps are not protected, some discoloration may occur. In most cases this will not affect the operation of the pipe. If unsure, contact the NOV Fiber Glass Systems personnel on site.

## Pressure Testing

Contact NOV Fiber Glass Systems for recommendations concerning field hydro pressure tests. The test procedure must be reviewed and accepted by the pertinent site personnel prior to hydro pressure tests.

## Supporting Documents Description

| ADH4000 | Adhesive Systems Summary |
| :--- | :--- |
| TLS6619 | $18 "-42 "$ Come-Along Instructions |
| TLS6636 | $30 "-42 "$ Tapering Tool Instructions |
| TLS6640 | 1"-42" Heat Collar Instructions |

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## CERAM CORE®PIPING

## Installation Data


#### Abstract

Handling The abrasion resistant liner may be damaged by severe impact or pipe deformation. Abusive handling can cause fracture and loss of some of the liner. Fine cracks in the liner will cause no problems, but if the liner is so severely damaged as to flake away chips and pieces, the overwrap will be exposed to abrasion and pipe will fail prematurely.


## Caution:

1. Do not throw pipe from trucks onto rocks, into ditches or subject it to similar rough treatment.
2. Avoid striking the pipe. Any blow which causes a delamination of the overwrap will damage the liner.
3. A NOV Fiber Glass Systems representative should inspect the pipe before installation if there is any suspected damage.
4. Avoid striking end of pipe against objects which may damage liner, and keep flange protectors in place until ready to install.

## Installation

## Joining Methods

CERAM CORE pipe is joined by a self-aligning flange joint. The pipe is fabricated with flanges on both ends. An O-ring and an alignment ring, which are supplied by NOV Fiber Glass Systems, are required for matching the flange. When properly installed and compressed there will be a very minimal gap between the ends of the liner of adjacent pipe. See Table II for recommended bolt torque. Particular attention must be given to accurately align pipe bores at all joints. The rate of wear of the reinforcing overwrap vs. that of the ceramic bead liner is on the magnitude of 1000:1. Severe misalignment which will expose the overwrap to the abrasive material will cause an undercutting of the liner and early pipe failure. Misalignment should not exceed $1 / 2$ " bead diameter for optimum service (approximately ${ }^{1 / 32 ")}$. Transition fittings are necessary to join the pipe to systems with different inside diameters. (See the following section for details). If it is not possible to perfectly align pipe, such as when adapting to existing lines, it is preferable that the downstream side of the joint be oversized to avoid impact on a cut edge of the liner. In no case should the overwrap be exposed.

## Fittings

CERAM CORE fittings are flanged with a radius sweep of three times diameter. Standard fittings available are $45^{\circ}$ and $90^{\circ}$ elbows, except on $14^{\prime \prime}$ and $16^{\prime \prime}$ diameters where $45^{\circ}$ elbows only are available as standard.

## Connecting to Other Systems

CERAM CORE pipe can be installed to new or existing systems by two methods:

## Transition Fittings

When joining to materials other than CERAM CORE pipe or fittings, it is extremely important that the inside diameter of pipe-to-pipe and pipe-to-fitting match. Mismatched I.D.'s can cause the liner to be undercut and "scooped" away, causing premature failure. If the I.D. of the existing line or fitting at the point of entry into CERAM CORE is $\pm .050$ " (or more) larger or smaller than the I.D. of the pipe, a special adapter must be used to assure a smooth transition. Transition fittings for adapting to new or existing lines or other openings are considered essential and will be designed as needed for each installation upon receipt of the necessary dimensional information from the customer. A minimum of two transition fittings generally will be required on each installation.

When installing transition fittings it is recommended that the inside diameter of the transition fittings be aligned to the inside diameter of the existing system before the spool is connected to the transition fitting. Since transition fittings are usually one foot long, this procedure can be accomplished by sight. Also, make sure that there are no gaps between the existing system and the transition fittings which could cause undercutting.

## Flanges

Flanges have standard ANSI B16.5 150 lb . flange bolt hole dimensions. Flange seals should be 60-70 durometer Orings when joining pipe to pipe. Use a stiff grease to hold the O-ring in the groove when assembling the flanged joints. $1 / 8$ " thick full face gaskets or half size O-rings should be used when joining pipe to other equipment. (See Table II.) When the piping system is being connected to another type of system (flange is flush), the inside diameter of the gasket should be such as to match the inside diameter of the pipe when the flange bolts are tightened. The bore of the pipe piece MUST be aligned as concentric as possible with the bore of the system to which it is being connected. If there are irregularities or "scooped away" places due to previous wear, these should be grouted with CeramSurf ${ }^{\text {TM }}$ surfacing material (available from NOV Fiber Glass Systems).

## Field Preparation

## Special Equipment

Under normal circumstances, field preparations consist of having the proper torque wrenches, bolts, nuts, and washers. NOV Fiber Glass Systems normally manufactures all pipe sections to the desired length so the installer need only assemble flanged joints. The close tolerances necessary to maintain proper joint alignment are difficult to reproduce in field cut joints. For this reason field bonded joints should be eliminated or kept to a minimum. Special diamond blades and a large lathe or special NOV Fiber Glass Systems tools are required for the field installation of flanges. The following sections give a brief description of procedures necessary to make field joints. Additional tool instructions and matching tolerances are available upon request.

## Cutting

The end of the pipe must be cut squarely and smoothly. Due to extreme hardness of the liner, standard cutting tools will not cut the liner without chipping. Therefore, when the pipe is cut anywhere except within two inches or less of the end (dressing cut), it is necessary to make two cuts (rough and dress) to produce the desired smoothness. If only a dressing cut is needed, then a single cut can be used.

## Rough Cutting

Scribe or draw a line around the pipe at the desired rough cut dimension. Allow approximately one inch for dressing cut.

Using a power circular hand saw and abrasive blade, or hack saw, cut through the laminate to the liner completely around the pipe. Note: All glass fiber filaments should be cut.

Snap the pipe in two by placing pipe on support with cut slightly overhanging support. Apply a downward impact load to end of pipe with a $2 \times 4$ or rubber mallet while pipe is rotated such that one full rotation is made before separation. The pipe is now ready for the finish cut to dress up the edge.

## Dress Cutting

The method to obtain a square cut requires a lathe large enough to turn the pipe and a tool post grinder equipped with a diamond blade. Only a diamond blade is hard enough to cut the ceramic liner. Water must be used at all times to keep the blade cool. The pipe must be rotated by hand unless the lathe is capable of extremely slow speed (1-2 RPM). Cut through the overwrap down to the liner, then advance the blade through the liner far enough to cut off in one revolution. Rotate the pipe into the blade. Do not overload the blade. With a little practice, the proper feed rate can be determined by listening to the motor pitch. Support the ring being cut off to prevent the liner from breaking as the saw approaches a complete cut.

Caution: Be sure the final dress cut removes all chipped or broken liner.

## Bonding

## Pipe Preparation

Scarfing the O.D. is necessary to remove the gloss and true the O.D. of the pipe to receive the flange. Scarf until a snug, dry fit is achieved between the pipe and the flange. This can be done on a lathe or with the NOV Fiber Glass Systems dressing tool. Eccentricity should not exceed $\pm .015$ ".

Use $\mathbf{8 0 0 0}$ Series adhesive kits.
Clean the machined surfaces of both the pipe and flanges. Use solvent and the paper towels provided in the kit, carefully following the instructions provided in the kit.

Apply adhesive to both pipe and flange bonding surfaces being sure to cover all machined surfaces.

Lightly drive the flange onto the pipe. The flange face must be flush and square with the end of the pipe.

Wipe off all adhesive on the flange face. An uneven surface or filled grooves due to cured residual adhesive will cause gasket sealing problems. A rag slightly dampened with solvent may be used. DO NOT flood with solvent as this may wash adhesive out of the bond area and weaken the bond.

Heat curing the joints will cause beads of adhesive to exude from the bond. These must be removed when partially hardened, but not fully cured, by cutting away with a sharp knife. Be careful not to damage the gasket sealing surface. After clean up, fit to a mating flange to make sure there is no interference.

## Buried Installations

## Preparing the Trench

The final bedding of the trench should be done as uniform and smooth as possible. Rocks or high spots in the trench bottom cause uneven bearing on the pipe and may damage the liner due to stress during backfill and cause unnecessary wear at these points. This is particularly significant if pulsation is present in the lines due to pumps. Sharp bends and changes in elevation or lateral direction in the line must be accomplished through the use of appropriate elbows. A bell hole should be dug for each set of flanges so the pipe rests on the bottom of the ditch.

## Rocky Areas

If the trench is excavated through rock or shale ledges, the trench should be slightly deeper and a layer of sand used in the bottom of the trench and over the pipe to assure protection of the pipe from the rocks.

## Road Crossings

In laying pipe under road crossing, it is recommended that the pipe be laid through a conduit. Firm, well compacted bedding under the pipe at the entrance and exit is essential to prevent shear loads due to backfill and settling. Check Table I for burial depths when pipe will experience surface loads. If a flange joint occurs within the casing, centering devices must be installed at the recommended support spacing.

## Backfilling

The installation should be backfilled with sufficient fill to hold in place with all of the fittings and joints left open for inspection during the testing period. Once the testing is completed, then the backfilling may be finished.

## 1. Timing

The pipe should be covered as soon as possible to eliminate the chance of damage to the pipe; floating of the pipe due to flooding and shifting of the line due to cave-ins.

## 2. Material

The material used for the backfill should be free of sharp rocks, heavy boulders, large clods of dirt and frozen lumps of dirt. Pipe should be completely supported underneath before overburden is applied. Frozen earth will eventually thaw leaving the pipe with insufficient support and voids around the pipe. Vibratory or similar tamping equipment can drive small stones into the pipe wall. Clean backfill should be used with this type equipment. Multiple lines in the same ditch should be separated with clean backfill or sand.

## Above Ground Installations

Above ground installations can be broadly divided into two categories-lines which are laid directly on the surface of the ground and those which are hung or supported as in a typical plant. In either case, there are certain basic guidelines to be followed.

On any lines laid directly on the surface, care should be taken to insure that there are no severe bends and that adequate protection is provided in areas where possible mechanical damage could occur. If the line is connected into a system which could impart a vibration or pulsing action to the pipe, areas of point loading should be protected to prevent the pipe from abrading. Since pipe is flanged, wooden bolsters or similar supports should be provided at support spacing intervals so pipe will not rest on flanges. Pipe resting only on flanges may warp and make future rotation for best wear difficult.

## Anchors

Pipe anchors divide a pipeline into sections. In most cases pumps, tanks, and other similar equipment function as anchors. Additional anchors are required at all changes in direction and at all changes in elevation. Anchors are required on both ends of elbows, either at the elbow or within 5 feet of the elbow ends. On long straight runs only, anchors should be installed at approximately 300 foot intervals. Do not use anchors which apply point loads directly to the bare pipe. Anchors that apply point loads can be used only if a protective sleeve is used between the pipe and the anchor. Guides must be used in conjunction with anchors. See Guide Spacing in Manual Cl1500 CERAM CORE. When joining CERAM CORE product to other piping systems, the adjoining system must be securely anchored to prevent the transfer of thermal end load.

## Supports

NOV Fiber Glass Systems pipe should be supported at intervals designated by the support spacing data in the literature. Supports that have point contact or narrow supporting areas should be avoided, and valves or other heavy equipment should be supported independently of the pipe. Standard sling, clamp, and clevis hangers and shoe supports designed for use with steel pipe can be used to support NOV Fiber Glass Systems pipe. Any other type of support that gives a wide band of contact with at least $120^{\circ}$ of contact with the pipe can be used. Any support that does not provide $120^{\circ}$ of contact should be at least $4 "$ wide or have a width equal to ${ }^{1} / 3^{\prime \prime}$ of the diameter of the pipe, whichever is larger. If it is not possible to achieve this, the pipe should be protected with a protective sleeve of rubber lined metal, or other means of increasing the supporting area. In all cases, the support must be wide enough so that the bearing stress does not exceed 85 psi.

## Expansion

The forces created by the expansion of NOV Fiber Glass Systems systems are approximately only ${ }^{1 / 25}$ that of Schedule 40 steel. In cases where the piping system has long runs or is subjected to large changes in temperature, the changes in length must be handled by anchors and guides. See Product Manual "CERAM CORE" for the anchor and guide spacing information. Consult a NOV Fiber Glass Systems representative for specific recommendations.

## Pipe Rotation

For the longest service life and best economics, the system should be designed and installed so that pipe can be periodically rotated on a regular basis to insure even wear. This is particularly important where there is sliding abrasion on the bottom by heavy particles that do not remain suspended in the fluid stream. This precaution, plus careful alignment of the joints, will give a system with optimum performance. Since the pipe is extremely light, rotation can usually be accomplished by unbolting only a minimal number of joints and rotating several lengths at a time.

TABLE I
CERAM CORE Pipe Burial Depths ${ }^{(1)}$

| Nominal Pipe <br> Size |  | With H-20 Loading ${ }^{(2)}$ |  | Without Live <br> Loading |
| :---: | :---: | :---: | :---: | :---: |
| in | mm | Min. Burial <br> Depth <br> ft. | Max. Burial <br> Depth <br> ft. | Max. Burial <br> Depth <br> ft. |
| 6 | 150 | 2 | 27 | 27 |
| 8 | 200 | 2 | 17 | 17 |
| 10 | 250 | 2 | 15 | 15 |
| 12 | 300 | 2 | 12 | 12 |
| 14 | 350 | 2 | 9 | 10 |
| 16 | 400 | 2 | 9 | 10 |

TABLE II
CERAM CORE Flange ${ }^{(6)}$ Bolt Make-up Torque, Bolt, Washer, and O-Ring for Flanges and Flanged Fittings ${ }^{(3)}$

| $\begin{aligned} & \text { Nom } \\ & \text { Pipe } \\ & \text { Size } \\ & \text { in. } \end{aligned}$ | Max. <br> Torque <br> Ft.-Lbs. ${ }^{(3)}$ | $\begin{aligned} & \text { Bolt } \\ & \text { Size } \\ & \text { in. } \end{aligned}$ | Bolt Length in. | Washer Size ${ }^{(4)}$ in. | $\begin{gathered} \text { No. } \\ \text { of } \\ \text { Bolts } \end{gathered}$ | O-Ring Sizes ${ }^{(5)}$ ARP 268 N. |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | $\underset{\text { Full }}{\substack{\text { Fizo }}}$ | Half Size |
| 6 | 30 | $3 / 4$ | $4^{1 / 2}$ | $11 / 2$ | 8 | 442 | 264 |
| 8 | 100 | $3 / 4$ | 5 | $1^{1 / 2}$ | 8 | 448 | 273 |
| 10 | 100 | 7/8 | $51 / 2$ | $1^{3 / 4}$ | 12 | 452 | 277 |
| 12 | 100 | 7/8 | 6 | $13 / 4$ | 12 | 457 | 280 |
| 14 | 100 | 1 | 6 | 2 | 12 | 459 | 281 |
| 16 | 100 | 1 | 6 | 2 | 16 | 465 | 284 |

(1) Basis for calculations are: (a) $3 \%$ maximum allowable diametrical deflection of the pipe; (b) soil modulus is 1000 psi; (c) the pipe is not subjected to a vacuum; (d) the water table is not above the top of the pipe. Other variables such as bedding constant assume worst case (most conservative) values. Reference ASTM D3839 for details on these assumptions (including an explanation of "soil modulus"). If actual conditions are different, contact your NOV Fiber Glass Systems representative.
(2) H -20 wheel loading is $32,000 \mathrm{lbs}$. per tandem axle; however, the allowable truck loading is now $34,000 \mathrm{lbs}$. per axle. Calculations are based on 34,000 lbs. per axle.
(3) The torque required to seal the gasket is usually lower than the maximum (3) The torque required to seal the gasket is usually lower than the maximum
torque. Torque is based on non-lubricated bolts; therefore, torque levels should be lowered for lubricated bolts.
(4) Use SAE light washers.
(5) These numbers are from the SAE uniform numbering system. Full size Orings are used with SF flange to SF flange. Half size are used with SF flange to smooth (flat) face flange.
(6) NOV Fiber Glass Systems flanges should be joined only to flat-faced flanges, When mating to raised-face flanges or lug-type valves, spacers are necessary.

[^37]
[^0]:    ${ }^{(1)}$ The differential pressure between internal and external pressure which causes collapse.
    ${ }^{(2)} \mathrm{A} 0.67$ design factor is recommended for short duration vacuum service. A full vacuum is equal to $14.7 \mathrm{psig}(0.101 \mathrm{MPa})$ differential pressure at sea level.
    ${ }^{(3)}$ A 0.33 design factor is recommended for sustained (long-term) differential collapse pressure design and operation.

[^1]:    ${ }^{(1)}$ Based on $1 / 2$ " deflection at mid-span.

[^2]:    (1) Weight per 25 -foot length of Ceram Core pipe includes two flanges

[^3]:    (1) $v_{a h}=$ The ratio of hoop strain to axial strain resulting from stress in the axial direction
    $v_{\text {ha }}=$ The ratio of axial strain to hoop strain resulting from stress in the hoop direction.

[^4]:    Tolerances or maximum/minimum limits can be obtained from NOV Fiber Glass Systems.

[^5]:    Tolerances or maximum/minimum limits can be obtained from NOV Fiber Glass Systems.

[^6]:    * At $200^{\circ} \mathrm{F}\left(94^{\circ} \mathrm{C}\right)$ using Bondstrand type $\mathrm{PSX}^{\top m} \cdot 34$ adhesive. For sustained service above $200^{\circ} \mathrm{F}$, reduce ratings linearly to $50 \%$ from $200^{\circ} \mathrm{F}$ to $250^{\circ} \mathrm{F}\left(121^{\circ} \mathrm{C}\right)$.
    ** At $70^{\circ} \mathrm{F}\left(21^{\circ} \mathrm{C}\right)$. Reduce linearly to $90 \%$ at $150^{\circ} \mathrm{F}\left(66^{\circ} \mathrm{C}\right), 80 \%$ at $200^{\circ} \mathrm{F}\left(94^{\circ} \mathrm{C}\right)$, and $65 \%$ at $230^{\circ} \mathrm{F}\left(110^{\circ} \mathrm{C}\right)$

[^7]:    Do not bend pipe until adhesive has cured. At rated pressure sharper bends may create excessive stress concentrations.
    ** For 100-ft (30m) Bending length (S)

[^8]:    * Per ASTM D2412.
    ** Use these values to calculate permissible spans.

[^9]:    ) Span recommendations includ
    must be supported separately.
    2) Span recommendations are calculated for a maximum long-term deflection of $1 / 2$ inch to ensure good appearance and adequate drainage.
    3) Continuous spans are defined as interior (not end) spans that are uniform in length and free from structural rotation at the supports. Simple spans are supported only at the ends and are hinged or free to rotate at the supports.

[^10]:    (1) value obtained at $65^{\circ} \mathrm{C}$

[^11]:    ${ }^{(1)}$ Quality Control minimum
    ${ }^{(2)}$ For vacuum service above ground in sizes 10 inches and above consult NOV Fiber Glass Systems.

[^12]:    ${ }^{(1)}$ In an unrestrained system due to pressure effects alone.
    ${ }^{(2)}$ At $5 \%$ deflection.

[^13]:    ${ }^{(1)}$ Quality control minimum
    ${ }^{(2)}$ For vacuum service above ground in sizes 8 inches and above consult NOV Fiber Glass Systems.
    ${ }^{(3)}$ At $210^{\circ} \mathrm{F}$, derate $2^{\prime \prime}-6$ " sizes by a factor of 0.73 and $8^{\prime \prime}-16^{\prime \prime}$ sizes by a factor of 0.63 . Linearly interpolate derating factors for temperatures between $150^{\circ} \mathrm{F}$ and $210^{\circ} \mathrm{F}$.

[^14]:    ${ }^{(1)}$ In an unrestrained system due to pressure effects alone.
    ${ }^{(2)}$ At 5\% deflection.

[^15]:    ${ }^{(1)}$ At rated pressure. Sharper bends may create excessive stress concentrations. Do not bend pipe until adhesive has cured.

[^16]:    ${ }^{(1)}$ Ratings shown are for $90^{\circ}$ and $45^{\circ}$ elbows. Ratings in 8 to 16 inch sizes are also applicable to elbows of other angles.
    ${ }^{(2)}$ ANSI B16.5 150psig bolt pattern
    ${ }^{(3)}$ At $210^{\circ} \mathrm{F}$ derate the pipe by a factor of 0.63 , linearly interpolate derating factors for temperatures between $150^{\circ} \mathrm{F}$ and $210^{\circ} \mathrm{F}$.

[^17]:    ${ }^{(1)}$ In an unrestrained system due to pressure effects alone
    ${ }^{(2)}$ At $5 \%$ deflection.

[^18]:    Each component shall be marked to show the following:
    Manufacturer's name and address
    Nominal pipe size
    Pressure class
    Hydrostatic test pressure (if so ordered)
    Date and shift of manufacture (pipe only)

[^19]:    ${ }^{(1)}$ At rated pressure. Sharper bends may create excessive stress concentrations. Do not bend pipe until adhesive has cured.

[^20]:    ${ }^{(1)}$ In an unrestrained system due to pressure effects alone.
    ${ }^{(2)}$ At $5 \%$ deflection.

[^21]:    (1) Based on structural wall thickness at room temperature unless noted.
    ${ }^{(2)}$ The first subscript denotes the direction of applied stress and the second subscript the measured strain contraction. x denotes longitudinal direction. y denotes circumferential direction.
    ${ }^{(3)}$ Test fixtures were free-end type (full end thrust on samples).

[^22]:    *At $21^{\circ} \mathrm{F}\left(99^{\circ} \mathrm{C}\right)$ using Bondstrand PSX•60 adhesive.
    ${ }^{* *}$ At $70^{\circ} \mathrm{F}\left(21^{\circ} \mathrm{C}\right)$. Reduce linearly to $90 \%$ at $150^{\circ} \mathrm{F}\left(66^{\circ} \mathrm{C}\right)$ and $80 \%$ at $200^{\circ} \mathrm{F}\left(93^{\circ} \mathrm{C}\right)$.

[^23]:    ${ }^{(1)}$ Nominal make-up dimension for drawing layout work only using non-threaded spigots. Do not use for assembly dimensions.
    ${ }^{(2)}$ Compatible with Victaulic ${ }^{\circledR}$ HP70ES couplings.

[^24]:    ${ }^{(1)}$ Nominal make-up dimension for drawing layout work only using non-threaded spigots. Do not use for assembly dimensions.
    ${ }^{(2)}$ Saddle is manufactured by bonding a reducer bushing into a saddle with a 2" outlet.

[^25]:    x - Standard available size

[^26]:    ${ }^{(1)}$ This is a nominal make-up dimension for drawing layout work only. Do not use for assembly dimensions

[^27]:    (1) This is a nominal make-up dimension for drawing layout work only. Do not use for assembly dimensions.

[^28]:    * Nipples and flanges
    ${ }^{(1)}$ This is a nominal make-up dimension for drawing layout work only. Do not use for assembly dimensions.

[^29]:    * Available on order only - nonreturnable
    $\dagger$ CL weight, multiply by 1.07 for RB, 1.1 for ZC

[^30]:    * Available on order only - nonreturnable
    $\dagger$ CL weight, multiply by 1.07 for RB, 1.1 for ZC

[^31]:    * Available on order only - nonreturnable.

[^32]:    * Available on order only - nonreturnable.

[^33]:    Note: Eccentric Reducers are available on request

[^34]:    WARNING: These procedures must be followed to avoid serious personal injury or property damage. Failure to do so will result in loss of warranty. Buyer, installer or any employee, agent or representative thereof assumes the risk of any damage or injury to person orproperty.

    Testing with air or gas can be extremely dangerous. Review safety precautions before starting the test and follow all testing procedures.

[^35]:    ${ }^{1}$ Based on testing at Oklahoma State University in Stillwater, OK.
    ${ }^{2}$ Cameron Hydraulic Data, Ingersoll-Rand, Seventeenth Edition, 1988.

[^36]:    Note: One foot of water at $62^{\circ} \mathrm{F}$ equals 0.433 pound pressure per square inch. To find the pressure per square inch for any feet head not given in the table above, multiply the feet head by 0.433 .

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